Corrosion and Protection of Steel (Cont.)

SOV/3133

Andreyeva, V.G. [Engineer], P.V. Strekalov [Engineer], and M.A. Vedeneyeva. Corrosion Resistance of 1Kn18N9T-steel Welded Joints 228

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PHASE I BOOK EXPLOITATION SOV/3587

THE PARTY OF THE P

# Tomashov, Nikon Danilovich

- Teoriya korrozii i zashchity metallov (Theory of Corrosion and Protection of Metals) Moscow, Izd-vo AN SSSR, 1959. 591 p. Errata slip inserted. 4,000 copies printed.
- Sponsoring Agency: Akademiya nauk SSSR. Institut fizicheskoy khimii.
- Eds. of Publishing House: N.G. Yegorov and A.V. Shreyder; Tech. Ed.: I.F. Kuz'min.
- PURPOSE: This book is intended for scientific research workers, metallurgists and engineers studying the corrosion of metals and methods of prevention.
- COVERAGE: The book is an analytic study of the corrosion of metals. Scientific principles governing the process of corrosion of metals and means of prevention are investigated. The author explains the theory of corrosion and outlines its stages of development, gives an analysis of solid bodies, and describes the crystalline

Card 1/24

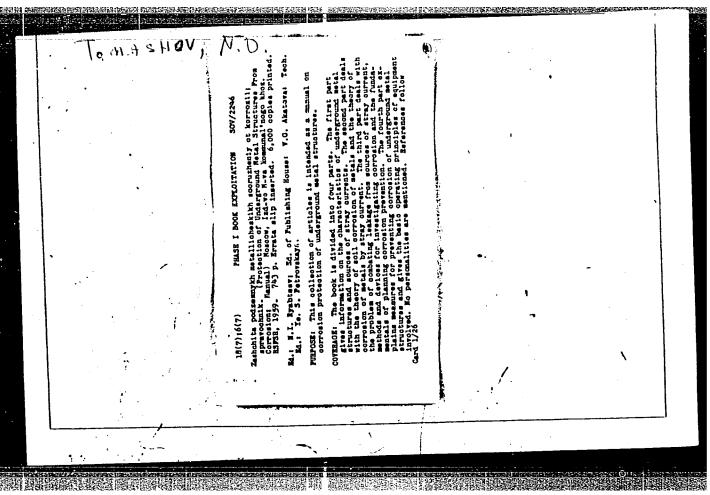
Theory of Corrosion (Cont.)

sov/3587

structure of metals and the main features of electrolytes. Part I treats chemical corrosion: the mechanism of oxidation, growth of films and the laws governing this phenomenon, and protection of metallic structures by alloying and coating. Part II analyzes problems of electrochemical corrosion: electrode potentials, the operation of corrosive galvanic cells, corrosive currents, the operation and depolarization phenomena, and factors inhibiting polarization and depolarization phenomena, and factors inhibiting and accelerating electrochemical corrosion. Part III outlines the mechanism of corrosion and analyzes factors of atmospheric, soil and marine corrosion. Part IV investigates the corrosion resistance of various metals and alloys, analyzes the composition of different metals, and lists the metals most resistant to corrosion. The conclusion contains a number of suggestions for further study in corrosion prevention. The author thanks for further study in corrosion prevention. The author thanks for further study in corrosion prevention. The author thanks for further study in corrosion prevention. The author thanks for further study in corrosion prevention. The author thanks for further study in corrosion prevention. The author thanks for further study in corrosion, G.P. Chernova, IYu.N. Mikhaylovskiy, A.F. Lunev, M.A. Timonova, V.N. Modestova, T.V. Matveyeva, A.V. Byalobzheskiy, N.P. Zhuk, A.V. Shreyder, V.A. Titov, M.A. Vedeneyeva, A.A. Lokotilov, G.K. Berukshtis, O.G. Deryagina, A.Z. Fedotova, M.N. Fokin, Ye.N. Mirolyubov, N.I. Isayev, R.M. Al'tovskiy, P.V. Shchiglev, L.S. Kupriyanova, O.N. Markova,

Card 2/24

Theory of Corrosion (Cont.) SOV/35	87
S.A. Baykova, L.A. Leonidova, and Professors S.G. Vedenk A.V. Ryabchenkov. Each chapter is accompanied by refere	in and nces.
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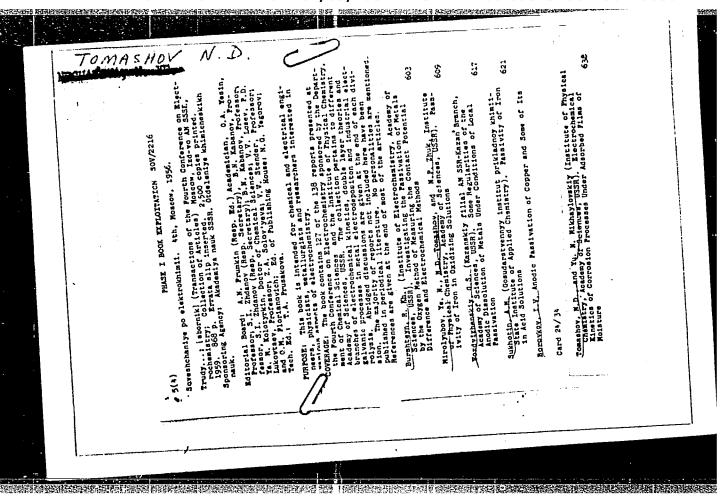


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s/081/60/000/020/008/014 A006/A001

Translation from: Referativnyy zhurnal, Khimiya, 1960, No. 20, p. 295, # 81439

AUTHORS:

Tomashov, N.D., Berukshtis, G.K.

TITLE:

A Method of Determining the Rate of Corrosion Processes Under Thin

Electrolyte Films 18 Tr. In-ta fiz. khimii, AN SSSR, 1959, No. 7, pp. 5-10

The authors describe a new electrochemical method of determining PERIODICAL: the corrosion rate from the magnitude of current on the model of a micro-corrosion element, assembled from thin dissimilar metal plates having different electrochemical potentials and serving as cathodes and anodes. The anode and cathode plates, alternating in the packet, are insulated from each other by a varnish or mica layer. The operating surface of the model is formed by the well-polished faces of the metal plates and the insulation. The conventional thickness of the metal plates in ~ 0.5 mm, and that of the insulation is 30 - 50 m. Contact panels are arranged on the lower section of the packet, connected with the model anodes by conductors; all the cathodes are parallel switched to one common conductor.

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85546

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A Method of Determining the Rate of Corrosion Processes Under Thin Electrolyte Films

1

This method of switching makes possible to switch off any number of electrodes in case of necessity and to change the correlation of the cathode and anode surfaces of the model. It is shown that this method makes possible the study of basic regularities: the effect of temperature, concentration and composition of the electrolyte, and the intensity of mixing the medium, on the corrosion rate in adsorption and visible moisture films and in the electrolyte volume; the method can be used to investigate the corrosion rate under various conditions.

A. Moskvicheva

Translator's note: This is the full translation of the original Russian abstract.

Card 2/2

s/081/60/000/020/004/014 A006/A001

Translation from: Referativnyy zhurnal, Khimiya, 1960, No. 20, p. 294, # 81433

Tomashov, N.D., Modestova, V.N., Blinchevskiy, G.K.

Methods of Investigating Corrosion and Electrochemical Behavior of AUTHORS:

Metals Under Stress TITLE:

Tr. In-ta fiz. khimii, AN SSSR, 1959, No. 7, pp. 64-77 PERIODICAL:

The design of a machine was developed for corrosion tests under stress with a time-constant load, permitting the operation at higher temperatures and measuring simultaneously the potential of the specimen. The corrosion behavior under stress of MA9 alloy was tested (low-alloy magnesium base alloy) in 0.001 n. NaCl solution and in a solution containing 35 g/l NaCl + 20 g/l  $K_2CrO_4$ . It is shown that in 0.001 n. NaCl solution, when stress is absent, the corresion defects appear in the form of multiple rounded micropittings. In the presence of stress, the micropittings transform into slits or intercrystallite cracks. In a 35 g/l

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CIA-RDP86-00513R001756210008-1" **APPROVED FOR RELEASE: 04/03/2001** 

S/081/60/000/020/004/014 A006/A001

Methods of Investigating Corrosion and Electrochemical Behavior of Metals Under Stress

NaCl + 20 g/l  $K_2\text{CrO}_h$  solution, coarse spotty corresion is observed. The stress does practically not affect the shape of pittings.

From the authors' summary

Translator's note: This is the full translation of the original Russian abstract.

Card 2/2

3/137/60/000/008/009/009 A006/A001

Translation from: Referativnyy zhurnal, Metallurgiya, 1960, No. 8, p. 316, # 18903

AUTHORS:

Tomashov, N. D., Isayev, N. I.

TILE:

Using the Ohmic-Capacity Method to Investigate the Behavior of Protective Films During Corrosion of Metals in Strained State

PERIODICAL: Tr. In-ta fiz. khimiy, AN SSSR, 1959, No. 7, pp. 78-84

The authors describe a method consisting in the combined measurement of a double electric layer on metal surfaces (metal-electrolyte) and of the chmic resistance, to study the state of a protective oxide film during corrosion under tensile stress conditions. There are 7 references.

Yu, L.

Translator's note: This is the full translation of the original Russian abstract.

Card 1/1

5373

S/081/60/000/017/007/016 A006/A001

26./620
Translation from: Referativnyy zhurnal, Khimiya, 1960, No. 17, pp. 74-75, # 68756

AUTHORS:

Fekin, M.N., Matveyeva, T.V., Tomashov, N.D.

TIPLE:

Cells for Testing Metal-Solution Systems Under the Effect of Electronic Radiation With Consideration of Polarization Phenomena

PERIODICAL: Tr. In-ta fiz. khimii AN SSSR, 1959, No. 7, pp. 114-118

Designs of a cell are suggested where the metallic electrode is pelarized anodically (cell a) and cathodically (cell b) during electronic irradiation of the metal solution system. Characteristics of radiation are: electron tion of the metal solution system. Characteristics of radiation are: electron tion of the metal solution system. Characteristics of radiation are: electron tion of the electron flux: 3.3 x 10<sup>13</sup> electron/cm<sup>2</sup>. sec; energy 1 Mev; density of the electron flux: 3.3 x 10<sup>13</sup> electron/cm<sup>2</sup>. sec; power of a dose in a layer of the solution near the electrode of 1-mm thickness; power of a dose in a layer of the solution near the electrode of 1-mm thickness; power of a dose in a layer of the electron radiation energy). In cell ness of the layer of full absorption of the electron radiation energy). In cell "a" at a thickness of the solution layer equal to 1 mm, the corrosion rate of "a" at a thickness of the solution layer equal to 1 mm, the corrosion rate of

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85373

S/081/60/000/017/007/016 A006/A001

Cells for Testing Metal-Solution Systems Under the Effect of Electronic Radiation With Consideration of Polarization Phenomena

1X 18H9T (1Kh18N9T) steel is by 2 orders of magnitude higher than that of a non-irradiated specimen. The nature of destruction and the corrosion rate in irradiation are different from those with anodic polarization of the specimen from an external current source. These differences were not observed if the thickness of the layer was 10 mm. The placing of a protector or cathodic polarization of the specimen in cell "a" protects it against increased corrosion during irradiation/

D. Kokoulina

Translator's note: This is the full translation of the original Russian abstract.

Card 2/2

S/081/60/000/017/008/016 A006/A001

Translation from: Referativnyy zhurnal, Khimiya, 1960, No. 17, p. 75, # 68757

Tyukina, M.N., Zalivalov, F.P., Tomashov, N.D. AUTHORS:

18

TIME:

Electron-Microscopical Study of the Microstructure of Anodic Oxide

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Films on Aluminum

Tr. In-ta fiz. khimii, AN SSSR, 1959, No. 7, pp. 165-174

The authors studied the effect of electrochemical conditions of ob-PERIODICAL: taining accide oxide films on Al upon their structure and physicc-chemical properties. The Al surface was investigated after removal of the oxide film in hot solution of 35 mi/1 H\_PO4, and 20.g/1 CrO. The surface of the oxide film and the transverse and longitudinal splits of the oxide film were also studied. A method is described of obtaining carbon imprints from anodic oxide film splits. It is shown that anodic oxide films on Al surfaces consist of close-packed cells in the form of hexagonal prisms, arranged with their base faces parallel to the ancde surface. The cellular structure is formed within 3-7 sec after application of the anode current, and does not change with a further growth of the oxide film

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Electron-Microscopical Study of the Microstructure of Anodic Oxide Films on Alaminum

thickness. The pore size in the exide film increase linearly with an increase of the forming tension. It is shown that the particular properties of anodic exite films (nardness, resistance against corrosion and wear) obtained by the method of hard anodizing, are explained by the increased size of exide cells, forming the exide film, due to the thickening of their walls.

Yu. Polukarov

Translator's note: This is the full translation of the original Russian abstract.

Card 2/2

#### CIA-RDP86-00513R001756210008-1 "APPROVED FOR RELEASE: 04/03/2001

9 (6)

Zalivalov, F. P., Tyukina, M. N.,

507/32-25-6-17/53

AUTHORS: Tomashov, N. D.

TITLE:

Investigation of the Microstructure of Anodic Oxide Films on

Aluminum by the Aid of the Electron Microscope (Issledovaniye mikrostruktury anodnykh okisnykh plenok na

alyuminii pri pomoshchi elektronnogo mikroskopa)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, pp 696-698 (USSR)

ABSTRACT:

A method was devised, permitting the determination of the cell structure of anodic oxide films on aluminum (Fig 1). By this method no impression is taken of the film on the metallic anode surface (Ref 1); instead, replicas are prepared of such films. The method is based on the operation of taking off and subsequently comminuting the oxide film, thus obtaining microscopic particles which are split along the side-(longitudinal section) or bottom- (cross section) plane of the hexagon lattice structure. Reproductions of these planes of shear may be obtained by the carbon-replica method (Ref 2). The preparation procedure is described. Observations were made with the electron microscope EM-3 or UEM-100, and the samples under investigation were of AVOOO aluminum (99.99 % Al), which

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Investigation of the Microstructure of Anodic Oxide SOV/32-25-6-17/53 Films on Aluminum by the Aid of the Electron Microscope

were oxidized anodically in a 4 % sulphuric acid solution by the method of the hard anodization (Refs 3, 4) (Figs 2, 3). The figures show that the oxide film is a dense packing of cells in the form of hexagon prisms. Data are supplied of the dimension and quantity of cells (Table); they agree with data obtained with an earlier described method (Ref 1). There are 3 figures, 1 table, and 4 references, 2 of which are Soviet.

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

Card 2/2

SOV/32-25-6-19/53

28(5) AUTHORS: Tomashov, N. D., Isayev, N. I.

TITLE:

Method of Investigating Corrosive and Electrochemical Properties of Metals in the State of Stress (Metod issledovaniya komrozionnykh i elektrokhimicheskikh svoystv metallov v napryazhennom sostoyanii)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, pp 700 - 702 (USSR)

ABSTRACT:

Phase oxide films on metal surfaces exhibit a greater electric resistance so that a change in electric resistance and capacity is observable when submitting a sample to a stress causing the destruction of the oxide film. The degree of film destruction may be evaluated by the rate and magnitude of such variations. A system was devised besed on this principle and used for the investigation of the surface oxide layer state according to the electric resistance-capacity method in sample stressing treatments. It may be observed from the scheme of the system (Fig 1) and from the description that an electric current supplied by an AC generator ZG-10 and having a potential of 10-15 mv is used here. The circuit compensation is done by selecting appropriate capacities with the AC current resistor KMS-6. The

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Method of Investigating Corrosive and Electrochemical SOV/32-25-6-19/53 Properties of Metals in the State of Stress

compensation moment is determined according to the minimum of the AC current amplitude on the oscillograph. The test takes place in a special vessel (Fig 2) in which the wire-shaped sample is stretched (diameter 1-2 mm). The experimental results obtained (Fig 3 on anodized aluminum, Fig 4 electropolished Al, Fig 5 stainless 3Kh13 steel) show that in the case of deformations damaging the oxide film the capacity of the latter is increased, electric resistance drops and the electrode potential shifts to more negative values. This holds for the case that the new-formed oxide films (on the damaged spots) exhibit a weaker electric resistance than the primary films. To be sure, also new oxide films may form whose conductivity is lower than the one of primary films as, for example, is the case with 3Kh13 steel in 12 n HNO3 (Fig 6). There are 6 figures.

ASSOCIATION: Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences of the USSR)

Card 2/2

28 (5) AUTHORS:

Tomashov, N. D., Byalobzheskiy, A. V., SOV/32-25-6-31/53

Val'kov, V. D., Zalivalov, F. P.

TITLE:

Device for the Rapid Determination of the Quality of Anodic Oxide Films on Aluminum and Its Alloys (Pribor dlya bystrogo

opredeleniya kachestva anodnykh okisnykh plenok na

alyuminii i yego splavakh)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, pp 738-739 (USSR)

ABSTRACT:

For the detection of defective parts of anodic films the device K-1 by G. V. Akimov and Ye. N. Paleolog is usually used. The device permits the detection of very small defects, does, however, not indicate the general quality of the film; another disadvantage is the use of a sodium chloride solution which may lead to a corrosion of the film. Therefore, a new device was designed, K-2 - very similar to K-1; the mode of operation of the new device is based upon the fact that the conductivity of the anodic oxide film is the greater the more porous it is. The construction of the detector of defects (Fig 1) is somewhat modified, stainless steel 1 Kh18N9 or zink serve e. g. as electrode as copper

and aluminum may together form an electric cell. The device

Card 1/2

Device for the Rapid Determination of the Quality of SOV/32-25-6-31/53 Anodic Oxide Films on Aluminum and Its Alloys

(Fig 2, Scheme) has piles as direct-current transmitters (2-4 v) so that a non corroding electrolyte may be used (0.1 % solution of potassium or sodium bichromate). There are 2 figures.

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

Card 2/2

18 (7) AUTHORS:

Tomashov, N. D., Andreyev, L. A.,

05727 s0v/32-25-10-16/63

Isayev, N. I.

TITLE:

Comprehensive Investigation of Stress-Corrosion Cracking Processes

PERIODICAL:

Zavodskaya laboratoriya, 1959, Vol 25, Nr 10, pp 1200 - 1203

(USSR)

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ABSTRACT:

A device and a suitable method for simultaneous microscopic and electrochemical investigation of stress-corrosion cracking processes were developed. The device includes a tensile-testing machine with a visual and measuring recording system. Axial machine with a visual and measuring recording system. Axial tensile loads up to 250 kg can be applied; the total electrode potential of the metal, and the potentials in the resulting cracks, are automatically recorded, and visual observation of the propagation kinetics of cracks is possible. The tests are carried out in a corroding medium which is constantly renewed. The loading (stretching) takes place on the tensile-testing machine (Fig 1) by means of a metal spring, and is adjusted by a set wheel. Visual observation of the sample (of cracks) is done by a microscope of type MIS-11. The tensile-testing machine was adjusted by a dynamometer of type DS-1. Immediately before the test loading, the corroding liquid was put on the

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Comprehensive Investigation of Stress-Corrosion Cracking Processes

sample by a glass tube. The changes in the electrochemical potential in the cracks were measured by means of appropriate capillaries, an electron amplifier (Fig 2, Diagram), and a loop oscillograph of type MPO-2. The corrosion of alloy MA 2 was tested in a solution of  $Na_2CrO_4(20 \text{ g/1})$  and NaCl (35 g/1). The oscillogram (Fig 3) of the potential changes on the sample surface on stretching shows that, by the destruction of the oxide film, an intense formation of anode segments occurs producing a maximum in the oscillogram. New microcells (oxide-film pores) formed at the same time effect a retardation of anodic polarization on the whole metal surface. The appearance of cracks causes the formation of a steadily increasing anodic segment. From a visual point of view, the propagation of cracks can be divided into 3 periods: (1) The incubation period (from the beginning of loading until the formation of cracks); (2) the period of uniform propagation of cracks (formation of hydrogen bubbles), and (3) the period of accelerated crack development (apparently of purely mechanical character). An increase in load shortens the first and second periods, and slightly ac-

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05727

Comprehensive Investigation of Stress-Corrosion Cracking 50V/32-25-10-16/63 Processes

celerates the third one. The results obtained confirm the assumption of a film-electrochemical mechanism of stress corrosion cracking. There are 3 figures and 2 references, 1 of which is Soviet.

ASSOCIATION: Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

Card 3/3

sov/76-33-3-17/41 5(4), 18(7) Tomashov, N. D., Al'tovskiy, R. M. AUTHORS: Investigation of the Mechanism of Electrochemical Corrosion of Titanium (Issledovaniye mekhanizma elektrokhimicheskoy TITLE: korrozii titana). I. Effect of the Halogen Ions Upon the Corrosion and Electrochemical Behavior of Titanium in Sulfuric Acid (I. Vliyaniye galoidnykh ionov na korrozionnoye i elektrokhimicheskoye povedeniye titana v sernoy kislote) Zhurnal fizicheskoy khimii, 1959, Vol 33, Hr 3, PERIODICAL: pp 610 - 616 (USSR) Recently several investigations have been carried out dealing with the corrosion properties of titanium, for ABSTRACT: titanium has properties well suited for construction material. The present paper deals with the effect of the Cl -, Br and J- ions upon the behavior of Ti in sulfuric acid solutions. Cold-rolled titanium tin VT-1D (0.12% Fe, 0.022 - 0.023% H, 0.23 - 0.26% O, 0.05% Si and 0.017% N) was investigated. The experiments were carried out in the air and in hydrogen atmosphere. The rate of corrosion was Card 1/ 3

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

Investigation of the Mechanism of Electrochemical SOV/76-33-3-17/41 Corrosion of Titanium. I. Effect of the Halogen Ions Upon the Corrosion and Electrochemical Behavior of Titanium in Sulfuric Acid

determined according to the loss in weight and the halogen ions were added in form of their Na-salts. The experimental results obtained confirm the assumption that the corresion behavior of Ti is determined by a coating of an oxide film on the metal. Thus, it is possible to explain observations as to a Ti-activation in diluted sulfuric acid in the presence of oxygen and a considerable potential shift towards more negative values in connection with a purification of the titanium surface. The addition of J-ions produced in several cases an increased corrosion resistance of titanium which is due to a passivation by the formation of a complex ion J3. Cl - and Br - ions have a double effect; in diluted acid solutions where titanium is passivated they cause an activation; and in concentrated acid solutions with activated titanium they cause a passivation. The nature of the effect of Cl - and Br - ions depends on the state of the Ti-surface and the formation of an adsorption- or phase protective film respectively. There are 5 figures and 13 references, 6 of

card 2/3

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sov/76-33-3-17/41 Investigation of the Mechanism of Electrochemical Corrosion of Titanium. I. Effect of the Halogen Ions Upon the Corrosion and Electrochemical Behavior of Titanium in Sulfuric Acid

Which are Soviet.

ASSOCIATION:

Akademiya nauk SSSR, Institut fizicheskoy khimii, Moskva (Academy of Sciences, USSR, Institute of Physical Chemistry,

Moscow)

July 18, 1957 SUBMITTED:

Card 3/3

SOY/20-124-6-29/55 Tomashov, H. D., Mikhaylovskiy, Yu. N. 5(2,4)

Mechanism of Anodic Dissolution of Metals in Soils (Mekha-AUTHOR: TITLE:

nizm anodnogo rastvoreniya metallov v pochvakh)

Doklady Akademii nauk SSSR, 1959, Vol 124, Hr 6, PERIODICAL:

pp 1285 - 1288 (USSR)

For the dissolution mentioned in the title as well as for ABSTRACT:

electrolytes the general equation holds:

 $\text{Me}^{+n}$   $\text{mH}_2\text{O}$  +  $\text{ne}_0$ , in which the primary stage

of the process is a migration of the metal ion into the soil electrolyte. As far as the anodic process is accompanied by a hydration of the forming metal ions the presence of a certain amount of moisture in the soil is an indispensable condition (Ref 1). Greater variations in the moisture of natural soils may have a considerable influence upon the rate of anodic metal dissolution. In this connection the authors mention the investigation results of the aforesaid process in the case of "Armko" iron in soils of different

card 1/3

CIA-RDP86-00513R001756210008-1"

**APPROVED FOR RELEASE: 04/03/2001** 

Mechanism of Anodic Dissolution of Metals in Soils

SOV/20-124-6-29/55

moisture. Figure 1 gives anodic polarization curves obtained in the case of iron electrodes in sand with 1-20% moisture in which case the moisture was added in form of MaCl solution. From the results it can be seen that the stable potential of iron is shifted into the positive range in the case of decreasing soil moisture; the inhibitions of the anodic reaction increase. A similar dependence exists in loam coils. From the results obtained it can be seen that the density of the self-dissolution currents increases with decreasing soil moisture, i.e. in connection with making less complicate the cathodic process (Ref 1) whereas, the stable potential of iron is shifted on the general curve 1 into the positive range (Fig 5). Thus, the corrosion rate increases as calculated for the active (just moistened) anodic surface with decreasing soil moisture. If the this rate is calculated for the visible surface the former will increase only as long as the making less complicated at the cathodic process proceeds more rapidly then the shrinking of the active surface. In the case of a further decrease in moisture the entire rate of metal corrosion will decrease in consequence of the passivation of the basic surface of

Card 3/3

Mechanism of Anodic Disselution of Metals in Soils

507/20-124-6-29/55

the metal. There are 3 figures, 1 table and 6 Soviet refer-

ASSCCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USUR)

PRESENTED:

November 6, 1958, by V. I. Spitsyn, Academician

SUBMITTED:

November 3, 1958

Card 5/3

5 (4) AUTHORS:

Mirolyubov, Ye. N., Kurtepov, M. M.,

SOV/20-125-6-32/61

Tomashov, N. D.

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TITLE:

On Some Particular Features of the Cathode Process on Stainless Steel in Solutions of Nitric Acid (O nekotorykh osobennostyakh katodnogo protsessa na nerzhaveyushchikh stalyakh v rastvorakh azotnov kisloty)

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 125, Nr 6, pp 1288-1291 (USSR)

ABSTRACT:

The processes mentioned in the title were investigated by plotting cathode-polarization curves (Fig 1). Investigations were carried out for chromium- and chromenickel steels

containing niobium, and, for comparison, a platinum electrode. The dependence of corrosion on the potential is shown by figure 2. The following was found: The maximum current depends on the composition of the electrode; overvoltage in the cathode process is lower in the case of steel than in that of platinum. These phenomena are explained by a

disturbance of passivation as a result of cathodic polarization

followed by the formation of nitrous acid (as autocatalyst) by the reducing effect exercised by the substances removed

Card 1/2

6

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On Some Particular Features of the Cathode Process on SOV/20-125-6-32/61 Stainless Steel in Solutions of Nitric Acid

from the steel upon the nitric acid. There are 2 figures and 11 references, 5 of which are Soviet.

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute for Physical Chemistry of the Academy of Sciences, USSR)

PRESENTED:

January 24, 1959, by A. M. Frumkin, Academician

SUBMITTED:

January 24, 1959

Card 2/2

5(4)

AUTHORS:

Tomashov, N. D., Isayev, N. I.

SOV/20-126-3-45/69

TITLE:

The Stability of the Passive State of Mechanical Stresses in Metals (Ustoychivost' passivnogo sostoyaniya mekhanicheski

PERIODI CAL:

Doklady Akademii nauk SSSR, 1959, Vol 126, Nr 3, pp 619-622 (USSR)

ABSTRACT:

It is said in the introduction to the present paper that the influence of mechanical stresses upon the electrode potential has hitherto been hardly investigated and that it may be seen from such publications as are available that mechanical stresses shift the electrode potential in the negative direction. It is looked upon as obvious that the variation of the cathode potential is caused by a variation of the internal energy of the metal; a corresponding equation is given with formula (1). For the case in which the thermal effect of deformation is low compared to the mechanical work of deformation, formula (2) is given for the variation of the cathode potential. The variations of the cathode potential are described as being very small on the basis of these formulas, even in the case of strong deformation, and they never exceed 3 - 5 mv. As experimental measuring values are higher, the destruction of the oxide film is considered to be a

Card 1/3

**APPROVED FOR RELEASE: 04/03/2001** CIA-RDP86-00513R001756210008-1"

The Stability of the Passive State of Mechanical Stresses SOV/20-126-3-45/69

further cause of the variation of the cathode potential in the case of further stresses. It is then said that the state of the oxide film determines the active or passive state of the metal, and that it is thus possible to investigate the influence exercised by mechanical stresses upon the passive state of the metal. The experiments were carried out on wire samples, and the alloys and their mechanical properties are given. As a corroding medium, a solution of NaNO, and K2Cr2O7 is given. The results obtained are shown by diagrams. The first diagram (Fig 1) shows the variation with respect to time of the potential and of capacity in the primary passivation of carbon steel, and the second diagram (Fig 2) shows the same for stainless steel. It was found that, in the case of the carbon steel investigated, the potential goes over into the active state if the short-time stress causes a plastic deformation of the metal. In the case of the stainless steel investigated, only very slight activation is caused even in the case of mechanical stress being very high. Finally, it is shown that at the moment at which the stress is applied two factors become active in the metal. The one is

Card 2/3

The Stability of the Passive State of Mochanical Stresses SOV/20-126-3-45/69

mechanical stress, which has an activating effect, the other is the oxidizing agent, which counteracts activation. After the decrease of the deformation of the oxide film, passivation by the solution predominates. There are 3 figures and 10 references,

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

PRESENTED:

February 11, 1959 by P. A. Rebinder, Academician

SURMITTED:

January 29, 1959

Card 3/3

"The corrosion and passivity of titanium."

report to be submitted at Gordon Research Conferences - New London, New Hampton, and Meriden, N.H., 13 June-2 Sep 60.

Institute of Physical Chemistry.

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	Dymov, A. M., Doctor of Chemical Sciences, a Candidate of Chemical Sciences [Department of tard 9/10]	The ablut, N. D., Doctor of Chemical Sciences, and N. P. Duk, and T. R. Mirolyukov, Candidates of Chemical Sciences (Department of Corrosion of Netals). Behavior of Iron and Steel in Oxidizing Solutions	<pre>Opting_R_TCandidate of Technical Sciences [Department Lieotrotechnics]. Magnetic Viscosity of High-Coercivity Al</pre>	Rolling). A. T., and O. S. Popov, Engineer [Department of Rolling). Investigation of the Deformation of Metal in Diagonal Beam Passes	Gorelik, 3. 3. Docent, Candidate of Technical Sciences, Y. M. REMANDY. Engineer, and Is. I. Shchedrin, Engineer Department of the Engrals of Metals and K-Rays Mailysis). Effect of Strain Distortions and Aging on the Diffusion Rate in Mickel-Based Alloys	Card 2/10	al investigations of metallurgical and heat-enrineering processes in open-hearth and electric Nurnaces. Data are included on the following: deaulivrizing of pig iron outside the blast furnace, interaction of oxides of the carbide-forming metals with solid carbon, the change of centent of gases in the bath of the open-hearth furnace in warlous periods of melting, intensitication of the science melting of steal, etc. Other articles deal with the normalformity of deformation in rolling, because the study of the continuous rolling process, the dependence of the triction—alippage coefficients in rolling on a number of factors, and other problems in the pressworking of metals. Articles on physical metallurgy and the theoretical principles and techniques of the art mentioned. References accompany most of the articles. There are 207 references, both Joviet and non-Joviet.	also be used by students specializing in GOVERAGE: The book contains results of thec	PURPOUR: This book is intended for technical personnel in industry, selectific institutions and schools of higher education, dealing with open-hearth and electric-furnance steelhading, setal rolling, physical metallurgy, metallography, and heat-treatment. It may card 1/10	Ed.: Ye. A. Borko: Ed. of Publishing House: S. L. Inger; Tech. Ed.: M. R. Kleymann; Editorial Council of the Institute: W. A. Glinkow, Frofessor, Doctor of Technical Sciences; R. N. Grigorash, Docest, Candidate of Technical Sciences; Y. Telyutin, Frofessor, Doctor of Technical Sciences; A. A. Zunkhowitskiy, Frofessor, Doctor of Chemical Sciences; A. A. Zunkhowitskiy, Doctor of Technical Sciences; B. G. Livshits, Frofessor, Doctor of Technical Sciences; A. P. Nublmoy, Frofessor, Doctor of Technical Sciences; A. R. Pavboy, Corresponding Nesber, Academy of Sciences USSR; and A. M. Fokhvisney, Frofessor, Doctor of Technical Sciences	Prolyrodstro 1 obrabotka stall 1 splayov (Production and Treatment of Steel and Alloys) Moscow, Metallurgizat, 1960. 462 p. (Series: Its: Sbornik, 39) 2,100 copies printed.	PRASE I BOOK EXPLOITATION - Moscow. Institut stall	
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Methristallitanya borroziya i korroziya metallov v naprysahemosa sostoyanii (Literorretalline and Stress Corrosion of Metall) Moscov, Mashpit, 1960,	Methiristallitonya korrosiya i korrosiya metallov v naprysahornom sosteyunii (Intercrystalline and Stress Corrosion of Metalu) Moscov, Mashgir, 1960, 198 p. 3,000 copies primad.
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27215 S/081/61/000/014/013/030 B103/B217

AUTHORS:

Tomashov, N. D., Mikhaylovskiy, Yu. N.

TITLE:

Electrochemical theory of underground corrosion of metals

PERIODICAL:

Referativnyy zhurnal. Khimiya, no. 14, 1961, 332, abstract 14 182. (Tr. In-ta fiz. khimii. AN SSSR, 1960, vyp. 8,

190 - 216

TEXT: The authors examined data on the effect of soil structure and properties (humidity, permeability) on cathodic and anodic processes in underground corrosion. It was found that the rate of uniform total corrosion  $I_{corr}$  of a metal in the soil can be calculated from the equation  $I_{corr} = KI_KI_a/(I_K + I_a)$ , where K is a constant,  $I_K$  is the density of the cathodic limiting current at an iron electrode in the soil concerned (oxygen permeability of soil),  $I_a$  is the density of the anodic current at a given potential. The rate of local corrosion ( $\bullet$ ) can be estimated from the oxygen permeability of soil  $I_K$  and from its resistance (?):  $AI_K/?$ ,

Card 1/2

Electrochemical theory of ...

27215 S/081/61/000/014/013/030 B103/B217

where A is a constant. The possibility of formation of large macrofields is determined by the equation  $I = B\Delta I_{K}/\Delta I_{F}^{-1}$ , where B is a constant,  $I_{K}/\Delta I_{F}^{-1}$  is the change of oxygen permeability in a soil section of length  $\Delta I$ . On the basis of these assumptions a device for estimating the corrosive activity of soils was designed and constructed. [Abstracter's note: Complete

X

Card 2/2

TOMASHOV, N.D.; MIKHAYLOVSKIY, Yu.N.; LEONOV, V.V.

Investigating the work of differential aeration couples in soils.
Trudy Inst.fiz.khim. 8:217-225 160.

(Soil corrosion)

TOMASHOV, N.D.; KRASNOYARSKIY, V.V.; MIKHAYLOVSKIY, Yu.N.

Field testing of the corrosion of steels insoils. Trudy Inst.fiz.
khim. 8:226-234 '60. (MIRA 14:4)

(Steel—Corrdsion) (Soil corrosion)

TOMASHOV, N.D.; LUNEV, A.F.; IGNATOVA, Z.I.

Studying the protective properties of coatings by the capacitance—
-resistance method. Trudy Inst.fiz.khim. 8:254-263 '60.

(MIRA 14:4)

(Protective coatings—Testing) (Electric testing)

TOMASHOV, N.D. LUNEV, A.F.; GEDGOVD, K.N.

Investigation of ion penetration and the portative of protective coatings by means of tagged atoms. Trudy Inst.fiz.khim. 8:264-275 '60. (MIRA 14:4)

(Protective coatings—Testing) (Ions—Migration and velocity)
(Radioactive tracers)

TOMASHOV, N.D.; MIKHAYLOVSKIY, Yu.N.; LOPOVOK, G.G.

Testing of insulation coatings for cracking during flexure. Trudy
Inst.fiz.khim. 8:276-280 '60. (MIRA 14:4)

(Protective coatings—Testing)

KRASNOYARSKIY, V.V.; LUNEV, A.F.; TOMASHOV, N.D.

Field testing of protective coatings on underground pipelines.
(NIRA 14:4)
(Pipelines—Corrosion) (Protective coatings—Testing)

TOMASHOV, N.D.; MIKHAYLOVSKIY, Yu.N.; LEONOV, V.V.

Kinetics of the deterioration of portective coatings on metals in electrolytes. Trudy Inst.fiz.khim. 8:291-296 '60. (MRA 14:4)

(Protective coatings) (Electrolytic corresion)

TOMASHOV, N.D.; MIKHAYLOVSKIY, Yu.N.; LEONOV, V.V.

Kinetics of cathodic processes in the corrosion of metals under protective coatings. Trudy Inst.fiz.khim. 8:297-304 '60.

(MIRA 14:4)

(Protective coatings) (Electrolytic corrosion)

TOMASHOV, N.D., doktor khimicheskikh nauk; ZHUK, N.P., kand.khimicheskikh nauk; MIROLYUBOV, Ye.N., kand.khimicheskikh nauk

Behavior of iron and steel in oxidising solutions. Shor. Instabli no.39:438-449 160. (MIRA 13:7)

1. Kafedra korrozii metallov Moskovskogo ordena Trudovogo Krasnogo Znameni instituta stali im. I.V.Stalina. (Iron--Corrosion) (Steel--Corrosion) (Oxidizing agents)

TOMASHOV, N.D.; AL'TOVSKIY, R.M.; KUSHNERBY, M.Ya.

Method for removing thin oxide films from titanium surfaces and study of their structures. Zav.lab. 26 no.3:298-301 '60. (MIRA 13:6)

1. Institut fizicheskoy khimii Akademii nauk SSSR. (Titanium oxides)

18,8310

27514 \$/080/60/033/006/019/041/XX D217/D302

AUTHORS:

Tomashov, N.D., Chernova, G.P., and Markova, O.N.

TITLE:

Influence of anodic polarization on the intercrystalline corrosion of stainless chromium-nickel steels

PERIODICAL: Zhurnal příkladnov khimii, v. 33, no. 6, 1960, 1324 - 1334

TEXT: The possibility of protecting steels against general and intercrystalline corrosion by means of anodic polaritation in sulphuric acid solutions and in solutions used for testing the tendency to intercrystalline corrosion, was investigated. The material tested was 2X18H9 steel (2Kh18N9) (free from titanium), containing 0.15 - 0.25 % C. This steel, as quenched from 1050° and subsequently tempered at 650° for 2 hours, is known to be liable to fail by intercrystalline corrosion. Untempered, however, it does not tend to fail by this mechanism. This steel was therefore tested in both conditions. The tendency to failure was determined after boiling in a solution of the following composition: 160 g

Card 1/3

27514 S/080/60/033/006/019/041/XX D217/D302

Influence of anodic polarization ... DZI(/DDOZ)

CuSO<sub>4</sub> · 5H<sub>2</sub>O + 100 cm<sup>3</sup>H<sub>2</sub>SO<sub>4</sub> (s·g· = 1.84) + 1000 ml H<sub>2</sub>O with addition of copper filings. The behavior of the stainless steel 2Khl8-tion of copper filings. The behavior of the stainless steel 2Khl8-N9 was investigated in the above range of potentials (from - 0.13 N9 was investigated in the above range of potentials (from - 0.13 N9 was investigated in the above range of potentials (from - 0.13 N9 was investigated in the above range of potentials corrosion. The methods of protecting it against intercrystalline corrosion. The methods of protecting it against intercrystalline corrosion was carried out by plotting polarization curves by pocorrosion was carried out by plotting polarization curves by pocorrosion was carried out by plotting polarization of It was found that the range of the stable, passive condition of It was found that the range of the stable, passive state, this range reduces to 0 to + 0.4 V. In the tempered condition, this lies between + 0.51 and + 0.83 V. In the tempered condition, this range reduces to 0 to + 0.4 V. In the stable, passive state, this range reduces to 0 to + 0.4 V. In the stable, passive state, this sion is extremely slight and anodic protection in this case is sion is extremely slight and anodic protection in this case is sion is extremely slight and anodic protection in this case is sion is extremely slight and anodic protection in this case is sion is extremely slight and anodic protection in this case is sion is extremely slight and anodic protection in this case is stable, passive range of the tempered steel is reduced to a greater extent than that of quenched steel, and in a strongly aggrester extent than that of quenched steel, and in a strongly aggrester

Card 2/3

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

27514 \$/080/60/033/006/019/041/XX D217/D302

Influence of anodic polarization ...

sive medium may be entirely absent. In the transpassivity region, the tempered steel is liable to fail be intercrystalline corrosion, whereas the quenched steel is not. Protection against intercrystalline corrosion in the passive potential range by means of crystalline corrosion in the passive potential range by means of anodic polarization is possible both in the copper supplate-base testing solution and in solutions containing 10 % HNO<sub>3</sub> + 1 or 2 %

NaF. There are figures, 4 tables and 10 references: 8 Sovietbloc and 2 non-Soviet-bloc. The reference to the English-language publication reads as follows: R. Edelenau, Nature, 17, 739, 1954.

SUBMITTED: November 24, 1959

X

Card 3/3

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

80232 8/076/60/034/04/22/042 BO10/BO09

5.4600 AUTHORS:

Tomashov, N. D., Paleolog, Ye. N., Fedotova, A. Z. (Moscow)

Electrochemical and Corrosion Behavior of Semiconductors in Electrolyte Solutions. I. Electrode Processes on Germanium in TITLE:

Sulfuric Acid Solutions in the Presence of Hydrogen Peroxide

Zhurnal fizicheskoy khimii, 1960, Vol. 34, No. 4, pp. 833 - 840 PERIODICAL:

TEXT: Since germanium is the electron semiconductor now most frequently used the kinetics of the electrode processes of germanium monocrystals of the n- and p-types in sulfuric acid solutions with different hydrogen peroxide contents was investigated in the present paper. The samples were polished or etched in an SR-4 solution (15 cm<sup>3</sup> CH<sub>3</sub>COOH, 25 cm<sup>3</sup> HNO<sub>3</sub>, 15 cm<sup>3</sup> HF, and 0.06 cm<sup>3</sup> Br<sub>2</sub>). The curves of cathodic polarization (Fig. 1) of n-type germanium show that this material behaves, in principle, like a metal electrode. With regard to the discharge of hydrogen ions n-germanium is not an effective cathode and exhibits a high hydrogen supertension. Table 1 shows the change in the hydrogen peroxide concentration of a sulfuric acid solution (pH = 1) + 0.11 M  $H_2O_2$  in the cathodic

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Electrochemical and Corrosion Behavior of Semiconductors in Electrolyte Solutions. I. Electrode Processes on Germanium in Sulfuric Acid Solutions in the Presence of Hydrogen Peroxide

80232 s/076/60/034/04/22/042 B010/B009

polarization of n-germanium in the presence of air at 25°C. The process continues until H<sub>2</sub>O<sub>2</sub> is reduced, and the cathodic polarization of germanium is greatly decreased. The cathodic polarization of p-germanium is more inhibited than that of creased. The cathodic polarization as well as the hydrogen ion discharge. This n-germanium, i.e., the H<sub>2</sub>O<sub>2</sub> reduction as well as the hydrogen ion discharge. This may be due to an additional potential drop on account of the reduction of the may be due to an additional potential drop on account of the reduction reaction on p-germanium is played by the electrons in the zone of valency. The anodic tion on p-germanium differs from that of n-germanium. The anodic dissolution behavior of p-germanium differs from that of n-germanium. The anodic dissolution p-germanium is similar to that on normal metal. With current densities up to on p-germanium remains active in all solutions and dissolves into Ge<sup>4+</sup>.

30 ma/cm<sup>2</sup> p-germanium remains active in all solutions and dissolves into Ge<sup>4+</sup>.

The velocity of delivery of the holes to the surface of n-germanium. This results garded as determining the anodic dissolution process of n-germanium. This results in a marked ability of the electrode to be polarized and in the occurrence of an anodic saturation current whose magnitude is independent of the composition of the solution and increases when the electrode is exposed to light. There are

Card 2/3

80232

Electrochemical and Corrosion Behavior of Semiconductors S/076/60/034/04/22/042 in Electrolyte Solutions. I. Electrode Processes on B010/B009 Germanium in Sulfuric Acid Solutions in the Presence of Hydrogen Peroxide

5 figures, 2 tables, and 7 references, 1 of which is Soviet.

 $\mathcal{H}$ 

ASSOCIATION: Akademiya nauk SSSR Institut fizicheskoy khimii (Academy of

Sciences USSR Institute of Physical Chemistry)

SUBMITTED: July 4, 1958

Card 3/3

S/076/60/034/05/14/038 B010/B002

5.4600 AUTHORS:

Paleolog, Ye. N., Tomashov, N. D., Fedotova, A. Z.

TITLE:

Electrochemical and Corrosion Behavior of Semiconductors in Electrolyte Solutions. II. The Rate of Solution of Germanium

in Sulfuric Acid in the Presence of Hydrogen Peroxide

PERIODICAL:

Zhurnal fizicheskoy khimii, 1960, Vol. 34, No. 5,

pp. 1027-1031

TEXT: The dissolution of germanium in electrolyte solutions has not yet been investigated systematically though this problem is of special importance for the production of semiconductors, i.e., for the etching of the surface of germanium. In the present paper, the authors studied the dissolution of n-type and p-type germanium in  $H_2SO_4$  (pH=1),  $H_2SO_4$  (pH=1) + + 0.12 M  ${
m H_2O_2}$  and 8.8 M  ${
m H_2O_2}$ . The solution was carefully mixed, and the rate of dissolution was determined at 25°C by a colorimetric determination of the germanium content of the solution in certain intervals. The analyses were carried out by L. S. Kupriyanova. The results obtained (Table) show that the rate of dissolution is independent of the type of germanium (n-type or p-type) and rises in the presence of H202. Furthermore, it changes little in time. A cathodic or anodic polarization of the germanium electrode

Card 1/2

Electrochemical and Corrosion Behavior of Semiconductors in Electrolyte Solutions. II. The Rate of Solution of Germanium in Sulfuric Acid in the Presence of Hydrogen Peroxide

S/076/60/034/05/14/038 B010/B002

leads to a decrease in the rate of dissolution. On the strength of the results obtained the authors establish that under the present experimental conditions the dissolution of germanium has an electrochemical nature. As the dissolution of n-type germanium by means of H<sub>2</sub>O<sub>2</sub> is raised with the

same intensity as in the case of p-type germanium, it is assumed that on the surface of n-type germanium the concentration of holes is higher, and that the cathodic process is facilitated by the reduction of hydrogen peroxide. There are 2 figures, 1 table, and 4 references: 1 Soviet, 2 German, and 1 American.

ASSOCIATION:

Akademiya nauk SSSR Institut fizicheskoy khimii

(Academy of Sciences of the USSR, Institute of Physical

Chemistry)

SUBMITTED:

August 4, 1958

Card 2/2

1018

1145

\$/076/60/034/009/008/022 B015/B056

5.4600 1153

AUTHORS:

Deryagina, O. G., Paleolog, Ye. N, and Tomashov, N. D.

TITLE:

Electrochemical and Corrosion Behavior of Semiconductors 74 in Electrolytic Solutions. III. Dissolution of Germanium

in Contact With Other Metals

PERIODICAL:

Zhurnal fizicheskoy khimii, 1960, Vol. 34, No. 9,

pp. 1952-1959

TEXT: In the fusion of n-type germanium with indium, a narrow band of a point of the fusion may be obtained. If electric contacts (Cu wires) are soldered onto the germanium and indium with tin, and if the whole is insulated against air/with the exception of the free Cu wire ends (e.g., with an epoxy resin shell), a plate cathode Ge - In - Sn - Cu is obtained (Fig. 1). As the surface of this diode is edged before being embedded into the resin shell, the electrochemical behavior of Ge in the many-electrode system Ge - In - Sn - Cu was investigated, and the mechanism of its dissolution was explained. The experiments were carried out in 1 N NaOH solutions of different H<sub>2</sub>O<sub>2</sub> contents (0.3 N H<sub>2</sub>O<sub>2</sub> and 1.0 N H<sub>2</sub>O<sub>2</sub>), or in pure Card 1/3

Electrochemical and Corrosion Behavior of Semiconductors in Electrolytic Solutions. III. Dissolution of Germanium in Contact With Other Metals 1240 5/076/60/034/009/008/022 B015/B056

17.5 N H<sub>2</sub>O<sub>2</sub> solutions. Samples of n-type Ge (of the type ДM(DM) or БM(BM)), In, Cu, and Sn embedded in polystyrene, as well as pairs of n-type Ge-Cu and n-type Ge-In, and ready diodes (of the type ДΓЦ-22 (DGTs-22)) were used. The area of the electrodes in the diodes investigated are given in Table 1. The corrosion current of Ge, as well as the quantity of the dissolved Ge were determined by a colorimetric method (Ref. 7); the surface profile of Ge was measured by means of a microscope, or the current face profile of Ge was measured by means of a microscope, or the current face profile and dissolution rate of Ge (in the pair Ge-Cu) was calculated density and dissolution rate of Ge (in the pair Ge-Cu) was calculated from the polarization diagram. A comparison between the experimental from the polarization diagram. A comparison between the experimental data and the calculated values (Table 2) shows that a self-dissolution of Ge takes place, and that the latter increases with the H<sub>2</sub>O<sub>2</sub> content.

In the many-electrode system investigated, Ge is the anode and Cu is the most effective cathode, whereas Sn and In are highly polarized and, according to conditions, act as a cathode or anode. The total loss of netype ing to conditions, act as a cathode or anode. In and Sn is determined by Ge (Table 3, Geo.Cu loss) in contact with Cu, In, and Sn is determined by the rate of anodic dissolution or self-dissolution, the ratio between

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APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

Electrochemical and Corrosion Behavior of Semiconductors in Electrolytic Solutions. III. Dissolution of Germanium in Contact With Other Metals

\$/076/60/034/009/008/022 B015/B056

the two rates depending on the  ${\rm H_2O_2}$  content (Table 4), i.e., self-dissolution predominates in pure  ${\rm H_2O_2}$  solutions. The behavior of n-type Ge during etching in the afore-mentioned solutions corresponds to the activity of the Ge electrode in the system Ge - In - Sn - Cu, and is subject to electrochemical rules. There are 6 figures, 4 tables, and 8 references: 7 Soviet and 1 US.

ASSOCIATION:

Akademiya nauk SSSR, Institut fizicheskoy khimii, Moskva

(Academy of Sciences USSR, Institute of Physical Chemistry,

Moscow)

SUBMITTED:

December 13, 1958

Card 3/3

S/020/60/133/01/47/070 B004/B007

5.4600

AUTHORS: Paleolog. Ye. N., Korotkova, K. S., Tomashov, N. D.

TITLE: The Kinetics of the Electrode Processes on a Silicon

Electrode in Acid and Alkaline Solutions

PERIODICAL: Doklady Akademii nauk SSSR, 1960, Vol. 133, No. 1,

pp. 170 - 173

TEXT: The authors investigated the discharge rate of hydrogen ions on silicon and the anodic dissolution rate of silicon in 0.2 N H<sub>2</sub>SO<sub>4</sub>, 1.0 N HF, and 5.0 N KOH at 25°C. n= and p=type single crystals of silicon with different resistivity (0.2, 10.0, and 23.0 ohm.cm) and a diffusion length of 0.5 mm were used for the investigation. The samples had the same crystal orientation. The surface was mechanically ground by means of boron carbids or etched at 80°C with a KOH-solution. Contact was established by means of rhodium electrolytically deposited on the sample and a soldered=on copper wire. Fig. 1 shows the curve of the cathodic polarization of n=type Si. In H<sub>2</sub>SO<sub>4</sub> a considerable inhibition of the

Card 1/3

The Kinetics of the Electrode Processes on a Silicon Electrode in Acid and Alkaline Solutions

S/020/60/133/01/47/070 B004/B007

H-ion discharge was observed also on Si with a ground surface. The presence of a semiconductive oxide layer is assumed, which proved that by means of a partial reduction of the layer with current reversal, and further by etching the KOH, polarization is considerably reduced. In 5.0 N KOH the oxide layer is soluble, the discharge rate of the H-ions depends only little on the resistivity of the Si-electrode, and the n-type Si behaves like a metal electrode. Fig. 2 shows the curve of the cathodic polarization of p-type silicon. Polarization is stronger than in n-type Si, the nature of the solution exerts little influence upon the kinetics of Haion discharge. The anodic polarization is shown in Fig. 3. In H2SO4, the oxide layer is not soluble and has a high degree of chmic resistivity. Si is highly polarized, and oxygen is separated. The presence of the oxide layer is proved by grinding-off the silicon electrode during the experiment. In this case, the slope of the polarization curve was considerably flattened up to a current density of 15 ma/cm2. In the case of higher current densities, the oxide layer could not be completely removed. In 1.0 N HF, a different behavior of n- and p-type Si was observed. p-type Si was not passivated up to a current density of

Card 2/3

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APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

The Kinetics of the Electrode Processes on a Silicon Electrode in Acid and Alkaline Solutions

S/020/60/133/01/47/070 B004/B007

30 ma/cm<sup>2</sup>. In the case of n-type Si, a hindrance of the anodic process occurred already at 1.0 ma/cm<sup>2</sup>, which is explained by the hole limiting current being attained. The electrochemical behavior of silicon thus in electrolytes is in principle similar to that of germanium, and is determined by the type of conductivity. Silicon, however, differs from germanium by the formation of the chemically inactive SiO<sub>2</sub>-layer with high chmic resistivity which hinders the cathodic and anodic reactions. There are 3 figures and 6 referencess 2 Soviet, 3 British, and 1 German.

ASSOCIATION: Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

PRESENTED: March 3, 1960 by A. N. Frumkin, Academician

SUBMITTED: March 3, 1960

X

Card 3/3

#### CIA-RDP86-00513R001756210008-1 "APPROVED FOR RELEASE: 04/03/2001

Tom Ashov, N.D.

81865

5/020/60/133/02/39/068 B004/E064

AUTHORS:

Deryagina, O. G., Paleolog, Ye. N., Tomashov, N. D.

TITLE:

Anodic Dissolution of Germanium With a p-n Transition

PERIODICAL:

Doklady Akademii nauk SSSR, 1960, Vol. 133, No. 2,

pp. 388 - 391

TEXT: The objective of the present paper was to determine the conditions for a selective etching of the p-n transitions of germanium taking into account the electrochemical processes of the diode components at the boundary of the solution. The authors investigated the distribution of the potential, the current density, and the dissolving speed in the components of a germanium diode at various anodic polarizations. Indiumgermanium diodes were used for the test in which germanium of the  $\Box M$ (DM) type, as well as a germanium single crystal with p-n transition were applied. The samples were embedded in epoxy resin and ground at a right angle to the In-Ge contact plane. They were then polished and after etching in H<sub>2</sub>O<sub>2</sub> they were anodically polarized in O.1 N NaOH or

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CIA-RDP86-00513R001756210008-1" **APPROVED FOR RELEASE: 04/03/2001** 

. Anodic Dissolution of Germanium With a p-n Transition

\$/020/60/133/02/39/068 B004/B064

0.1 N  ${\rm H_2SO_4}$  at room temperature and in dispersed daylight. The positive pole of the circuit was cornected to the indium. The potential distribution was measured with a capillary detector, the depth of the solution (the profile of the surface) with a Linnik double microscope. The width of the zone of p-type germanium was determined by the precipitation of copper with cathodic polarization of the p-n transition in pyrophosphate solution. Fig. 1 shows the curve of the anodic polarization of indium, p- and n-type germanium in O.1 N NaOH. A strong polarization occurs in In and n-Ge. In contrast to In the high degree of polarization of n-type germanium is not due to passivity but to the low degree of hole concentration. Fig. 2 shows the potential distribution on the surface of the diode at an anode current of 0.05 - 4.00 ma, Fig. 2b shows the surface profiles after 60 min and Fig. 2v gives the amperages obtained. The current density of n-Ge is greater than that of the anode current on the boundary of the solution. In the authors' opinion this is due to the injection of holes in n-Ge above the p-n transition. This is confirmed by Fig. 3 which shows that the anodic polarization of the n-Ge surface decreases as the distance from the

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4

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

正是的是我们的表情的证明,但是是是是我们的是不是的问题,但是是是不是一种正常的是有更多的。 第一章

Anodic Dissolution of Germanium With a p-n Transition

S/020/60/133/02/39/068 B004/B064

p-n transition increases. This is due to a decreased concentration of the injected holes. If the germanium diode is anodically polarized from indium a high degree of anodic polarization of indium occurs and it is above all the p-Ge and the adjacent zones of n-Ge which dissolve. With a cathodic polarization from n-Ge its dissolution can be stopped and concentrated to the narrow zone of p-Ge. Indium is not polarized in  $\rm H_2SO_4$  and mainly indium and the adjacent zone of p-type germanium are dissolved. Similar results were obtained with the germanium single crystal. Because of the different anodic polarizability of n-Ge, p-Ge, and In and because of the existing p-n transition a selective etching of a germanium diode or triode is possible. There are 3 figures and 9 references: 4 Soviet, 1 American, 3 British, and 1 German.

ASSOCIATION: Institut fizicheskoy khimii Akademii nauk SSSR (Institute

of Physical Chemistry of the Academy of Sciences, USSR)

PRESENTED: February 3, 1960, by A. N. Frumkin, Academician

SUBMITTED: March 2, 1960

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4

TOMASHOV, Nikon Danilovich; ZHUK, Nikolay Platonovich; TITOV, Vasiliy Alekseyevich; VEDENEYEVA, Mariya Aleksandrovana; EL'KRID, L.M., red. izd-va; ISLENT'YEVA, P.G., tekhn. red.

[Laboratory work on the protection of metals from corrosion] Laboratornye raboty po korrozii i zashchite metallov. Moskva, Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1961. 239 p. (Metals--Corrosion) (MIRA 14:7)

32624 8/137/61/000/011/102/123 A060/A101

18.8300

Vedeneyeva, M.A., Tomashov, N.D. AUTHORS:

Effect of deformation upon the intercrystalline failure of nichrome TITLE:

Referativnyy zhurnal. Metallurgiya, no.11, 1961, 48-49, abstract 111323 (V sb. "Korroziya i zashchita konstrukts. metallich. materi-PERIODICAL:

alov", Moscow, Mashgiz, 1961, 116 - 126)

The authors studied the effect of deformation caused by cold rolling and dressing of the surface by emery paper upon the intercrystalline failure of Cr-Ni steel. The steels OX 18H9, 1X18H9, and X23 H23 M3 L3 (OKh18N9, 1Kh18N9, and Kh23N2XNZ) and Kh23N23M3D3) were tested. The cold deformation (rolling) with degrees of reduction 20-60% was carried out both before and after tempering at 650°C for 2 hours. As result of the treatment the tendency of these steels to intercrystalline failure is reduced. This is related to the fact that in the process of deforming along the cleavage planes carbides and the & -phase separate out. The carbide phase which is precipitated in the course of tempering and deformation, separates out on a great area and its concentration is reduced. As result of this,

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### "APPROVED FOR RELEASE: 04/03/2001 C

CIA-RDP86-00513R001756210008-1

32624 8/137/61/000/011/102/123 A060/A101

Effect of deformation ...

the corrosion resistance of the boundaries increases. The deformation of steel before tempering (in the zone of dangerous temperatures) lowers the tendency to intercrystalline corrosion in a greater degree than does deformation after tempering. Cold deformation before tempering at 650° entirely eliminates the tendency of steel Kh23N23M3D3 to intercrystalline cracking under reductions of 21 - 60%, and that of steels OKh18N9 and 1Kh18N9 - under reductions of 49 and 58% respectively. The rate of intercrystalline etching of specimens of steel 1Kh18N9 with etched surface notably exceeds the corrosion rate of the specimens dressed with emery paper. There are 10 references.

Ye. Layner

[Abstracter's note: Complete translation]

Card 2/2

S/137/61/000/011/101/123

A060/A101

18-8300

Tomashov, N.D., Andreyev, L.A.

TITLE:

AUTHORS:

Oxidation of titanium at high temperatures

FERIODICAL:

Referativnyy zhurnal. Metallurgiya, no. 11, 1961, 46, abstract 11I308 (V sb. "Korroziya i zashchita konstrukts. metallich. materialov", Moscow, Mashgiz, 1961, 127 - 132)

A study was performed of the oxidation kinetics of Ti mark BT  $-1\,\mathrm{I\!I}$ TEXT: (VT-1D) in the interval 800-1,150°C in gaseous mixtures of 02+N2 in various proportions. Under soakings longer than one hour the oxidation follows a linear law in the entire temperature range under investigation. For 1,000°C a functional dependence was obtained of the oxidation-rate constant, characterizing the linear portion of the kinetic curve, on the partial pressure of 0 in the gaseous mixture. The kinetics of O dissolution in the metallic base was studied for the temperature of 1,000°C. It is assumed that the oxidation process is controlled by the 0 diffusion into the metallic base of the specimen. There are 8 references.

[Abstracter's note: Complete translation]

Card 1/1

Ye. Layner

S/081/61/000/022/032/076 B110/B101

AUTHORS:

Tomashov, N. D., Mil'vidskiy, M. G.

TITLE:

Etching of titanium in acid solutions and alkali melts

PERIODICAL:

Referativnyy zhurnal. Khimiya, no. 22, 1961, 259, abstract 22I182 (Sb. "Korroziya i zashchita konstrukts. metallich.

materialov". M., Mashgiz, 1961, 133 - 150)

TEXT: A study of the possibilities of etching Ti in H<sub>2</sub>SO<sub>4</sub>, HCl (acid), and HNO<sub>3</sub> with fluoride additions showed the etching efficiency of industrial Ti scale to depend on the oxidation temperature. Scale forming at 800 - 850°C was chemically stable to acids, but was sufficiently easy to remove at >1000°C. The anodic and cathodic behavior of Ti in the acids mentioned, and in HF containing admixtures, was studied. For etching Ti in alkali melts (NaOH melt), a 10 - 20 min treatment at 400-430°C and subsequent washing in hot 15% H<sub>2</sub>SO<sub>4</sub> are recommended. [Abstracter's note: Complete translation.]

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

s/137/62/000/001/186/237 33843 A006/A101

18.83.00

Tomashov, N.D., Al'tovskiy, R.M., Prosvirin, A.V., Shamgunova, R.D.

AUTHORS:

Corrosion of titanium and its alloys in sulfuric acid

TITLE:

PERIODICAL:

Referativnyy zhurnal. Metallurgiya, no. 1, 1962, 82 - 83, abstract
11583 (V sb. "Korroziya i zashchita konstrukts. metallich. materialov", Moscow, Mashgiz, 1961, 151 - 163)

The general aspect of BT 1 (VT1) Ti corrosion rate as a function of H2SO4 concentration under air atmosphere is also preserved in tests under O2, H2 and N<sub>2</sub> atmospheres and also during tests of some Ti alloys (VT5, VT3, VT3-1) under air atmosphere. The corrosion rate of Ti VTI in H<sub>2</sub>SO<sub>14</sub> under atmospheres of O<sub>2</sub>, H<sub>2</sub> and N<sub>2</sub> (with the exception of diluted H<sub>2</sub>SO<sub>1</sub> solutions) is somewhat less than under air atmosphere. Alloys T1 VT5, VT7 and VT3-1, are in general somewhat less than stable than technically mine arm at a ungo. Solutions stable than technically pure VII Ti in H2804 solutions. Saturation of the Ti surface with oxygen, and in particular N2 and H2, raises considerably the corrosion resistance of Ti in H2SO4. Preliminary hydrogenization of the Ti surface by cathodic polarization during self-diffusion in H<sub>2</sub>SO<sub>4</sub>, inhibits the corrosion process of Ti dissolving in H<sub>2</sub>SO<sub>4</sub>, in particular of 50 - 65% concentration. A

Card 1/2

**APPROVED FOR RELEASE: 04/03/2001** CIA-RDP86-00513R001756210008-1"

33843 \$/137/62/000/001/186/237 A006/A101

Corrosion of titanium ...

decrease of the Ti corrosion rate in  $\rm H_2SO_4$  of > 80% concentration is explained by the oxidation of the metal surfaces by concentrated acid and the formation of a protective film consisting of  $\rm Ti_3O_5$ .

The authors' summary

[Abstracter's note: Complete translation]

Card 2/2

S/081/61/000/023/028/061 B138/B101

AUTHORS:

Tomashov, N. D., Al'tovskiy, R. M., Vladimirov, V. B.

TITLE:

Investigation of the corrosion of titanium and its alloys

in solutions of bromine and methyl alcohol

PERIODICAL:

Referativnyy zhurnal. Khimiya, no. 23, 1961, 288, abstract 231255 (Sb. "Korroziya i zashchita konstrukts.

metallich. materialov". M., Mashgiz, 1961, 164 - 172)

TEXT: An investigation of the corrosion resistance of Ti and Ti alloys in solutions of Br in  $CH_3OH$  has shown that alloys with an  $\alpha$ -structure, BT1(VT1) and BT5 (VT5), are less resistant than those with an  $\alpha$  +  $\beta$  structure, BT3 (VT3) and BT3-1 (VT3-1). It is noted that in all the Ti alloys the rate of corrosion increased with the Br concentration of the solution, and that Ti iodide is more stable than technically pure Ti. An addition of water to the CH3OH + Br2 was found to reduce the rate of corrosion, due to the formation of a protective oxide film. Ti is also subject to

Card 1/2

S/081/61/000/023/028/061 B138/B101

并是我们的主义是这种的特殊的。

Investigation of the corrosion...

intercrystalline corrosion, which increases with a reduction of the  $\mathrm{Br}_2$  concentration in CH\_3OH from 5 to 1 %. If the water content of the solution is more than 30 %, however, both intercrystalline and general surface corrosion cease. The corrosion of Ti in  $\mathrm{Br}_2$  + CH\_3OH solutions is found to be of an electrochemical nature. In anhydrous solutions Ti can be protected by cathode polarization. For total protection in a 2% solution of  $\mathrm{Br}_2$  the potential must be maintained at around -0.350 v. [Abstracter's note: Complete translation.]

Card 2/2

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

18.8380

33844 s/137/62/000/001/187/237 A006/A101

AUTHORS:

Tomashov, N. D., Al'tovskiy, R. M., Chernova, G. P., Arteyev, A. D.

TITLE:

Corrosion resistance of titanium alloyed with molybdenum, chromium

and palladium

PERIODICAL:

Referativnyy zhurnal, Metallurgiya, no. 1, 1962, 83, abstract 11584 (V sb. "Korroziya i zashchita konstrukts. metallich. materialov",

Moscow, Mashgiz, 1961, 173 - 186)

Alloying of Ti with palladium raises considerably its corrosion resistance in H<sub>2</sub>SO<sub>4</sub> and HCl. Considerable reduction of the Ti corrosion rate is already observed when it is alloyed with a small Pd amount (0.1%). An increase of the Pd content in the alloy > 2% is not recommended. Electrochemical investigations have shown that an increase in the Ti corrosion resistance when it is alloyed with Pd, results from the shift of the stationary potential of the alloy to a range of values where Ti is partially or fully passive, due to the reduced overvoltage of the cathodic reaction. Alloying of Ti with molybdenum increases Ti resistance due to the considerably reduced ability of the alloy to anodic dissolving as compared with non-alloyed Ti. Alloying of Ti with chromium does not

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Corrosion resistance of titanium alloyed with...

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raise its corrosion resistance, and even reduces same in some cases, since Cr is less prone to passivity than Ti in  $\rm H_2SO_4$  and HCl, at a potential corresponding to a stationary potential of Ti. Ternary Ti-Pd-Mo alloys and Ti-Pd-Cr alloys are more resistant than the binary Ti-Pd alloy. This is due to a decrease in the current of ancdic Ti dissolving near the potential of full passivation, when it is alloyed with Mo or Cr. There are 17 references.

Author's summary

[Abstracter's note: Complete translation]

Card 2/2

33842 8/137/62/000/001/185/237 A006/A101

18.8300

AUTHORS: Titov, V.A., Agapov, G.I., Tomashov, N.D.

high temperatures

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 1, 1962, 82, abstract 11581 ("Korroziya i zashchita konstrukts. metallich. materialov", Moscow,

Mashgiz, 1961, 187 - 195)

TEXT: The authors studied the behavior of Ta, Nb and their alloys, containing 21.6; 34.0; 49.4; 67.3 at. % Ta, in  $H_2SO_4$  at high temperature. In 90%  $H_2SO_4$ , at  $250^{\circ}C$ , during the transition from an alloy containing 34.0 at. % Ta to an alloy containing 49.4 at. % Ta, an over 30-fold decrease of the corrosion rate was observed (from 15.1 to 0.5 g/m².hour) and also an abrupt change of the potential toward the positive side (from 0.25 to 0.77 v, i.e. more than by 0.5 v). The abrupt changes in the anti-corrosion properties of the alloy correspond to the first threshold of stability in the Ta and Nb correlation, equal to 4/8 atomic fraction. Extended tests (120 hours) of Ta-Nb alloys under experimental conditions, do not shift the threshold of stability towards the rate of other Ta-Nb

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33842 8/137/62/000/001/185/237 A006/A101

Corrosion of tantalum ....

correlations in the alloy. In 10%  $\rm H_2SO_{ll}$  at boiling temperature of the solution ( $102^{\rm o}C$ ), the internal stresses (cold hardness) shift the electrode potential of the alloys to the negative side, by 0.05 v on the average, but both cold hardness and stress applied do not reduce the corrosion resistance nor cause corrosion cracking of the alloys. Tests with the Ta-Nb alloy containing 96.2 at % Ta in various  $\rm H_2SO_{ll}$  solutions at 250 °C, have shown that 70%  $\rm H_2SO_{ll}$  is the most aggressive medium as compared with its solutions of other concentrations. There are 11 references.

The author's summary

[Abstracter's note: Complete translation]

Card 2/2

18.8300

33838 8/137/62/000/001/180/237 A006/A101

AUTHORS:

Tomashov, N. D., Strekalov, P. V.

TITLE:

Investigating the corrosion rate of ferro-carbon alloys in acids at elevated temperatures

经通过的数据分别,我们是这个人的人,我们是这个人的人,我们就是这个人的人,我们们就是一个人的人,我们们们就是一个人的人,我们们们的人,我们们们们的人,我们们们们

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 1, 1962, 80 - 81, abstract 1T569 ("Kerroziya i zashchita konstrukts. metallich. materialov", Moscow, Mashgiz, 1961, 196 - 199)

TEXT: Increased temperature of acid causes a sharp increase of the corrosion rate of Fe-C alloys; the corrosion rate increases also at a higher C content in the alloy in non-oxidizing acids, and in oxidizing acids it decreases due to the partial inhibition of the anodic process. The effect of temperature on the diffusion rate of carbon steels in HCl, HNO, and H2SO4, can be described by the exponential equation K = Aexp ( - E/RT). The authors determined the activation energy of processes of carbon-steel diffusion in HNO2, H2SO4 and HCl. For HNO3 the activation energy is equal to 10.5 kcal, for H2SO4 and HCl it is 13.5 and 17.35 kcal, respectively.

[Abstracter's note: Complete translation]

Author's summary

Card 1/1

s/081/61/000/023/031/061 B138/B101

18.8310

Titov, V. A., Balandin, I. M., Tomashov, N. D.

AUTHORS:

Investigation of the efficiency of different methods of protecting metals in solutions of sulfuric and phosphoric

TITLE:

acids at elevated temperatures

Referativnyy zhurnal. Khimiya, no. 23, 1961, 290, abstract zashchita konstrukts. metallich. 231276 (Sb. "Korroziya i zashchita konstrukts. metallich. naterialov". M., Mashgiz, 1961, 200 - 214)

PERIODICAL:

TEXT: The effect of cathodic (As and Bi ions) and anodic (Cu, Ag, and Au ions) corrogion inhibitors has been investigated, as also electrolytic

protection by anodic polarization using Cu, Ag, and Au depositions and Au and Au content on the rate of compagion of stainless steels 191820. Ag and Au contact, on the rate of corrosion of stainless steels 1X1849T (1Kh18N9T) and X23H28M3D3T (Kh23N28M3D3T) and the alloy 3/461(EI461) in 10% golutions of H go (KNIUNYT) and XZ2HZUM7H21 (KNZ2NZUM2H2H2H2T) and the alloy JVHOI (E1461) and 10% solutions of H2SO<sub>4</sub> and H<sub>3</sub>PO<sub>4</sub> at a temperature of 250°C. The cathodic corrosion inhibitor, Bi, has been found to have the greatest inhibiting effect for stainless steels in H SO. Corrosion of the Ni inhibiting effect for stainless steels in H SO. catnoalc corrosion innibitor, pr, has been round to have the greatest in H<sub>2</sub>SO<sub>4</sub>. Corrosion of the Ni inhibiting effect for stainless steels in H<sub>2</sub>SO<sub>4</sub>.

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31966 S/081/61/000/023/031/061 B138/B101

alloy is more effectively reduced if it has a Cu coating. In H<sub>3</sub>PO<sub>4</sub> an addition of Ag ions to the acid solution is the most efficient way of reducing corrosion of the stainless steels and the Ni alloy. [Abstracter's note: Complete translation.]

Card 2/2

s/137/62/000/001/201/237 A154/A101

: EROHTUA

Titov, V. A., Tomashov, N. D.

TITLE:

A study of the endurance of card wire

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 1, 1962, 87, abstract 11616 (Sb. "Korroziya i zashchita konstrukts, metallich, materialov".

Moscow, Mashgiz, 1961, 215-222)

Steel brands 55, 50r (500), 50rc (5008), 50ri and 60 were studied. Steel 55 has the best fatigue and corrosion-fatigue indices. For wire made of this steel Tw = 25 kg/mm<sup>2</sup> was obtained in air. When high stresses are applied, wire made of steel 55 has a fatigue resistance over 50 to 90 times higher than wire of steel 50Ti and 60 respectively. At comparatively low stresses, the fatigue-resistance indices of wire made of steels 55, 50Ti and 60 become close to each other. The endurance of wire made of the test brands of steel in tap water decreases to such a degree that even for the best wire made of steel 55, at the lowest stress tested by us (25 kg/mm<sup>2</sup>), the conditional ultimate corrosion fatigue was not reached. Wire made of steels 55 and 60 has the highest indices of corrosion-fatigue resistance in tap water, and wire of steels 500, 500S and

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APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R001756210008-1"

A study of the endurance of card wire

S/137/62/000/001/201/237 A154/A101

50Ti have the lowest indices. The emulsions used in fiber-combing are less aggressive media than tap water. A conditional ultimate corrosion fatigue of 55 kg/mm² was established for wire of steels 55 and 50G in emulsion of the Krasnokholmskaya fabrika (Krasnyy Kholm factory), while for wire of steels 60, 50GS and 50Ti this limit was reached at a stress of 35 kg/mm² in these conditions. The emulsion of the Kupavinskaya fabrika (Kupava factory) is less agressive than the emulsion of the Krasnyy Kholm factory. In the former emulsion a conditional corrosion-fatigue limit of 55 kg/mm² was established even for wire of the worst steel - 50 Ti. Card wire of steel 55 made of polished wire rod has higher endurance indices in tap water than wire of the same steel, but made of unpolished wire rod. Preliminary grinding of the wire rod before the latter is drawn into wire may be considered as one of the methods for prolonging the service life of card clothing.

Authors summary

[Abstracter's note: Complete translation]

Card 2/2

5/062/61/000/002/002/012 B115/B207

AUTHOR:

Tomashov, N. D.

TITLE:

Control factor and corrosion protection of metals

PERIODICAL:

Izvestiya Akademii nauk SSSR. Otdeleniye khimicheskikh

nauk, no. 2, 1961, 236-245

TEXT: The author classified the various methods of corrosion protection not with respect to their application or technology, but on the basis of the theory of electrochemical corrosion and the mechanism of each method. For this purpose, it was necessary to determine the control factor of each individual protection method, i.e., the degree of inhibition of the corrosion process with application of the respective protection method. It is known from publications that the dependence of the corrosion current characterizing the corrosion rate on the factors of electrochemical corrosion is represented by the following

equation:  $I = \frac{v_k^0 - v_a^0}{P_k + P_a + R}$ , where  $v_k^0 - v_a^0$  denotes the difference of

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Control factor and corrosion ...

S/062/61/000/002/002/012 B115/B207

the initial equilibrium potentials of the cathodic depolarizing process  $(\overline{V}_k^0)$  and the anodic reaction of metal dissolution  $(\overline{V}_k^0)$  or, in other words, the degree of thermodynamic instability of the respective system; the denominator characterizes the general inhibition of the system;  $P_k$  the mean cathodic,  $P_k$  the mean anodic polarizability,  $P_k$  the total ohmic resistance of the system. Proceeding from this method, the author establishes a scientific classification of various protection methods on the basis of their effect upon: I) Reduction of the degree of instability of the system, II) inhibition of the cathodic process, III) reduction of the anodic process, IV) increase of the ohmic resistance of the system. The most important data of the table are as follows: I, II, III, and IV are compiled as A: change of the promoting or inhibiting factors of the corrosion process.

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Control factor and corrosion	S/062/61/000/002/002/012 B115/B207
В	С
General characteristics of the protective measure	Concrete methods of corrosion protection
Change of internal factors (of metal)	1) Alloying increasing the thermodynamic stability of the alloy; 2) admixtures to the alloy increasing the continuity of the resulting corrosion products
Change of surface factors of the product	1) Coating with a continuous layer of a nobler metal; 2) insulationand varnish coatings; 3) lubricants; 4) lining and coating with nonmetallic substances; 5) oxide-, phosphate-, and other films;
	6) enameling; 7) metal coatings forming corrosion layers of higher protection

s/062/61/000/002/002/012 Control factor and corrosion ... B115/B207 Change of external factors 1) Change of the external medium (of external conditions or forming a layer with higher proof the corrosive medium) tection; 2) change of the corrosion conditions causing a layer of higher protection; 3) change of the corrosion conditions in such a way that the corroding agent is kept apart from the metal surface Change of internal factors 1) Reduction of the surface of (of the metal) cathodic spots in the metal; 2) introduction of admixtures to the alloy increasing the overvoltage of cathodic depolarization Change of surface factors 1) Metal coatings with a high of the product overvoltage of cathodic depolariza-II tion; 2) non-metallic coatings with the same effect as above, or an inhibiting effect toward the diffusion of cathodic products in the film Card 4/7

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Control factor and corrosion ...

Change of external factors (of external conditions or of the corrosive medium)

Change of internal factors (of the metal)

Change of surface factors of the product

III

Change of external factors

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S/062/61/000/002/002/012 B115/B207

- 1) Introduction of cathodic inhibitors into the solution; 2) reduction of concentration of the cathodic depolarizers on the cathode;
- 3) cathodic electrochemical protection
- 1) Alloying increasing the anodic passivation capacity of the alloy; 2) introduction of active cathodes into the alloy
- 1) Surface treatment of the metal increasing the passivation capacity (polishing); 2) coating of the product with a layer of stronger passivating metal; 3) varnish coatings or lubricants with a passivating dye
- 1) Introduction of anodic inhibitors or production of a stronger passivating external medium; 2) anodic

Control factor and corrosion ...

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Change of internal factors
(of the metal) or the surface
factors
Change of external factors

electrochemical protection (inhibition of anodic processes due to the occurrence of passivity) No clear examples

Increase of the ohmic resistance, e.g.: drying of the bottom or dehydration of liquid fuels

In general, those protection methods are most efficient which act upon the chief control factor of corrosion. If several protection methods with the same control protection factors are applied at the same time, efficiency increases; if control protection factors are not the same, it may decrease. The protection methods reducing the degree of thermodynamic instability, always entail a corrosion reduction, the effect of these methods is, however, smaller if the total inhibition in the system is very high.

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IV

Control factor and corrosion ...

S/062/61/000/002/002/012 B115/B207

There are 1 table and 14 references: 8 Soviet-bloc and 6 non-Soviet-bloc.

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR

(Institute of Physical Chemistry of the Academy of

Sciences USSR)

SUBMITTED:

August 3, 1959

Card 7/7

18.8310 also 1138, 1573

5/184/61/000/003/002/004 D041/D113

AUTHOR:

Tomashov, N.D., Doctor of Chemical Sciences, Professor,

Chernova, G.P., Candidate of Chemical Sciences

TITLE:

New method of electrochemical protection of metals against

corrosion-anode polarization.

PERIODICAL: Khimicheskoye mashinostroyeniye, no. 3, 1961, 30-33

TEXT: The authors state that there are many electric-protection methods which are applied in industry in order to prevent metals from corroding as described by N.D. Tomashov (Ref. 1: Teoriya korrozii i zashchity metallov [Theory of corrosion and metal protection], Izd. AN SSSR, 1959), (Ref.2: Zashchita metallicheskikh konstruktsiy ot korrozii protektorami Protection of metal structures from corrosion by means of protectors], Oborongiz, 1940), and by V.A. Pritula (Ref. 3: Katodnaya zashchita zavodskoy apparatury Cathode protection of industrial equipment], Goskhimizdat, 1954). these methods use anode polarization. Nevertheless, anode polarization can be used as corrosion protection, if a metal in a given medium tends to passivation; the passivity of the metal considerably reduces the anodic dis-The resistance to corrosion of some metals and alloys (iron, stainsolving. Card 2

S/184/61/000/003/002/004 D041/D113

New method of electrochemical protection .....

less steel, titanium, zirconium, tantalum, etc.) is based on the passivity The passivity of these metals can be established by increasing the oxidation effect of the medium, or by anode polarization of the metal. A constant passivity potential of the metal can be maintained by an electronic The displacement of the automatic-regulation device, i.e. a potentiostat. metal-potential in the electrolyte solution necessary for obtaining the passive state can be generated by the following methods: by changing the oxidation-deoxidation potential of the medium as described by J.D.Berwick and U.R. Evans (Ref.4: "Journal of Applied Chemistry", v. 2, no. 10, 1952), by anode polarization from an external electric source as described by C. Edeleanu (Ref. 6: "Nature", v. 173, no. 4407, 1954), through contact with an electrically positive metal having a large enough surface as described by the authors (Ref. 7 Tomashov, N.D., Chernova, G.P., Issledovaniya po nerzhaveyushchim stalyam Stainless-steel investigations, izd. AN SSSR, 1956), by B.W. Buck Sloope and H. Leidheiser (Ref. 8: "Corrosion", v. 15, no. 11, 1959) and by M. Stern and H. Wissenberg (Ref. 9: "Journal of the Electrochem. Soc." v. 106, no. 9, 1959), by introducing ions of precious metals into the solution, and by introducing a cathode hardener into the alloy. In order to determine the potential range within which the metal has the smallest dissolving speed, potentiostatical curves must be plotted. Fig.2 shows such curves for 2X18H9 Card 2/9

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s/184/61/000/003/002/004 D041/D113

New method of electrochemical protection .....

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(2Kh18N9) steel. Since inter-crystalline corrosion is one of the disadvantages of stainless steel, the authors together with O.N. Markova (Ref. 16: "Zhurnal prikladnoy khimii", v. 33, no. 6, 1960) investigated the effects of anode polarization on the above-mentioned phenomena using 2Kh18N9 steel which tends considerably to inter-crystalline corrosion after tempering at 650° for 2 hours. The results are compiled in table 2. Table 3 shows the limits of the stable passive-state range of 2Kh18N9 steel hardened at 1050° (15 minutes) and tempered at 650° (2 hours) in H<sub>2</sub>SO<sub>4</sub> solutions. Fig.4 shows the anode polarization curves for titanium. The authors state that shows the anode polarization curves for titanium. anode electrochemical protection can be used when the aggressive fluid has The potential range in which the metal is sufficienta good conductivity. ly passive is large enough for the reliable operation of an industrial automatic potentiostat, this value must not be smaller than 50 millivolts as described by J.D. Sudbury, O.L. Riggs and D.A. Schock (Ref. 17: "Corrosion", v. 16, no. 2, 1960). At present, the anode protection method is being introduced into industry. It has been proposed for titanium under the effect of HCl and H2SO4 as described by A.H. Barber (Ref. 19: "Corrosion, prevention and control", v. 6, no. 11, 1959). Anodic protection of devices during sulfurization is already being used as treated by D.A. Schock, O.L.Riggs,

X

New method of electrochemical protection .....

S/184/61/000/003/002/004 D041/D113

and J.D. Sudbury (Ref. 21: "Corrosion", v. 16, no. 2, 1960) and by O.L.Riggs, M. Hutchison, N.L. Conger (Ref. 22: "Corrosion", v. 16, no. 2, 1960). passivity of the metal can be kept constant not only through anode polarization from an external current source, but also through electric contact of the protected part with the metallic protector of an electric furnace. Prazak (Czechoslovakian patents, 86080, 150157) has proposed such a protection method for chrome-nickel steels in hot H2SO4 solutions; he recommends metal oxides, i.e.  ${\rm Fe_3O_4}$  or  ${\rm MnO_2}$  as protector materials. The experimental results obtained and the above-mentioned literature show that widescale industrial application of the anodic method for protecting carbon steel, stainless steel, titanium and other metals (which have a passivation tendency) from corrosion, is possible. There are 5 figures, 4 tables, and 22 references, 14 Soviet-bloc and 8 non-Soviet bloc. The four most recent English-language publications read as follows: J.D. Sudbury, O.L. Riggs, D.A. Schock, "Corrosion", v. 16, no. 2, 1960; A.H. Barber, "Corrosion, prevention and control", v. 6, no. 11, 1959; D.A. Schock, O.L. Riggs, J.D. Sudbury "Corrosion", v. 16, no. 2, 1960; O.L. Riggs, M. Hutchison, N.L. Conger, "Corrosion", v. 16, no. 2, 1960.

Card 4/9

s/081/62/000/013/024/054 B177/B101

AUTHORS:

Matveyeva, T. V., Tyukina, M. P., Pavlova, V. A.,

Tomashov, N. D.

TITLE:

Research on the anodizing of titanium in sulfuric acid

solutions

PERIODICAL:

Referativnyy zhurnal. Khimiya, no. 13, 1962, 410, abstract

13K166 (Sb. "Titan i yego splavy". no. 6. M., AN SSSR,

1961, 211-220)

TEXT: Research into a process of anodizing Ti is described. The composition (in %) tested was Fe 0.13; Ni 0.15; Si 0.17; C 0.05;  $N_2$  0.098, Cu0.34; with Ti forming the remainder in solutions of  $H_2$ SO<sub>4</sub>. The authors studied the growth and properties of the films in relation to the time of anodizing (up to 8 hours);  $D_a$  (1-10 a/dm<sup>2</sup>); temperature (20-100%C) and concentration of  $H_2SO_4$  (0-80%). Anodizing of Ti in  $H_2SO_4$ at about 20°C occurs at a high terminal voltage (up to 100 v) and results

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