

21 (1)

AUTHORS:

Kogan, A. V., Petrov, I. V., Chudov,
L. A., Yampol'skiy, P. K.

SOV/89-7-4-6/88

TITLE:

The Tissue Dose of Neutrons

PERIODICAL:

Atomnaya energiya. 1959, Vol 7, Nr 4, pp 351-360 (RUSS)

ABSTRACT:

The present paper deals with the determination of the dosimetric properties of medium-energy neutrons, viz, for thermal neutrons and for neutrons with the energies of 100 ev; 1; 30; 240; 500 kev, and 1 Mev by using the results obtained by means of computers and those of experimental work performed by A. L. Kogan et al (Refs 6, 7). A broad beam of monoenergetic neutrons impinges perpendicularly upon the plane surface of a semi-infinite space, which is filled with a biological tissue. The neutrons impinging upon the tissue surface are partly reflected or scattered, or they are absorbed by the tissue, on which occasion they transfer their energy to the tissue. The main part of the neutrons is absorbed and is scattered within the first 10-15 cm of the tissue. A table shows the chemical composition of the tissue investigated by the authors. The following reactions of neutrons with energies of up to 1 Mev with the tissue elements are possible: (1) Elastic scattering

Card 1/3

The Tissue Dose of Neutrons

SOV/89-7-4-6/28

on the hydrogen nuclei. (2) Elastic scattering on heavy nuclei (carbon, nitrogen, oxygen). (3) Absorption on hydrogen nuclei with radiation of a γ -quantum having an energy of 2.19 Mev. (4) Absorption on nitrogen nuclei according to the reaction $N^{14}(n,p)C^{14}$ (the energy of the proton here amounts to 0.62 Mev). (5) Radiation capture on nitrogen according to the reaction $N^{14}(n,\gamma)N^{15}$, where, in the case of each capture, an energy of 0.9 Mev is radiated. In the first part of the present paper the energy is calculated which is left over by the neutrons in the tissue in the case of elastic scattering. For this purpose, Boltzmann's kinetic equation was solved by employing numerical methods by means of the electronic computer of the AS USSR. For the determination of the total neutron dose it is necessary, in addition, to take the neutron dose produced in the capture of neutrons into account. Computations are followed step by step. Two tables contain data concerning the flux of the thermal neutrons as well as the distribution of the absorbed energy and the energy albedo in the tissue. Neutrons with energies of 1 Mev and less are mainly scattered on hydrogen. The spatial energy distributions of the recoil

Card 2/3

The Tissue Dose of Neutrons

SOV/89-7-4-6/28

protons in 1 cm³ paraffin and in a tissue agree with respect to range units, and the absolute values are proportional to the density of hydrogen nuclei in these substances. In the next two parts the tissue dose due to the recoil protons of the reaction $\text{H}^{14}(n,p)$ and the dose due to absorption of γ -radiation are calculated. For the purpose of determining the biological dose the amount of the tissue dose must be multiplied by the coefficient of the relative biological efficiency (according to the nature of the radiation). According to the authors' opinion, 5 is the most suitable value to select for this coefficient. From the maximum values of the biological doses corresponding to the depth of the tissue, the relative values of the biological harmfulness per flux unit of neutrons of various energies were then calculated. There are 10 figures, 4 tables, and 20 references, 5 of which are Soviet.

SUBMITTED: April 2, 1959

Card 3/3

21(8)

AUTHORS:

Kogan, A. M., Petrov, G. G., Chudov, L. A., Yampol'skiy, P. A. SOV/89-7-4-17/28

TITLE:

The Reflection by Paraffin and Water of Neutrons With Different Energies

PERIODICAL:

Atomnaya energiya, 1959, Vol 7, Nr 4, pp 385-386 (USSR)

ABSTRACT:

In the course of the solution of the problem of the biological effect of neutrons it is of great importance to know such quantities as characterize the reflection of neutrons of different energies by a tissue. Besides, the dependence of the reflection coefficient on the geometrical conditions of the beam must be known. The authors therefore carried out measurements of the amount and the angular dependence of neutron reflection by a tissue-like substance within a wide energy interval. In these experiments the ratio between the flux of neutrons of all energies coming from the medium and the incident flux of the neutrons to be investigated was determined. It was thus necessary to find out what portion of the total number of incident neutrons is absorbed in the substance. The authors employed two methods for measuring reflection: The first method

Card 1/4

The Reflection by Paraffin and Water of Neutrons
With Different Energies

SOV, 89-7-4-17, 1

is used for neutron sources of small dimensions (nearly punctiform) and is based upon the following: In a large container filled with water, on the center of which the source was located, the radial distribution of the density of the absorption was measured by means of manganese foils. Integration of foil activity over the entire volume of the container then made it possible to determine the strength of the source in relative units, which are connected with the activity of the standard foil. By means of this method the reflection of neutrons of a polonium-beryllium source (mean energy 5 Mev) and of the photo-neutrons of a sodium-beryllium source (0.83 Mev), a sodium-deuterium source (0.22 Mev) and of an antimony-beryllium source (25 kev) on paraffin was measured. For measurements carried out on the reactor a second method was employed. For the relative determination of the incident flux a collimated neutron beam from the reflector of a nuclear reactor was introduced into a device, which, for the neutrons, plays the part of an absolutely black body. This device had the shape of a thin-walled tube ending in a hollow sphere which is surrounded by a thick layer of a weak aqueous solution of manganese chloride. The activity of the solutions was determined from the standard samples of

Card 2/4

The Reflection by Paraffin and Water of Neutrons
With Different Energies

SOV/89-7-4-17, 20

metallic manganese. The results of all measurements are given by the following tables:

Neutron energies	Paraffin reflection coefficient	Neutron energies	Reflection coefficient of water
5 Mev	0.06	2.7 kev	0.47
0.83 Mev	0.12	130 ev	0.56
0.22 Mev	0.19	5 ev	0.71
25 kev	0.38	thermal	0.58

The dependence of the reflection coefficient on the angle of incidence of the neutrons:

Neutron energies	Angle of incidence					
	0°	15°	30°	45°	60°	75°
5 Mev	0.06	0.110	0.21	0.32	0.50	0.74
0.22 Mev	0.19	-	-	0.44	0.61	-
5 ev	0.71	-	0.74	-	0.80	-
thermal	0.58	-	0.63	-	0.76	-

Card 3/4

The Reflection by Paraffin and Water of Neutrons
With Different Energies

SOV/89-7-1-17, 18

The dependence of the albedo on the angle of incidence θ may be described for all energies investigated by the relation

$$(1 - \alpha)_{\theta} = (1 - \alpha)_{\theta = 0} \cos \theta .$$

The authors thank undergraduate degree student of the Leningradskiy politekhnicheskii institut (Leningrad Polytechnic Institute) G. P. Gordeyev, who took active part in the measurement of the albedo of slow neutrons. There are 2 tables and 2 references.

SUBMITTED: April 2, 1959

Card 4/4

21(8)

AUTHORS:

Kogan, A. M., Petrov, G. G., Chudov, L. A., Yampol'skiy, F. A.

SOV/89-7-4-16, 25

TITLE:

Neutron Absorption Density Distribution in Paraffin

PERIODICAL:

Atomnaya energiya, 1959, Vol 7, Nr 4, pp 386-388 (USSR)

ABSTRACT:

A tissue dose due to neutrons is determined partly by the energy liberated within the tissue in neutron capture. According to the initial neutron energy, this part of the tissue dose will make a different contribution to the total dose. Thus, for neutrons with an initial energy of some kev, the tissue dose is determined practically entirely by the energy liberated in capture. For the neutrons with an initial energy of 1 Mev the essential part of the dose is determined by that energy which is scattered during the slowing-down process by the neutrons. In order to determine the capture component of the neutron dose, the spatial distribution of neutron absorption in paraffin (which simulates a biological tissue) was investigated. These measurements were carried out during the perpendicular incidence of a broad beam of neutrons upon a plane paraffin surface. The paraffin block had the shape of a rectangular parallelepiped of

Card 1/3

Neutron Absorption Density Distribution in Paraffin

SOV/89-7-4-18, 19

40.40.60 cm. The neutrons impinged upon the surface of 10.4 cm. Neutron density was measured by means of thin manganese foils. In these experiments the depth distribution of the absorption density of the incident neutrons with the following energies was measured: 1. The thermal neutrons were filtered through cadmium of 1 mm thickness out of a beam emerging from the channel of a nuclear reactor. 2. Neutrons with ~ 5 ev were filtered out of a beam of resonance neutrons at a nuclear reactor by means of a combination of a boron- and a cadmium filter. 3. Photon neutrons of an antimony-beryllium source with an energy of 25 kev. 4. Photon neutrons of a sodium-deuterium source with an energy of 220 kev. 5. Photon neutrons of a sodium-beryllium source with the energy of 0.87 Mev. 6. The neutrons of the reaction $H_1^2(d,n)He_2^3$ with the energy of 2.9 Mev. 7. The neutrons of a polonium-beryllium source with the mean energy of 5 Mev. The maximum statistical error in measuring the activity of the foils was $\sim 3\%$. The results of these measurements are shown by a diagram. The existence of a maximum, which shifts into the interior of the paraffin with increasing energy is characteristic of all curves.

Card 2/3

Neutron Absorption Density Distribution in Paraffin

SOV/69-7-4-18, '59

In the transition of thermal neutrons to thermal deuteron with an energy of several ev, the maximum shifts abruptly from 0.5 to 2.5 cm. This may be due to the fact that maximum absorption probably takes place in a depth of the order of one transport-length of the range of the incident neutron. Also the comparatively slow shifting of the maximum into the interior of the paraffin with an energy increase to 5 Mev may be explained by the weak dependence of the scattering cross section in this energy interval. The diagram mentioned indicates a tendency towards increasing on the part of the ratio between absorption in the maximum and absorption on the surface. The velocity of absorption density decrease decreased with an increase of the energy of the incident neutrons. There are 1 figure and 1 reference.

SUBMITTED: April 2, 1959

Card 3/3

PETROV, G.G., inzhener; YEGOROV, F.I., inzhener

Using cutters with screw thread cutting edges. Der.prom. b no. 5:28
My '55. (MIRA 8 10)

1. Shumerlinskiy mebel'nyy kombinat
(Woodworking machinery)

1 F T R O V, G G.

PETROV, G.G., NOVIKOV, A.G.: MARKOVICH, M.B., redaktor; MELENT'YEV, A.N.
tekhnicheskiiy redaktor.

[Construction and repair of bookkeeping (invoice) machines] Kon-
struktsiia i remont schetno-tekstovoi (fakturnoi) mashiny. 2e
perer. izd. Moskva, Gos. statisticheskoe izd-vo, 1954. 319 s.
(Bookkeeping machines) (MLRA 8:8)

EMINOV, Ye.A.; OSHER, R.N.; PATSUKOV, I.P.; CHEKAVTSEV, N.A.; MAZYRIN, I.V.;
FUKS, G.I.; VLADZIIHVSIIY, A.P.; PATSUKOV, I.P.; AVDEYEV, A.V.;
LOPOYAN, G.S.; PETROV, G.G.; KOZOREZOVA, A.A.; LISITSIIY, K.Z.;
YAKOBI, M.A.; BELYANCHIKOV, G.P.; IVANOV, V.S.; VORONOV, H.M.; RU-
MYANTSEV, V.A.; ZILLER, G.K.; BEREZINAYA, V.D.; LEVINA, Ye.S.,
vedushchiy red.; TROFIMOV, A.V., tekhn.red.

[Manual on the uses and consumption standards of lubricants] Spra-
vochnik po primeneniю i normam raskhoda smazochnykh materialov.
Moskva, Gos.nauchno-tekhn.izd-vo neft. i gorno-toplivnoi lit-ry.
1960. 703 p. (MIRA 13:4)
(Lubrication and lubricants)

S/056/00/01/108/048/100
B006/BC000

AUTHORS: I. I. Gansel, V. I. Kargin, and A. I. [redacted]

TITLE: Observations of the Positronium Reaction in Aqueous Solutions

PERIODICAL: Zhurnal eksperimental'noy i teoreticheskoy fiziki, 1976, Vol. 61, No. 1, pp. 117-117b

TEXT: The present "Letter to the Editor" brings a contribution to the problem of the positronium annihilation in aqueous solutions and the influence of different additions on these. The purpose of the tests whose results are compiled in a table was to prove that the different additions act mainly kinetically on the positronium annihilation in aqueous solutions and also to show a comparison of these effects with the oxidation-reduction characteristics and magnetic characteristics of different ions. The authors investigated the rate of γ -annihilation of positrons formed in Na⁺ solution in the presence of different ions. The table shows the results of the γ -annihilation rate compared with the rate of annihilation.

Card 1/4

Observation of the reaction between
Aqueous Sulfuric Acid

S/386/22/11-101
HCO₃/BO₃

influence of different all... mainly different...
 en... of positive... A general...
 of the C_{17} counting rate is found if stronger oxidizers are used...
 strong deviations can be found... The deviations may frequently be
 raised through a $S \rightarrow S$ transition at unpaired electrons...
 netic ions, but there is a specific connection between the...
 properties of the ions and the quantity C_{17} . A strong...
 C_{17} counting rate was found also by other authors, if NO_3^- ions were added
 and also that MnO_4^- ions acted stronger yet. The following data charac-
 terize the concentration dependence of C_{17} for MnO_4^- additions and com-
 pared to neutral sulfates.

Observation of the Positronium Reaction in Aqueous Solutions

S/056/60/035/113/0001
B006/B077

Concentration MnO_4^- in mole/l	saturated solution	0.1	0.01	0.001	[factor]
$\tau_{3\gamma}$ min ⁻¹	3.6±0.42	5.08±0.45	5.08±0.12	5.52±0.47	1.01±0.01

The authors thank Academician A. N. Frumkin for discussions of the results obtained. There are 1 table and 4 non-Soviet references.

ASSOCIATION: Fizicheskiy institut im. P. N. Lebedeva Akademii nauk SSSR (Physics Institute imeni P. N. Lebedev of the Academy of Sciences USSR). Institut khimicheskoy fiziki Akademii nauk SSSR (Institute of Chemical Physics of the Academy of Sciences USSR)

SUBMITTED: August 2, 1960

S/056/00/032/00/00/000
 3006/3077

Вещество 1	Концентрация, моль/л 2	Стандартный окислительно-восстановительный потенциал для указанной в скобках пары окислитель-восстановитель 3	Число перенесенных электронов 4	Разница в C_{27} (мин 5) по отношению к таблице 5
KOH	1	+2,92 (K ⁺ K)		-0,02 ± 0,31
BaCl ₂	2	+2,92 (Ba ²⁺ Ba)		-0,55 ± 0,39
NaCl	2	+2,71 (Na ⁺ Na)		+0,07 ± 0,25
MnCl ₂	2	+1,10 (Mn ²⁺ Mn)	5	-0,57 ± 0,26
ZnCl ₂	2	+0,76 (Zn ²⁺ Zn)	4	+0,24 ± 0,34
FeCl ₂	0,1	+0,44 (Fe ³⁺ Fe)	4	-0,90 ± 0,27
CrCl ₃	2	+0,41 (Cr ³⁺ Cr ²⁺)	3	-1,70 ± 0,28
TiNO ₂	6 насыщение	+0,34 (Ti ³⁺ Ti)		-1,24 ± 0,29
CoCl ₂	2	+0,27 (Co ³⁺ Co)	3	-1,17 ± 0,40
NiSO ₄	2	+0,23 (Ni ³⁺ Ni)	2	-1,93 ± 0,36
CuCl ₂	2	+0,34 (Cu ³⁺ Cu)	1	-1,85 ± 0,31
FeCl ₃	2	+0,77 (Fe ³⁺ Fe ²⁺)	5	-2,62 ± 0,33
FeCl ₂	0,1	+0,77 (Fe ³⁺ Fe ²⁺)	5	-1,41 ± 0,28
KMnO ₄	6 насыщение	+1,63 (MnO ₄ ⁻ → 3e MnO ₂)		-2,44 ± 0,42
H ₂ O ₂	30 вес % 7	-1,78 (H ₂ O ₂ + 2e H ₂ O)		-1,55 ± 0,28

Table

Card 4/4

Legend to the Table:
 1) Substance; 2) Concentration in mole/l; 3) Standard redox potential for the oxidizer-reducer pairs given; 4) Number of unpaired electrons; 5) Difference of C_{27} as compared to water; 6) Saturation; 7) % by weight.

GOL'DANSKIY, V.I.; KARPUKHIN, O.A.; PETROV, G.G.

Observing the reactions of positronium in water solutions. Zhur.
eksp.i teor.fiz. 39 no.5:1477-1478 N '60. UMIRA 14:4

1. Fizicheskiy institut imeni P.N.Lebedeva AN SSSR i Institut
khimicheskoy fiziki AN SSSR.
(Positronium)

PETROV, G.I.

Sowing winter barley in packed soil. Zemledelie 4 no.7:63-66 J1 '56.
(Budennovsk District--Barley) (MLRA 9:9)

CATEGORY : Cultivation of plants. General directions. M
 DATE : 1965
 TITLE :
 SUBJECT :
 SUMMARY :
 The text describes agricultural practices, mentioning a layer of soil and the use of a plow. It discusses the relationship between the first and second crops, specifically mentioning the effect on the second crop compared to the first. The text is written in a technical or scientific style, likely from a manual or report.

PETROV, G.I.,_ kand.sel'skokhozyaystvennykh nauk

For increased production of winter grain. Zemedelie 24 no.6:
70-75 Je '62. (MIRA 15:1)

1. Stavropol'skaya vostochnaya sel'skokhozyaystvennaya opytnaya
stantsiya.

(Grain)

K. T. VOY, S.I.; PETROV, G.I.; TIKHONOVA, G.P., red.; ZHUKOVA,
Ye.G., text. red.

[Agricultural collective and state farm administrations
Izvodstvennye kollektivno-sovkhosnye upravleniia. Leningrad,
Izd-vo Leningr. univ., 1963. 43 p. (MIRA 16:10,
(Agricultural administration)

PETROV, G.I., kand. sel'skokhoz. nauk

Sowing winter barley on stubble in Stavropol Territory.
Zemledelie 25 no.6:37-45 Je '63. (MIRA 16:7)

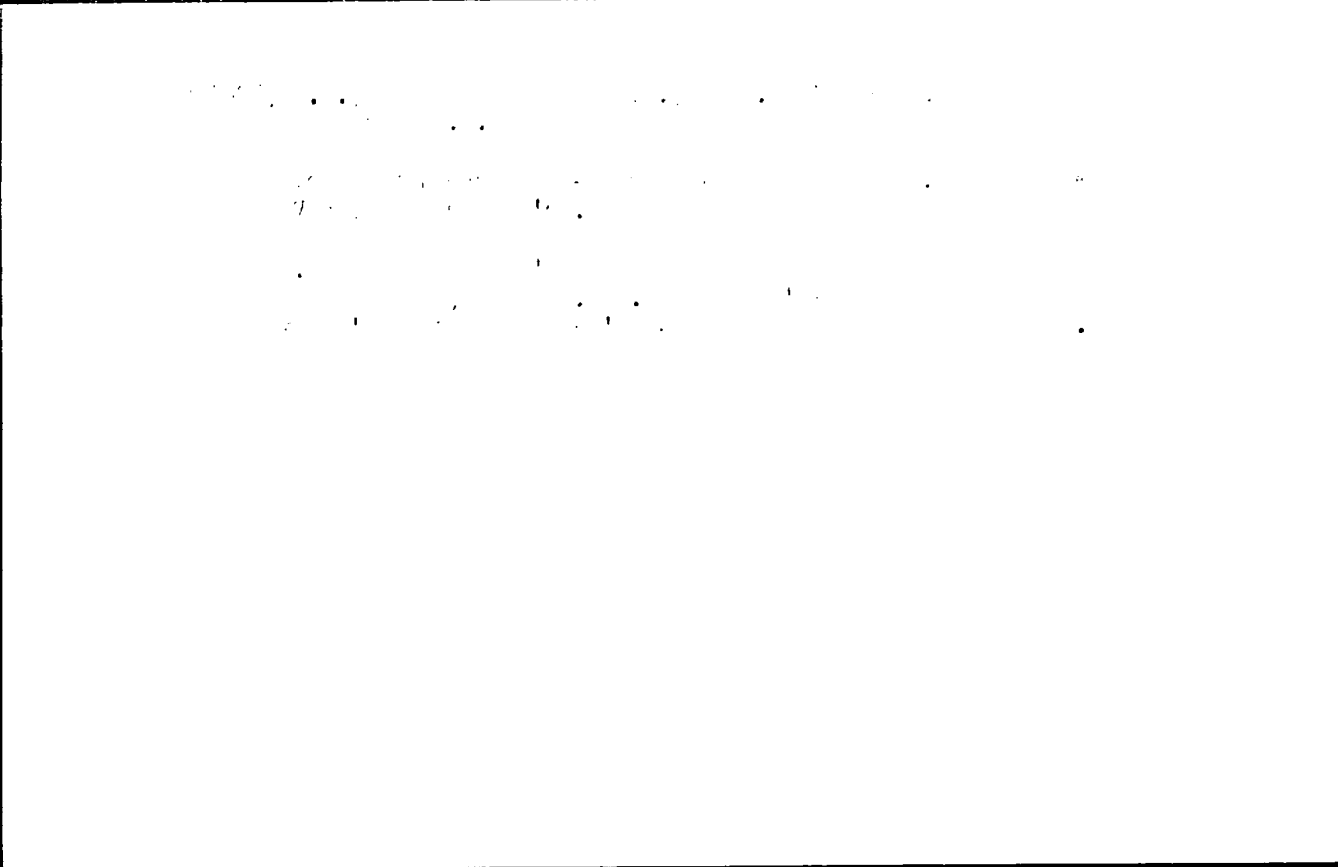
1. Stavropol'skaya vostochnaya sel'skokhozaostvennaya opytnaya
stantsiya.

(Stavropol Territory—Barley)

LEVIN, B.I.; ROZENBERG, V.M.; YAKOVLEV, P.A.; KORF, Z.G.; KULYGIN, B.A.;
PETROV, G.I.

Unification of structures of sea and river mooring installations. Transp. stroi. 15 no.9:39-42 S '65. (MIRA 18:11)

1. Gosudarstvennyy proizvodstvennyy komitet po transportnomu stroitel'stvu SSSR (for Levin). 2. Gosudarstvennyy institut proyektirovaniya i izyskaniya na rechnom transporte (for Yakovlev, Korf). 3. Gosudarstvennyy proyektno-konstruktorskiy i nauchno-issledovatel'skiy institut morskogo transporta (for Kulygin, Petrov).



PETROV, G.I.

Brigade has mastered the technology of constructing bored piles.
Transp. stroi. 15 no.6:31-32 Ja '86. CIA 111.

"APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2

APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2"

PETROV, G.I. (Moskva, Zh-68, Novo-Ostapovskaya ul., no. 20).

Influencing metabolism as a factor in the increase of the activity of the organism in antineoplastic therapy; two cases of cancer treatment with large doses of auranin. Vop. onk. 9 no.10:88-90, 1968.

1. Iz gigiyenicheskogo otdela (zav. - deystvitel'nyy chlen AMN SSSR prof. L.K.Khotsyanov) Instituta gigiyeny imda i profesornal'nykh zabolevaniy AMN SSSR (direktor - deystvitel'nyy chlen AMN SSSR prof. A.A.Letavet).

L 10717 65 ECT(a)/EWP(b) LTR(c) ID

ACCESSION NR: AP4046410

S/0186/64/000/009/0074/0076

AUTHOR: Petrov, G. I., Andreyev, V. M., Andreyeva, L. I.

TITLE: Effect of the physical properties of germanium dioxide on its reduction B

SOURCE: Tsvetnyye metally*, no. 9, 1964, 74-76 21 27

TOPIC TAGS: germanium dioxide, germanium dioxide physical property, germanium dioxide reduction, germanium tetrachloride hydrolysis, calcination

ABSTRACT: The paper considers some of the physical properties of GeO_2 prepared by hydrolysis of germanium tetrachloride in detonized water, and their effect on the reduction rate with hydrogen. The physical structure of the dioxide was found to be affected by the method of hydrolysis. Simultaneous loading of the tetrachloride and water results in a fine structure with a highly developed surface, while continuous loading of both leads to coarse, dense dioxide grains. The reduction rate was determined from the pressure drop in the system due to freezing out of water vapor produced by the chemical reaction. The reduction rate was found to increase sharply with decreasing specific gravity of the sample. After filtration under similar conditions, the light-weight germanium dioxide contained 25-30%

cards 1/2

L 10717-65

ACCESSION NR: AP4045410

moisture, while the "heavy" dioxide contained only 6-10%. This also affects the reduction. The usual calcination of germanium dioxide in air may also change its physical properties. Thus, an increase in the calcination temperature leads to an increase in hygroscopicity up to 400-500C, the quantity of hygroscopic moisture removed from light-weight GeO_2 being 3.6 times as high as from "heavy" germanium dioxide. The amount of water of crystallization removed is exactly the same for both light and heavy germanium dioxide. At higher temperatures, the hygroscopicity decreases, probably due to decreased porosity. Many publications (L. A. Sokolov, T. L. Joseph and others) have noted the relationship between the reduction rate of oxides and their porosity, meaning the porosity after preliminary calcination. The article concludes that the decrease in rate of reduction of GeO_2 after calcination at high temperatures is caused not only by the decrease in porosity, but also by the formation of a new β - GeO_2 modification which is reduced with difficulty. In tests at high temperatures, the partially reduced germanium powder always contains β - GeO_2 . Orig. art. has: 5 figures.

ASSOCIATION: None

SUBMITTED: 00

ENCL: 00

SUB CODE: MM

NO REF SOV: 002

OTHER: 002

Card 2/2

PETROV, G. I.

"On the Diffusion of waves in a Viscous Fluid and the Origin of Turbulence,"
Moscow, 1938

PETROV, G. I.

"Application of Galerkin's Method to the Problem of the Stability of Current
in Viscous Fluid," *Irik. mat. i mekh.*, novaya seriya, 4, No.3, 1940

AUTHOR: Petrov, G.I. Moscow.

11-21-1-1/1

TITLE: The Estimation of the Exactness of an Approximate Calculation of the Eigenvalue According to the Galerkin's Method (Otsenka tochnosti priblizhennogo vychisleniya sobstvennogo znacheniya metodom Galerkina)

PERIODICAL: Prikladnaya Matematika i Mekhanika, 1977, Vol. 31, No. 1
 PP 141-145

ABSTRACT: Given the linear functional equation

$$(1) \quad L(\lambda, U) = 1(U) - l_\lambda(\lambda, U) = 0$$

in which $1(U)$ is a linear operator with the derivatives of higher order and $l_\lambda(\lambda, U)$ is an operator the coefficients of which depend on λ . The author seeks values λ_k such that the functions $U_k(\lambda_k, x)$ satisfying the equation (1) on the interval (a, b) and the corresponding boundary conditions, are not vanishing everywhere on (a, b) . In an earlier paper [Ref. 1] the author has shown that if the eigenfunctions are represented in the form

$$U_k = \sum_{i=1}^n a_i^{(k)} \psi_i$$

Card 1/2

The Estimation of the Exactness of an Approximate Calculation of the Eigenvalue According to the Galerkin's Method 40-11-1-10

where ψ_1 is a complete system of functions satisfying the boundary conditions of the given problem, and if the $a_1^{(n)}$ are determined from a certain linear homogeneous system of equations, then the $u_1^{(n)}$ and the corresponding $\lambda_1^{(n)}$ approximate the exact eigenfunctions and eigenvalues:

$$u_1^{(n)} \rightarrow u_1, \quad \lambda_1^{(n)} \rightarrow \lambda_1 \quad \text{as } n \rightarrow \infty$$

By a decomposition with respect to the elements of the first row of the determinant of the mentioned linear system of equations the author obtains the difference between the exact and the approximate solutions: $(\lambda_1 - \lambda_1^{(n)})$. After numerous transformations then an evidently very rough estimation of this difference is obtained. There are 5 references, 2 of which are Soviet, and 3 Hungarian.

SUBMITTED: July 20, 1956
AVAILABLE: Library of Congress

- 1. Analytic functions
- 2. Transformations
- 3. Topology

ACCESSION NR: AP4041396

S/0020/64/156/006/1316/1319

AUTHOR: Anfimov, N. A. Petrov, G. I.

TITLE: Diffusion separation of a gas mixture in the presence of dissociation

SOURCE: AN SSSR. Doklady*, v. 156, no. 6, 1964, 1316-1319

TOPIC TAGS: diffusion gas separation, gas dissociation, gas boundary layer, diffusion coefficient, gas temperature gradient, hydromechanics

ABSTRACT: The gas composition in the mixture of dissociating gases differs in the boundary layer from that in the outer flux, if there is a temperature gradient at the surface. The separation is caused by differences in the diffusion coefficients of different components. This phenomenon was discussed in an earlier paper (Izv. AN SSSR, Mekh i mashinostz. #5, 117 (1963)). The present work deals with the effect of various factors, such as the degree of dissociation of the gas in the outer flux

$$\alpha = \left(\frac{C_A}{C_A + C_{A2}} \right)$$

Card 1/2

ACCESSION NR: AP4041396

concentration of the other (inert) gas, and the ratio of diffusion coefficients of atoms and molecules of the dissociating gas. The assumptions are made in computations, that the rate of the chemical reaction $A_2 \rightleftharpoons 2A$ is zero in the boundary layer, and is infinitely high at the body surface, and that thermal diffusion inside the boundary layer is absent. The following cases are considered: O-O₂-N₂; O-O₂-He; O-O₂-Kr; H-H₂-He; H-H₂-N₂; J-J₂-Kr. Orig. art. has: 2 figures and 5 equations.

ASSOCIATION: None

SUBMITTED: 15Jan64

DATE ACQ: 00

ENCL: 00

SUB CODE: ME

NO REF SOV: 002

OTHER: 000

Card 2/2

PHASE I BOOK EXPLOITATION SOV/6201

Vsesoyuznyy s"yezd po teoreticheskoy i prikladnoy mekhanike. 1st, Moscow, 1960.

Trudy Vsesoyuznogo s"yezda po teoreticheskoy i prikladnoy mekhanike, 27 yanvarya -- 3 fevralya 1960 g. Obzornyye doklady (Transactions of the All-Union Congress on Theoretical and Applied Mechanics, 27 January to 3 February 1960. Summary Reports). Moscow, Izd-vo AN SSSR, 1962. 467 p. 3000 copies printed.

Sponsoring Agency: Akademiya nauk SSSR. Natsional'nyy komitet SSSR po teoreticheskoy i prikladnoy mekhanike.

Editorial Board: L. I. Sedov, Chairman, V. V. Sokolovskiy, Deputy Chairman; G. S. Shapiro, Scientific Secretary, G. Yu. Dzhanelidze, S. V. Kalinin, L. G. Loytsyanskoy, A. I. Lur'ye, G. K. Mikhaylov, G. I. Petrov, and V. V. Rumyantsev, Resp. Ed. L. I. Sedov, Ed. of Publishing House: A. G. Chakhirev, Tech. Ed. R. A. Zamarayeva.

Card 1/6

Transactions of the All-Union Congress (Cont.)

SOV/6201

(25)

PURPOSE. This book is intended for scientific and engineering personnel who are interested in recent work in theoretical and applied mechanics.

COVERAGE: The articles included in these transactions are arranged by general subject matter under the following heads: general and applied mechanics (5 papers), fluid mechanics (10 papers), and the mechanics of rigid bodies (8 papers). Besides the organizational personnel of the congress, no personalities are mentioned. Six of the papers in the present collection have no references, the remaining 17 contain approximately 1400 references in Russian, Ukrainian, English, German, Czechoslovak, Rumanian, French, Italian, and Dutch.

TABLE OF CONTENTS:

SECTION I. GENERAL AND APPLIED MECHANICS

• Artobolevskiy, I. I. Basic Problems of Modern Machine Dynamics	5
• Bogolyubov, N. N., and Yu. A. Mitropol'skiy. Analytic Methods of the Theory of Nonlinear Oscillations	25

Card 2/6

Transactions of the All-Union Congress (Cont.)

SOV/6201

5

Golitsyn, G. S., A. G. Kulikovskiy, and K. P. Stanyukovich.
Magnetohydrodynamics

84

Gurevich, M. I. Theory of an Ideal-Fluid Jet

114

Ivanilov, Yu. P., N. N. Moiseyev, and A. M. Ter-Krikorov.
Asymptotic Methods for Problems of Motion of a Fluid With
Free Boundaries

135

Loytsyansky, L. G. Semiempirical Theories of the Interaction
of the Processes of Molecular and Molar Exchange in the
Turbulent Motion of a Fluid

145

Petrov, G. I. Boundary Layer and Heat Exchange at High Speeds

167

Sedov, L. I. On the Theory of Constructing Mechanical Models of
Continuous Media

176

Card 4/6

PETROV, G. I., BONDAREV, E. N. (Moscow)

"Experimental Results Concerning the Interaction of a Shock Wave with
Turbulent Boundary Layers."

report presented at the First All-Union Symposium on *High-Speed Flow and Applied
Mechanics*, Moscow, 17 Jun - 2 Feb 1968.

SEDOV, L.I., otv. red.; SOKOLOVSKIY, V.V., red.; DZHANELIDZE, G.Yu., red.; KALININ, S.V., red.; LUYTSYANSKIY, L.G., red.; LUR'YE, A.I., red.; MIKHAYLOV, V.V., red.; PETROV, G.I., red.; RUMYANTSEV, V.V., red.; SHAPIRO, G.S., red.; CHAKHIL'EV, A.G., red. izd-va; ZAPARAYEVA, B.A., tekhn. red.

[Proceedings of the All-Union Congress on theoretical and Applied Mechanics, January 27- February 3, 1960] Trudy Vsesoyuznogo s"ezda po teoreticheskoi i prikladnoi mekhanike. 1st, Moscow, 1960; obzornye doklady. Moskva, Izd-vo Akad. nauk SSSR, 1962. 467 p. (MIRA 15:0)

1. Vsesoyuznyy s"ezd po teoreticheskoy i prikladnoy mekhanike. 1st, Moscow 1960.

(Mechanics- Congresses)

PETROV, G.I.; ANDREYEV, V.M.; ANDREYEVA, L.I.

Effect of the physical properties of germanium dioxide on its
reduction. TSvet. met. 37 no.9:74-76 S '64. (MIRA 18:7)

"APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2

APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2"

PETROV, G.I.

Building bridge supports on bored pilings. Gen., fund. 1
mekh. grup. 5 no. 4:10-13 '53. MIRA 12:11

LUKOV, B.N., prof. (Kuybyshev); PETROV, V.I., dotsent (Moskva);
 PAVLENKO, T.M., aspirant (Moskva); YERMOLAYEV, V.G., prof.
 (Leningrad); ADG, A.D., prof.; VOYSI, M.S., prof.;
 YERMOLAYEV, V.G., prof. (Leningrad); KUPRIYANOVA, N.A. (Kazan');
 PETROV, G.I. (Moskva); DOLGOPOLOVA, A.V. (Moskva); SAYLARCIV, P.P.,
 prof.; BYKHOVSKIY, Z.Ye., prof.; MIN'KOVSKIY, prof. (Chelyabinsk);
 KHREL'CHONOK, I.P. (Irkutsk); TEMKIN, Ya.S., prof. (Moskva);
 MIN'KOVSKIY, A.Kh., prof. (Chelyabinsk); MIL'SHTEYN, T.N., doktor
 med.nauk (Leningrad); TRUTNEV, V.K., zasluzhennyy deyatel' nauki,
 prof. (Stavropol'); TSYRESHKIN, E.D., kand.med.nauk (Moskva); SOBOL', I.M.,
 prof. (Stavropol'); TURIK, G.M. (Moskva); FRENKEL', M.M. (Moskva);
 MAZO, I.L.; POKRYVALOVA, K.P.; PROSKURYAKOV, S.A., prof.;
 ATKARSKAYA, A.A., prof.; GCL'DFARB, I.V., prof. (Izhevsk);
 PORUBINOVSKAYA, N.M. (Moskva); RUTNEV, G.P., prof.; VOLLFSON, I.Z.,
 prof. (Stalingrad); DOROSHENKO, I.T., prof. (Kalinin);
 ROZENFEL'D, M.O., prof. (Leningrad); SHUL'GA, A.G., prof. (Orenburg);
 MIKHLIN, Ye.G., prof.; TRET'YAKOVA, Z.V. (Moskva); KANUYLOV, Ye.N.,
 prof. (Moskva); DOROSHENKO, I.T., prof. (Kalinin); YERMOLAYEVA, V.G.,
 prof.

Speeches in the discussion. Trudy gos. nauch.-is.l. inst. ukha,
 gorla i nosa no.11:79-87,129-146,179-186,233-248,311-333 '59.
 (MIRA 15:6)

1. Chlen-korrespondent AMN SSSR (for Ado). 2. Direktor Moskov-
 skogo gosudarstvennogo instituta ukha, gorla i nosa (for Trutnev).
 (OTORHINOLARYNGOLOGY—CONGRESSES)

PETROV, G.I. (Novosibirsk)

Apparatus for automatic testing of central heating equipment.
Vod.i san.tekh. no.5:36-37 My '62. (12A 1.)
(Radiators--Testing)

PETROV, G.I., inzh.

Jet pump for conveying cement. Transp. stroi. 13 no.5:70
My '63. (MIRA 14:1)

(Pumping machinery
(Cement—Transportation)

PETROV, G.I., inz .

Switchless active ... (MIRA 1977)

ET 11, 1.1, inch.

Using the SM-1 pistols for installing sanitary engineering equipment.
Mont. 1 spec. r.b. v. stroi. 24 no. 1:26-27 Ja '61. (MI 1:17)
(Building--Tools and implements)

PETROV, G.I.; KUTENKOV, M.V.; TENENBAUM, I.M.; YEVSEYEVA, L.S.;
KONSTANTINOV, M.M., nauchnyy red. [deceased]; SHASHKIN, V.L.,
nauchnyy red.; SURAZHSKIY, D.Ya., nauchnyy red.; ZAVODCHIKOVA,
A.I., red.; MAZEL', Ye.I., tekhn.red.

[Methods of geological and geophysical exploration and control in
uranium mines] Metody geologo-geofizicheskogo obaluzhivania
uranovykh rudnikov. Moskva, Izd-vo Gos.kom-ta Soveta Ministrov
SSSR po ispol'zovaniu atomnoi energii, 1960. 217 p.

(MIRA 13:10)

(Mining geology)

(Uranium ores)

PETROV, G. I., inzh.

All-purpose compressionless sprayer. Transp. strof. 9 13:55
D '59. (MIRA 13:5)
(Plastering--Equipment and supplies)

1. BEYS, A. A.; PETROV, G. I.
2. USSR (67)
4. Zoology and Geography
7. Theoretical Principles of the Science of the Deposit. By I. I. Tolstoy. (Hirovskiy, Vladimir State Technical Press, 1967). Reviewed by A. A. Beys and G. I. Petrov. Sov. Fauna, No. 6, 1967.

9. [REDACTED] Report U-3031, 14 Jan. 1955. Volume 1161.

PETROV, G.I., inzh.

Work of mixed brigades. Transp.stroi. 9 no.5:13-14
My '59. (MIRA 12:12)
(Krasnoyarsk Territory--Electric railroads)
(Electric lines--Poles)

PETROV, G.I., inzh.

Switch for mortar pumps. Transp.stroi. 9 no.10:59 0 '59.

(MIRA 13:7)

(Mortar--Transportation)

PETROV, G.K.

Automatic water depth indicator service (radio gauge). Rech.
transp. 18 no.5:49-50 My '59. (AIRn 12:?)
(Hydrography--Equipment and supplies)
(Gauges)

1955, G. I.

USSR/Petroleum Industry
Acetylene

May 48

"Study of an Electropolymer and an Electro-
polymer Gas," G. L. Petrov, Cand Tech Sci,
Leningrad Polytech Inst, 4 pp

"Avtogen Delo" No 5 - p. 9-12

Methods to produce acetylene containing gas from
petroleum derivatives, studies of operation of
Electropolymer Works imeni Mart, and studies
conducted on polymer gas.

2/4096

PETROV, G. L., Doc Tech Sci -- (diss) "Chemical non-uniformity in welded assemblies." Leningrad, 1960. 26 pp; (Ministry of Higher and Secondary Specialist Education M.E.P., Leningrad Polytechnic Institute M. I. Kalinin); 150 copies; price not given; list of author's works on pp 25-26 (12 entries); (Kb, 17-60, 150)

USSR/Metals - Flame Cutting

Jun 50

"Deformation of Plates in Oxyacetylene Cutting,"
G. L. Petrov, Cand Tech Sci, Leningrad Polytech
Inst imeni M. I. Kalinin, 6 pp

"Avtogen Delo" No 6

Describes experiments for studying deformations in process of oxygen cutting, and develops graphoanalytic method for determining such deformations. Suggests some measures for preventing deformations, such as electromagnetic tables for fixing plate position, and formers with reverse bend for compensating deformation.

161T95

ACCESSION NR: AT4038448

S/2563/63/000/229/0065/0072

AUTHOR: Petrov, G. L.; Shchipkov, M. D.

TITLE: Sources of gases in titanium alloy welds

SOURCE: Leningrad. Politekhnicheskii institut. Trudy*, no. 229, 1963. Svarochnoye proizvodstvo (Welding production), 65-72

TOPIC TAGS: titanium alloy, titanium alloy weld, alloy weld, TIG weld, MIG weld, submerged arc weld, AN TZ flux, weld gas content, gas source, weld oxygen content, weld hydrogen content, weld nitrogen content, gas content

ABSTRACT: In the TIG, MIG, and submerged arc welding of titanium alloys, gases may come into the weld metal from the base metal, the electrode or filler wire, shielding gases, or from the flux. The nitrogen content in the weld metal usually does not exceed 0.04—0.05%, depending on the nitrogen content in the electrode, filler wire, or base metal. The main source of hydrogen and oxygen in shielding gases is water. At hydrogen contents in the base metal up to 0.001%, the use of commercial-grade argon (dewpoint, -40C) may increase the hydrogen content in the weld metal to 0.002—0.003%; high-purity argon with a

Card 1/3

ACCESSION NR: AT4038448

dew point of -70C causes little or no increase in hydrogen content. The hydrogen and oxygen contents of weld metals deposited in different shielding media with an electrode wire containing 0.001—0.004% hydrogen and 0.14% oxygen are shown in Table 1 of the Enclosure. The AN-T2 flux requires degassing prior to application. Orig. art. has: 4 figures and 4 tables.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 12Jun64

ENCL: 01

SUB CODE: NM

NO REF SOV: 008

OTHER: 002

ATD PRESS: 3041

Card 2/3

ACCESSION NR: AT4038448

ENCLOSURE: 01

Table. 1. Hydrogen and oxygen contents of weld metals

Shielding medium	Oxygen %	Hydrogen %	Electrode wire
High-purity argon	0.15	0.0032	
80% helium 20% argon	0.14	0.0021	with 0.004% hydrogen
AN-TZ flux	0.44	0.0010	
AN-TZ flux with expelled air	0.20	0.00070	with 0.001% hydrogen

Card 3/3

PETROV, G.L.; MILLION, A.

Contributions to the study of hydrogen diffusion influence
on fissure formation in welded joints. *Stal i sero metalurgie*
9 no.2:253-274. '64.

PETROV, G. L.

USSR/ Engineering - Welding

Card 1/1 Pub. 128 - 23/34

Authors : Petrov, G. L., and Kyrchenov, V. V.

Title : Investigating the welding of the turbine-rotor type air blower

Periodical : Vest. mesh. 12, 73-76, Dec 1954

Abstract : The condition of weld seams and welded components of the turbine-rotor type air blower was investigated by the I. I. Balzunov Central Scientific Research Institute for Boilers and Turbines. Technical data specifying the types of steel, temperatures and welding procedures employed during the above mentioned experiments are presented. Drawing; tables; illustrations; graphs.

Institution :

Submitted :

PETROV, G. L.

USSR/Engineering - Welding

Card : 1/1

Authors : Kondrat'ev, V. M., Engineer; Petrov, G. L., Cand. Tech. Sc., Docent

Title : Causes of flaws in welded seams of small-diameter pipes

Periodical : Vest. Mash., 34, Ed. 6, 78 - 83, June 1954

Abstract : The development of flaws in high-pressure water heaters was traced to defective welding. A description is given of experiments conducted in the gas-welding of pipes of the dimensions 25 x 3 and 38 x 4.5 mm. An analysis is made of the results of such experiments to determine the nature and origin of welding defects and ways are indicated for avoiding them. Illustrations; drawings; graph; tables.

Institution : ...

Submitted : ...

Evaluation: B-83422

PETROV, G. L., dotsent; KYRCHENOV, V. V., inzhener

Electrodes for welding austenitic steel intended for protracted
workings at high temperature. Svar.proizv. no.8:9-13 Ag'55.
(Steel--Welding) (Electrodes) (MLRA 8:11)

PETROV, G. L.

USSR/ Engineering - Oxygen cutting

Card 1/1 Pub. 11 - 7/E

Authors : Petrov, G. L.

Title : Concerning the nature of chemical heterogeneity of metal in the vicinity of the cut, during an oxygen cutting

Periodical : Avtom. svar. 8/1, 60-74, Jan-Feb 1955

Abstract : The effect of oxygen cutting of steel and metal on their chemical heterogeneity and affinity in the vicinity of the cut, was analyzed on the basis of experimental materials and calculus. Technical data are given on carburization and decarburization processes, diffusion coefficients, temperature coefficients, rate of cutting and the concentration of carbon in metals. Fourteen references: 12 USSR and 2 USA (1929-1954). Tables; graphs; drawing.

Institution : Leningrad M. I. Kalinin Polytechnical Institute

Submitted : July 25. 1954

PETROV G L
USSR/Engineering - Metallography

FD-3026

Card 1/1 Pub. 41 - 10/15

Author : Petrov, G. L., Leningrad

Title : On the macro-heterogeneity of the chemical composition of the metal in weld seams.

Periodical : Izv. AN SSSR, Otd. Tekh. Nauk 9, 137-154, Sep 58

Abstract : Studies the macro-heterogeneity of the chemical composition of the metal in weld seams resulting from the very welding process itself, i.e., fusion of the base and weld metals and subsequent crystallization, variation of base and weld metal content in the seam, possibility of altering composition of the non-fused metal by thermal action during welding, etc. Presents thorough analysis of tests conducted to determine the effect of welding process on the macro-heterogeneity of the chemical composition of the weld seam. Microphotographs, tables, formulae, diagrams. Seven references, all USSR.

Institution:

Submitted : May 12, 1958

RUSSO, Vladimir Leonidovich; PETROV, O.L., otvetstvennyy redaktor; OSVENSKAYA, A.A., redaktor; FRUMKIN, P.S., tekhnicheskiy redaktor

[The welding of aluminum and its alloys] Svarka aluminia i ego splavov. Leningrad, Gos. soizusnoe izd-vo sudostroit. promyshl., 1956. 136 p. (MLBA 9:9)
(Aluminum--Welding)

PETROV, G.L.

Diffusion of elements during cutting and welding and causes for
the heterogenous chemical composition of weld macrostructures.
Avtom. svar. 9 no.6:77-82 N-D '56. (MLRA 10:3)

1. Leningradskiy politekhnicheskii institut im. M.I. Kalinina.
(Welding) (Diffusion)

1958-1964

Translation from: *Referativnyi Zhurnal Metallovedeniya* (USSR)

AUTHOR Petrov, G. L.

TITLE Composition of Weld Metal at the Vicinity of the Zone of Fusion
(O sostave metala saryezh sovmedneny v rayone zony splavleniya)

PERIODICAL *Tr. Leningr. politekh. inst.* 1958, No. 183, pp. 2, 4.

ABSTRACT Calculated and experimental data on the dimensions of the zone of fusion, the diffusion of certain elements from the weld into the parent metal, and the effect of the fused parent metal on the composition of the weld metal near the zone of fusion in arc welding are presented. The magnitude of the zone of fusion depends upon the liquidus-solidus temperature difference and the temperature gradient near the boundary of the welding bath. Excess alloying elements are diffused from the welding bath into the parent metal. The depth of their penetration in mm is: C: 0.001-0.002; Mn: 0.001-0.003; Cr: 0.01-0.03; Mo and Ni: 0.001-0.007. Higher rates of crystallization at the boundary of fusion and the absence of that region of intensive interdiffusion of the fused metal in this region gives rise to chemical inhomogeneity there. The weld metal at the fusion boundary is enriched by the excess

Card 1 2

137-58-2-3046

Composition of Weld Metal in the Vicinity of the Zone of Fusion

elements of the parent metal and deposited in terms of elements of the weld metal. The size of this zone of transition composition is 0.4-0.5 mm. in single pass welding of austenitic steels.

I. S

1. Welds—Metallurgical analysis

Card 2 2

137-58-5-0681

Translation from Referativnyi Zhurnal Metallurgiya, 1957, No. 5, p. 116, USSR

AUTHORS Zenzin, V. I., Petrov, G. L., Bruk, B. I.

TITLE The Latest Achievements of the Scientific Research Organizations of Leningrad in the Welding of Alloy Steels (Noveystye dostizheniya nauchno-issledovatel'skikh organizatsiy Leningrada v oblasti svarki legirovannykh staley)

PERIODICAL V sb. Svirchnove proiz-vo. Leningrad, Lenizdat, 1957, pp. 38-55

ABSTRACT The results of investigations in the field of the welding of alloy steels related to problems of the chemical inhomogeneity of welded joints, determination of a rational composition of austenitic heat-resistant facing metal, and study of the zone of fusion of welds of different steels are presented. Radioactive isotope and metallographic methods of analysis were employed in the investigations.

B. V.

Card 1 1

PETROV, G.L.

Processes of stabilization of the chemical composition of weld metal bounding on the fusion zone. Avtom. svar. 10 no.5:19-37 S-O '57.

(MIRA 10:12)

1. Leningradskiy politsekhnikheskiy institut im. M.I. Kalinina.
(Electric welding) (Diffusion)

Translation from: *Report on Scientific Methods*, 1957, No. 159, p. 1-10. USSR

AUTHORS Petrov, G. I. Polubny, I. P.

TITLE A Novel Technique for the Evaluation of the Effects of Welding Materials and Certain Basic Parameters of Welding on the Susceptibility of Welds to Hot Cracking. (Novaya metoda opredeleniya svyazani svarkoi sraznymi materialami i nerolovnykh parametrov i tehnologii svarki na seromost' metalla svarnykh shvotov i razvira nny gorvachiny. *Abstract*)

PERIODICAL *Tr. Leningr. konform. inst.*, 1957, No. 159, pp. 1-10.

ABSTRACT The method described makes it possible to establish a relation between such factors as the employment of various welding materials, the size of the root opening, the included groove angle, the welding current, and other technological parameters, and the tendency of welds toward hot cracking (HC). In order to determine the critical temperatures corresponding to permissible deformations of the metal, preliminary investigations were carried out on metal which had been welded with a K20N10G6 welding wire (nickel) and with an alkaline flux; the properties of the weld metal were studied.

Card 1 of 1

SOV. ...

A Note: Technique for the Evaluation of the Effects of Welding Materials

at elevated temperatures maintained in an oven. The heating of specimens was conducted in a stepwise fashion, the exposure to the testing temperature lasting 30-40 minutes. The rate of deformation of the specimens amounted to 4 mm/min. Regions of brittle failure of metal were observed at temperatures above 1500°C. The following procedure was employed in evaluating the HC tendency of welds. Two halves of a specimen 20x15 mm in cross section were mounted in a rigid frame with an initial Δl of 0.2 mm between them. The specimen was heated to a certain distance Δl by means of heating of the sections of the specimen. The frame being rigid, the two sections of the specimen were heated to the same extent of filler metal being rigidly controlled, the heated portion of the specimen was cooled in water, thereby avoiding a torsion deformation of the specimen. The magnitude of the maximum deformation possible in a weld with the absence of hot cracks in the latter was taken as the criterion of its quality. It was established that the HC tendencies of the weld metal become more pronounced as the root opening gap Δl is increased and the elevated groove angle is increased. Compared with TsT-7 electrodes, which produce welds of a composition similar to that of Kh20N10G6 steel, KF-5 electrodes exhibit the least tendency to HC. Even more susceptible to HC than TsT-7 electrodes are electrodes of the K-1 type. In the case of automatic welding, maximum stability is to be observed.

Card 2/3

SC 11-10-10-10-10

A Novel Technique for the Evaluation of the Effects of Welding Materials

performed with welding wire of the E6013 grade in conjunction with AN-11 flux.
Less stable are welds performed with the same grade of welding wire and
flux of the 11-5 type. Welding wire of the St-Kal-Ni-Gr grade is more stable
when used with either flux. Bibliography and references.

7-5

Card 3-3

SOV 137 58-7 15003

Translation from Referativnyi Zhurnal Metallurgiya, 1957, No. 11, pp. 1500-1503, 1504

AUTHORS Petrov, G.L., Korzhov, V.I.

TITLE Welding of Nickel and Monel Metal (Svarka nikelovykh i monel'nykh metallov)

PERIODICAL Izv. Leningr. politekhn. inst. 1957, No. 189, pp. 1500-1503, 1504

A. STRACT The possibility of obtaining high-quality arc-welded joints between Ni and Monel metal was investigated, together with the possibility of welding of Ni to austenite steel, 1Kh18N9Ti. Welding electrodes made of Ni-nickel and Ni-Mn alloys were employed in welding of both Ni and Monel metal. The electrodes were covered with a UONI 13745 coating and a 44-44-12 coating manufactured by Krupp. Welding of Ni to 1Kh18N9Ti steel was accomplished with the aid of electrodes which produced welded joints composed of metal of any of the following types: Kh30, Kh22N15, Kh20N10G6, Kh20N12G2M2F, and Ni-Ni-Mn welding rods submerged in fluxes AN-20 and BKFI were employed in the investigation of the process of automatic welding of Ni. Current, welding rate, the method of advancing the arc, and the temperature of preliminary heating - all these

Card 1/2

SOV 137-88-741-10

Welding of Nickel and Monel Metal

factors were varied in the course of the investigation. The materials investigated were 4-5 mm thick. It was established that satisfactory joints may be obtained with rolled Ni stock of medium thickness if UONI-13745 electrodes with NMs-2.5 cores are employed ($\sigma_b = 42-49 \text{ kg/mm}^2$, $\phi = 160-180^\circ\text{C}$). The porosity of welded Ni joints constitutes their major drawback. This condition may be remedied by employing moderate currents and rates of welding as well as procedures aimed to reduce the rate of cooling in the welding pool (longitudinal vibrations of the electrode etc.). Welded joints with mechanical properties identical to those produced by manual welding can be attained by automatic welding methods. Welding of Ni to steel 1K618N9E is readily accomplished by means of electrodes that produce welded joints composed of Cr-Ni-austenite steel (electrodes - K11-5, type of metal in the weld - ER29Ni12ZMF).

$\sigma_b = 46-48 \text{ kg/mm}^2$, rupture occurs in the vicinity of the weld. Monel sheet metal lends itself readily to the production of satisfactory joints with UONI-13745 electrodes. The mechanical properties of the joints are similar to those of the base metal. The following mechanical properties are obtained: $\sigma_b = 42-49 \text{ kg/mm}^2$, $\phi = 160-180^\circ$.

Card 2/2

PETROV, G. L. (Cand. Techn. Sci.)

"Chemical Nonhomogeneity of Welded Connections," p. 102
in book Reports of the Interuniversity Conference on Welding, 1950.
Moscow, Mashgiz, 1953, 266pp.

66505

18.7200

[Faint, mostly illegible text, possibly bleed-through from the reverse side of the page. Some words like "activity" and "information" are partially visible.]

AUTHOR: Gulyaev, B.B.
 TITLE: Conference on Crystallization of Metals (Sovetskoye Mashinostroyeniye)
 PERIODICAL: Vestnik Akademiya Nauk SSSR, Fiziko-Metallurgiya, 1958, No. 1, pp. 153-155 (USSR)

ABSTRACT: This conference was held at the Institute of Mechanical Engineering (IMES) of the Academy of Sciences of the USSR in Moscow on June 28-31, 1958. About 400 people of the Academy of Sciences and other scientific institutions participated in the conference. The main topics of the conference were: heat treatment, physical chemistry, crystallography, physical metallurgy, and related subjects. In addition to Soviet participants, foreign visitors included Professor D. G. Clark, East London University, and Professor D. G. Clark, East London University. The general program of the conference was as follows: 1. Crystallization of Non-ferrous Metals. 2. Crystallization of Ferrous Metals. 3. Crystallization of Polymers. 4. Crystallization of Glasses. 5. Crystallization of Composites. 6. Crystallization of Metals in the Solid State. 7. Crystallization of Metals in the Liquid State. 8. Crystallization of Metals in the Vapor State. 9. Crystallization of Metals in the Plasma State. 10. Crystallization of Metals in the Superconducting State. 11. Crystallization of Metals in the High Pressure State. 12. Crystallization of Metals in the Low Pressure State. 13. Crystallization of Metals in the High Temperature State. 14. Crystallization of Metals in the Low Temperature State. 15. Crystallization of Metals in the High Strain Rate State. 16. Crystallization of Metals in the Low Strain Rate State. 17. Crystallization of Metals in the High Frequency State. 18. Crystallization of Metals in the Low Frequency State. 19. Crystallization of Metals in the High Magnetic Field State. 20. Crystallization of Metals in the Low Magnetic Field State. 21. Crystallization of Metals in the High Electric Field State. 22. Crystallization of Metals in the Low Electric Field State. 23. Crystallization of Metals in the High Pressure and High Temperature State. 24. Crystallization of Metals in the Low Pressure and Low Temperature State. 25. Crystallization of Metals in the High Pressure and Low Temperature State. 26. Crystallization of Metals in the Low Pressure and High Temperature State. 27. Crystallization of Metals in the High Pressure and High Temperature State. 28. Crystallization of Metals in the Low Pressure and Low Temperature State. 29. Crystallization of Metals in the High Pressure and Low Temperature State. 30. Crystallization of Metals in the Low Pressure and High Temperature State. 31. Crystallization of Metals in the High Pressure and High Temperature State. 32. Crystallization of Metals in the Low Pressure and Low Temperature State. 33. Crystallization of Metals in the High Pressure and Low Temperature State. 34. Crystallization of Metals in the Low Pressure and High Temperature State. 35. Crystallization of Metals in the High Pressure and High Temperature State. 36. Crystallization of Metals in the Low Pressure and Low Temperature State. 37. Crystallization of Metals in the High Pressure and Low Temperature State. 38. Crystallization of Metals in the Low Pressure and High Temperature State. 39. Crystallization of Metals in the High Pressure and High Temperature State. 40. Crystallization of Metals in the Low Pressure and Low Temperature State. 41. Crystallization of Metals in the High Pressure and Low Temperature State. 42. Crystallization of Metals in the Low Pressure and High Temperature State. 43. Crystallization of Metals in the High Pressure and High Temperature State. 44. Crystallization of Metals in the Low Pressure and Low Temperature State. 45. Crystallization of Metals in the High Pressure and Low Temperature State. 46. Crystallization of Metals in the Low Pressure and High Temperature State. 47. Crystallization of Metals in the High Pressure and High Temperature State. 48. Crystallization of Metals in the Low Pressure and Low Temperature State. 49. Crystallization of Metals in the High Pressure and Low Temperature State. 50. Crystallization of Metals in the Low Pressure and High Temperature State. 51. Crystallization of Metals in the High Pressure and High Temperature State. 52. Crystallization of Metals in the Low Pressure and Low Temperature State. 53. Crystallization of Metals in the High Pressure and Low Temperature State. 54. Crystallization of Metals in the Low Pressure and High Temperature State. 55. Crystallization of Metals in the High Pressure and High Temperature State. 56. Crystallization of Metals in the Low Pressure and Low Temperature State. 57. Crystallization of Metals in the High Pressure and Low Temperature State. 58. Crystallization of Metals in the Low Pressure and High Temperature State. 59. Crystallization of Metals in the High Pressure and High Temperature State. 60. Crystallization of Metals in the Low Pressure and Low Temperature State. 61. Crystallization of Metals in the High Pressure and Low Temperature State. 62. Crystallization of Metals in the Low Pressure and High Temperature State. 63. Crystallization of Metals in the High Pressure and High Temperature State. 64. Crystallization of Metals in the Low Pressure and Low Temperature State. 65. Crystallization of Metals in the High Pressure and Low Temperature State. 66. Crystallization of Metals in the Low Pressure and High Temperature State. 67. Crystallization of Metals in the High Pressure and High Temperature State. 68. Crystallization of Metals in the Low Pressure and Low Temperature State. 69. Crystallization of Metals in the High Pressure and Low Temperature State. 70. Crystallization of Metals in the Low Pressure and High Temperature State. 71. Crystallization of Metals in the High Pressure and High Temperature State. 72. Crystallization of Metals in the Low Pressure and Low Temperature State. 73. Crystallization of Metals in the High Pressure and Low Temperature State. 74. Crystallization of Metals in the Low Pressure and High Temperature State. 75. Crystallization of Metals in the High Pressure and High Temperature State. 76. Crystallization of Metals in the Low Pressure and Low Temperature State. 77. Crystallization of Metals in the High Pressure and Low Temperature State. 78. Crystallization of Metals in the Low Pressure and High Temperature State. 79. Crystallization of Metals in the High Pressure and High Temperature State. 80. Crystallization of Metals in the Low Pressure and Low Temperature State. 81. Crystallization of Metals in the High Pressure and Low Temperature State. 82. Crystallization of Metals in the Low Pressure and High Temperature State. 83. Crystallization of Metals in the High Pressure and High Temperature State. 84. Crystallization of Metals in the Low Pressure and Low Temperature State. 85. Crystallization of Metals in the High Pressure and Low Temperature State. 86. Crystallization of Metals in the Low Pressure and High Temperature State. 87. Crystallization of Metals in the High Pressure and High Temperature State. 88. Crystallization of Metals in the Low Pressure and Low Temperature State. 89. Crystallization of Metals in the High Pressure and Low Temperature State. 90. Crystallization of Metals in the Low Pressure and High Temperature State. 91. Crystallization of Metals in the High Pressure and High Temperature State. 92. Crystallization of Metals in the Low Pressure and Low Temperature State. 93. Crystallization of Metals in the High Pressure and Low Temperature State. 94. Crystallization of Metals in the Low Pressure and High Temperature State. 95. Crystallization of Metals in the High Pressure and High Temperature State. 96. Crystallization of Metals in the Low Pressure and Low Temperature State. 97. Crystallization of Metals in the High Pressure and Low Temperature State. 98. Crystallization of Metals in the Low Pressure and High Temperature State. 99. Crystallization of Metals in the High Pressure and High Temperature State. 100. Crystallization of Metals in the Low Pressure and Low Temperature State.

Card#10

Card#9/10

PETROV, G.L., kand.tekhn.nauk, dots.; YEFIMOV, L.A., inzh.

Selection of electrodes for welding thin elements of EI417(Kh23H18)
steel. Energomashinostroenie 4 no. 6:25-27 Je '58 (MIRA 11:8)
(Electrodes)
(Steel--Welding)

30V-135-58-10-16 19

AUTHORS: Skerblom N.S., Doctor of Technical Sciences, Professor,
Demyantsevic, V.B., and Petrov, G.L., Candidates of Techni-
cal Sciences

TITLE: Problems of Electrode Standardization in Arc Welding K
voprosu standartizatsii elektrodov dlya dugovoy svarki

PERIODICAL: Svarochnoye proizvodstvo, 1958, Nr 10, pp 40 - 42 USSR,

ABSTRACT: With reference to an article published by A.A. Yerokhin in
a previous copy of this periodical, entitled "Principal
Problems of Standardization For Arc-Welding Electrodes", the
authors present some principal and practical observations
dealing with the classification and requirements of differ-
ent electrode types. As an example, 4 tables containing
approximate requirements of electrodes for welding differ-
ent steel grades, are included. There are 4 tables.

ASSOCIATION: Leningradskiy politekhnicheskii institut (Leningrad Poly-
technical Institute)

1. Arc welding--Electrodes 2. Electrodes--Standardization

Card 1/1

PETROV, G.L.

Characteristics of metal solidification in fusion welding.
Trudy LPI no.129:123-135 '58. (MIRA 12:9)
(Welding research) (Solidification)

PETROY, G.L.

Carbon and sulfur migration in the zone of the fusion
weld boundary. Trudy LPI no.139:143-156 '58. (MIRA 12:9)
(Welding--Testing) (Diffusion) (Metallography)

13(5)

PHASE I BOOK EXPLOITATION

SOV 2/59

Akademiya nauk SSSR. Institut metallurgii

Goryachiye treshchiny v svarnykh soyedineniyakh slitkakh i otlivkakh (Hot Cracks in Welds, Ingots, and Castings) Moscow, Izd-vo AN SSSR, 1959. 163 p. 2,700 copies printed.

Ed.: N. N. Rykalin, Corresponding Member, USSR Academy of Sciences; Ed. of Publishing House: V. S. Rzhiznikov; Tech. Ed.: Yu. V. Rylina.

PURPOSE: This book is intended for metallurgists and welding engineers.

COVERAGE: This is a collection of scientific papers dealing with the formation of hot cracks in ingots, castings, and welded products. Some papers are concerned mainly with the nature or mechanism of the phenomenon; others examine the effect of factors such as steelmaking procedure. Sufficient evidence is presented to identify some of the causes of hot cracks. Various means of investigating and preventing the phenomenon are described. A number of references, both Soviet and non-Soviet, accompany the papers. For further coverage see the Table of Contents.

Card 1/3

Hot Cracks in Welds (Cont.)

SOV/2859

TABLE OF CONTENTS:

Dobrokhotov, N. N. Effect of Steelmaking Technique on Quality of Open-hearth Steel

The author makes the following recommendations: At the end of the run the basicity of the slag, i.e., the ratio of CaO to SiO_2 , should be within the limits of 2.5 and 3.0, and the fluidity of the slag, as tested by viscosimeter, should amount to some 30-60 mm. Preliminary deoxidation of the steel in the furnace by means of blast-furnace ferrosilicon should not be carried out. If ferrochrome and ferromanganese have been added, the time for holding the heat should be determined by the formula $z = \frac{1.5q}{P}$, min., where q = the weight of ferroalloys added (in kg), and P = the output of the furnace (*, 24 hr). In the production of carbon and low-alloy steel, alloying and deoxidation should be carried out in the teeming ladle. Government standards (GOST 300-50 and 5521-50) for rimmed steel should be revised so as to specify a manganese content of 0.30-0.50 percent instead of the present 0.35-0.60 percent.

Card 2, 3

Hot Cracks in Welds (Cont.)

NOV 1964

Yefimov, V. A. Causes of Cracks in Steel Ingots and Means of Preventing Them

10

The following causes of ingot cracks are discussed: shrinkage and plasticity of steel at high temperatures, crystallization conditions in the ingot mold, ingot-mold design and teeming conditions, hydrodynamics of ingot-mold filling, and sticking of the ingot to the mold and other factors associated with top pouring.

Pronov, A. P. Mechanism of Hot-crack Formation on Steel Ingot Surfaces

30

Bidulya, P. N., V. G. Gruzin, and V. N. Saveyko. Formation and Prevention of Hot Cracks in Steel Castings

39

As a criterion for the quantitative determination of the resistance of steel to the formation of exterior hot cracks, the author finds it convenient to employ the concept of "crack resistance", or the force required to form a crack during the shrinkage of a standard cast specimen with rigidly fastened ends. For mild carbon steel and low-alloy (Cr, Mo, V) structural steel, pouring temperature is one of

Card 3 of 3

Hot Cracks in Welds (Cont.)

SOV/2859

the most important factors in crack development. Filling the molds with steel at the temperature of the liquidus or below should be avoided. A direct relationship between crack resistance and linear shrinkage, fluidity, and gas liberation was established. Increasing the fluidity of the mushy stage by changing the composition or the conditions helps to increase the crack resistance. Sulfur, hydrogen, and methane decrease the crack resistance of steel. Additions of manganese, molybdenum, and vanadium to carbon steel or low alloy steel increase the crack resistance. The manganese content should be held at a maximum so as to assure a ratio of Mn, S \leq 13.

Guliyayev, B. B., I. I. Lopyrev, and L. M. Postnov. Formation of Hot Cracks in Steel Castings

51

The author recommends the following measures for controlling hot cracks in steel castings: 1) decreasing the size of the casting and eliminating projections by casting in several pieces with subsequent welding of the components; 2) Equalization of the cooling rates of various parts of the casting and elimination of conjugate parts through a rational determination of the thickness of their elements; 3) increasing fillet radii; 4) rejection of X-shaped designs and conjugate walls at angles of less than 90°; 5) increasing the pliancy of molds through the use of more pliable molding media and by

Card 4/8

Hot Cracks in Welds (Cont.)

30V 1964

pitting the molds; 6) strengthening weak spots through the use of chills and ribbing; 7) regulating the metal composition, insofar as possible, and the pouring conditions so as to reduce the probability of crack development. Consistent application of these measures, the author states, will effectively prevent hot cracks from developing. Consistent application of these measures, the author states, will effectively prevent hot cracks from developing.

Pokhodnya, I. K. Hot (Crystallization) Cracks in the Hard Facing of High-Carbon Low-Chrome Steels

58

The author discusses the nature and mechanism of hot-crack formation and examines various factors contributing to it (chemical composition of added metal, cooling rate, etc.).

Medovar, B. I. Hot Cracks in the Welding of Chrome-Nickel Austenitic Steels

92

Prokhorov, N. N. Intergranular Strength of Metals

108

The author points out that hot cracks are one of the main causes of rejection of welded and cast products. To solve the problem he suggests intensive study of the hot strength of metals, using several different approaches: 1) investigation of deformations caused by

Card 5/8

Hot Cracks in Welds (Cont.)

SOV. 2859

welding and casting processes, accompanied by development of computational methods of determining deformations and their concentration at high temperatures; 2) study of the mechanical properties of metals during crystallization and cooling; 3) development of a single working hypothesis of intergranular strength of metals which would guide investigators and manufacturers in solving theoretical and practical problems connected with hot-crack formation (in this connection the author suggests the utility of his own hypothesis, based on a comparison of the numerical values of the deformation and plasticity of metals within a definite temperature range of brittleness); development of unified methods of testing metals for susceptibility to hot-crack formation in welding and casting; 4) development of quantitative methods of determining the effect of the shape of the product, as required by manufacturing and constructional considerations, on intergranular strength of welded and cast products; 5) systematic adoption of new scientific methods by manufacturers.

Lashko Avakyan, S. V., and N. F. Lashko. Intergranular Crystallization Cracks in the Casting and Welding of Aluminum Alloys

According to the author, certain alloys ordinarily subject to the formation of crystallization cracks after welding can be

131

Card 6/8

Hot Cracks in Welds (Cont.)

SOV, 28, 9

rendered resistant to such cracks by the use of an added metal (alloy) which satisfies the following conditions: (a) the weld metal must not be subject to crack formation after welding; (b) the liquidus temperature of the weld metal must not be higher than that of the parent metal; (c) the weld metal must not contain components that in penetrating the base metal along the boundaries of fused grains in the heat-affected zone would form alloys with significantly lower eutectic temperatures than that of the base metal.

Petrov, G. L. New Methods of Determining the Susceptibility of Weld Metal to Hot-Crack Formation

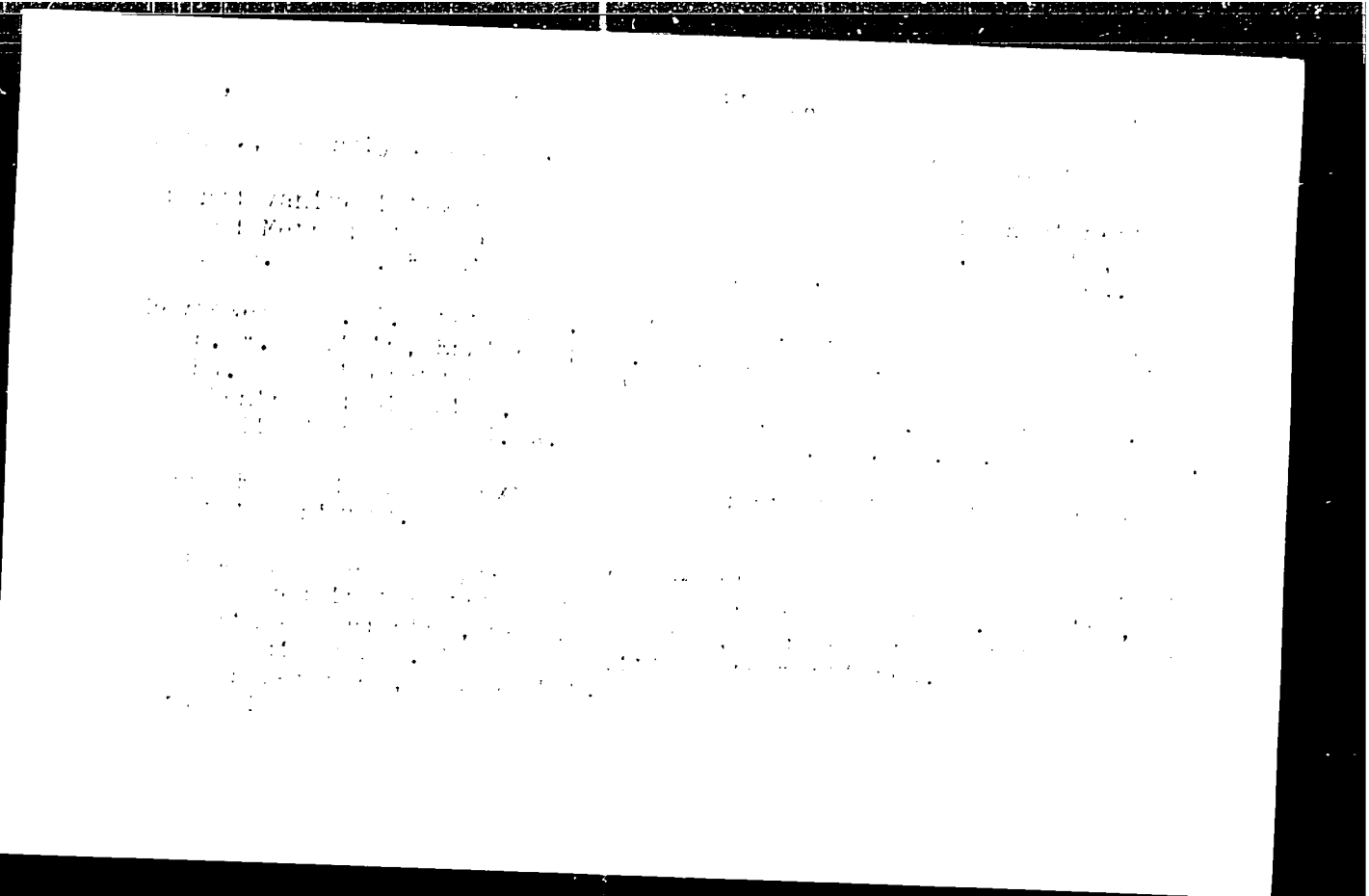
147

The article describes new methods developed by N. O. Okerblom and associates, Welding Department, Leningrad Polytechnic Institute. The methods make it possible to determine the effect of various welding materials and basic welding parameters on the development of hot cracks in weld metal.

Card 7, 8

BHUK, Boris Il'ich; PETROV, G.L., dotsent, retsenzent; ZHUKOV, O.N.,
nauchnyy red.; NIKITINA, R.D., red.; SHISHKOVA, L.M., tekhn.red.

[Use of radioactive isotopes in welding metallurgy and metallo-
graphy] Radioaktivnye izotopy v metallurgii i metallovedenii
svarki. Leningrad, Gos.soiuznoe izd-vo sudostroit.promyshl.,
1959. 231 p. (MIRA 12:6)
(Radioisotopes--Industrial applications)
(Electric welding) (Metallography)



"APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2

APPROVED FOR RELEASE: 07/19/2001

CIA-RDP86-00513R001240420015-2"