

PETUKHOV, B.S.; ROYZEN, L.I.

Generalized relations for neat transfer during turbulent gas flow in circular tubes. Teplofiz. vys. temp. 2 no.1:78-81 Ja-F 164. (MIRA 17:3)

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1. Moskovskiy energetiche, kiy institut.

PETUKHOV, B.S., doktor tekhn.nauk; NOL'DE, L.D., kand.tekhn.nauk

Heat exchange during a viscous gravitational flow of a liquid in pipes [with summary in English]. Teploenergetika 6 no.1: 72:80 Ja 159.

1. Moskovskiy energeticheskiy institut.
(Heat-Transmission) (Fluid dynamics)

APPROVED FOR RELEASE: 06/15/2000 CIA-RDP86-00513R001240710002-4"

24,5200 AUTHUR: Petuknov, B. S., Douter of Termina Double PITLE: The Present Condition and the proste is of Development of the Study of Heat Exc: William PERIODICAL: Teploenergetika, 1959, No. 12, pt 1-13 (USDR) ABSTRACT: The systematic study of new texturns the following the instance of s and in the USSR the first systematic investigation. If the subject were made by M. V. Kiroliner. Physical heat exchange emerged as an independent occurrence of cur 30 years ago and is still developing mapping. Since the war the work has been intensified to meet the demands of nuclear engineering. Porticularly important problems in heat exchange orise in the detalogment of controlled thermo-nuclear realthons. Sin - the was normal power engineering nor also talled many proteen in heat exchange. Heat exchange problems are of tribing importance in rocket engineering. In view of the prospective rapid development in this actions the present article attempts to summerise the main trents in new methods of studying heat exchange that t indicate certain fundamental problems and particulat Card 1/1/ tasks which are of particular importance of the tre en-

The Present Condition and the Prospects of Developed Study of Heat Exchange

time. The subject of thermal rank, there is a reviewed. The mathematical formation of the thought of τ seconductivity is threed on the selection of the simple carriers equations in partial differential confirmation partial parabolic and elliptical types. In applying the classical methods of solution extension and a man lvin irritions being made of operational coloulus in o of thermal conductivity. This has not been in the for the case of several variable, ph. to two and three-dimensional problem. Therefore, increasing need to colculate temperature flort. In machine parts with wise runes of being satures which chame the physical properties of are conproblem is certical rly companied who have been been tion is advempensed by phase conversion one over latent heat. Therefore, one of the months of the conversion the theory of thermal confectivity of the introduction of semeral actions I solven men-rape at the most Sair /if partial differential coefficients. In the in the

The Present Condition on the Profession of Development of Study of Heat Exchange

approximate solutions are runtiquest carottent where of such procedures are tased on the wethou of finite differences, the theory and resistice of which has achieved considerable development in the Soviet Union. A number of approximate methods have teen evalved. The eaproximate, and particularly numerical, mathematical much more universal than the appurate methods and thear disadvantage of involving laborious calculation of being evercome by the use of computer. In addition to digital computers many of the estimations of the line. to solution to various types of and lefterther use of approximate on their of conductivity equations, based on the results and by finite differences, talset problem of that there programming. In thermal conductivity of the contractions involving large heat flows the resistance to week surfaces in contact is significant and much work remains to be done on this aspect. The thermal properties of new materials and of old materials in new auxiliarities Card 3/13 require much more study. There is a particular need

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The Present Condition and the Proster's of Development of the Study of Heat Exchange

to standarting wetrothe foot the community and although such has the test of the test of the test meeds to be extended. For all the test of the t retrainm cheft, with firm a constitution of the constitution of th tolia. It is a little to the first of the control o phase medium is then bevieves. The postless of except, can be appropriately and the hydrocal matter of the period for its with leminar flow size 2 to the of 1 into attach mathematical forces: 1 to 1 to 10 of 1 into attach mathematical forces: 1 to 1 to 10 of 1 into attach and the object, the state of 1 to 10 of 1 into is lacking out a semi-embirate. The most functions has been developed. The manufacture of the following terms. without alteration of the tar. The first to Regnound Prandtl and Karman, take letter to the rodern reduction of empirical theory of real end one and front on the first one.

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The Present Condition and the Prospects of Development of the Study of Heat Exchange

turbulent flow of viscous fluids. This is taked on the assumption that the mechanism of heat transfer is identical with that of transfer of momentum, which theath benerally valid is not always necessarily so. Diversencies between theory and practice that are observed in the case of heat exchange in liquid metals are associated with this circumstance. The keynolds ypothesis has not been generally verified experimentally, althous it cannot always be strictly true. Meanwhile, the semi-empirical theory has to be applied to problems of heat exchange and friction in flows covering a very wide range of Prandtl numbers. Over this range there may be a considerable change in the physical characteristics of both an incompressible fluid and compressible gas. It is evident that progress with the semi-empirical theory of heat exchange in friction depends on experimental investigation of the distribution in the flow of the coefficients of turbulent neat exchange and impulse. Such investigations call for very accurate measurements of temperature and velocity Card 5/13 distributions in turbulent flows of heat t.sfer medium,

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The Present Condition and the Prospects of Development of the Study of Heat Exchange

which present considerable experimental problems. Were is going on on some aspects of this problem but it is still far from fully solved. Although the semi-empirical theory is the only one that is available new in in the forseeable future it is clearly founded on highly simplified concepts of the mechanism of turbulent exchange. There is clearly a need for a more strict theory of heat exchange and friction in turbulent flow. Angineering solutions are particularly required for high values of Reynolds Numbers. Methor of the boundary-layer theory are now established and are wately used in practice. Approximate methods I rob tourdery layer of finite thickness are better developed than those of an asymptotic boundary rayer, and the latter method needs further attention. An important application of the theory of the boundary layer is in heat exchange and friction calculations at very righ temperatures above 2500°K, such as arise during motion of a body in Card 6/17 the atmosphere at high supersonic speeds. Exoti-raid

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The Present Condition and the Propose to of Development of the Study of Heat Exchange

or endothermic chemical resultions may seem by there temperatures and this complicates the problem. At still higher temperatures, of the orier of 10000 K, ionication of the gas may occur so that it becomes electrically conducting and subject to the influence of a maintain field. In this case, motion of the grant descrited ty the equations of magneto-nydrodynamics. The application of boundary-layer theory and stray of convective heat exchange in these conditions is a pres. in, problem experimental methods play a predominant eart in the stady of heat exchange and indeed many tratlems can only to tackled in this way, the theory of similarity this assumes importance, and appreximate semi-entirized methods of studying problems of this and have considerable practical value. A humber of particular problems of convective heat exchange in a single-phase medium or then mentioned, commencing with those of heat exchange and resistance when the physical properties of the part transfer medium are variable. A good real of work has Card 7/13 been done on specific problems of this in

The Present Condition and the Prospects of Development of the Development of Heat Exchange

is a need to unify that teneralize the work of the local with the problem as a whole is still for from a ethic contemporary requirements. Fritzens railed to the inof liquid metal heat-transfer media dre find . etc. good deal of the work that has been less with it... metals related to round pitch: there is a practical need for heat-exchange data in pires with other abster of section, such as eval or restanciate. But it heat transfer with liquit as all 1. requires to low values of Reynolds number with laminar and transitional flow conditions. Convection heat-transfer and reclatance problems arise during the motion of botter in a caseous medium at high operats. These and other masters concerning the turbulent flow of a compressible gas need theoretical and experimental study. Special interest of opening ne study of heat exchange and resistance in symmilia and axially symmetrical todies in the presence of considerable prescure-gradients. The translation from laminer to turtulent flow should be a sugget of you

Jard of 1% high Mach numbers. Special effects ago a at Mach name

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The Present Condition and the Prospects of Development of the Divity of Heat Exchange

of 10 and above, at which surface temperatures may te very high, and if chemical reactions occur simultaneously, close investigation is needed. Flights at high altitudes and in space pose the special problem of heat exchange and resistance during high-speed motion in a rarefied Bas. Distinctive problems also arise in high vacua because of the presence of a free molecular path, A number of investigators have applied modern molecular-kinetic theory to this subject and analytic solutions have been obtained for heat transfer and resistance of plates, cylinders and spheres under these conditions. The intermediate region of somewhat his her pressures present greater theoretical difficulties and only very approximate theoretical results have been achieved. Little experimental data is available for either of these regions and work should accordingly be carried out at high Mach values over a range of low pressures. Heat exchange during boiling and condensation is then considered. Little work has been done on the Card 9/13 theory of boiling; however. American contr butions to

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The Present Condition and the Prospects of Development of the Staby of Heat Exchange

this subject are briefly reviewed. In order to the object to develop the theory, further experimental evidence is required about the mechanism of boiling, Barlier weigh concentrated mainly on boiling during conditions of natural convection, and the majority of the work has account concorned with the determination of heat-transfer coefficients and critical thermal loadings. Resent work has been more concerned with hest transfer during boiling of liquids undergoing forced flow in tires. A great deal of attention has already seen given to builting during free flow. However, the general formulae decided previously do not accommodate recent exterimental laste on certain liquids. Therefore, new formulae with 3 better basis in physics are required for this two There is a need to generalise experimental data of heat exchange during boiling in pipes at temperatures up to the caturation temperature. Further experimental data are required on heat transfer, critical loadings and hydraulic resistance over a wide camee of steam content Cars 10/12 with simultaneous operation of other parameters over a

The Present Condition and the Prespects of Development of the Study of Heat Exchange

wide range. Data are needed for other fluids besides water. American work on boiling when head is evolved within the volume of the heat transfer medium is reviewed. Most available theoretical work on film-wire condensation has been concerned with extending Nusselt's theory for laminar flow, and the theory of this subject is now fairly complete. Whilst a good deal of attention has been given to film-wise condensation of steam moving at low speed, much less has been done at higher film speeds. There is a need for improved design formulae for this case. Ideas are accumulating about the physics of grop-wise condensation but satisfactory methods of making theoretical calculations on this subject are not yet available. Further information is required about condensation of steam from a steam/sa. mixture. This work could be extended to mixture: of various vapours and bases in containers of infierent proportions. Further work is required on heat exchange during toiling and condensation of mixtures and solutions Radiant heat-exchange is then considered. A peneral Card 11/13 review is given of the use of strict about 10.1 methods

SOKOLOVA, T.F., tekhn.red.

ANTSYFEROV, M.S., kand.fiz.-mat.nauk; VUKALCVICH, M.P., prof., doktor tekhn.nauk, laureat Leninskoy premii; KRIPETS, B.S., inzh.;

LAZAHEV, L.P., prof., doktor tekhn.nauk; MAZYHIN, I.V., inzh.;

NIKITIN, N.N., kand.fiz.-mat.nauk; OCHKIN, A.V., inzh.; PANICHKIN,

I.A., prof., doktor tekhn.nauk; PETUKHOV, B.S., prof., doktor tekhn.nauk; PODVIDZ, L.G., kand.tekhn.nauk; SIMONOV, A.F., inzh.;

SMIRYAGIN, A.P., kand.tekhn.nauk; TOKMAKOV, G.A., kand.tekhn.nauk;

PAYNZIL'BER, B.M., prof., doktor tekhn.nauk; KHALIZEV, G.P., kand.tekhn.nauk; CHESACHENKO, V.F., kand.tekhn.nauk; YAN'SHIN, B.I., kand.tekhn.nauk; ACHERKAN, N.S., prof., doktor tekhn.nauk, red.;

KUDRYAVTSEV, V.N., prof., doktor tekhn.nauk, red.; PONOMAREV,

S.D., prof., doktor tekhn.nauk, laureat Leninskoy premii; red.; SATEL',

B.A., prof., doktor tekhn.nauk, red.; KARGANOV, V.G.,

RESHETOV, D.N., prof., doktor tekhn.nauk, red.; KARGANOV, V.G.,

inzh., red.graficheskikh materialov; GIL'HENBERG, M.I., red.izd-va;

[Manual of a mechanical engineer in six volumes] Spravochnik mashinostroitelia v shesti tomakh. Red.sovet N.S.Acherken i dr. Izd.3., ispr. i dop. Moskva, Gos.nauchno-tekhn.izd-vo mashinostroit.lit-ry. Vol.2. 1960. 740 p. (MIRA 14:1)

1. AN USSR (for Serensen).
(Mechanical engineering) (Machinery--Construction)

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Petukhov. Doctor of Technical Sciences and Kirillov, V. V., Candidate of Technical Sciences

AUTHORS: Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to 4 TITLE:

Teploenergetika, 1960, Nr 5, pp 64-73 (USSR)

ABSTRACT: Because of developments in high-speed aircraft and in gas turbines, the question of heat exchange during highspeed gas flow is acquiring considerable practical importance. Most of the theoretical work that has been done on heat exchange and resistance during turbulent flow

of a compressible gas relates only to the single case of a flat sheet in a longitudinal flow of gas. Heat exchange and resistance in pipes and nozzles has received much less study. The least study has been devoted to heat exchange and resistance conditions during the flow of a compressible gas in pipes, though experimental work has been done on this subject in the USSR and in the USA. The influence of gas compressibility on heat exchange

during flow in pipes is still obscure, and the present card 1/8 article describes experimental work on the subject.

APPROVED FOR RELEASE: 06/15/2000

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Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to $4\,$

Preliminary results of this work have already been published. The experimental equipment and procedure is first described. The thick-walled pipe method was used, because it permits very accurate measurement of local heat flows during heating or cooling of fluid in a pipe. The method is based on determination of local heat flow from measurements of the temperature distribution on the inside and outside surfaces of the experimental pipes. In the general case, the temperature field in the pipe wall is two-dimensional, and equations for hear-flow density are of complex form. However, if changes in axial heat-flow are neglected, the problem is much simplified and the local heat flow is given by Eq (1). The tests were made with air delivered from a compressor which could give a flow of up to 900 kg/hour at a pressure of 7 atm. The air was cleaned and dried. The experimental pipe is illustrated diagrammatically in Fig 1. Its internal diameter of 15.95 mm was chosen to give the maximum value of Reynolds number for the available rate of air flow and retardation pressure.

Card 2/8

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Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to 4

The pipe was made of steel grade lKhl8N9T which has a low coefficient of thermal conductivity; special attention was paid to the internal finish. Arrangements were made to measure the temperature with thermo-couples. Seven different nozzles could be used, giving one subsonic and six supersonic speeds corresponding to Mach numbers of 2, 2.5 (two nozzles), 3, 3.5 and 4. cooling tests were made. In working out the test results, the flow velocity and temperature were determined on the assumption of unidimensional flow. The local heattransfer coefficient is given by expression (2). For supersonic flow, the restoration factor is given by expression (4), which represents the experimental results with an accuracy of ± 1%. During the investigations, 83 tests were made consisting of seven series, each for a definite Mach number at the inlet to the tube. Some of the tests were made with artificial turbulation of the boundary layer. The tests cover the Mach number range from 0.5 to 4 and Reynolds numbers

Card 3/8

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Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to 4

from 40000 to 900000. The retardation temperature and the wall temperature were approximately constant and equal to 4200K and 3000K. The flow temperature ranged from 400 to 1000K. Graphs showing the change of heat transfer over the length of the pipe are shown in Fig 4. They indicate that at the start of the pipe there is a region of laminar flow and a transitional boundary layer. As the Reynolds number increases the size of The first graph of Fig 2 shows this section diminishes. that heat transfer in the transitional region depends considerably on the degree of turbulence of flow at the inlet to the tube. Analysis of the process of heat exchange during the flow of a compressible gas in pipes based on the theory of similarity shows that under these conditions heat exchange depends on five criteria, as in expression (5). It is then shown how the influence of the gas compressibility on heat exchange may be determined, using expression (6). The curve corresponding to this formula is plotted in Fig 3a, and it will be seen that most of the experimental points lie within

Card 4/8

indicate that the experimental points lie closely around a Card 5/8

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Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to 4

line given by expression (10). Comparison of formulae (10) and (7) shows that in both the relationship between the heat transfer and the Reynolds number is the same, though at Mach O formula (10) gives results about 7% lower than formula (7). It is concluded that for the case of flow in pipes the method of governing temperature may be used to allow for the influence of gas compressibility on heat exchange. In the tests described, heat transfer was measured in a comparatively short tube; during flow in short tubes, much of the tube is occupied by the so-called initial section in which the distributions of velocity and temperature are set up. Strictly speaking the influence of the walls extends to the entire section of the tube, but at the beginning of the tute there is only appreciable disturbance of flow in a thin layer near the walls, which increases in thickness as the distance from the inlet increases. In order to study the relationship between the heat transfer during flow in pipes and with external flow over a plate, the experime tal data were worked out in the form of the so-called

Card 6/8

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Heat Exchange During Turbulent Flow of a Compressible Gas in Pipes in the Region of Mach Number up to 4

two-dimensional model of flow. According to this, the flow in the initial section of the tube is sub-divided into a boundary layer and an iso-entropic core. It is assumed that the retardation temperature and pressure in the core are constant. On this basis, expression (12) is derived and is valid for Reynolds numbers from 40×10^5 to 30×10^6 . The relationship between heat transfer and Reynolds number in this case is plotted in Fig 6; the scatter of experimental points is approximately the same as in the single-dimensional case. Formula (12) for heat transfer in the initial section of the tube was compared with the published formula for heat transfer from a flat sheet in the subsonic region of air flow. It is found that the relationship between heat transfer and the Reynolds number is approximately the same in the two cases, though heat transfer is a bit less in the tubes than on the sheet. The results of the comparison, plotted in Fig 7, show the experimental data to be in good

Card 7/8

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E194/E135

AUTHORS:

Petukhov, B.S., Shlykov, Yu.P., Kurayeva, I.V.,

Kazakova, Ye.D., and Prozorov, V.K.

TITLE:

Calculation of Transient Temperature Fields in Multi-Layer Walls with Internal Heat Evolution by

the Hydrothermal Analogy Method

PERIODICAL: Teploenergetika, 1960, No 10, p 95

TEXT: The temperature distribution is calculated in two and three layer walls with internal sources of heat, required to determine the temperature gradients during calculation of the strength of assemblies in several types of heat exchange

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ASSOCIATION: Moskovskiy energeticheskiy institut

(Moscow Power Institute)

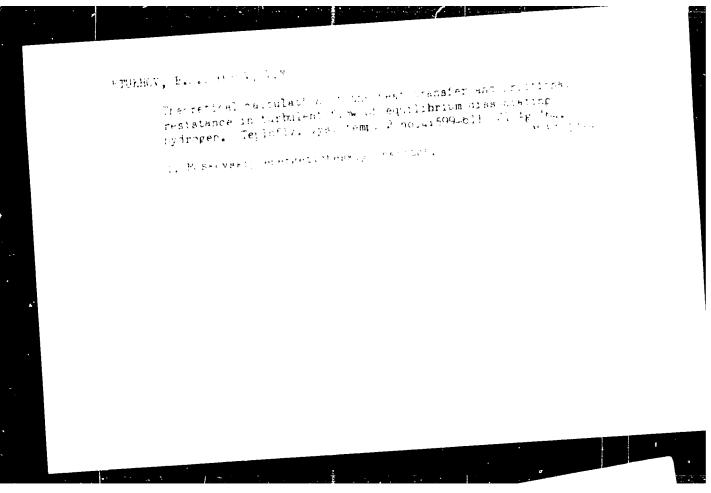
Card 1/1

PETUKHOV, B.S.; ROYZEN, L.I.

Experimental study of heat transfer during turbulent gas flow in circular tubes. Teplofiz. vys. temp. 1 no.3:416-424 NLD '63.

(MIRA 17:3)

1. Moskovskiy energeticheskiy institut.



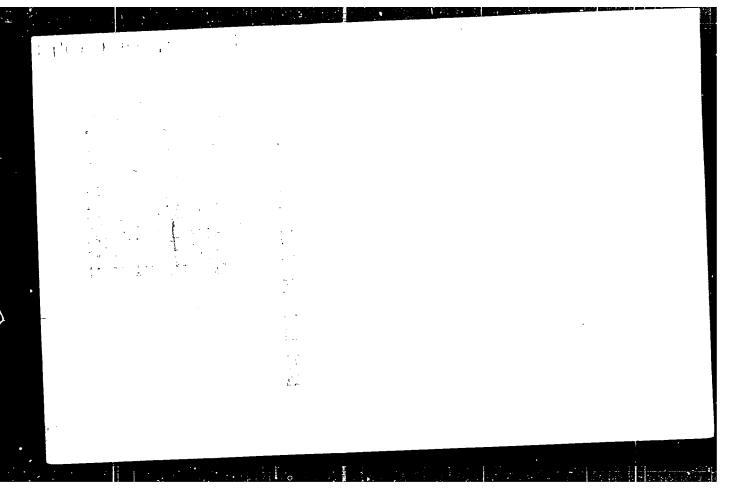
CIA-RDP86-00513R001240710002-4 "APPROVED FOR RELEASE: 06/15/2000 84310 5/170/60/005/005/ BO13/B060 Genin, L. G., Mal'ter, V. L. Heat Exchange in Tubes in the Presence of Inner Heat 5.1230 - 1284 enly Petukhov, B. S., 11.9200 Inzhenerno-fizicheskiy zhurnal, 1960, Vol. 3, No. 9, Sources in the Liquid Flow AUTHORS: TEXT: The authors start from the differential equation (1) which describes TITLE: TEXT: The authors start from the differential equation (1) which searces the steady flow of a liquid with uniformly distributed inner heat sources the steady flow of a liquid with uniformly tube walls. They obtain for and a constant density of heat flow on the tube walls. the steady flow of a liquid with uniformly distributed inner heat source They obtain formand a constant density of heat flow on the tube walls. They whe lines and a constant density of heat flow on the leminar flow. The lines are all the temperature distribution of a leminar flow. and a constant density of heat flow on the tube walls. They obtain formula (4) for the temperature distribution of a laminar flow. The authors slee for calculated by (A) are graphically shown in Fig. 1. The authors slee for PERIODICAL: mula (4) for the temperature distribution of a laminar flow. The lines found to the authors also found are graphically shown in Fig. 1. The authors also found to the difference to be proportional to the difference to be proportional to the tube is traversed the heat exchange coefficients to be proportional to the tube is traversed the heat exchange denotes the wall temperature when the tube is traversed to the heat exchange denotes the wall temperature when the tube is traversed to the heat exchange the heat exchange denotes the wall temperature when the tube is traversed to the heat exchange the heat exchange denotes the wall temperature when the tube is traversed to the heat exchange t the near exchange coefficients to be proportional to the difference traversed the Here, traversed the wall temperature when the tube is traversed by a liquid with inner heat sources, and tat is the adiabatic wall temperature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange ature, i.e., the wall temperature at which there is no heat exchange at the contract at ature, i.e., the wall temperature at which there is no near exchange at the same at the contract at the same at the contract at the c

Card 1/2

PETUKHOV, B. s.

"Heat Transfer and Hydraulic Resistance at Turbulent Flow of a Liquid with Variable Physical Properties in Tubes."

Report submitted for the Conference or Heat and Mass Transfer, Minsk, BSSR, June 1961.



APPROVED FOR RELEASE: 06/15/2000 CIA-RDP86-00513R001240710002-4"

PETUMFO", B. 5.

"Rest-exchange and hydraulic resistance in the turbulent course of a could with verying chysical or ; rises flowing through a tube."

Resort presented at the let All-Union Conference on heat- and has - Exchange.

Unak, WASR, 5-0 tune 1261

PICTUKHOV, B.S.; RUDAKOV, Yu.P.

Units for checking technological processes in preparing abrasive materials. Maslinostroitel no.2:18 F '61. (MIRA 14:2) (Abrasives) (Electric controllers)

5/170/61/004/004/004/ B117/B209

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Petukhov, B. S., Tsvetkov; F. F.

TITLE.

AUTHORS -

Calculation of heat exchange in laminar liquid flow in tutes within the range of low Peclet numbers

PERIODICAL ×

Inzhenerno-fizicheskiy zhurnal, v. 4, no. 3, 1961, 10-17

TEXT. The authors used an approximation method in calculating the heat exchange in a laminar flow of liquid within the range of low Pe numbers. This method is base on a stepped, instead of a continuous, radial temperature variation with the longitudinal temperature distribution remaining continuous. During these studies on stabilized flow and heat exchange in a cylindrical tube it is assumed that he liquid is not compressed, that its physical parameters are constant, that frictional heat is but ittle, and that the flow is hydrodynamically stabilized. The tube is divided along its radius into a number of coaxial layers whose thickness of may differ in any general case. The wall of the tube is counted as one of those layers. By dividing the tube into n layers and establishing a heat balance equation for each of these layers one obtains n ordinary second-order differential

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Calculation of heat ...

equations which take the boundary conditions at the wall into consideration. The solution of those equations yields the temperature variation as depending on x accurate except for a constant, for each of these layers. The integration constants are determined from the boundary conditions at the inflow and at the outflow end of the tube (or in infinity). After the equations for the temperature field have been found it is easy to calculate the local heat exchange coefficient. For a more exact calculation of the integrain, the temperature distribution is approximated by a discontinuous line. The suggested method is the more effective, the smaller the number of layers securing an accurate computation. Comparison of the results obtained by this method with the accurately computed values of heat exchange in laminar flow through tubes, known from competent publications, showed that on division of the tube into three layers the error amount to 3% at most. and to 1% in the case of four layers. The suggested method was used in solving the problem of heat exchange in a laminar flow of liquid through a round tube with constant heat flux density at the wall (the wall was assumed to be infinitely thin). Formulas were derived for the temperature field (i' a)

Card 2/8

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Calculation of heat ...

 $\theta_{i} = 4X + \sum_{j=1}^{3} A_{ij} \exp(-\hat{\epsilon}_{j}X) + A_{i4} (XSO) \text{ and } (11.b) \theta_{i} = 4\sum_{j=1}^{4} B_{ij} \exp(-\hat{\epsilon}_{j}X)(XSO)$

Fig. 1, for the mean calorimetric temperature of the liquid (12 a)

 $\theta_{\text{liq}} = 4X + \frac{3}{\sum_{j=1}^{3}} c_j \exp(-\epsilon_j X) + c_4 (X>0) \text{ and } (12.b) \theta_{\text{liq}} = \frac{4}{\sum_{j=1}^{4}} D_j \exp(-\sum_j X)(X>0)$

(Fig. 2), and for the local Nusselt number (13) $1/Nu = \sum_{j=1}^{3} E_j \exp(-\xi_j X) + E_j$

(Fig. 3). Here, A_{ij} , B_{ij} , C_{j} , E_{j} , C_{j} and u_{j} denote constants depending on the Pe number the values of which are given in Table 1. It was shown that the temperature gradient at the wall, in accordance with the boundary conditions, remains constant for X/O and vanishes at X(O). The $G_{liq} = F(X)$ curves

are located the higher, the lower the Pe number. The effect of axial heat conductivity becomes conspicuous for the fact that, first, at low X values the Nu number rises with Pe and that, secondly, the reduced length of the thermal initial section $\left[(1/\text{Pe})(1_{\text{t.A.}}/\text{d})\right]$ decreases with rising Pe, tending

Card 3/8

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Calculation of heat ...

towards a limit of 0.07; the relative length of the chermal initial section increases thereon. In Fig. 4 the theoretical value of the Nusselt number Nu = 4.36 is compared with the experimental data with respect to the heat exchange during the flow of mercury in a round tube, and it shows satisfactory agreement. These data were ascertained at the Moskovskiy factory agreement. These data were ascertained at the Moskovskiy energeticheskiy institut (Moscow Power Engineering Institute) by A. Ya. energeticheskiy institut (Moscow Power Engineering Institute) by A. Ya. energeticheskiy and B. K. Strigin under the supervision of one of the Yushin A. S. Sukomel, and B. K. Strigin under the supervision of one of the authors. There are 4 figures, 2 tables, and 5 references: 2 Soviet-bloc.

ASSOCIATION: Energeticneskiy institut, g Moskva (Institute of Power

Engineering, Moscow)

SUBMITTED: December 12, 1960

Card 4/8

21, 4240

\$/020/61/136/016/01/124 B104/B204

AUTHORS:

Petukhov, B. S. and Yushin. 4 Ta.

TITLE:

Heat exchange in the flow of a liquid metal in laminar

and intermediate regions

PERIODICAL:

Doklady Akademii nauk SSSR, v. 136. no. 6, 1961, 15, 111324

TEXT: By means of the experimental arrangement shown in Fig. 1, the heat exchange was studied on mercury with hydrodynamic and thermal stabilization of the flow. During filling, mercury was purified by distillation, and the two containers were filled with argon from which oxygen had been removed. The heat transfer coefficient was calculated from the relation $\alpha = q_1/\pi d \triangle t$, where q_1 is the density of the neat flow (kcal/m.hr) per unit length of the test tube; d is the inner diameter

(kcal/m.hr) per unit length of the test tube; d is the inner draw expectation of the tube; $\Delta t = t_w - t_{liq}$, where t_w is the wall temperature and the liquid temperature in a certain cross section. A correction of the relation, from which t_{liq} is calculated, is discussed, which takes heat

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20634 \$/020/61/136/006/010 024 B104/B204

Heat exchange in the flow of a ...

transfer through the mercury and the tube in the longitudinal direction into account. For the purpose of further reducing the effects produced by heat transfer in the longitudinal direction, the heat transfer coefficients were determined in cross sections which were at a distance of 18 d and 43 d from the beginning of the heated section of the tube Thus, the numbers determined here are limits, i.e., they are minimum values. Tests with turbulent water showed satisfactory results. The experiments with mercury were carried out in the following ranges. The experiments with mercury were carried out in the following ranges. The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 = 0.020). In Fig. 2, the Nu number is graphically represented as a function of the Fig. 2, the Nu number is graphically represented as a function of the Pe number. As may be seen, Nu = 4.36 for the laminar region, and Nu = 4.36 + 0.0053 Pe for the intermediate region. It is further noted that the results obtained here agree with an accuracy of +5% with the formula Nu = 5 + 0.014 Pe o.8 with Pe o.400 (Re - 1000) developed by the

formula Nu = 5 + 0.014 Pe with Pe 3 400 (Re 3 400) developed by the Energeticheskiy institut AN SSSR (Institute of Power Engineering of the AS USSR). It may further be seen that at the critical Reynolds number Re = 2300 no considerable change of the dependence of the Nu number upon the Pe number occurs. Finally, the effect of cross grooves in the

Card 2/5

Heat exchange in the flow of a ...

-20634 s/020/61/136/006/010/024 B104/B204

tube upon the heat transfer is investigated. It is found that as a result of these cross grooves, considerable irregularities in the distribution of q over the experimental length of the tube occur, and that the use of cross grooves is not convenient at small Pe numbers, because this may cause considerable errors. M. V. Vol'kenshteyn, M. A. Yel'yashevich, B. I. Stepanov, L. S. Mayants, L. A. Ignat'yev, and I. K. Bayev are mentioned. There are 3 figures and 5 references: 3 Soviet-bloc and

ASSOCIATION:

Moskovskiy energeticheskiy institut

(Moscow Institute of Power Engineering)

PRESENTED:

September 14, 1960, by P. L. Kapitsa, Academician

SUBMITTED:

August 24, 1960

Card 3/5_

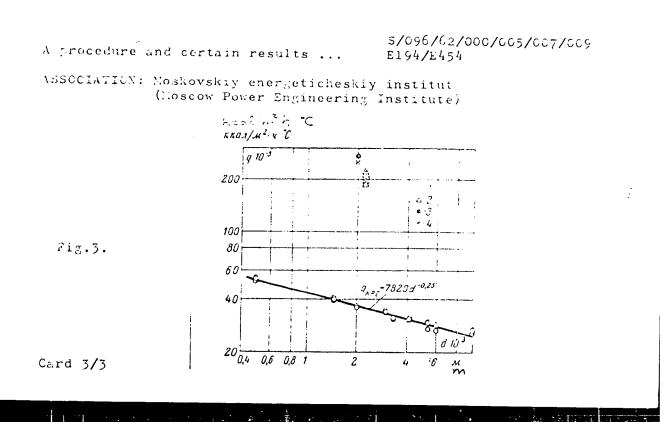
5/096/62/000/005/007/009 D194/E454 Metulhov, B.S., Doctor of Technical Sciences, Professor 1400 A procedure and certain results of measurement of Rovalev, Engineer CTHCK3: critical loads on transition from filmwise to bubile 717.200 PERICUICAL: Teploenergetika, no.5, 1962, 65-70 boiling This article analyses available methods of making tests or the critical condition of change from film boiling with evolution of bubbles and suggests a new one. Accurate knowledge is required to ensure stable overation of modern boilers and atomic reactors in which film boiling is possible. Experimental results obtained by the usual electrical heating methods are unreliable. Accordingly, special tests were made using distilled water at atmospheric pressure under conditions of free convection. The heating surfaces were horizontal electrically heated tubes and wires. Film boiling was ensured by preliminary heating of the specimens in the vapour phase. Special care was taken to ensure uniformity of heating over the length of the specimen: Card 1/3

A procedure and certain results ...

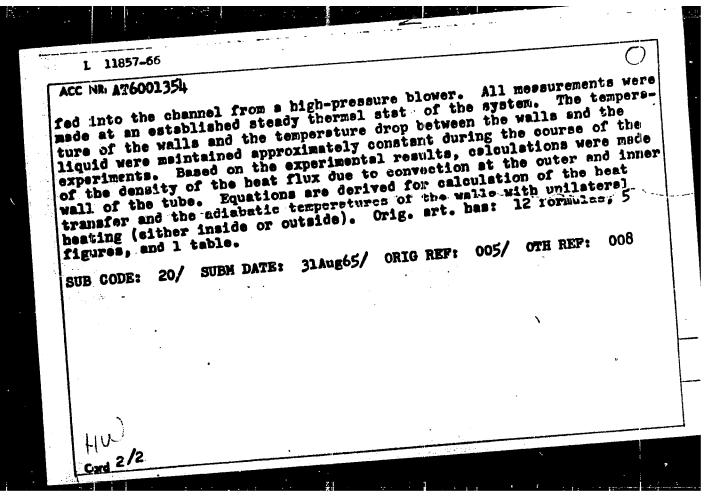
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equations are derived for this temperature distribution. experimental equipment with electrically heated specimens is described. Specimens heated to a temperature of 350 to 400°C were inversed in boiling water and the current through their was cradually reduced until the second critical point was reached, when the film broke away from the specimen. The experimental results are plotted in Fig. 3 as loading in kcal/m2 hr °C against specimen diameter in mm; the points on the graph are denoted as follows: I - experimental results for second critical loat loading; 2 - results of M.V. For shanskiy article in the Symposium "Problems of Heat Exchange on Altering the Aggregate condition of Substance", Gosenergoizdat, 1953); 3 - experimental equilibrium loading; 4 - calculated equilibrium loading. The results show that increasing the specimen diameter reduces the second critical heat loading and that the material of which the specimen is made has little effect on the results. It is shown how to use the test results to calculate the loading at which there is equilibrium between bubble- and film-boiling. There are 4 figures and 1 table. Card 2/3

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EWT(1)/EWP(m)/ETC(F)/EPF(n)-2/EWG(m)/EWA(d)/FCS(k)/EWA(1) SOURCE CODE: UR/0000/65/000/000/0066/0075 1 11857-66 ACC NR: AT6001354 44,55 44 S.; Royzen, L. I. ORG: Moscow Power Institute (Hoskovskiy energeticheskiy institut);
AlloUnion Electrotechnical Institute im. V. I. Lenin (Vsesoyuznyy TITIE: Hest transfer in the flow of a gas in tubes with an annular SOURCE: Teplo- i messoperenos. t. 1: Konvektivnyy teploobmen v odnorodnoy srede (Heat and mass transfer. V. 1: Convective heat exchange in an homogeneous medium). Minsk, Nauks i tekhniks, 1965, 66-75 TOPIC TAGS: convective heat transfer, gas flow, thermodynamics ABSTRACT: The article gives the results of an experimental investigation of heat transfer in the turbulent flow of air in annular tubes over a range of variation of the geometric parameter d1/d2 from 0.07 to 0.84. The experimental apparatus (shown in a diagram) consists of two concentric tubes. A table gives the geometric characteristics of the channels.
The outer brass tube (wall thickness 0.003 meters) was heated with an electric heater. The inner tube, made of 1Kh18M9T, was suspended at a single point by a wire with a thinkness of 0.001 meters. The air was Cord 1/2



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SS TAWY(1)/EWP(m)/EPF(n)-2/EWG(m)/EWA(d)/ETC(m)/EWA(1)/ETC/FOS WW/GS ACC NR AT6001363 UR/0000/65/000/000/0172/0182 SOURCE CODE: AUTHOR: Petukhov. B. S.; Chang, Chang-yung 44.55 94.55 3+1 Hosoow Power Institute ((Moscovskiy energeticheskiy institut) 21,44,55 TITLE: Best transfer in a hydrodynemic inlet section of a round tube with leminer flow of a fluid, 53 SOURCE: Teplo- i massoperenos. t. 1: Konvektivnyy teploobmen v odnorodnoy srede (Hest and mass transfer. v. 1: Convective heat exchange in en homogeneous medium). Minsk, Neuke i tekhnika, 1965, 172-182 TOPIC TAGS: convective heat transfer, hydrodynamics, metal tubes, fluid flow, Musselt number ABSTRACT: The problem of heat transfer in the hydrodynamic inlet section of a round tube when the heat flux at the wall is constant is solved with the following assumptions: 1) the flow and heat transfer are steedy-state; 2) the fluid is incompressible and its physical properties are constant; 3) the change in the heat flux due to heat conductivity slong the axis and the heat of friction are negligibly small; h) the temperature and velocity of the fluid in the inlet section are iniformly distributed and the velocity vector coincides with the exis of Cord 2 /2

Inner surface or Busselt number 1 velocity profile a comperison of	the tube wall. The article in the inlet section of a roun along the length of the tube the values of the Musselt numbers and the calculations of the state of the sections of the section of the sections of the section of	d tube as a function of , and a second curve all ber ascording to the conformation of la for salculation of	the hows plou-
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of [$\frac{1}{\text{Pe}} \frac{x}{d} < 0.038.$		
Orige arte bast	18 formulas and 3 figures.		-
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33667-66 EWT(1)/EWP(m) WW ACC NRI AP6014068 SOURCE CODE: UR/0294/66/004/002/0228/0232 Petukhov, B. S.; Mukhin, V. A. AUTHOR: Moscow Power Institute (Moskovskiy energeticheskiy institut) Experimental investigation of heat transfer during the supersonic flow of a gas in a round tube Teplofizika vysokikh temperatur, v. 4, no. 2, 1966, 228-232 SOURCE: TOPIC TAGS: convective heat transfer, supersonic flow, gas flow ABSTRACT: The working section of the experimental apparatus was a brass tube with an inside diameter of 20.2 mm, and outer diameter of 87 mm, and a length of 575 mm. The tube was water cooled. The local density of the heat flux was determined from the temperature drops in the walls of the tube. Air, previously cleaned of oil, moisture, and dust, was heated in an electric furnace to a temperature of from 200 to 800°C and was introduced into the working chamber through replaceable nozzles. Five series of experiments were made, with Mach numbers at the inlet of the tube of < 1,2.5, 3.0, 3.5, and 4. The change in pressure and velocity along the length of the tube in subsonic and supersonic flow corresponded in general to the one dimensional theory. Based on the Card 1/2 UDC: 536.242:533.6.011.35

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ACC NR: AP6014068

experimental data the article derives the following two empirical relationships:

St = 0.031 $R_{\theta_x}^{-0.2}P_{\Gamma}^{-0.5}$

(6)

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 $\mathrm{St} = 0.013\,\mathrm{Pe_{7}}^{\circ\,\circ} \stackrel{-0.25}{\mathrm{Pr}^{-0.8} T^{0.02}},$ гдо $P_{7}^{\circ\,\circ} = \int\limits_{0}^{x} q_{\mathrm{c}} dx \, / \, \lambda \, (t_{\mathrm{a.~c}} - t_{\mathrm{c}})$ (7)

These equations are said to agree satisfactorily with experimental data on heat transfer in the initial section of a tube, and for flow around a body, under conditions of cooling at Mach numbers M < 7. Orig. art. has: 7 formulas and 4 figures.

SUB CODE: 20/ SUBM DATE: 15May65/ ORIG REF: 007/ OTH REF: 007

Card 2/2/11/C

	ACC NR. AP6029778 SOURCE CODE: UR/C294/66/504.004/053170-3.
	AUTHOR: Popov, V. N.; Petukhov, B. S.
	ORG: Moscow Power Engineering Institute (Moskovskiy energeticheskiy institut)
:	TITLE: Theoretical calculation of heat transfer and resistance in laminar price flow of hydrogen dissociated in equilibrium
	SOURCE: Teplofizika vysokikh temperatur, v. 4, no. 4, 1966, 531-539
	ABSTRACT: In high-temperature heat exchangers, the viscosity of the gas becomes so high that a laminar flow regime is frequently established. Therefore, a theoretical study was made of the local heat transfer coefficients and the flow resistance during laminar pipe flow of dissociated hydrogen. The heat flux through the wall was assumed to be constant. The results calculated for pressures of 1, 10, and 100 atm at 2000—5000K are presented in graphs. Orig. art. has: 5 formulas and 8 figures. [FV] SUB CODE: 21/ SUBM DATE: 270ct65/ ORIG REF: 002/ OTH REF: 003 ATD Press 5765
	Cord 1/1 UDC; 536.24.01.532.542.2

1 45629-65 EWT(1)/EWP(m)/EWT(m)/EWA(d)/EWP(t)/EWP(z)/FCS(k)/EWP(b)/EWA(1) AP50061113 8/0294/65/003/001/0102/0108 ACCESSION NR: AUTHOR: Petukhov, B. B.; Kirillov, V. Y.; Chu, Tzu-helang; Maydanik, V. N. Experimental investigation of the effect of the temperature factor on heat exchange in turbulent flow of gas in tubes SOURCE: Teplofizika vysokikh temperatur, v. 3, no. 1, 1965, 102-106 TOPIC Dids: temperature factor, heat exchange, turbulent flow, Reynolds number, Nusselt number, heat transfer ABSTRACP: This is part of a systematic investigation parried out for several years at MITYT (Scientific Research Institute of High Temperatures) on heat exchange inder conditions of appreciable variation of physical properties of flowing liquid. The purpose of the present investigation was to extend the range of previous investigations of local heat transfer and turbulent flow of gas in tubes at high temperature gradients, and to accumulate experimental data on the subjent. An earlier stage of the research was laready published (Teplofizika vysokikh tem-peratur v. 1, no. 1, 1963). The experiments were made with ritrogen in a stilln-less steel tube heated with electric covrent flowing through the tube wall. The **Cord** 1/2

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were made and 500 experience of the gas temperature of the gas temperature of the gas temperature of that the influence of tably over the length of formula Nu = 0.022.Refe	imental points obtained. The temperature factor was value ranging from 100 to 500K as maintained within 5%. The ture at the inlet to the turansfer even at large value, the tube. The experimenta 8 0.4 which is in good actions of the authors (Temperature).	he Reynolds numbers ranged ried between 1:1 and 3.6, if the wall temperature remembers noting the does not exert any noting of the temperature factors hen; transfer varies not:	from dish ched is- eable , and ce- r
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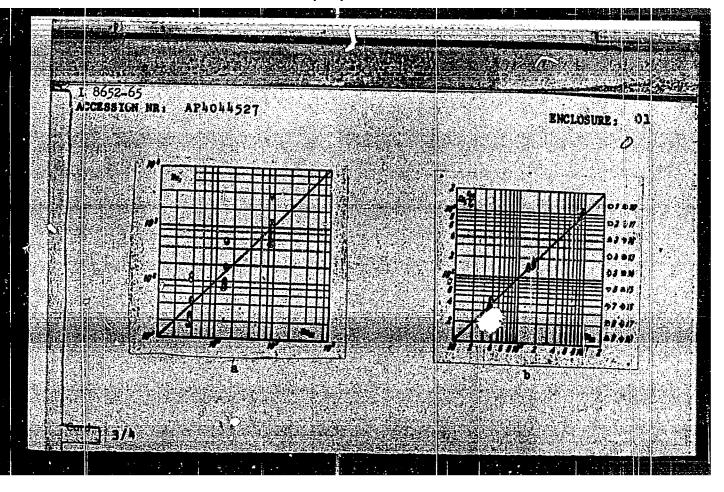
1 8652-65 ENT(1)/ENF(n)/ENT(n)/EPF(6)/EPF(n)-2/EPF(T/EPA(bb)-2/FCS(k)/ENP(b)/ TNA(1) Pd-4/Pr-4/Ps-4/Pu-4 AFTC(a)/ASD(d)/ASD(p)-3/AS(mp)-2/ASD(t).2/BSD/ AEDC(a)/SSD/ESD(t) Jr/44/JW 8/0294/64/002/004/0599/06:11 ACCESSION NR: AP4044527 JUTHOR: Petoknov B. S.; Popov. V. A. Theoretical calculation of heat transfer and friction resisance in a turbulent flow in a pipe of equilibrium dissociating hydrogen HOURCE: Teplofizika vy sokikh temperatur, v. 2, no. 4, 1964, 599-611 TOPIC TAGE: heat transfer, dissociation, turbulent flow, hydrogen dissociation, hydrogen oxygen mixture, equilibrium dissociation ABBIRACT: A method is given for theoretical calculation of heat trans fer and friction resistance in a turbulent flow of dissociating hydrogen in a pipe. It is assumed that the dissociation rate exceeds considerably the convective and diffusional mass transfer rates. In this page, chemical equilibrium is established in each point of the flow, and the pomposition of the mixture is a function of pressure and ten-peratura only. In the case of equilibrium dissociation, the concentra-tion profile in the flow may thus be defined without solving the diffusion equation. The heat transfer; friction resistance, and different Gill 1/12

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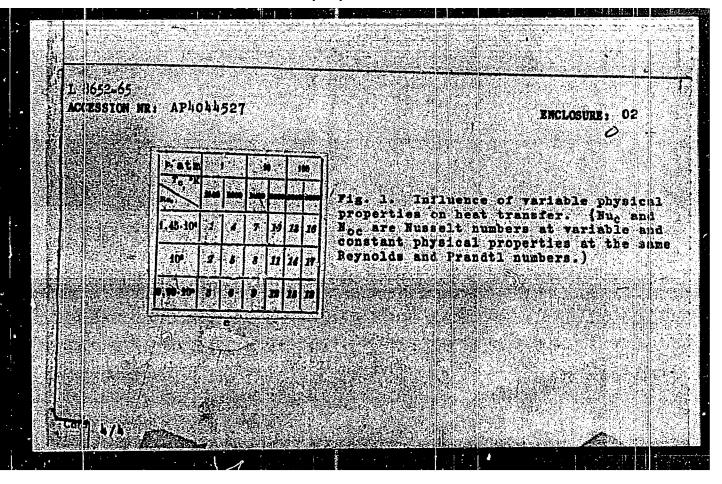
1, 8652-65 EWT(1)/EWP(m)/EWT(m)/EPF(c)/EPF(n)-2/EPR/T/EPA(bb)-2/FCS(k)/EWP(b)/ EWA(1) Pd-4/Pz-4/Ps-4/Pu-4 AFTC(a)/ASD(d)/ASD(p)-3/AS(mp)-2/ASD(f)-2/ASD/ JEDC(a)/SSD/EBD(t) JD/WA/JW ACCRESTON DR: APAONA527 8/0294/64/002/004/0599/0611 Patulhov. B. B.; Popov. V. M. Theoretical calculation of heat transfer in a turbulent flow in a pipe of equilibrium lescolating bydro BOURCE: Teplofizika vysokikh temperatur, v. 2, no. 4, 1964, 599-611 TOPIC TAGS: heat transfer, dissociation, turbulent flow, hydrogen dissociation, hydrogen oxygen mixture; squilibrium dissociation ABBURACT: A method is given for theoretical calculation of heat trans fer and friction resistance in a turbulent flow of dissociating hydrogon in a pipe. It is assumed that the dissociation rate exceeds considerably the convective and diffusional mass transfer rates. In this chae, chemical equilibrium is established in each point of the flow, and the composition of the mixture is a function of pressure and tenpirature only. In the case of equilibrium dissociation, the concentra tion profile is the flow may thus be defined without solving the diffe-The heat transfer, friction resistance, and different Card 71/4

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PETUKHOV, B.S.; POPOV, V.N.

Theoretical conculation of the heat transfer and frictional resistance in the laminar flow in tubes of an incompressible fluid with variable physical properties. Teplofiz. vys. temp. 1 no.2 228-237 S-C163. MIRK 1715

1. Moskovskiy energeticheskiy institut.

ACCESSION NR: AP4017720

5/0294/63/001/003/0416/0424

A CONTRACTOR OF THE PROPERTY O

AUTHORS: Petukhov, B. S.; Royzen, L. I.

TITLE: Experimental investigation of heat exchange in the case of turbulent flow of gas in tubes of annular cross section

SOURCE: Teplofizika vy*sokikh temperatur, v. 1, no. 3, 1963, 416-424

TOPIC TAGS: heat exchange, annular cross section tube, turbulent air flow, unilater heat supply, heat transfer coefficient, Reynolds number, heat flux density, thermal flow stabilization, hydrodynamic flow stabilization

ABSTRACT: In order to ascertain the effect of the geometry on heat exchange in tubes with annular cross sections, a topic far from fully explained in the literature, the authors consider a procedure and the results of an experimental investigation of heat exchange for turbulent flow of air in such tubes with a diameter ratio ranging

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ACCESSION NR: AP4017720

from 0.07 to 0.7. The principal measurements were made with unilateral heat supply, i.e., with constant density of heat flow in one of the walls, the other wall being thermally insulated. The heat transfer coefficients were measured on the heated walls and the adiabatic wall temperatures on the insulated walls. The Reynolds number range was from 10 to 3 x 10 The coefficients were calculated using relations derived in an earlier paper (Inzh.-fiz. zh. no. 3, 1963). To check on these relations, some of the experiments were carried out with both walls heated simultaneously. The data obtained make it possible to calculate the heat exchange for an arbitrary ratio of heat-flux densities on the inner and outer walls. The data can be used to calculate heat transfer in annular tubes in regions with thermal and hydrodynamic stabilization of the flow, for an arbitrary ratio of heat load on the walls. Orig. art. has: 7 figures, 6 formulas, and 3 tables.

Card 2/4

ACCESSION NR: AP4017720

ASSOCIATION: Moskovskiy energeticheskiy institut (Moscow Power

Engineering Institute)

SUBMITTED: 060ct63 DATE ACQ: 23Mar64

ENCL: 01

SUB CODE: PH

NR REF SOV: 004

OTHER: 005

PETUKHOV, B.S.; KIRILLOV, V.V.; TSZYUY TSZY-SYAN [Chu TS'K-hsiang]; MAYDANIK, V.N.

Experimental study of the effect of the temperature factor on heat transfer during turbulent gas flow in pipes. Teplofiz. vys. temp. 3 no.1:102-108 Ja-F *65. (MIRA 18:4)

1. Moskovskiy energeticheskiy institut.

ACTING APTONSOSS (A) Section Color Unitary, so to Alexander ACTING APTONSOSS (A) Section Color Unitary, so to Alexander ACTING: Network, G. G.; Svirezheva, S. S.; Druzhkov, O. N.

CRS: none

A TITLE: Thermal decomposition of Unitarylable and Action of Unitarylable and Unitarylable

tricyclohexy permane at 400-4500 was studied. The main decomposition products of tricyclohexy permane at 400-4500 was studied. The main decomposition products of tricyclohexy permanes, containing cyclohexyl rings; no hydrogen was product on the composition products of tricyclohex was producted. The finite accomposition products of tricyclohexyl mane to hydrogen was producted. The finite accomposition products of tricyclohexyl mane to hydrogen was producted and highly condensed compounds containing cyclohexyl rings. It was proposed that the thornal decomposition of tricyclohexylsilane and tricyclohexylgermane occurs in stages according to a hydride mechanism, accompanied by secondary processes of conversion of the maction products formed (hydrogenation, dehydropolymerization, condensation). Orig. art. has: 1 table. (JPRS)

Cord 1/1 3 6

ACC NRI AP7000777

SOURCE CODE: UR/0208/66/000 8/10/3/1028

AUTHOR: Petukhov, I. V. (Moscow)

ORG: none

TITLE: On one scheme of difference approximation for the numerical solution of parabolic type equations

SOURCE: Zhurnal vychislitel'noy matematiki i matematichesoy fiziki, v. 4, no. 6, 1966, 1019-1028

TOPIC TAGS: approximate solution, approximation calculation, approximation convergence, approximation method, parabolic differential equation, differential equation solution

ABSTRACT: An autonomous scheme for the difference approximation of the privative $\partial u/\partial x$ of the second order of precision was proposed. This is used without loss of precision or degree of calculation stability in the case of the degeneration (full or partial) of a parabolic type equation to an ordinary differential equation (in y). The scheme is useful in boundary layer problems of gas flow, and one such problem for a spherical truncated cone is analyzed. The equation is of the type

 $au = L[u], \quad a(x, y) \geqslant 0,$

 $L[u] = (mu')' + k_2u' + k_1u + k_0, \quad m(x, y) > 0$

Card 1/3

VDC: 519:517.944/.947

in scheme II. The method is compared with the iteration process and also the studies in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions. Orig. art. met.; tables, in regard to a Fourier series of normalized eigenfunctions.

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ACC NR: AP6028344 SOURCE CODE: UR/0293/66/004/004/0641/0644

AUTHOR: Petukhov, S. V.

ORG: none

TITLE: On one method for approximate solution of the Euler-Lambert equation

SOURCE: Kosmicheskiye issledovaniya, v. 4, no. 4, 1966, 641-644

TOPIC TAGS: approximation calculation, elliptic orbit, hyperbolic orbit, orbit semimajor axis, orbit calculation, electronic computer

ABSTRACT: A method described in this paper allows the semimajor axis of an orbit to be determined in explicit form directly from the flight time in the range of angular distances of $0^{\circ} < \phi < 360^{\circ}$. The following normalized energy characteristic of the orbits is examined

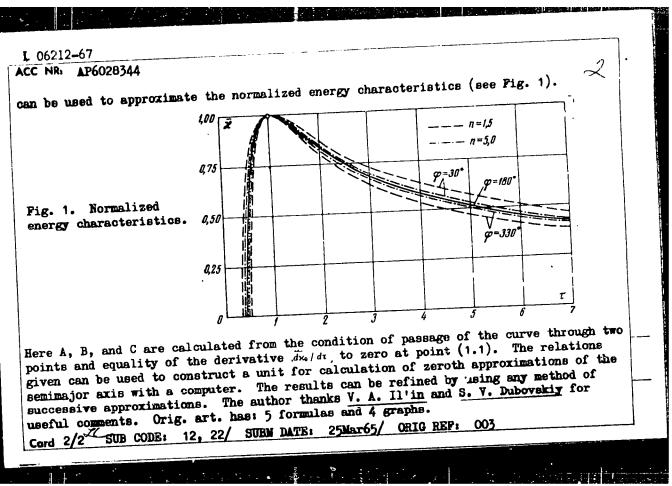
 $\bar{\chi} = \frac{a_b}{a} = f(\tau),$

where a is the semimajor axis of the flight orbit; $\mathcal{T} = \Delta t/\Delta t_b$, and where a and Δt_b correspond to the flight in the boundary elliptic orbit and are completely determined by the geometry of the flight (r_1, r_2, φ) . The relation

 $\vec{x}_0 = A + \frac{B}{\tau} + \frac{C}{\tau^2}$

Card 1/2

UDC: 629.197.7



L 08374-67

ACC NR: AR6028150

SOURCE CODE: UR/0058/66/000/005/11079/11079

31

AUTHOR: Grigor'yeva, V. M.; Petukhova, S. V.

TITLE: Methodological hints on the measurement of noise of ultrasonic installations

under production conditions

9m

SOURCE: Ref. zh. Fizika, Abs. 5Zh554

REF. SOURCE: Nauchn. raboty in-tov okhrany truda VTSPS, vyp. 6(38), 1965, 55-64

TOPIC TAGS: ultrasonics, acoustic noise, acoustic measurement

ABSTRACT: Measurement conditions are formulated, measuring apparatus is suggested, and a procedure is described for carrying out the measurements and for processing the results. The appendices contain the permissible levels of sound pressures at operating locations of ultrasonic installations (from Gigenich. trebovaniya (Hygiene Requirements) no. 515a - 64), and also the characteristics of measuring instruments and some tables for reference. [Translation of abstract]

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Translation from: Referativnyy zhurnal, Mekhanika, 1958. Nr 9, p 107 (USSR)

Petukhov, A. I AUTHOR:

Determination of the Water Seepage Rate During the Desiccation TITLE:

of a Coal-particle Medium Having a High Degree of Nonuniformity of the Particle Size (Opredelenive skorosti fil'tratsii vody pri obezvozhivanii ugol'nov sredy s bol'shim koeffitsiyentom neod-

norodnosti chastits uglya po krupnosti)

PERIODICAL: Izv. Dnepropetr gorn in ta, 1957 Vol 27, pp 113-119

Results of tests are adduced relative to the determination of ABSTRACT:

the influence of the grain-size composition (presence of a filler) on the filtration properties of a mixture of coal grains. A maximal diminution of the filt ation properties of the mixture of coal grains was observed for a 32-34% content of small filler grains. The seepage rate of the water in a coalgrain medium with small-grain filler can be determined by the formula $v_c = cv_3m_1$, where m_1 is the porosity coefficient of the "skeleton" of the coal-grain medium, v3 is the seepage rate in the filler; and c is an empirical coefficient having a

mean value of 1.42 (in eight different mixtures). minim--War

2. Water--Penetration 3. as particles--Determination A.R.Chairles Card 1/1

4. Mathematics--Applications

PETUKHOV, F.S., doktor tekhm.nauk, prof.; KOVALEV, S.A., inzh.

Methods and some results of the critical load measurement nurion the transition from film- to table hallow. Included the no.3165-70 My *62.

1. Moskovskiy energeticheskiy institut.

(Erellition)

ACCESSION NR: AP4004144

s/0294/63/001/002/0228/0237

AUTHORS: Petukhov, B. S.; Popov, V. N.

TITLE: Theoretical calculation of heat transfer and friction resistance in laminar flow in pipe of incompressible fluid with variable physical properties

SOURCE: Teplofizika vy*sokikh temperatur, v. 1, no. 2, 1963, 228-237

TOPIC TAGS: heat transfer, laminar flow, coolant, air heat transfer, hydrogen heat transfer, MS-20 oil heat transfer, transformer oil heat transfer, hydraulic resistance, Nusselt number, incompressible fluid, fluid flow, incompressible flow

ABSTRACT: Although calculations of heat exchange and hydraulic resistance in laminar flow of liquids with variable physical properties in pipes are encountered in many branches of engineering, the existing theoretical papers are devoted only to limited aspects of the problem, and none contain an analytic expression for the heat transfer. The authors derive analytic expressions for the Nusselt number and the hydraulic resistance coefficient for laminar flow in

Card 1/2

ACCESSION NR: AP4004144

a pipe, away from the inlet, for an incompressible liquid with arbitrary temperature variation of the physical properties. These analytic expressions are used to calculate the heat emission and the friction resistance for air, hydrogen, water, Ms-20 oil, and transformer oil. In the calculations for oil and water, the viscosity ratio $\mu_{\rm wall}/\mu_{\rm liq}$ ranged from 0.16 to 51. The temperature factor $T_{\rm wall}/T_{\rm liq}$ for air and hydrogen ranged from 0.4 to 1.75. Empirical equations are derived for the Nusselt number and the friction resistance. Orig. art. has: 3 figures, 14 formulas, and 1 table.

ASSOCIATION: Moskovskiy energeticheskiy institut (Moscow Power Engineering Institute)

SUBMITTED: 18Jul63

DATE ACQ: 26Dec63

ENCL: 00

SUB CODE: AI, PR

NO REF SOV: 004

OTHER: 006

Card 2/2

PETUKHOV, B.S.; GENIN, L.G.

Heat transfer in tubes with internal heat sources in a liquid flow. Insh.-fiz. zhur. 6 no.4:3-8 Ap '63. (MIRA 16:5)

1. Institut vysokikh temperatur pri Moskovskom energeticheskom institute.

(Heat-Transmission) (Hydrodynamics)

1. 11181-63 EPR/MPF(c)/EWT(1)/RDS/T-2--AFFTC/ASD--Ps-li/Pr-li/P1-li 67 ACCESSION NR: AP3001548 S/0143/63/000/004/0081/0089

AUTHOR: Petukhov, B. S. (Dr. of technical sciences, Prof.); Kovalev, S. A. (Engineer)

TITE: Critical boiling-liquid thermal loads

SOURCE: IVUZ. Energetika, no. 4, 1963, 81-89

TOPIC TAGS: boiler load, film-type boiling, nucleate-type boiling

ABSTRACT: At a certain "equilibrium" thermal load, both types of boiling — the film and the nucleate — are stable at a given heating surface (see article in Toplosnergetika, No 5, 1962, by the same authors). When the load is higher than the equilibrium, only the film type is stable; when the load is lower than the equilibrium, then the nucleate type is stable. The present article submits: (a) some results of experiments with the nucleate boiling of large volumes of water at pressures up to 85 atm. and (b) a general method for calculating the equilibrium loads. The experimental outfit included an electrically heated 2-mm nichrome wire immersed in a pressure tank with water. At 80 atm., the critical load was measured around 150 x 10 sup 3 kilocalories/sq. m. hr. Engineer V. V. Karelin took part in the experimental work. Equilibrium load with boiling at the

Card 1/2

L 11181-63

ACCESSION NR: AP3001548

outer surface of an infirite cylinder is described mathematically. Some peculiarities of the film-type boiling in tubes are considered. In conclusion, the authors criticize the existing method of selecting the maximum permissible load for a given heating surface. Orig. art. has: 4 figures and 8 formulas.

ASSOCIATION: Moskovskiy ordena Lenina smergeticheskiy institut, Kafedra inzhenernov teplofiziki (Moscow Power-Engineering Institute, Chair of Engineering Thermal Physics)

SUBMITTED: 03Dec62

DATE ACQD: 21Jun63

ENCL: 00

SUB CODE: 00

NO REF SOV: 003

OTHER: 001

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S/170/63/006/003/001/014 B104/B186

AUTHORS: Petukhov, B. S., Royzen, L. I.

TIPLE: Heat transfer in tubes with annular cross section

PERIODICAL: Inzhenerno-fizicheskiy shurnal, v. 6, no. 3, 1963, 3 - 11

TEXT: In this study the following assumptions are made: there is stationary flow of an incompressible liquid through a tube with annular cross section; the heat flow densities $\mathbf{q_{c_1}}$ and $\mathbf{q_{c_2}}$ to the inner and to the

outer tube wall are constant; the heat transfer along the tube axis by heat conduction is small compared with the convective heat transfer; the physical properties of the liquid are independent of temperature; energy dissipation is negligible. Applying the condition of a stabilized temperature field yields the equation $\frac{\partial \{p_{ij}\}_{i=1}^{n}}{\partial \{p_{ij}\}_{i=1}^{n}} \frac{\partial \{p_{ij}\}_{i=1}^{n$

 $CW_x R = \frac{\partial}{\partial R} \left[R \left(1 + \frac{\epsilon_q}{a} \right) \frac{\partial t}{\partial R} \right].$

 $C = \frac{2(q_{c_1}r_1 + q_{c_2}r_2)r_2^2}{\lambda(r_2^2 - r_1^2)}.$ (6)

Card 1/3

S/170/63/006/003/001/014 B104/B186

Heat transfer in tubes with ...

which is solved for the boundary conditions

$$\left(R\frac{\partial t}{\partial R}\right)_{R=R_1} = \frac{q_{c_1}r_1}{\lambda}, \quad \left(R\frac{\partial t}{\partial R}\right)_{R=1} = \frac{q_{c_1}r_2}{\lambda}, \quad (a_0)_{R=R_1, 1} = 0. \tag{A}.$$

Here, W_{X} is the reduced velocity of the liquid, $R = r/r_{2}$, $R_{1} = r_{1}/r_{2}$, r is the running parameter. Integrating (6) from R_{1} to R and introducing the reduced temperature $(t - t_{1})\lambda$

$$\Theta = \frac{2}{(1-R_1^2)} \int_{R_1}^{R} \frac{\int_{R_1}^{R} W_x R dR}{\left(1+\beta \frac{a_x}{v} Pr\right) R} dR - P \int_{R_1}^{R} \frac{dR}{\left(1+\beta \frac{a_x}{v} Pr\right) R},$$

$$\Theta = \frac{2}{(1-R_1^2)} \int_{R_1}^{R} \frac{\int_{R_1}^{R} W_x R dR}{\left(1+\beta \frac{a_x}{v} Pr\right) R} dR - P \int_{R_1}^{R} \frac{dR}{\left(1+\beta \frac{a_x}{v} Pr\right) R},$$

where \mathcal{E}_q /a is replaced by $\Delta \mathcal{E}_{\tau} Pr/v$; $\beta = \mathcal{E}_q/\mathcal{E}_{\tau}$, $P = q_{01}r_1/(q_{01}r_1 + q_{02}r_2)$.

Card 2/3

8/170/63/006/003/001/014 B104/B186

Heat transfer in tubes with ...

Here $\xi_{\bf q}$ is the factor of turbulent heat transfer, and $\xi_{\bf r}$ the factor of turbulent momentum transfer. Prom these equations integral relations for the temperature field and for the heat transfer coefficients are derived for arbitrary heat loads on the walls. Finally the heat transfer of a laminar flow in annular tubes is calculated numerically. There are 4 figures and 1 table.

ASSOCIATION: Energeticheskiy institut, g. Moskva (Power Engineering Institute, Moscow)

SUBMITTED: October 2, 1962

Card 3/3

A transfer to the second of th

PETUKHOV, B.S., doktor tekhn.nauk, prof.; KOVALEV, S.A., inzh.

Critical thermal loads during the boiling of a liquid. Izv. vys.

ucheb. zav.; energ. 6 no.4:81-89 Ap 163.

(MIRA 16:5)

1. Moskovskiy ordena Lenina energeticheskiy institut.
Predstavlena kafedroy inzhenerney teplofiziki.
(Thermodynamics) (Fluid dynamics)

ETUKHOV, B.S.; POPOV, V.N.

Theoretical calculation of heat transfer and frictional resistance in the turbulent flow of an incompressible fluid of variable physical properties in pipes. Teplofiz. vys. temp. 1 no.1:85-101 (MIRA 16:10) J1-Ag 163.

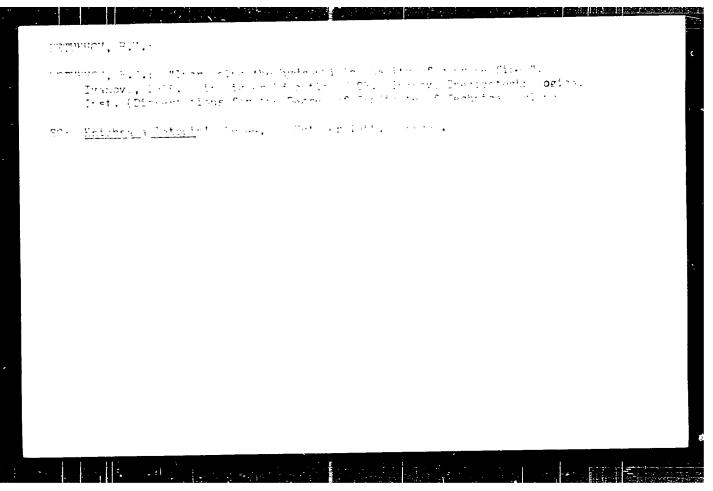
1. Moskovskiy energeticheskiy institut.

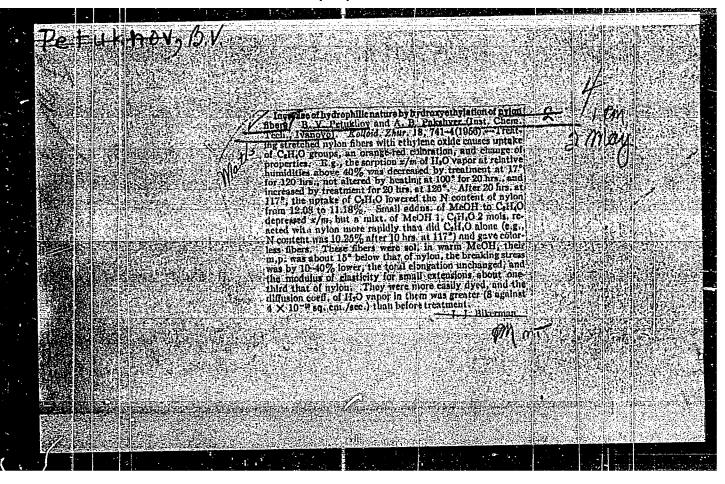
CIA-RDP86-00513R001240710002-4" APPROVED FOR RELEASE: 06/15/2000

PETUKHOV, B.V!

ARKHANJEL'SKIY, P.Ye., inzhener; ARKHIPOV, P.P., inzhener; VAS'KOV, M.P., agronot; ZHMUDSKIY, D.A., arkhitektor; IVANOV, A.P., arkhitektor; KIBI-HEV, S.F., arkhitektor; ERYLOV, N.V., inzhener-arkhitektor; KULAKOV, D.V., arkhitektor; MARTYNOV, P.F., inzhener; NIKIFOROV, V.S., inzhener; NOSKOV, B.G., arkhitektor; PETUKHOV, B.V., kandidat tekhnicheskikh nauk; RYAZANOV, V.S., kandidat arkhitektury; SOKHRANICHEV, N.S., inzhener-arkhitektor; TARASOV, D.I., arkhitektor; SHMIDT, N.E., kandidat arkhitektury; KHOMUTOV, Ye.Ye., arkhitektor; VOL'FOVSKAYA, V.N., redaktor; FEDOTOVA, A. F., tekhnicheskiy redaktor.

[Handbook on the construction of farm buildings] Spravochnik po sel'skokhoziaistvennomu stroitel'stvu. Avtorskii kollektiv: P.E.Arkhangel'skii i dr., avtor-sost. N.V.Krylov. Moskva, Gos.izd-vo sel'khoz.lit-ry. Vol.3 1955, 843 p. (Farm buildings)





The same of the sa

1 シェアレルム USSE/Higgieal Chemistry. Surface Phenomena, Adsorption B-15 Chromatography. Ion Exchange.

Abs Jour : Ref Zhur - Khimiya, No 7, 1957, 22545.

Author : B. V. Fetulnov, A. B. Pakshver. : Not given here he I he had : Storm sormtion by approne fiber. Title

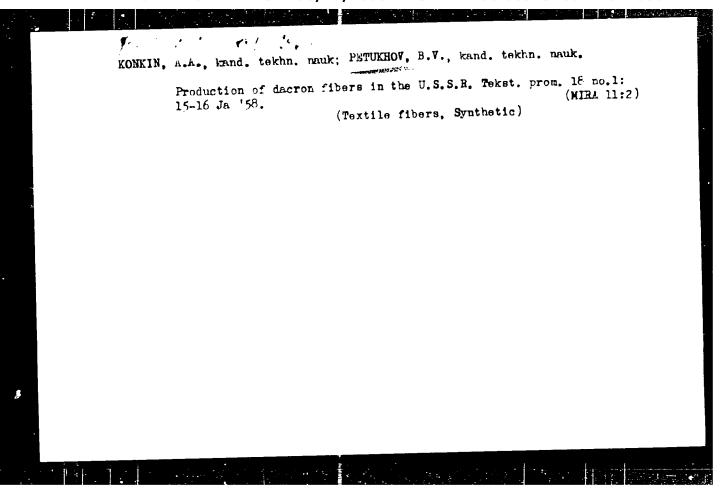
Orig Pub : Zh. priki. knimii, 1956-29, No 5, 1236-1258 (ruso).

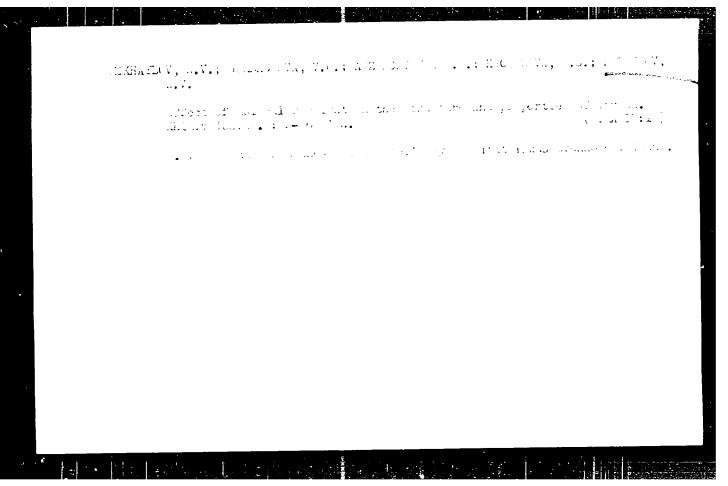
Abstract : Oriented caprone fil rs, treated without tension by an aque-

ous phenol solution reduce steam sorption (3) at low values of relative humidity a and increase S at high s. Treatment of fiber under tension had no influence on the value and rate of S. Thermal treatment reduces S of steam, this reduction is stronger if the fiber is heated under tension, then when heated without one. The process of compression of molecular structure by heating caprone fiber proceeds very fast and ends in 30 sc onds. Steam S does not depend on uncromolecule orientation, but depends on the quantity of intermolecular bonds. At the relative humidity \$\leq 25\%, the diffusion coefficient does not depend on steam elasticity at given temperature. Deformation index of the caprone fiber increases sharply with the heating of the fiber by overfeated sterm under tension.

 $C_rd 1/1$

-188-





L 24694-65 EMT(m)/EMP(j)/T Pc-4 RM

ACCESSION NR: AP4049878

5/0183/84/000/008/0018/0022

AUTHOR: Ayzenshteyn, E. M.; Petukhov, B. V.

TITLE: Effect of molecular weight on orientative drawing and properlies of Dacron fiberate

SOURCE: Khimicheskiye volokna, no. 8, 1984, 18-22

TOPIC TAGS: Dacron, polyethylene terephthalate, fiber, film, crystallization, mechanical property, plastic deformation, strength, fatigue property, creep

ABSTRACT: The effect of changing the molecular weight of the polyethylene terephthalate from 17500 to 25000 on the drawing of the Dacron fiber (drawn from #6.2-8 5 to #34-36) and the fiber properties were investigated. The tendency of the isotropic (unstretched) fiber to age and to crystallize on heating decreased with increasing molecular weight. With increasing molecular weight the tension upon drawing increased, the maximum extent to which the fiber could be effectively drawn decreased, and the fiber adhered less to the metal surface of the heating element. A study of the drawing temperature-mechanical property relationship

Cord 1/2

L 21696-65 Accession NR; AP4049878

2

showed the optimum drawing temperature was determined by the drawing rate and factor and the material molecular weight. Drawing at temperatures above the optimum decreased the dynamic resistance of the fiber. The modulus of elasticity of isotropic fiber was almost independent of molecular weight, but increased in anisotropic fiber as the molecular weight increased. Increase in molecular weight reduced the tendency toward irreversible plastic deformation, improved the fatigue properties, fiber strength, pliability and dynamic resistance of the polyester fiber, permitted a higher optimum drawing temperature, and decreased the creep on heating. Orig. art. has: 8 figures and 3 tables

ASSOCIATION: VNITY; VNITSV

SUBMITTED: 22Nov63

ENCL: 00

SUB CODE: MT

NO REF SOV: 019

OTHER: ODD

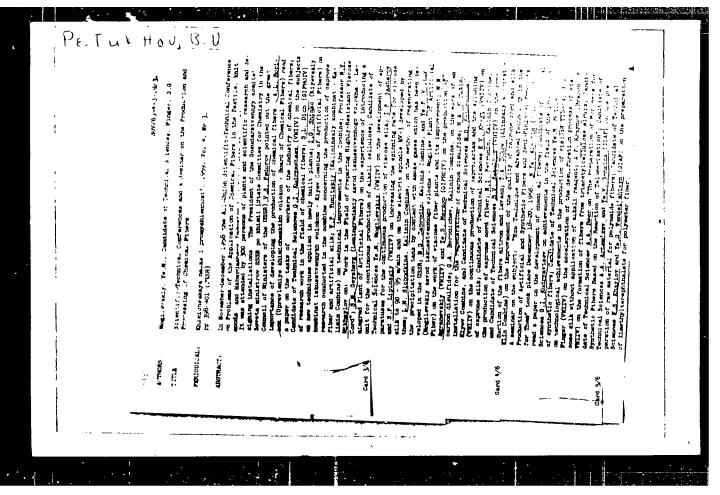
Card 2/2

PETUKHOV, B.V.; KONKIN, A.A.

Technology of the manufacture of the polyester fiber "lavsar".

Khim. volok. no.2:11-16 '59. (MIRA 12:9)

1.Vsesoyuznyy nauchno-issledovatel'skiy institut iskuastvennogo volokma. (Ravon)



5(3)

30V/80-32-5-4T/52

AUTHORS:

Petukhov B. V. Konkin, A.A.

TITLE:

The Combination of the Reactions of Reesterification and Folycondensation in the Synthesis of Polyethyleneterephthalate

PERIODICAL:

Zhurnal prikladnoy khimii, 1959, Vol 32, Nr 5, pp 1171-1173 (USSR)

ABSTRACT:

Polyethyleneterephthalate is the base of the polyester fiber "lavsan". It is produced by the reesterification of the dimethyl ether if the terephthalic acid and ethylene glycol to diglycol ether, and the provecondensation of the latter to polyethyleneterephthalate. Ethylene glycol is used in the quantity of more than two moles per one mole of diethyl other. Experiments were made to use less than two moles in the reaction. For this purpose 0.05% of zinc acetate was used as a catalyst. The yield was approximately the same as in the ratio 2.7: I The products obtained had a sufficiently high molecular weight, which could not be expected, if the unreacted methoxy-groups had blocked the ends of the chain. The formed ethyleneglycol remains in the sphere of reaction due to the increasing viscosity and the ratio may be therefore

Card 1/2

less than 2 : 1.

sov/80-32-5-47/52

The Combination of the Reactions of Reesterification and Polycondensation in the Symthesis of Polyethyleneterephthalate

> There are: I diagram, I graph, I table and 2 references, I of which is Scylet and 1 English.

ASSOCIATION:

Vsesoyuznyy nauchno-issledovatel skiy institut iskusstvennogo volokna

(All-Union Scientific Research Institute of Artificial Fiber)

SUBMITTED:

January 20, 1958

Card 2/2

POLYAKOV, Yu.I.; PETUKHOV, B.V.

Energy-impulse tensor in the S-matrix theory. Vest. Mosk. on. Ser. 3: Fiz., astron. 20 no.5:18-23 S-0 65.

(MIRA 18:11:

1. Nauchno-issledovatel'skiy institut yadernoy fiziki Moskovskogo universiteta. Submitted February 29, 1964.

PETUKHOV, B.V., POLYAKOV, Yu.I.; SHIROKOV, Yu.Y.

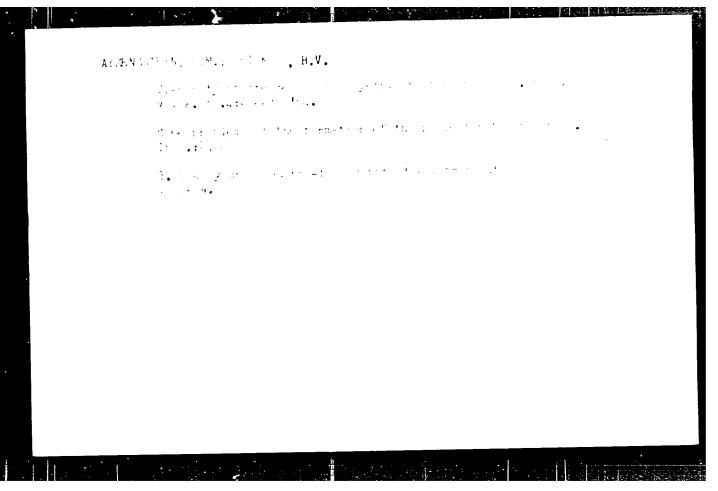
Relationship between form factors of the single-partition matrix element of the energy-impulse tensor and the charge and magnetic moment. Vest. Mosk. un. Ser. 3: Fiz., astron. 2: no.5:14-17 C-0 to6. (MJRA 18:11)

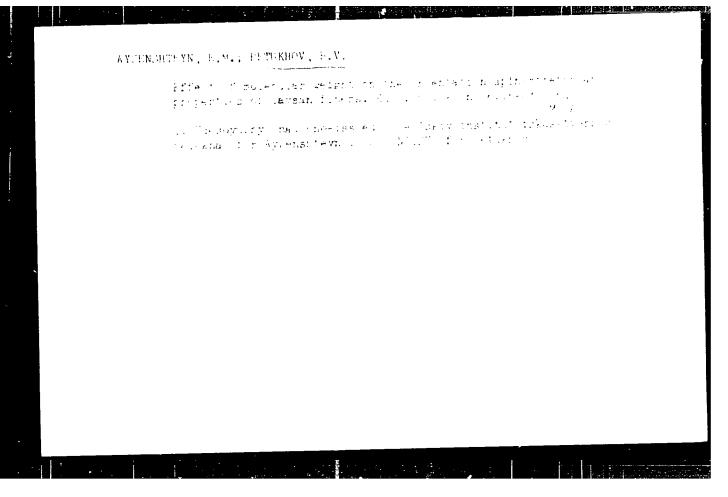
l. Nauchno-iasledovateliskiy institut yadernoy firiki Moskovskogo universiteta. Submitted February 20, 1964.

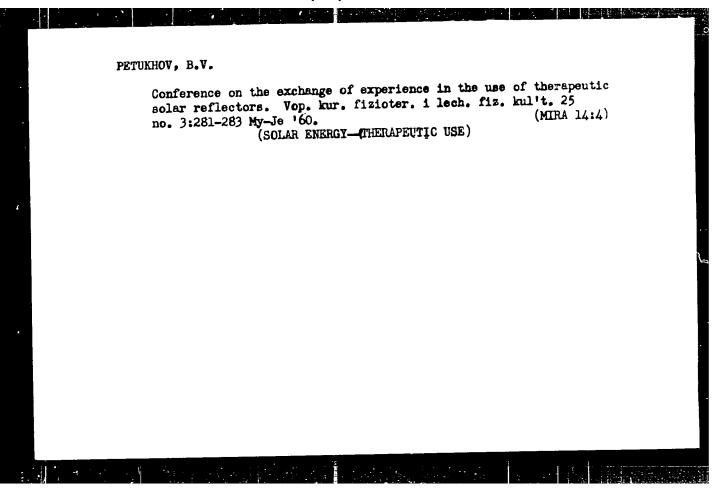
PETUKHOV, B.V.; KONDRASHOVA, S.M.

Properties of the copolymer of poly-fethylene terephthalate - ethylene adipinate) and of the fibers based on it. Khim. volok. no.1:55-60 '62.

1. Vsesoyuznyy nauchno-issledovatel'skiy institut steklyannogo volokna.







PETUKHOV, B.V.; KONDRASHOVA, S.M. Isomorphous substitution in polyethylene terephthalate. Vysokom. (MIRA 14:5)

soed. 3 no.5:657-661 My 161.

1. Vsesoyuznyy nauchno-issledovatel'skiy institut iskusstvennogo volokna.

(Terephthalic acid) (Adipic acid)

TERECHOVA, G.M.; PETUKHOV, B.V.

Blocking of the end groups of polyethylene terepethalate by o-phosphoric acid. Knim.volok. no.4:8-10 '60. (MIRA 13:10)

1. Vsesoyuznyy nauchno-issledovatel skiy institut iskusstvennogo volokna.

(Terephthalic acid) (Phosphoric acid)

PHASE I BOOK EXPLOITATION

SOV/5098

Petukhov, Boris Vladimirovich

Poliefirmoye volokno; terilen, lavsan (Polyester Fiber; Terylene, Lavsan [Dacron]) Moscow, Goskhimizdat, 1960. 85 p. 6,000 copies printed.

Ed.: S. I. Babushkina; Tech. Ed.: V. V. Kogan.

PURPOSE: This booklet is intended for personnel in the chemical and synthetic fiber industries. It may also be used by specialists in other industries that the cess or use synthetic fibers.

COVERAGE: The booklet deals with the theoretical and practical principles of the manufacture of polyester fibers from polyethylene terephthalate. It describes the properties of these fibers and their fields of application. No personalities are mentioned. There are 145 references: 19 Soviet, English, 13 German, 12 French, and 12 other.

Card-1/4

PETUKHOY, Boris Vladimirovich; BABUSHKINA, S.I., red.; KOGAN, V.V., tekhn.red.

[Polyester fiber (terylene, lavsen)]. Poliefirnoe volokno; terilen, lavsen. Moskva, Gos.nauchno-tekhn.izd-vo khim.lit-ry, 1960. 85 p. (MIRA 13:11)

(Rayon)

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2109, 2203 00

S/183/60/000/004/002/008 B004/B056

AUTHORS:

Terekhova, G. M., Petukhov, B. V.

TITLE:

Blocking of the End Groups of Polyethylene Terephthalate

by Means of o-Phosphoric Acid

PERIODICAL:

Khimicheskiye volokna, 1960, No. 4, pp. 8 - 10

TEXT: The Lavsan fiber (polyethylene terephthalate), obtained by the reaction of dimethyl terephthalate with ethylene glycol, takes on a yellow color at the high polycondensation temperature (275-280°C) owing to oxidation and thermal destruction of the end groups, predominantly the hydroxyl groups. The authors report on experiments to block these end groups by means of ortho-phosphoric acid. The polycondensation took place at 1-2 torr. The phosphoric acid was added as 15% solution in ethylene glycol at various times of the process. Fig. 1 shows that the high additions of phosphoric acid retard polycondensation. Morecver, the molecular weight of the end product is reduced, as can be seen from Fig. 2, in which the viscosity reduction under the effect of the concentration of phosphoric acid is illustrated. An addition of 0.01% of

Card 1/2