OGIBALOV, P.M.; BIKKENINA, Yu.V. Calculating the strength of reinforced plastics. Vest.Mosk.ur.-Ser.l: Mat.,mekh. 17 no.3:44-57 My-Je '62, (MIRA 15: (MIRA 15:7) 1. Kafedra teorii uprugosti Moskovskogo universiteta. (Reinforced plastics)

PETROVSKIY, I.G., akademik; OGIBALOV, P.M., prof.; ZAYKIN, A.D., dotsent Leonid Nikolaevich Sretenskii; on his sixtieth birthday anniversary. Vest. Mosk. un. Ser. 1: Mat., mekh. 17 no. 2:76-80 Mr-Ap (MIRA 15:6) 1. Rektor Moskovskogo universiteta (for Petrovskiy). (Sretenskii, Leonid Nikolaevich, 1902-)

QGIBALOV, P.M., BIKKENINA, Yu.V. Mechanical properties of reinforced plastics. Vest.Mosk.un.Ser.l:-Mat., mekh. 17 no.2:44-52 Mr-Ap 62. (MIRA 15:6) 1. Kafedra teorii uprugosti Moskovskogo universiteta. (Plastics) (Strength of materials)

Short-period creep ... 6 figures and 5 tables. S/055/62/000/006/006/006 D251/D308 ASSOCIATION: Kafedra teorii uprugosti (Department of the Theory SUBMITTED: April 17, 1962 Card 2/2

## S/055/62/000/006/006/006 D251/D308

AUTHORS:

Ogibalov, P.M. and Tyuneyeva, I.M.

TITIE:

Short-period creep of textolite at normal tempera-

ture

PERIODICAL:

Moscow. Universitet. Vestnik. Seriya I. Matematika,

mekhanika, no. 6, 1962, 70-77

Tables and graphs are given, illustrating the results of experimental investigations of 6 to 10 mm thick textolite at normal temperatures. Samples were cut out of textolite along the base, and at 45° and 90° to the base, and kept for 0, 15, 30, 60 and 180 min under constant load. The deformation increased quickly during the first 10 min and relatively slowly up to 30 min. After that the process became steady. After quick unloading (10-15 sec) deformation of inverse sign took place and initial form and size was completely restored. Recovery of differently oriented specimens occurred in different periods of time. The rate of recovery is the lower and shorter the period of direct creep. There are

Card 1/2

Determination of forces ...

S/838/62/000/000/001/001 E191/E481

covered with uniform sand, a limiting pattern of repose appears, whose coordinates represent the value of pressure at corresponding points. The volume of the sand heap is proportional to the total pressure under conditions of plastic flow. This analogy is examined in the case of pressing a plate with a chessboard pattern of webs and a plate with hemispherical craters. Experimental results agree well with the analogy. The extrusion of bars and tubes is also considered in order to determine the total pressure required. There are 6 figures.

Card 2/2

## S/838/62/000/000/001/001 E191/E481

AUTHORS:

Ogibalov, P.M., Kiyko, I.A.

TITLE:

Determination of forces in the stamping and extrusion

of certain machine elements

SOURCE:

Raschety protsessov plasticheskogo formoizmeneniya

metallov. Inst. mashinovoved. AN SSSR. Ed. by

A. D. Tomlenov. Moscow, Izd-vo AN SSSR, 1962, 73-77

It is assumed that plastic material flows in a thin layer contained between rigid parallel plane faces of the die which approach each other along their common normal. If one or both faces contain slots of some profile, the material will flow into the slots to form webs. The slot depth is assumed large enough so that the pressing is unconstrained. The linear dimensions of the region of flow are assumed to exceed greatly the thickness of The inertia tems are neglected and the Prandtl law the layer. concerning friction at the contact surfaces is assumed leading to simplified equations of plastic flow. Adding the boundary condition, a so-called "sand model" is suggested after A.A.Il'yshin (Prikladnaya matematika i mekhanika, no.3, 1954). If a plate is made in the shape of the region of flow and is Card 1/2

Behavior of Materials (Cont.)

Moskvitin, Doctor of Physics and Mathematics, for their valuable comments.
They also thank N. A. Skoryy, Docent, Candidate of Physics and Mathematics,
S. A. Orlova, and G. N. Kuz'makova. There are 94 references: 78 Soviet,
TABLE OF CONTENTS:

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Foreword

Introduction

Ch. I. Some Properties of Materials Under Pressure

1. Compressibility

2. Polymorphic and phase transformations

3. Considerations on pressure classification

18

Card 2/4 2

## PHASE I BOOK EXPLOITATION

SOV/6109

Ogibalov, Petr Matveyevich, and Igor' Anatol'yevich Kiyko

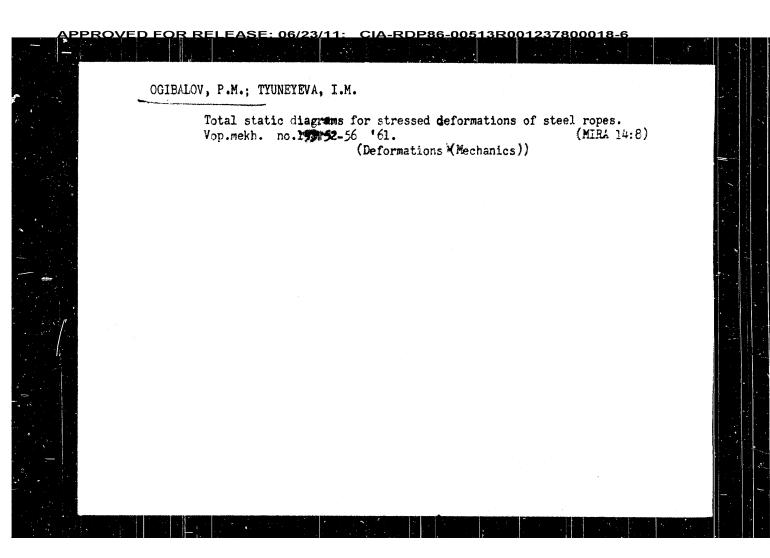
Povedeniye veshchestva pod davleniyem (Behavior of Materials Under Pressure). Moscow, Izd-vo Mosk. univ., 1962. 153 p. 5000 copies printed.

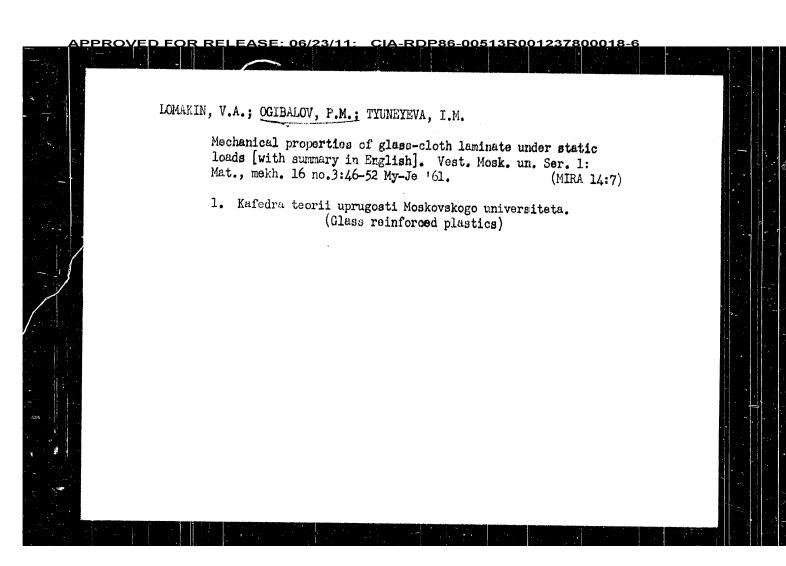
Ed.: I. A. Skoryy; Tech. Ed.: L. V. Lazareva.

PURPOSE: This book may serve as a textbook for students, aspirants, and teachers at universities and schools of higher technical education. It may also be useful to engineers and scientific research workers concerned with problems of the strength of materials.

COVERAGE: An attempt is made to give a general idea of the effect of pressure on the physical and mechanical properties of various materials and especially on the mechanical properties of solids. The authors thank L. F. Vereshchagin, Professor, Corresponding Member, Academy of Sciences USSR, and V. V.

Card 1/4 2





OGIBALOV, P.M.; SENTYURIN, G.G. Aging of industrial lubricants undergoing compression by high pressure of short durati n. Izv. vys. ucheb. zav.; neft' i gaz 4 no.2:65-67 161. (MIRA 15:5) 1. Moskovskiy gosudarstvennyy universitet imeni Lomonosova. (Lubrication and lubricants)

29407 \$/055/61/000/005/002/004 D205/D303 On formulating the problem of ... Sci., 24, no. 5, May 1957. SUBMITTED: May 3, 1961 Card 3/3

29407 3/055/61/000/005/002/004 D205/D303

On formulating the problem of ...

an undisturbed state. Then the force  $Z = \frac{BV}{R} \frac{\partial \Omega}{\partial t^2} - B_1 \frac{\partial \Omega}{\partial t}$ efficient of oscillation,  $B_1 = damping$  coefficient. The limits of V are treated quantitavely with respect to Z. The problem of shells can be summarized by & (C, A, t) = 0. The problem of flutter consists of determining conditions, in which undisturbed motion is stable. Consider the equation  $\phi$   $(\alpha, \beta, t)$  $= \psi(\alpha, \beta) e^{\alpha t}$  where  $\omega = p + iq$  is a complex number,  $\psi(\alpha, \beta) = a$  complex function. The condition for instability is Re 6 > 0. Critical velocities are those which separate regions of stable and unstable states of a shell. Let  $\lambda_1$ ,  $\lambda_2$  be points on the "stability parabola", then  $\lambda_1 = \rho Eh^2 / B^2 h^2$ ,  $\lambda_2$ where E = coefficient of elasticity. To find the critical velocity the values of A have to be investigated. There are 19 references: 16 Soviet-bloc and 3 non-Soviet-bloc. The references to the English-language publications read as follows: I.M. Hedgepeth, B. Budiansky, R.W. Leonhard, Analysis of Flutter in Compressible Flow of a Panel on Many Supports. J. Aeronaut, Sci. 21. no. 7, July, 1954; J.W. Miles, On the Aerodynamic Instability of Thin Panels. J. Aeronaut. Sci 28, no. 8, Aug. 1956; R.W. Leonhard, J.M. Hedgepeth, On the Flutter of Infinitely Long Panels on Many Supports. J. Aeronaut. Card 2/3

In 6300

29407 \$/055/61/000/005/002/004 D205/D303

AUTHOR:

Ogibalov, P.M.

TITLE:

On formulating the problem of flutter for shells and panels

PERIODICAL:

Moscow. Universitet. Vestnik. Seriya I. Matematika, Mekhani-

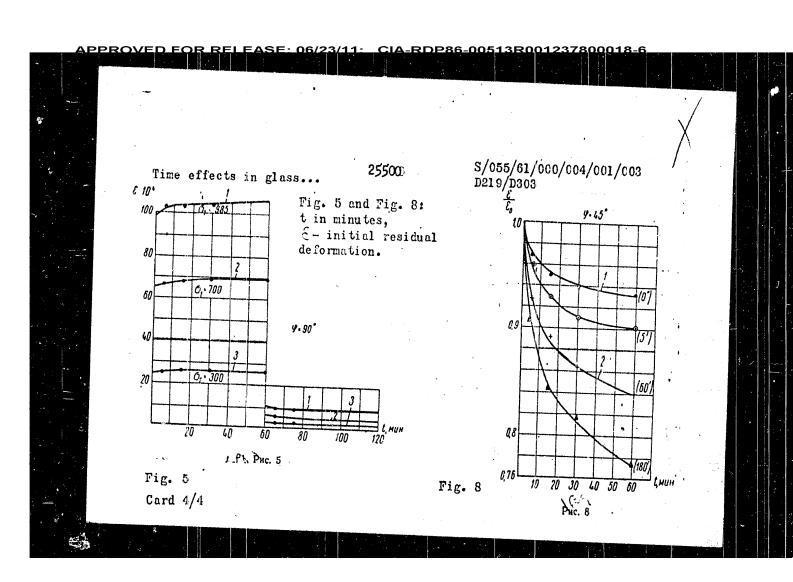
ka, no. 5, 1961, 60 - 65

TEXT:

The basic equation for the shells is

$$\nabla^2 \nabla^2 \nabla^2 \nabla^2 + \frac{1 - v^2}{2} \frac{3^4 \Phi}{\partial \alpha^4} = \frac{R^4}{D} Z. \tag{1}$$

where  $c^2$  = a constant, D = rigidity of the cylinder, R = radius, V - Poisson's coefficient, Z - component of transversal load, C, C - coordinates of a point on the cylinder,  $V^2$  =  $3^2/2c^2 + 3^2/3c^2$ , c - a scalar function which also determines the magnitude of internal forces. Transversal forces are determined by Kirchhoff's formulae. When a shell moves in a gas with a constant velocity V and is in an equilibrium position, it is said to be in Card 1/3



Time effects in glass...

S/055/61/000/004/001/003 D210/D303

deformation at loading  $(\mathcal{E}_m)$  and creep deformation  $(\mathcal{E}_n)$ . Experimental data can be represented by  $\mathcal{E}_o/(\mathcal{E}_m + \mathcal{E}_n)$  m const. There are 8 figures, 6 tables and 2 references: 1 Soviet-bloc and 1 non-Soviet-bloc.

ASSOCIATION:

Kafedra teorii uprugosti (Department of the Theory of Elasticity)

SUBMITTED:

October 6, 1960

Card 3/4

25500

S/055/61/000/004/001/003 D219/D303

Time effects in glass...

every 2 minutes during the next 20 minutes, then every 5, 10, 20, 30 minutes during each hour). For each value of  $\phi$ , 3 specimens were tested. To investigate the initial stage of creep and retrogressive creep, the specimen was loaded up to a certain tension  $o_1$ , remaining thus for a certain period  $t_1$ , then unloaded and left for another period  $t_2$ . Measurements were made during both periods. Results are given for  $t_1 = t_2 = 1$  hour and different values of  $o_1$ . Creep is maximal in the direction of minimal rigidity ( $\phi = 45^{\circ}$ ). More detailed analysis is said to show that there is anisotropy of creep similar to the anisotropy of elastic properties. Presence of creep at  $o_1$  changes essentially the speed and magnitude of restoration after unloading. The higher the speed of retrogressive creep, the larger is  $o_1$ , the duration of creep being the same (Fig. 5). If the duration of direct creep is varied, the speed of retrogressive creep is higher, the longer the former (Fig. 8). These effects were studied by varying  $t_1$  from 5 minutes to 3 hours,  $t_2$  being of the order of 24-48 hours. The instantaneous residual deformation ( $\xi_0$ ) depends both on instantaneous Card 2/4

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S/055/61/000/004/001/003 D219/D303

AUTHORS:

Lomakin, V.A., Ogibalov, P.M., and Tyuneyeva, I.M.

310 + 140 + 100 · 1

Time effects in glass textolite during deformation

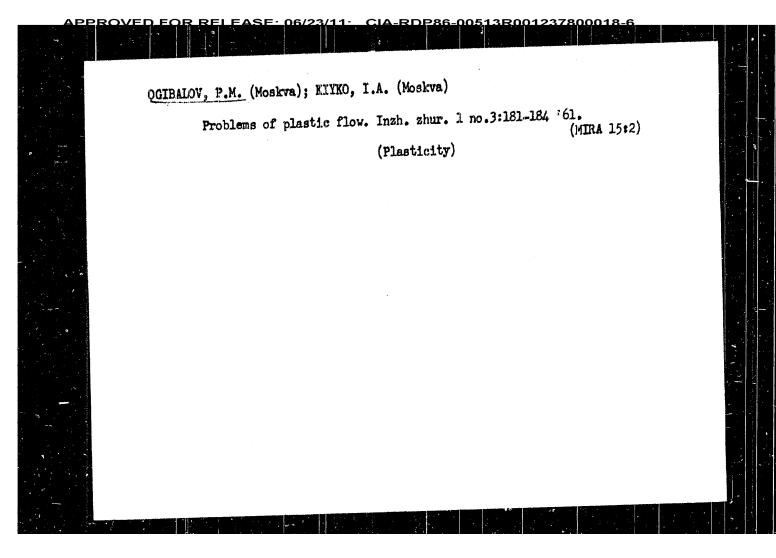
TITLE:
PERIODICAL:

Moscow. Universitet. Vestnik. Seriya 1: Matematika,

mekhanika, no. 4, 1961, 39-47

TEXT: The results are given of experimental investigations on short-period creep (order of magnitude—1 hour) at high stresses, and on restoration effects, in particular, retrogressive creep, carried out on standard sheets of textolite of type KAST-V (10mm thick) at room temperature. Measurements of deformation were made with a Marten's instrument diving high accuracy. If a specimen of glass textolite is stretched and giving high accuracy. If a specimen of glass textolite is stretched and then unloaded, there is a residual deformation which diminishes percepthen unloaded, there is a residual deformation which diminishes perceptibly with time, at first comparatively quickly, then with vanishing tibly with time, at angles  $\phi = 0$ ,  $\phi$ 

card 1/4



GRYAZNOV, Ivan Mikhaylovich; LENSKII, Viktor Stepanovich; QGIBALOV,
Fetr Matreygvich; SKORYY, Ivan Aleksendrovich; KIYKO, I.A., red.;
IERMAROV, M.S., tekhn.red.

[Laboratory manual on the strength of materials and on deformations]
Leboratory praktikum po soprotivleniiu materialov, deformirovaniiu. Pod obshchei red. P.M.Ogibalova i I.A.Skorogo. Moskva,
IERD-VO Mosk.univ., 1961. 199 p.

(Strenght of materials)

(Deformations (Mechanics))

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		Prokof yev, V. A. Infinitesimal Forced Waves in a Radiating Bar tronic Medium	
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Problems of Mechanics; (Cont.)

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Karmishin, A. V. New Analogues Between Problems of Motion of a Particle and Problems of Equilibrium of a Perfectly Flexible

Thread

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Card 2/3

OGIBALOV, PM

PHASE I BOOK EXPLOITATION

SOV/5724

Moscow. Universitet.

Voprosy mekhaniki; sbornik statey. vyp. 193. (Problems of Mechanics; Collection of Articles. no. 193) [Moscow] Izd-vo Mos. univ., 1961. 169 p. Errata slip inserted. 5,000 copies printed.

Sponsoring Agency: Moskovskiy gosudarstvennyy universitet imeni M. V. Lomonosova.

Ed.: L. N. Sretenskiy, Corresponding Member, Academy of Sciences USSR. Ed. (This vol.): I. Z. Pirogov; Tech. Ed.: G. I. Georgiyeva.

PURPOSE: This book is intended for engineers and scientific workers interested in the mechanics of materials, fluid dynamics, and radi-

COVERAGE: The book contains articles on problems of algebra, nonlinear programming, motion of particles, elasticity, stress-strain, vibration, and flow of liquids. No personalities are mentioned. References follow all but one article.

card 1/3

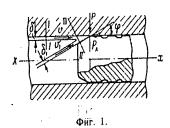
28005 S/508/60/030/000/007/013 D234/D306

On the effect of ...

units as before, w = 2.56/E;  $\sigma_1 = 0$ ;  $\sigma_2 = 2.88$ ;  $\sigma_3 = 0.96$  (the outer surface is supposed to be free). There are 2 figures.

SUBMITTED: May 27, 1959

Fig. 1.



Card 6/6

28005 S/508/60/030/000/007/013 D234/D306

On the effect of ...

rections, and at x=0 in the section where the concentrated annular pressure P acts, one can put dw/dx=0, D  $d^2w/dx^3=P/2$ . From her and (12)  $A=B=P/8k^3D$ , and

$$w = \frac{P}{8k^{3}p} = \epsilon_{2}R, \qquad \frac{d^{2}w}{dx^{2}} = -\frac{P}{4kD} = \frac{2\epsilon_{3}}{h}.$$
 (17)

Substituting the values in (17) and taking into account (11) one finds for the inner surface  $\gamma = 1,29$ , for the outer surface  $\gamma = 1,63$ . Analogous calculations give  $\zeta = 0.63$ . The quantities are (expressed in units by  $\frac{(Rh)^{1/2}}{h^2}$  pv<sup>2</sup> sin  $\varphi$ ); on the inner surface:  $\sigma_{ia} = 1,29$ ;  $\sigma_{1} = 0$ ;  $\sigma_{2} = 0,328$ ;  $\sigma_{3} = -0.935$ ; on the outer surface:  $\sigma_{ib} = 1,63$ ;  $\sigma_{1} = 0$ ;  $\sigma_{2} = 1,1$ ;  $\sigma_{3} = 1,4$ ; the radial displacement:  $\sigma_{ib} = 0.64/E$ . Assuming that the piston is at the free end of the pipe and putting the origin of coordinates at the end section one has  $\sigma_{2} = 0$ ,  $\sigma_{3} = 0$ ,  $\sigma_{3} = 0$ ,  $\sigma_{4} = 0$ ,  $\sigma_{5} = 0$ . In the same Card 5/6

28005 S/508/60/030/000/007/013 D234/D306

On the effect of ...

The indices 1, 2, 3 refer to the radial, tangential and axial stress or elongation. The solution of (6) is

w = 
$$(A \cos kx + B \sin kx)e^{-kx}$$
. (12)

The intensity of stresses on the inside and outside surface of the shell  $\sigma_1^2=\sigma_2^2-\sigma_2\sigma_3+\sigma_3^2$  will be

$$\sigma_i = \eta \, \frac{8 \, \sqrt{Rh}}{h^2} \, \rho v^2 \sin \varphi. \tag{13}$$

and the radial displacement

$$w = \frac{\hat{o}R}{h^2} \frac{\sqrt{Rh}}{E} \sin \varphi.$$
 (14)

The coefficients  $\eta$  and  $\xi$  depend on boundary conditions. If one considers a section at a distance larger than  $(Rh)^{1/2}$  from the end of the cylinder, one can treat the latter as infinite in both di-

Card 4/6

28005 S/508/60/030/000/007/013 D234/D306

On the effect of ...

$$\frac{\mathrm{d}^4 w}{\mathrm{d} x^4} + 4 k^4 w = 0, \tag{6}$$

x being the coordinate taken along the generating line of the cylinder. For Poisson's number m = 3 (steel)

$$k = \sqrt{\frac{2}{Rh}} \sqrt{\frac{2}{3}} = \frac{1.278}{\sqrt{Rh}} . \tag{7}$$

The bending moment and the shearing force acting on a strip are:  $M = -D d^{2}w/dx^{2}, N = -D d^{3}w/dx^{3}, D \text{ being the cylindrical rigidity} = 3 EH^{2}/32.$  The stresses on the inside surface and the corresponding relative elongations are

$$\sigma_{1} = 0, \quad \sigma_{2} = \frac{9E}{8}(\varepsilon_{2} + \frac{1}{3}\varepsilon_{3}), \quad \sigma_{3} = \frac{9E}{8}(\varepsilon_{3} + \frac{1}{3}\varepsilon_{2}), \quad (10)$$

$$\varepsilon_1 = \frac{1}{3E}(\sigma_2 + \sigma_3), \quad \varepsilon_2 = \frac{w}{R - \frac{1}{2}h} \approx \frac{w}{R}, \quad \varepsilon_3 = \frac{h}{2} \frac{d^2w}{dx^2}.$$
 (11)

Card 3/6

28005 s/508/60/030/000/007/013 D234/D306

On the effect of ...

 $\delta v_1 \rho_1 = \delta v \rho_0$  Assuming that the pressure in II is already stabilized, one obtains from (1) and Bernoulli's equation (taking into account that  $\rho=0$  in I and II):  $v=v_1$ ,  $\delta=\delta_1$ 

 $\rho v_1 \delta_1 = \rho v \delta$ .

The law of conservation of momentum gives the following values for the axial force  $P_{\chi}$  and annular force P referred to a unit of circumference of the section:

the of the section:  

$$P_{\mathbf{x}} = \rho \delta \mathbf{v}^{2} (1 + \cos \varphi), \quad P = \rho \delta \mathbf{v}^{2} \sin \varphi. \tag{4}$$

Since 
$$\varphi$$
 is not larger than  $\mathfrak{N}/2$ ,  $P < P_{\text{max}} = \rho \delta v^2$ . (5)

The author assumes that the walls of the pipe are relatively thin, h = b = a being the thickness of the wall, R the average radius of the pipe. The deflection on the central surface w satisfies the equation

Card 2/6

28005 S/508/60/030/000/007/013 D234/D306

26.2182

AUTHOR:

Ogibalov, P.M. (Moscow)

TITLE

On the effect of labrication on stresses in a pipe

with moving piston

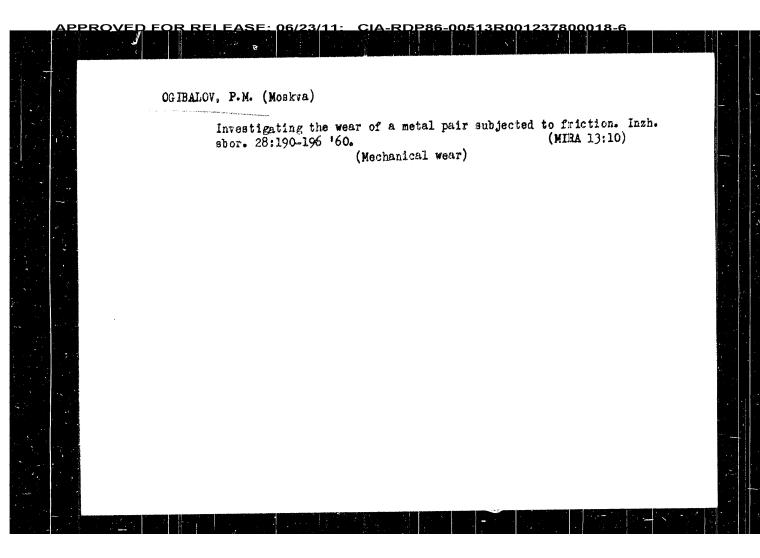
PERIODICAL: Akademiya nauk SSSR. Institut mekhaniki. Inzhenernyy

sbornik, v. 30, 1960, 106 - 111

TEXT: It is assumed that the inside surface of the hollow cylinder is covered homogeneously with a relatively thick layer of lubricant. The velocity of motion of the piston at a given moment is denoted by v, the thickness of the layer by  $\delta$  and the density of the lubricant by  $\rho=\gamma/g_{\circ}$  One can consider the lubricant as moving towards the piston with the velocity v and is reflected from the piston at a certain angle  $\phi_{\circ}$  One considers a cross-section I of the stream before reaching the piston and a section II, distant from the point of reflection, where the thickness is  $\delta_1$  and the velocity  $v_1(\text{Fig. 1})_{\circ}$  From the conservation of mass it follows that

Card 1/6

CGEBALOV, P.M. (Moskva); LOMAKIN, V.A. (Moskva) Mechanical properties of glass reinforced plastics. Inzh.sbor. 30:17-30 '60. (MJRA 13:10) 30:17-30 '60. (Class reinforced plastics--Testing)



Hardness of a thick ...

\$/508/60/\(\mathbf{e}\)28/000/010/022 D237/\(\mathbf{D}\)305

Expansion of Copper Bombardment by 19-Mev deuterons, Bull. Amer. Phys. Soc., vol. 29, no. 7, 1954; J.A.Brinkman, On the nature of radiation damage in metals, J. Appl. Phys., vol. 25, no. 961, 1954; J.C. Wielson, R.G. Berggren, Effects of neutron irradiation in steel, Pros. A.S.T.M., vol. 55, 1966, p. 689-707.

SUBMITTED: May 27, 1959

H

Card 6/6

27797

Hardness of a thick ...

S/508/60/028/000/010/022 D237/D305

and  $T = T(\alpha, \beta, z; p)$ . The problem of finding the value of  $p_*$ , for which flow occurs, i.e.  $\sigma_1 = \sigma_8$  at any point of the shell  $M^*$  ( $z = z_*$ ,  $\alpha = \alpha_*$ ,  $\beta = \beta_*$ ) is then stated and the solution when  $\frac{\partial N}{\partial \alpha} = \frac{\partial N}{\partial \beta} = 0$ , is

$$p_{*} = \frac{\sigma_{s}(N_{z_{*}})}{2\sqrt{3} G\sqrt{P} - 2z_{*} \overline{P}_{x} + z^{2} \overline{P}_{x}} . \tag{23}$$

For M on the surface z = ± h/2 the problem is solved by putting = 0. A hollow cylinder is considered next, whose inner and outer radii are a and b respectively, subject to radial outward directed radiation N, resulting in the inner pressure p. p is sought, for which a plastic deformation first occurs. G is assumed constant. There are 4 figures, and 14 references: 10 Soviet-bloc and 4 non-Soviet-bloc. The references to the English-language publications read as follows: Enyder, Foufeld, Disordering of Solids by Neutron Radiation, Phys. Rev., vol. 97, no. 1636, 1955; H. Kierstead, Card 5/6

27797

Hardhess of a thick ....

S/508/60/028/000/010/022 D237/D305

 $=+\frac{h}{2}$  where h = thickness of the shell, then for the layer z = const.

$$N_{z} = Ne^{-\frac{\lambda}{2}} + (\frac{\lambda}{2} - z)$$
 (14)

and by (7)

$$T = \sigma_{s}(N_{z}) - 3Ge_{z} = \sigma_{s}(Ne^{-\frac{h}{2} - z}) - 2\sqrt{3}G\sqrt{P_{e} - 2zP_{ex} + z^{2}P_{x}}$$
 (15)

Let p be a load parameter and

$$P_{\epsilon} = p^{2}\overline{P}_{\nu} P_{x} = p^{2}\overline{P}_{x\nu} P_{\epsilon x} = p^{2}\overline{P}_{\epsilon x}.$$
 (16)

Then

$$T = \sigma_{8}[Ne^{-\mu(\frac{h}{2}-z)}] - 2\sqrt{3}Gp\sqrt{P_{\epsilon}-2z\overline{P}_{ex}+z^{2}\overline{P}_{x}},$$

Card 4/6



27797

Hardness of a thick ...

\$/508/60/028/000/010/022 D237/D305

$$N_{r} = N \frac{\alpha}{r} e^{-\mu(r-\alpha)}$$
 (8)

and for the hollow sphere

$$N_{r} = N \frac{a^{2}}{r^{2}} e^{-\mu(r-a)}, \qquad (9)$$

Using the theory of elastic shells the author then obtains intensity of deformation  $\mathbf{e}_{\underline{i}}$  at the distance  $\mathbf{z}$  from the inner surface as

$$e_1 = \frac{2}{\sqrt{3}} \sqrt{P_e - 2zP_{gx} + z^2P_{x}},$$
 (12)

and stress intensity

$$\sigma_{i} = 3Ge_{i} \tag{13}$$

where P,  $P_{x}$ ,  $P_{\xi x}$  are known quadratic forms for  $\epsilon$  and x. If the stream N is incident from the direction in the inner surface z = Card 3/6

<u> APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6</u>

27797

Hardness of a thick .

\$/508/60/828/900/615/022 D237/D366

and is of the order of and where v effective nuclear cross section,  $\rho$  — density, A — atomic weight,  $A_{ij}$  — Avegadro's number,  $n_{o}$  — number of nuclei in 1 oc. If  $i_{o}$  is independent of time then

$$T = \tilde{x} \cdot \tilde{x} = T_0 = \text{te}^{-\mu \tilde{x}}, \tag{3}$$

It has been shown experimentally that on arradiation, the elasticity modulus change is 1.5  $\sim$  5 %, while hardness and critical stress values are affected to a greater degree. For a solid with a plane surface, the number of neutrops at the depth 2 in time t is

and hence  $\sigma_g = \sigma_g(z)$  and G = G(z). If it is assumed that G = G(nvt)  $\sigma_g = \sigma_g(nvt)$ , then

$$G = G(Ne^{-\varphi z}), \quad \sigma_{\alpha} = \sigma_{\alpha}(Ne^{-\varphi z}). \tag{7}$$

In the case of a cylindrical shell (6) becomes Card 2/6

W

S/508/60/028/000/0±0/022 D237/D305

21,2200

AUTHORS:

Il yushin, A.A., and Ogibalov, P.M. (Moscow)

TITLE:

Hardness of a thick walled sylundrical shell and a hollow sphere under the influence of radiation

The second secon

PERIODICAL:

Akademiya nauk SSSR. Otdel@niye tekhnicheskikh nauk. Inzhenernyy spornik, v. 28, 1960, 134 - 144

TEXT: Irradiated solids exhibit volume deformation 0 and changes in elastic and plastic properties. A neutron passing through a crystal lattice causes thermal or dislocation effects, and in case of neutron nucleus interaction produces fission. A homogeneous isotropic body occupying a semi space  $z \gg 0$  is considered. If the intensity of a normal neutron beam of z mean energy on z = 0 is 1 - 1 = 0 of then at z = 0 on z = 0.

$$I(z) = k_0 e^{-az} \alpha / ox^2 - sec.$$
 (1)

where Card 1/6

 $\mu = \sigma \sigma_{\sigma} + \sigma(A_{\sigma} \rho/A)$ 

LIN

\$/055/60/000/006/007/008 C111/C222

On the Calculation of Glass Plastics in the Plane State of Stress

The investigation shows that KA(T-B) can be understood as an elastic orthotropic body. Beside of the values given in the table the authors still give the following values for calculations:  $G_{12} = 20\ 700\ \text{kg/cm}^2$ ,  $V_{12} = 0.19$ . The values

 $y_{12} = 0.19$ . The value  $E_{45}$  in the table is the E-value for  $\varphi = 45^{\circ}$ 

There are 3 figures, 1 table and 4 Soviet references.

ASSOCIATION: Kafedra teorii uprugosti (Chair of Theory of Elasticity)

SUBMITTED: February 15, 1960

Card 5/6

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6

88416

S/055/60/000/006/007/008 C111/C222

On the Calculation of Glass Plastics in the Plane State of Stress

where

(6) 
$$a = \frac{E_2}{E_1}$$
,  $b = \frac{E_2}{G_{12}} - 2 y_{21}$ 

Furthermore

(9) 
$$\frac{G}{G_{12}} = \frac{1}{1 + \frac{1 + a - b}{b + 2 y_{21}} \sin^2 2 \varphi}$$

The figures 1,2,3 show these dependences (unbroken lines), where the mean experimental data are denoted by small circles.

(See card 6/6 for sketches 1-3)

Card 4/6

s/055/60/000/006/007/008 0111/0222

On the Calculation of Glass Plastics in the Plane State of Stress

Manager and a second se			
	h = 10mm	h = 6mm	mean value
$E_1(kg/cm^2)$	210 000	220 000	215 000
$E_2(kg/cm^2)$	120 000	125 000	122 500
$E_{45}(kg/cm^2)$	65 000	70 000	67 500
y <sub>21</sub>	0.12	0.10	0.11

For the E - modulus and the Poisson coefficient  $\nu$  for a stretching for the angle  $\phi$  to the  $x_1$ -axis, from the orthotropic theory there follow the expressions

(5) 
$$\frac{E}{E_1} = \frac{a}{a \cos^4 \varphi + b \sin^2 \varphi \cos^2 \varphi + \sin^4 \varphi}$$

$$\frac{y}{a \cos^4 \varphi + b \sin^2 \varphi \cos^2 \varphi + \sin^4 \varphi}$$
Card 3/6

Card 3/6

s/055/60/000/006/007/008 C111/C222

On the Calculation of Glass Plastics in the Plane State of Stress

(3) 
$$\varepsilon_1 = \frac{1}{E_1} (\delta_1 - \nu_{12} \delta_2), \quad \varepsilon_2 = \frac{1}{E_2} (\delta_2 - \nu_{21} \delta_1), \quad \chi_{12} = \frac{1}{G_{12}} \tau_{12}$$

 $\varepsilon_3 = -\frac{1}{E_3} \left( y_{31} \sigma_1 + y_{32} \sigma_2 \right)$ , where only four of the five constants appearing in (3) are independent since

(2) 
$$y_{12}E_2 = y_{21}E_1$$
,  $y_{23}E_3 = y_{32}E_2$ ,  $y_{31}E_1 = y_{13}E_3$ 

The authors report on the experimental examination of the correctness of the formulas (3) and their conclusions in the orthotropic theory for the KACT - B (KAST - V). They investigated foils of 6 and 10 mm for a step by step load (one step 100 kg). The determination of the constants yielded the values of the table

16.7300

AUTHORS: Lomakin, V.A., and Ogibalov, P.M.

s/055/60/000/006/007/008 C111/C222

On the Calculation of Glass Plastics in the Plane State of Stress TITLE:

Vestnik Moskovskogo universiteta. Seriya I. Matematika, PERIODICAL: mekhanika, 1960, No. 6, pp. 79 - 83

The authors consider an elastic orthotropic body; let the axes  $\mathbf{x}_{\mathbf{i}}$ TEXT: be the normals of the planes of the elastic symmetry; let 0' and  $\epsilon_i$ be the normal stresses and the corresponding elongations; let au ik be the tangential stresses and shifts. Let  $\mathbf{E}_{\mathbf{i}}$  be the normal moduli of elasticity in the directions  $x_i$ , let  $G_{jk}$  be the moduli of shear in the planes  $(x_j, x_k)$ ,  $y_{jk}$  be the Poisson coefficients for a contraction in the direction  $\mathbf{x}_k$  for a stretching in the direction  $\mathbf{x}_j$ . Then in the plane state of stress it holds:  $6_3 = 7_{23} = 7_{31} = 7_{23} = 7_{31} = 7_$ 

Card 1/6

Elastic-Plastic Deformations of (Cont.)

SOV/5455

effects, the theory of the boundary layer during thermal shock, and the action of repeated thermal pulses on a shick-walled cylinder. Solutions of some other problems conserning the strength of thick-walled cylinders are also give. The authors thank the coworkers of the Department of the Theory of Elasticity of the Moscow State University, I.M. Tyuneyeva and S. A. Orlova. There are 71 references: 58 Soviet (including 5 translations from English and 1 translation from German), 7 English, 3 German, 2 Polish, and 1 French.

TABLE OF CONTENTS:

Freface

Ľ.

Ch. I. Basic Relationships and Theorems in the Theory of Elastic-Plastic Deformations
1. Relationship between stresses and deformation

7 10

OGIBALOV, PM.

PHASE I BOOK EXPLOITATION SOV/5455

Il'yushin, Aleksey Antonovich, and Petr Matveyevich Ogibalov

Uprugo-plasticheskiye deformatsii polykh tsilindrov (Elastic-Plastic Deformations of Hollow Cylinders) [Moscow] Izd-ve Mosk. univ., 1960. 224 p. Errata slip inserted. 4,000 copies printed.

Ed.: S. F. Kondrashkova; Tech. Ed.: M. S. Yermakov.

PURPOSE: This book is intended for scientists and engineers, and for advanced students and aspirants concerned with problems in structural mechanics.

COVERAGE: The book is primarily concerned with various effects and possible methods of strengthening thick-walled cylinders. Methods involving strengthening through elastic-plastic autofrettage, nonuniformity of the material, nonuniform heating through the thickness, the action of high pressure and exposure to penetrating radiation are considered. Attention is given to problems pertaining to repeated loads and dynamic Card 1/5

S/179/59/000/05/015/029

Action of High Pressure in Strengthening a Hollow Cylinder

where p is the internal pressure under which flow begins at the internal surface of the cylinder. Using the linear in the case of the hollow cylinder; namerical (b = external radius of the tube, a = internal radius)

Sand 5 = 0.3, leads to the value 7 = 2.27. The substantial.

Catd Strengthening effect in this case is therefore

There are 1 table and 2 Soviet references.

SUBMITTED: June 29, 1959

68465 12 72 3 \$/179/59/000/06/015/029 E081/E141 AUTHORS: Il'yushin, A.A., and Ogibalov, P.M. (Moscow) Action of High Pressure in Strengthening a Hollow TITLE: Cylinder PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Mekhanika i mashinestroyeniye, 1959, Nr 6, pp 110-112 (USSR) ABSTRACT: The flow limit ( $\mathbb{D}_{S}$ ) for metals under hydrostatic pressure The flow 1...

( $\sigma$ ) is given by  $\varphi_s = \forall_0 S(\sigma)$ (1)where  $\mathbf{r}_0$  is the flow limit in shear when  $\mathbf{\sigma}=\mathbf{0}$ . Assaming a linear approximation, the function S(o) can be written (5 > 0) $S(\sigma) = 1 - \delta(\sigma/\eta)$ The solution of Lamé's problem where & is a constant. for a tube under the influence of internal pressure leads to expression (3) for the hydrostatic pressure and for the maximum shear stress. The strengthening coefficient is defined as the ratio Card g ( 6) 040(9) (6)170 b2 + 0a2  $(p)_{\delta = 0}$ 

Large Elastic - Plastic Symmetric Deformations of a Thick-Walled Tube

SOV/155-59-1-17/30

where

(1.9) 
$$S_a = a + w(a)$$
,  $S_b = b + w(b)$ 

a and b are the inner and outer radii and w(r) are the radial shifts. The obtained system of equilibrium is solved explicitly under consideration of corresponding boundary conditions. The author investigates especially plane finite deformations and the question concerning the maximal rigidity. The obtained results are more real than the results of the theory of small deformations (no infinitely increasing inner pressure!).

There are 5 references, 4 of which are Soviet, and 1 American.

ASSOCIATION: Moskovskiy gosudarstvennyy universitet imeni M.V. Lomonosova (Moscow State University imeni M.V. Lomonosov)

SUBMITTED: December 18, 1953

16(1) 1617300

sov/155-59-1-17/30

AUTHOR:

Ogibalov, P.M.

TITLE:

Large Elastic - Plastic Symmetric Deformations of a Thick-

Walled Tube

PERIODICAL:

Nauchnyy doklady vysshey shkoly. Fiziko-matematicheskiye nauki, 1959, Nr 1, pp 110-116 (USSR)

ABSTRACT:

The author considers a thick-walled tube under the influence of inner and outer pressure and of an axial force P. He uses the logarithmic deformations and the usual relations between tensions  $\sigma_{\xi}$ ,  $\sigma_{\psi}$ , and the corresponding deformations,

since the orientation of the principal axes does not change during the deformation. Because of the assumption of large deformations the conditions of equilibrium have to be set up

in the form

in the form

(1.7) 
$$\frac{d \delta' g}{d g} + \frac{5' g - 6' g}{g} = 0$$
(1.8) 
$$P = 2\pi' \int_{Sa} \delta'_{x} g d g,$$

$$(1.8) \qquad P = 2\pi \int_{a}^{b} \sigma_{x} \, g \, d \, g \, ,$$

41

Card 1/2

SOV/24-58-12-13/27

The Plastic Deformation of a Thick-Walled Tube Under the Action of Heat Impulses and Pressure

the duration of the heat impulse and  $Q_{\rm O}$  is the mean flow of heat from the gas to the tube. For a steel tube, the equations reduce to  $\delta = 5.45 \sqrt{T}$  mm (T in seconds),  $V = 3620 Q_0 \sqrt{T} \text{ deg.} (Q_0 \text{ in k cal/cm}^2 \text{sec}),$ or, for T = 0.01, s = 0.54 mm and for  $Q_0 = 2$ ,  $V_0 = 724$ °C. On the basis of these estimates, it is shown that in the heating period, the axial and tangential strains, which are predominantly of thermal origin, are compressive and are of the order of 1%, whereas in the cooling period, the strains are tensile and are also of the order of 1%. In each case, the strains are above the respective plastic limits and, on subjecting the tube to repeated thermal

and pressure cycles, it may fail by fatigue. SUBMITTED: 24th September 1957.

SOV/24-58-12-13/27

AUTHOR:

Il'yushin, A.A.,

Ogibalov, P.M.

(Moscow)

TITIE:

The Plastic Deformation of a Thick-Walled Tube Under

the Action of Heat Impulses and Pressure (O plasticheskikh deformatsiyakh tolstostennoy truby pod deystviyem

teplovykh impulisov i davleniya)

PERIODICAL: Izvestiya Akademii Nauk, Otdeleniye Tekhnicheskikh Nauk, 1958, Nr. 12, pp 85-89 (USSR)

ABSTRACT:

When a tube is subjected internally to impulses of heat and pressure, for example, from a jet of hot gas, a thin layer of the material adjacent to the inner

surface of the tube will be heated and cooled. Approximate consideration of the basic heat conduction

equation shows that the thickness  $(\delta)$  and the maximum temperature (Vo) of the layer will be of the order of

 $\delta = \sqrt{\frac{2\lambda T}{GY}}$ ,  $V_0 = Q_0 \sqrt{\frac{2T}{GY}}$ (8)

Card 1/2

where  $\lambda$  is the thermal conductivity, c the heat capacity and  $\gamma$  the density of the tube material, T

Testing of Thick-walled Tubes Under High Internal Pressures of Short Duration

10-15 repeated loadings at a pressure exceeding 20-25% of that causing an initial residual external strain of 0.4 - 0.6%.

There are 9 figures, 1 table and 3 Soviet references.

SUBMITTED: September 24, 1957

AUTHORI Ogibalov, P.M. (Moscow) 1501/24-58-9-24/31

TITLE:

Testing of Thick-walled Tubes Under High Internal Pressures of Short Duration (Ispytaniya tolstostennykh trub pri

kratkovremennykh vysokikh vnutrennikh davleniyakh)

PERIODICAL:

Izvestiya Akademii Nauk SSSR, Otdeleniye Tekhnicheskikh

Nauk, 1958, Nr 9, pp 134 - 139 (USSR)

ABSTRACT: The paper is a continuation of the author's earlier work (Refs 2, 3). Detailed drawings are given of a pneumatic apparatus, based on that of Il'yushin (Ref 1) for subjecting a thick-walled tube to controlled internal pressures up to 20 000 atm for periods of up to

10<sup>-3</sup> sec, with provision for measuring the external diameter of the tube. Tests were carried out on steel tubes of 260 mm length, 45-65 mm external diameter and ratio of external to internal diameter of about 2:1. Stress-strain curves are given and also a table showing the residual radial strain as a function of pressure and number of loadings. Rupture resulted as a rule after

Card 1/2

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6

Bending, Stability and Vibrations of Plates

1084

under every possible condition : bending and loss of stability, elasticity, plastic deformations, and vibrations. This book is concerned mainly with the mechanical aspects of the problem. Numerical calculations are carried out and new methods of solutions are investigated. In preparing this book the author used lectures which he gave during the past seven years at the Moscow State University, Faculty of Mechanics and Mathematics. Basic textbooks, monographs, and current journals (mainly Soviet) in this field were also used. The author gives recognition to professors A.S. Il'yushin and Yu.N. Rabotnov, Corresponding Members of the Academy of Sciences of the USSR, professors N.I. Bezukhov, G.Yu. Dzhanelidze, B.G. Korenev, M.G. Slobodyanskiy, Docent I.A. Skoryy, I.M. Tyuneyev (the author's faculty assoclate in the theory of elasticity at Moscow University), and S.A. Orlov for their participation in the compilation of this book. The introduction consists of a short review of contributions to the theory of plates and methods of calculation. The outstanding scientists (both Soviet and other) who have contributed to this field are listed along with their contributions and works. There are 156 references, of which 108 are Soviet, 23 English, 20 German, 5 French.

## PHASE I BOOK EXPLOITATION 1084

Ogibalov, Petr Matveyevich

Izgib, ustoychivost' i kolebaniya plastinok (Bending, Stability and Vibrations of Plates) [Moscow] Izd-vo Moskovskogo univ-ta, 1958. 389 p. 5,000 copies printed.

Sponsoring Agency: Moscow. Universitet.

Ed.: Skoryy, I.A.; Ed. of Publishing House: Kondrashkova, S.F.; Tech. Ed.: Mulin, Ye.V.

PURPOSE: This book is intended as a textbook for university students specializing in the theory of elasticity and plasticity. It may also prove useful to students and graduate students at technical institutes of higher learning and to engineers engaged in planning and calculating laminated elements widely used in the various branches of modern technology.

COVERAGE: The author throws light on present-day problems in the theory and calculation of isotropic and anisotropic thin plates

Card 1/9

A New Compressed Air Quick Blow Mechanism. 3 hypotheses. 1) The occurence of air expansion takes place adiabatically 2) The friction of the mallet during motion was not taken under consideration. 3) The gas escape through the slot was also not considered. The dependence of pressure behind the mallet on its position in the pipe is calculated, as well as the dependence of the velocity of motion of the mallet on its position in the pipe, and also themaximal acceleration of the mallet during the blow(overload-coefficient). Finally the manner in which the machine operates is desribed. (With 18 illustrations and 6 Slavic references). ASSOCIATION PRESENTED BY SUBMITTED 7.11.1956. AVAILBLE Library of Congress. Card 2/2

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6

AUTHOR

TITLE

IL'YUSHIN, A.A., OGIBALOV, P.M., (Moscow),

PA - 3073

A New Compressed Air Quick Blow Mechanism.

(Novyy pnevmatichekiy skorostnoy koper - Russian)

PERIODICAL Izvestiia Akad. Nauk SSSR, Otdel. Tekhn., 1957, Vol 21, Nr 3,

pp 57-65, (U.S.S.R.)

Received 6/1957

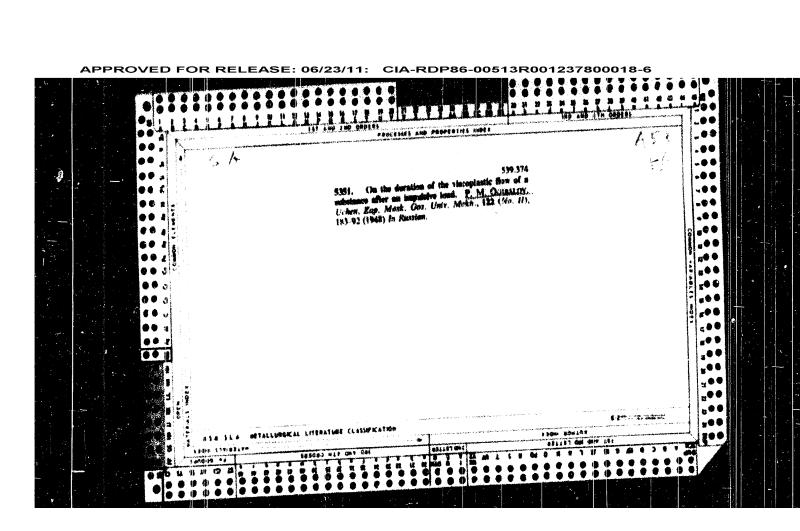
Reviewed 7/1957

ABSTRACT

The new PSK-3 rapid experimental engine is described. It was developed and built in the laboratory for material-festing of the Moscow State University. It is intended for dynamic tests and has higher characteristic values than its forerunners, the PSK-1 and PSK-2. The reconed striking velocity amounts to 3xlo m/sec and the striking energy over 3.5xlo4 mkg. The principle diagrams and a describtion of the construction are given. A thick walled cylinder serves as a frame and it is further strengthened by ribs. At the end of it is a compressed air block which consists of a thick walled pipe and which is rigidly fixed to a pressure tank. A starting mechanism is also mounted on it. On the other end is a massively heavy "swimming" anvil which serves in propping up the model under investigation and which is also capable of taking the reaction of the blow. The frame absorbs the recoil of the anvil by means of an oil shock absorber. The reaction of the starting and braking of the mallet is absorbed by the frame, hence the machine needs no special bases. One of the most complicated parts worked out as a slide which in the last position excludes the admission of compressed air. The jointing is taken care of with chloryynil "collars". The calculation of the dynamic characteristics was made under

Card 1/2

OGEBAIOV, P.M. (MOSCOW) Effect of internal pressure and varying temperature on the deformation of pipes. Inzh. sbor. 20'55-58 '54. (MIRA 8:7) (Pipe) (Deformations (Mechanics))



OGHINA, V.

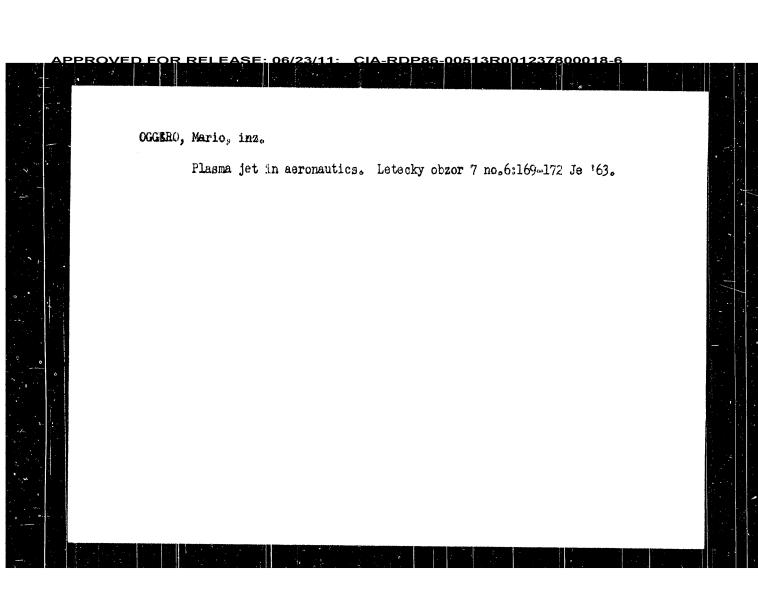
Decoppering pyrite ashes in order to extract copper and obtain iron ore of high quality. p. 70.

METALURGIA SI CONSTRUCTIA DE MASINI

Vol. 8, no. 1, Jan. 1956

Rumania

Source: EAST EUROFEAN LISTS Vol. 5, no. 10 Oct. 1956



Country : USSR
Category : Soil Science. Fertilizers. General. J

Abs Jour : RZhBiol., No 6, 1959, No 24634

Author : Inst : Title :

Orig Pub :

Abstract : green peas is of local importance. For potatoes and sugar beets, this method of P and K application is of no significance. -- O. P. Medvedeva

PPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6

Country

: USSR

Category

Soil Science. Fertilizers. General.

J

Abs Jour

: RZhBiol., No 6, 1959, No 24634

Author

Inst

;

Title

Abstract

the following are widely used: Na, Naa + CaCO<sub>3</sub> (calcium ammonium nitrate), Ns, (MH4)2PO4 and nitrophosphate. 60 percent of fertilizers are manufactured in Great Britain in the form of compounds. 90 percent of the compound and 50 percent of all fertilizers are manufactured in the form of granules. The tendency to increase the manufacture of concentrated fertilizers is characteristic. The most effective method of introducing P and K under grain, vegetables and

Card

: 3/4

Country USSR Soil Science. Fertilizers. General. Category J RZhBiol., No 6, 1959, No 24634 Abs Jour Author Inst Title Orig Pub Abstract under potatoes and sugar beets. Perennial grasses (meadow and pasture) are fertilized inadequately, and in the majority of the regions of the land are not fertilized at all. At the present time, about 50 percent of phosphoric fertilizers are applied in the form of the trivalent Ps; 25 percent, in the form of Thomas slag; 10 percent, in the form of phosphoric meal. Among the nitrogen fertilizers Card : 2/4

Country

USSR

Category

Soil Science. Fertilizers. General.

J

Abs Jour

RZhBiol., No 6, 1959, No 24634

Author

Ogg, U. G.

Inst

Title

The Application of Fertilizers in England.

Orig Pub

Vestn. s.-kh. nauki, 1958, No. 2, 127-130

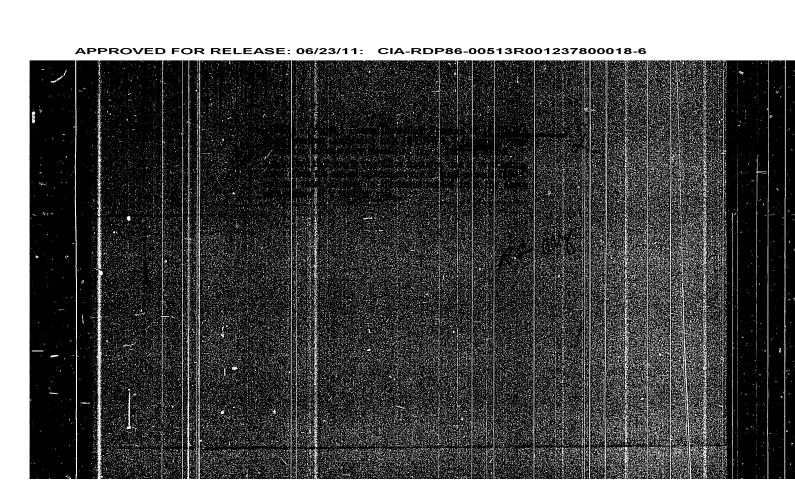
Abstract

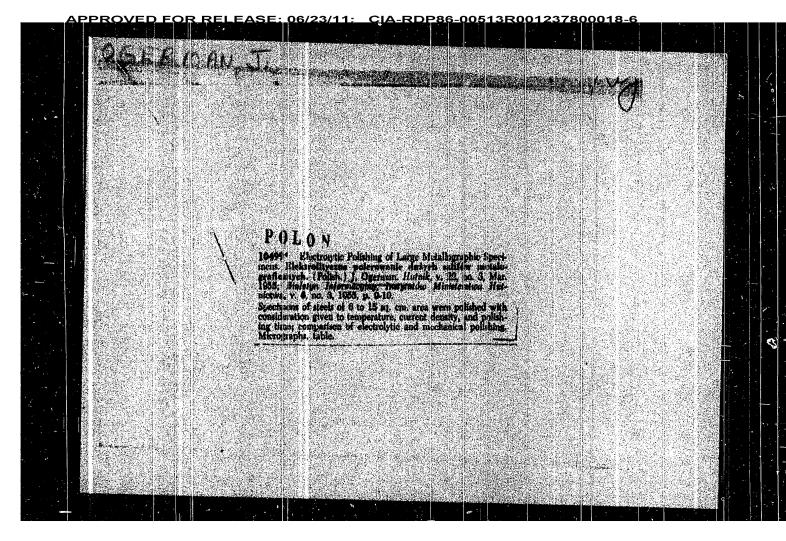
For the period of the years 1913-1916, the consumption of mineral fertilizers in Great Britain was greatly increased: N, 10 times; P<sub>2</sub>O<sub>5</sub>, twice, and K<sub>2</sub>O<sub>5</sub>, 13 times. In 1956, 4 million tons of fertilizers were applied to the soil. More than 20 kg of N and K20 and 36 kg of P205 are introduced per one ha of the land's cultivated area. The greatest quantity of the mineral fertilizers is appled

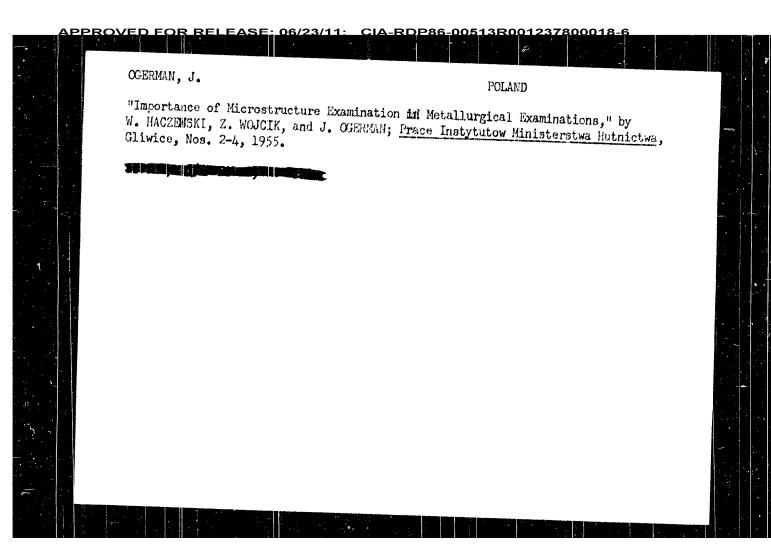
Card

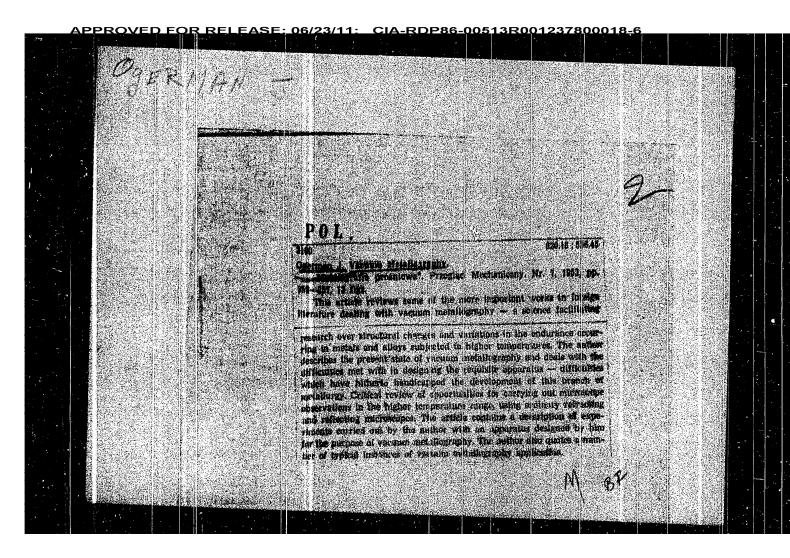
: 1/4

OGERMAN, Jerzy Jerzy Ogerman, "Korngrenzenschaedigung eines CrNiW-Stahles durch Ueberhitzen," Bergakademie (Berlin), 10/1, Jenuary 1958, pp. 28-30. Damage to Grain Boundaries of a Cr Ni W Steel Due to Overheating The author is affiliated with the Gliwice Polytechnic Institute. This paper was presented at the 2nd Student Comloquium on Metal Physics and Metal Technology in Freiberg, 20-22 June 1957.









OTENGENDEN, N.Ye., SERGIYENKO, S.F. Service life of coal mine suction pumps. Sbor.DonUGI no.22: 97-103 '61. (MIRA 15:6) (Hydraulic mining--Equipment and supplies) (Pumping machinery)

T/EWP(t)/ETI IJP(c) JD

ACC NR.

AP6024602

SOURCE CODE: RU/0017/65/COO/009/0480/0483

AUTHOR: Niculescu, Gr. (Engineer); Ogea, M. (Engineer); Nita, D. (Engineer)

ORG: [Niculescu; Orea] Technological Research Institute for Machine Building (Institutul de Cercetari Tehnologice Pentru Constructii de Masini); [Nita] Factory of Aggregates and Machine-Tools, Bucharest, (Fabrica de Masini-Unelte si Agregate)

TITLE: Studies on the induction hardening of cast iron guides for machine-tool frames

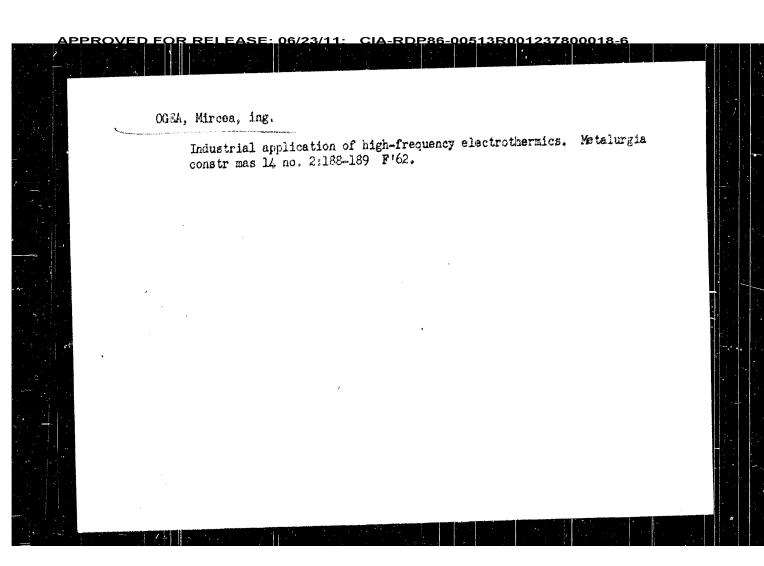
SOURCE: Metalurgia, no. 9, 1965, 480-483

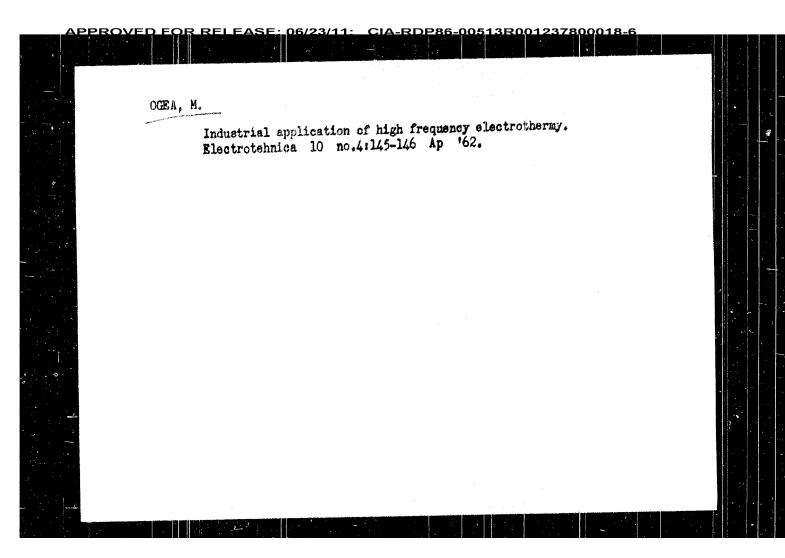
TOPIC TACS: cast iron, induction hardening, machine tool

ARSTRACT: Experimental studies reported by the authors show that very similar results are obtained with medium-frequency (8 kilocycles per second) or highfrequency (250 kc/sec) induction currents, with the muides having similar depths of hardened layers, hardness of essentially the same degree, and similar martensitic structures in the upper layers. Orig. art. has: 9 figures and 3 tables. [Based on authors Eng. abst.] [JPRS: 33,732]

SUB CODE: 13, 11 / SUBM DATE: none / ORIG REF: 001 / SOV REF: 002

Card 1/1 B1-G





RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6 OGDANETS, Z. Problems of issuing credit to state farms. Den.i kred. 21 no.1:55-58 Ja '63. (MIRA 16:2) 1. Nachal'nik otdela kreditovaniya i finansirovaniya sel'skogo khozyaystva Donetskoy oblastnoy kontory Gosbanka. (Donetsk Province-State farms-Finance)

OCLANETS, B.M., KHOTINSKAYA, Ye.Ye.; CGDANETS, N.D., ALENICH, Ye.M. Yellow pigments from aminophenylimides of naphthalic acid. Uch.zep. KHOU 71:253-254 '56. (KLRA 10:8) (Pigments) (Naghthalic acid)

On the magnetic properties of the Eu nucleus. Inst fiz jadr report no.359:1-8 Ag \*64. BOCHNACKI, Z.; OGAZA, S. 1. Institute of Nuclear Physics, Krakow.

OGAZA, Stanislav Magnetic properties of strongly deformed nuclei. Inst fiz jadr report no.362:1-52 '64. 1. Institute of Nuclear Physics, Krakow, of the Polish Academy of Sciences.

BOCHNACKI, Z.; OGAÇA, S. Spin polarization effect and magnetic moments of odd-A deformed nuclei. Inst fiz jadr report no.351:1-14 '64. 1. Institute of Muclear Physics, Krakow, of the Folish Academy of Sciences.

BOZEK, E.; HRYNKIFWICZ, A.Z.; OGAZA, S.; STYCZEN, J. Magnetic interaction of the 155 Gd nucleus in the 87 keV excited state with the electronic shell. Inst fiz jadr report no.299:1-10 '63. 1. Instytut Fizyki Jadrowej, Krakow.

BOZEK, E.; LEBEDEV, N.A.; NIEWODNICZANSKI, H.; OGAZA, S.; RYBICKA, M.; STYCZKN, J. Gemma-gamma directional correlations in 146Eu. Lota physica Pol. 24 no.1:131-133 J1:63. 1. Institute of Nuclear Physics, Krakow. 2. Joint Institute for Nuclear Research, Dubma, USSR (for Lebedev).

<u> APPROVED FOR RELEASE; 06/23/11; CIA-RDP86-00513R001237800018-6</u>

S/058/62/000/008/021/134 A061/A101

AUTHORS:

Božek, E., Hrynkiewicz, A. Z., Konieczna, Z., Ogaza, S.,

Rybicka, M., Szymczyk, S.

TITLE:

Attenuation of the angular correlation of the Ta<sup>181</sup> 133 - 482 keV

 $\gamma$  -cascade in liquid sources

PERIODICAL:

Referativnyy zhurnal, Fizika, no. 8, 1962, 42, abstract 8B301

(Rept. Inst. fizyki jądrow. Krakowie, 1962, no. 155, 8pp. illust.,

English; summaries in Polish and Russian)

TEXT: The time dependence of the anisotropy of the angular correlation of the Ta  $^{181}$   $^{182}$  kev  $_{7}$  -cascade was investigated. The measurements were conducted with a liquid Hf source (Hf(OH)  $_{\rm h}$  solution in concentrated sulfuric acid) at various temperatures (10, 30, 60, and 80°C). For all of the four temperatures the attenuation of anisotropy in time followed an exponential law; the  $\lambda_2$  attenuation constants were determined for all the temperatures. The temperature dependence of  $\lambda_2$ , established experimentally, was compared with the theoretical one. At a temperature increase the experimental  $\lambda_2$  dropped more slowly, than was required by the theory. [Abstracter's note: Complete translation] Card 1/1

BOZEK, E.: HRYNKIEWICZ, A.Z.; KONIECZNA, Z.; CGA7A, S.; RYBICKA, M.; SZYMCZYK, S.

The attenuation of the angular correlation of the <sup>181</sup>Ta 133-482 KeV cascade in liquids. Inst fiz jadr report no.155:1-9 Ja '62.

1. Institute of Nuclear Physics, Krakow, of the Polish Academy of Sciences.

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001237800018-6

Energy levels...

P/045/61/020/003/004/004 B133/B228

T. Walczak for assistance in measurements. There are 6 figures, 3 tables, and 7 references: 4 Soviet-bloc. The 3 references to English-language publications read as follows: Ref. 1: Mihelich, J. W., Harmatz, B., Handley, T. H., Phys. Rev., 108 989 (1957); Ref. 2: Jacob, K. B., Mihelich, J. W., Harmatz, B., Handley, T. H., Bull. Am. Phys. Soc., 3, 358 (1958). Ref. 6: Boskma, P. De Waard, H., Nuclear Phys., 12, 533 (1959).

ASSOCIATION: Institute of Nuclear Physics, Cracow; Joint Institute for

Nuclear Research, Dubna (Yu. V. Nerseyev)

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Energy levels...

P/045/61/020/003/004/004 B133/B228

Baranovskii, W. I., Pokrovskii, W. N., Izv. Akad. Nauk SSSR, 23, 819 (1959)]. Besides a confirmation of the results of [6] (see list of English references), the authors obtained the following coincidences: between the 710-kev line and the 460-, 710, 790-kev peaks; between the 790-kev line and the 185-, 460-, 710-kev peaks; between the 1180-kev line and the 880-kev peak; between the 1270-kev line and the 185- and 600-kev peaks, and between the 2070-key line and the 80- and 185-key photopeaks. On the basis of these experiments and the energy values of transitions given by Gromov et al., the authors suggest a new level scheme for 166Er from the decay of 166 Tm (Fig. 6). The branching ratios of transitions between the levels with K=2 and K=0 are calculated on the strength of Alaga's theory. For the level scheme proposed by the authors, they are in better agreement with the experimental values than for the scheme given in [6]. The present proposal of the level scheme for Er needs some more confirmation. To get this, the authors are starting now gamma-gamma directional correlation experiments in order to obtain definite values of spins for the 788-, 862-, 957-, and 2140-kev levels. The authors thank S. Chojnacki and I. A. Yutlandov for the preparation of sources, and K. Malinowski and

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Energy levels ...

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it was established that the coincidence measurements for 166 Yb may be carried out in the first week of measurements. In the next two runs, gamma-gamma coincidence measurements were performed. The single-count gamma spectrum was recorded by a scintillation spectrometer using a 1 1/2" x 1" NaI (T1) crystal, an EMI 6097 F photomultiplier and a 100-channel pulse-height analyzer. The resolution of this spectrometer for the 661-kev 137 cs line was 8.2%. The gamma-gamma coincidence spectra were recorded on the multichannel pulse-height analyzer, gating the spectrum from one counter with coincidence pulses from a fast-slow coincidence circuit (Fig. 1). NaI (T1) crystals !  $3/4" \times 2"$  and  $2" \times 2"$  and EMI 6097 F photomultipliers were used. Resolution was 9% for the 137 Cs The resolution time of the coincidence circuit was 27=5.5x10-8 sec. The existence of an 880-kev transition reported up to now only by Brabec et al. [Ref. 4: Branec, W., Gromov, K., Dzhelepow, B. S., Dmitriev, A. G., Morozov, W. A., Izv. Akad. Nauk SSSR, 23, 812 (1959)] is confirmed by the coincidence measurements of the authors, but they could not find the 153and 522-kev lines measured by BaranovskiY and PokrovskiY [Ref. 5:

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P/045/61/020/003/004/004 B133/B228

AUTHORS:

Božek, E., Niewodniczański, H., Ogaza, S., Szymczyk, S.,

and Norseyev, Yu. V.

TITLE:

Energy levels in the 166 Er nucleus

PERIODICAL: Acta Physica Polonica, v. 20, no. 3, 1961, 257-266

TEXT: In the present paper, some gamma-gamma coincidence experiments in the decay of 166 Yb are described, and a level scheme of 166 Er is proposed, which is more complete than that given by Gromov et al. [Ref. 7: Gromov, K. I., Dzhelepov, B. S., Pokrovskiy, V. N., Izv. Akad. Nauk SSSR, 23, 821 (1959)]. The isotopes of Yb were obtained by irradiation of Ta targets with 660-Mev protons from the synchrocyclotron of the Dubna Joint Institute of Nuclear Research (USSR). The measurements in Cracow were begun 1.5 to 3 days after the irradiations, which were performed in intervals of about two months. In the first two runs, the measurements of gamma radiation were made at different times for the decay analysis of the entire spectrum of the isotope mixture of ytterbium. From this analysis

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MOLICKA-HANIAWETZ, Anna, mgr inz.; OGAZA, Henryk, mgr inz. Possibilities of applying collective flotation of zinc-lesd ores. Rudy i metale 6 no.8:352-355 Ag \*61. OGAY, Ye.A. Nervous system disorders in children with subtoxic and toxic diphtheria. Zdravookhr. Kazakh. 23 no.1:45-47 '63 (MIRA 17:2) l. Iz kafedry detskikh infektsionnykh bolezney ( zav. - prof. T.N. Nikonova) Kazakhskogo meditsinskogo instituta. NIKONOVA, T.N., kandidat meditsinskikh nauk; OGAY, Ye.A., student VI kurse;

IAZARIDI, O.I., student VI kursa

Capillaroscopic changes in children in scarlet fever and diphtheria.

Zdrav.Kazakh. 16 no.9:31-34 \*56. (MERA 10:1)

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(SCARIET FEVER) (DIPHTHERIA) (CAPILLARIES)

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