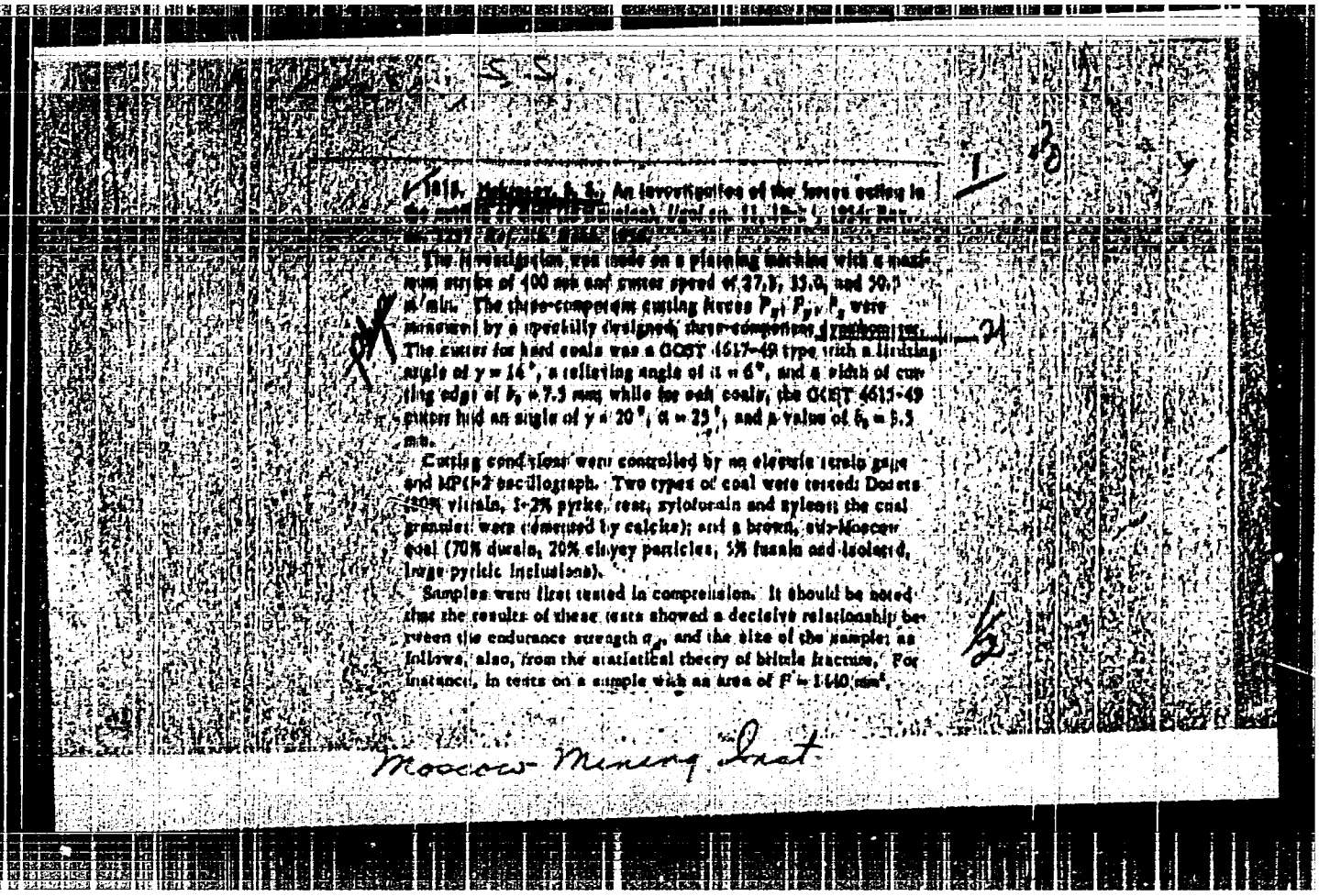


[illegible], February 6-8, An investigation of the forces acting in the [illegible]

The investigation was made on a planing machine with a maximum stroke of 400 mm and cutter speed of 27.9, 33.6, and 50.1 m/min. The three-component cutting forces P_z, P_y, P_x were measured by a specially designed, three-component [illegible]. The cutter for hard coals was a GOST 4617-49 type with a limiting angle of $\gamma = 14°$, a relieving angle of $\alpha = 6°$, and a width of cutting edge of $b_0 = 7.5$ mm; while for soft coals, the GOST 4617-49 cutter had an angle of $\gamma = 20°$, $\alpha = 25°$, and a b_0 value of $b_0 = 5.5$ mm.

Cutting conditions were controlled by an electric strain gage and MPO-2 oscillograph. Two types of coal were tested: Donets (80% vitrain, 1-2% pyrite, rest, xylotrain and xylem; the coal granules were cemented by calcite); and a brown, sub-Moscow coal (70% durain, 20% clayey particles, 5% fusain and isolated, large pyritic inclusions).

Samples were first tested in compression. It should be noted that the results of these tests showed a decisive relationship between the endurance strength σ_p, and the size of the sample; as follows, also, from the statistical theory of brittle fracture. For instance, in tests on a sample with an area of $F = 1440$ mm^2,

Moscow Mining Inst

Ne Kra/30/1,5,55

σ_g = 2.5 kg/mm², but with F = 100 mm², σ_g = 5.4 kg/mm².

(1) Depth of cut a. The test data showed good agreement with the author's theoretical calculation by the formula

$$P_{z\,max} = k a_{d\,max}^{n}$$

(k = 7, n = 0.17 for cutter GOST 4617-19, and k = 4, n = 1 for cutter GOST 4615-19 and GOST 4616-49). No derivation of this formula is, however, given in the article.

(2) Cutter setting angle. The experiments showed that with increase of the setting angle from 0° to 45°, the component $P_{z\,max}$ decreases, while $P_{y\,max}$ and $P_{x\,max}$ increase.

(3) Cutting angle β. With increased cutting angle for Donets coal from 60° to 90°, the components $P_{z\,max}$ and $P_{y\,max}$ increase by about 30%.

(4) Cutter wear. For very blunt cutters, $P_{z\,max}$ is about twice that for sharp-ground cutters.

(5) Cutting speed. The experiments showed that this has practically no influence on $P_{z\,max}$.

(6) Pyrite inclusions materially influenced the maximum values of the cutting forces. This aspect has not been fully investigated.

(7) Weathering markedly decreased the mechanical strength and cutting force for sub-Moscow coal.

Courtesy of Referativnyi Zhurnal G. S. Shapiro, USSR

Translation, courtesy Ministry of Supply, England

415. Nekrasov, S. S., Possibility of using the contact problem of the theory of elasticity for determining the distribution character of the load on the front edge of a cutting tool (in Russian), *Nauch. zap. kafedry tekhn. distsiplin Mosk. finans. in-ta*, Moscow, 50-53, 1955; *Ref. Zh. Mekh.* 1956, Rev. 5544.

A solution of the problem whether or not it is possible to apply I. Ya. Shtaerman's solution of the plane contact problem of the theory of elasticity for a die with rounded edges to the calculation of the pressure over the front edge of the cutting tool. For this purpose it is necessary to estimate the maximum error occuring when the action of one half of the semi-space on the other is disregarded. Author obtains this estimate by replacing the true curve of pressures under the die by a simplified trapezoidal one, which joins by a straight line the points having ordinates of q_{min}, q_{max}. The ordinates of this curve deliberately exceed the ordinates of the true curve. By this means author obtains an estimate of the error not exceeding 12.5% (at $\mu = 0.25$), and concludes from this that, in practice, I. Ya. Shtaerman's solution can be used.

Courtesy Referativnyi Zhurnal N. A. Rostovtsev, USSR

Translation, courtesy Ministry of Supply, England

124-57-1-9[illegible]

Translation from: Referativnyy zhurnal Mekhanika [illegible] No. [illegible] USSR

AUTHOR: Nekrasov S S

TITLE: Elements of a Theory of the Resistance Against Cutting Offered by Brittle Materials (Elementy teorii soprotivleniya khrupkikh materialov rezaniyu)

PERIODICAL: Nauch. tr. po ospr. gorn. dela Mosk. gorn. [illegible] 1956 No. [illegible] pp 63-93

ABSTRACT: Relative to the determination of the maximal value of the principal component of the cutting force C the author proposes the generalization of I. Ya. Shtayerman's formula for the indentation produced by an axial force acting on a forging die with rounded edges onto an elastic semiplane [Shtayerman, I. Ya. Kontaktnaya zadacha teorii uprugosti (The Contact Problem in Elasticity Theory) Gostekhizdat 1949]. Therein it is assumed that the law governing the distribution of the contact pressure along the forward cutting edge of the die is one-half of the symmetrical pressure curve over the contact surface of the die and the semiplane (the substantiation of this proposition on pp 65-68 does not strike the reviewer as very convincing). The author thus obtains formula (8) which connects the cutting force C

Card 1/2

Elements of a Theory of the Resistance Against Cutting Offered by Brittle [illegible]

and the maximal pressure p over the contact area. In order to obtain p the author suggests the employment of Prandtl's equation on the compression of a symmetrical obtuse wedge [ref. e.g. to Il'yushin, A.A. Plastichnost' (Plasticity) Gostekhizdat, 1948] generalized to include the case of the compress on of a nonsymmetrical wedge. This generalization is incorrect. The pressure must be constant over the contact area since the field of the slippage lines over the contact area consists of two families of straight lines. Instead of that the author obtains for point A of the contact area (Fig. 4) a pressure $p_A = \sigma_s$, and for point B a pressure $p_B = 4.2\sigma_s$. From the theorem on the limit equilibrium, which yields a quantitative appraisal of the upper carrying capacity, it is easy to see that the pressure must be $p = \sigma_s$ over the entire contact surface. The theoretical concepts expounded in the paper are stated vaguely and appear objectionable. For example, it is hardly permissible to apply to brittle materials, such as coal, the de Saint-Venant criterion of plasticity, the Coulomb-Mohr hypothesis appears more closely distributable here. The reviewer fails to comprehend the concepts referring to a crammed cutting phenomenon.

[illegible]--Elasticity--Bibliography [illegible]--Plasticity--Bibliography G.S. Shapiro
--Theory [illegible]--Theory

Card 2/2

NEKRASOV, S.S., dotsent, kandidat tekhnicheskikh nauk.

Effect of rock pressure on stress in cutting brittle. Nauch.trudy MGI no.16:283-290 '55 [cover '56]. (MLRA 10:4)
(Mining machinery) (Mechanics, Analytic)

AID P - 4483

Subject : USSR/Engineering

Card 1/1 Pub. 128 - 15/29

Author : Nekrasov, S. S., Kand. Tech. Sci.

Title : Dependance of the cutting force upon the strength of gray iron.

Periodical : Vest. mash., #4, p. 59-62, Ap 1956

Abstract : The process of cutting is considered as a local compression with the cutter's edge beyond the metal's compression strength. Thus the force necessary in cutting is in direct proportion to the metal's compression strength. In gray iron the matrix of steel has a different compression strength from the flakes of graphite embedded in it. The force necessary for cutting gray iron depending upon its structure and characteristics is analysed and tested. Tables, diagrams, 4 references, 1947-1954.

Institution : None

Submitted : No date

SOV 24-[illegible]-8254

Translation from: Referativnyy zhurnal. Mekhanika [illegible] SSSR

AUTHOR: Nekrasov S S

TITLE: On the Influence Exerted by Rock Pressure on the Force Needed to Cut Through Friable Rock (O vliyanii gornogo davleniya na usiliye pri rezanii khrupkikh materialo)

PERIODICAL: Nauch tr po sopr gorn. dela Mosk gorn [illegible] Nr [illegible] pp 283-290

ABSTRACT: In the course of the cutting process the [illegible] subjected to stresses of [illegible] The author concludes from [illegible] for example of coal subjected to triaxial compression [illegible] first strength criterion holds true [illegible] governing factor is the interval of the greatest principal stress [illegible] that the rock pressure does not affect those stresses [illegible] able rock by any cutting of the rock [illegible] more natural to assume that the Coulomb Mohr strength criterion ought to be used, which criterion allows for the effect on the cutting strength exerted by the mean rock pressure and hence predicts that

Card 1/2

On the Influence Exerted by Rock Pressure on the Force Needed to Cut Coal

the rock pressure does affect to some degree the stresses within the coal produced by cutting. This rock pressure influence becomes more noticeable as the depth increases and should be very much in evidence at depths of the order of several hundred meters and more. The experiments referred to in this paper were performed at depths at which the mean rock pressure was of the order of ten or more kg/cm². In Figure 2 the indicated direction of the shear stress τ_{xy} acting upon one of the faces of the prism depicted there is incorrect, this error is carried over into equation (1); however, it does not affect the author's other conclusions, since he disregards the shear stresses.

G. S. Snapir

Card 2/2

SOV [illegible]

Translation from: Referativnyy zhurnal Mekhanika 1958 Nr 1 p 154 (USSR)

AUTHOR: Nekrasov, S S

TITLE: The Forces Acting on a Coal Cutter (Usiliya deystvuyushchiye na vrubovuyu mashinu)

PERIODICAL: Nauchn tr Mosk gorn [illegible] Nr 17 pp 65-74

ABSTRACT: An examination of a method for the calculation of the forces that act on a coal cutter with due consideration of the operating conditions, including the hardness of the coal, the cross section of the cut, the culm resistance etc. The formulas given can serve as a basis for the stress analysis of such machines and for calculations relative to the forces acting on the trailing cable and the power expended on the coal cutting process.

Reviewer's name illegible

Card 1/1

NEKRASOV, S.S., dotsent, kand.tekhn.nauk

Determining the main composite cutting force by the hardness of steel. Nauch.trudy MGI no.17:289-295 '56. (MIRA 10:11)
(Metal cutting) (Steel--Testing)

NEKRASOV, S.S.

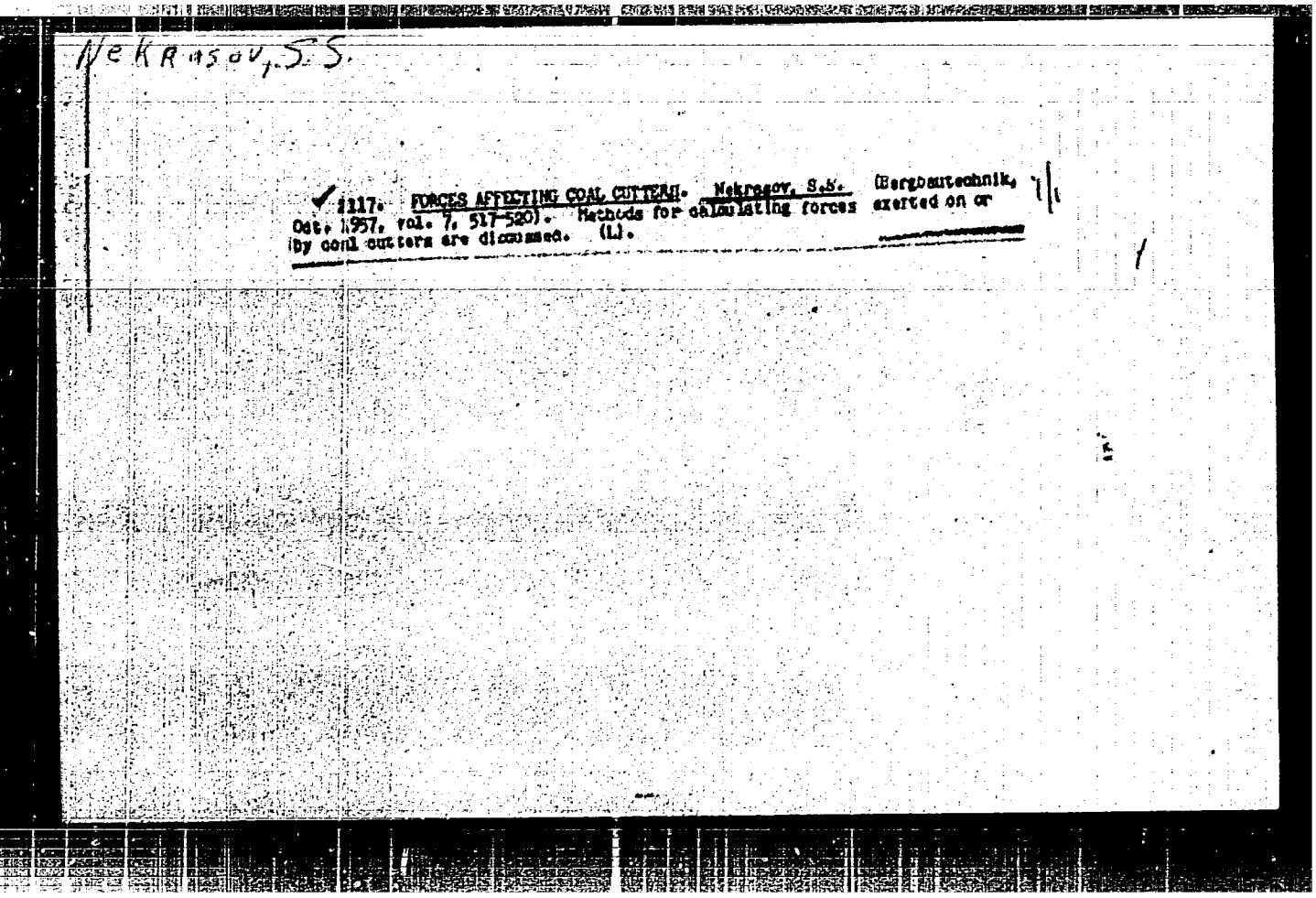
Effect of the size of gray iron specimens on compression strength.
Zav.lab.22 no.4:484-485 '56. (MLRA 9:7)

1.Moskovskiy gornyy institut imeni I.V.Stalina.
(Iron--Testing) (Strains and stresses)

NEKRASOV, S. S.

2

Ukr.
Nekrasov, S.S. PRINCIPLES OF THE THEORY OF STRESS IN CUTTING BRITTLE MATERIALS. (Gornyaut'omik, Feb. 1957, Vol. 7, 72-86). Application of the theories of elasticity and plasticity to coal cutting is discussed. (L).



Nekrasov, S.S.

#117. FORCES AFFECTING COAL CUTTERS. Nekrasov, S.S. (Bergbautechnik, Oct. 1957, vol. 7, 517-520). Methods for calculating forces exerted on or by coal cutters are discussed. (L).

NEKRASOV, S.S.

Chip formation during the cutting of materials. Nauch. trudy MGI no.21:109-127 '57. (MIRA 11:9)
(Cutting machines)

NEKRASOV, S. S., Doc Tech Sci -- (diss) "Resistance of coal and other materials to cutting." Mos, 19??. ?? pp with ills (Min of Higher Education USSR, Mos Mining Inst im I. V. Stalin, Chair of Technology of Mining Machine Building). ?? copies. List of author's works pp ?? (?? titles) (KL, 10-58, 117)

KRASOV, S.S., dotsent

Investigating and calculating forces needed for coal cutting with large cutters. Nauch. dokl. vys. shkoly: gor. dela no.1:221-235 58. (MIRA 11:6)

1. Predstavlena kafedroy gornoy mashin Moskovskogo gornogo instituta im. I.B. Stalina.
(Coal mining machinery)

NEKRASOV, S.S., dots., kand.tekhn.nauk

Using mathematical statistics for the calculation of strength and power in coal cutting. Nauch. dokl. vys. shkoly; gor. delo no.3: 70-77 '58. (MIRA 11:9)

1. Predstavlena kafedroy tekhnologii gornogo mashinostroyeniya Moskovskogo gornogo instituta im. I.V. Stalina.
(Coal mining machinery) (Mathematical statistics)

AUTHOR: Nekrasov, S.S. SOV/126-6-5-42/43

TITLE: On the True Strergth of Plastic Metals Under Compression and Extension (O deystvitel'noy prochnosti plastichnykh metallov pri szhatii i rastyazhenii)

PERIODICAL: Fizika Metallov i Metallovedeniye, 1958, Vol 6, Nr 5, pp 956 - 958 (USSR)

ABSTRACT: Diagrams of true extension of plastic metals differ somewhat from the diagrams of true compression. To find the reasons for this difference, the author tested samples of steels 20, 45 and U7 and brassLS59-1. Compression tests were made on samples of 10 mm dia and 10, 15 and 20 mm height. Samples tested by extension were of 5, 10 and 20 mm dia and 100 mm length. A 30-ton universal (TsNIITMASh) machine of IMCh-30 type was used. In extension tests, the load P and the minimum diameter were measured at several stages. The stress σ was obtained by dividing the load P by the minimum cross-sectional area F. The true deformation (strain) e was calculated from the formula:

$$e = \left(\ln \frac{F_0}{F} \right) \cdot 100\% \quad .$$

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On the True Strength of Plastic Metals Under Compression and Extension

In compression tests, the actual height of the sample h at a given load P was measured and the cross-sectional area F_1 was calculated from the condition of constancy of the sample volume; $F_1 = F_o h_o / h$, where F_o and h_o are the initial cross-sectional area and height of the sample, respectively. The true compressive stress was calculated from $\sigma_1 = P/F_1$. The true deformation (strain) on compression was taken to be equal to $e_1 = \ln(h_o/h) \times 100\%$. These formulae showed that the only difference in the method of calculation of true stresses and deformations on extension and on compression. The true extensional stresses are calculated from the smallest cross-section of the sample. In compression tests, the true stress is taken to be related to a certain mean cross-section; Figure 1 shows a sample deformed by compression in which the diameter d_1 corresponds to the cross-section F_1, used in calculations dealing with compression. Secondly, in extension tests there is a decrease in the diameter of the sample and,

Card2/6

On the True Strength of Plastic Metals Under Compression and Extension

therefore, the effective area to which the load is applied; the converse is true for compression tests. If samples used for extension and compression tests initially have the same diameter, their true stresses will differ because of the scale factor due to the differences in final dimensions. The results obtained by compression and by extension testing will become more similar if calculations are made on the same basis and if the scale factor is taken into account. Tests made on steels 20, 40 and U7 yielded similar results; the present paper quotes only results for steel 20. Figure 1 gives the true stress-strain diagrams obtained by extension (Curve 1) and compression (Curve 2) of steel 20 samples. Figure 2 shows that steel samples under compression are more plastic than under tension. To obtain results which are closer on compression and extension, it is necessary to calculate compression stresses from the minimal cross-sectional area, diameter d (Figure 1). A better agreement between compression and extension results was then obtained for steels 20, 40 and U7, as shown by Figure 3. On extension, the diameter of steel 20 samples

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SOV/126-6-6-42/43

On the True Strength of Plastic Metals Under Compression and Extension

was reduced from 10 to 5 mm. In compression tests, diameters of the samples of the same steel increased from 10 to 19 mm. To minimise this scale factor, it was necessary to compare the compression results obtained using samples of 10 mm diameter and extension results obtained on 10 and 20 mm samples. In this case, compression of a sample is compared with extension of two samples with diameters which cover the range of the change of the diameter on compression. Figure 2 gives also results of extension tests of samples with the initial diameters of 10 and 5 mm and compression tests of samples of 10 mm diameter; all the samples were made of steel 20. It is found that the experimental points obtained by compression lie between points obtained by extension. This shows that the true extension curves practically coincide with the true compression curves when the scale factor is taken into account and when both the compression and the tension stresses are calculated, using the minimum diameter. The true curves obtained by compression and extension of samples of LS59-1 brass were practically identical (Figure 3).

Card4/6 This may be because brass LS59-1 behaves [illegible]

On the True Strength of Plastic Metals Under Compression and Extension

that the true deformations produced by compression and extension are the same. On compression, the brass samples behaved first as a plastic material but then showed a hardening effect and finally failed. The coefficient of friction of brass on steel supports is smaller than the coefficient of steel on steel and therefore the samples of brass, when compression-tested, did not have the barrel-shape exhibited by steel; for brass, the diameters d_1 and d of Figure 1 were practically the same. The authors make the following conclusions. 1) The true stresses on compression are practically identical with the true stresses on extension when, in each case, calculations are made using the minimum diameter. 2) Because the experimental scatter is smaller on extension, the extension results are more reliable. This is an abridged translation.

There are 4 figures.

Card 5/6

SOV/126-6-5-42/43

On the True Strength of Plastic Metals Under Compression and Extension

ASSOCIATION: Moskovskiy gornyy institut (Moscow Mining Institute)

SUBMITTED: April 1[illegible], 1957

Card 6/6

AUTHOR: Nekrasov, S.S., Candidate of Technical Sciences

TITLE: On Contact Strength of Weak Materials (O prochnosti real'nykh materialov)

PERIODICAL: Vestnik mashinostroyeniya, No. [illegible] (USSR)

ABSTRACT: According to the theory of plasticity [illegible] dimensional case of driving a wedge-shaped die into an ideal plastic material (i.e. incompressible strain-hardening material) pressure on the head of the punch at the time it begins to penetrate the material is given by the equation $p = \sigma_s(1 + \gamma)$, where σ_s is the yield stress, γ is the semi-vertical angle of the wedge. When friction is present and the coefficient of friction is [illegible], the equation $p = \sigma_s(2.3 + \gamma)$

This paper shows that the premises of the theory of plasticity are also valid in the case of the [illegible] materials which are capable of strain-hardening, as well as in the case of brittle materials (in the latter case the yield stress is to be replaced by the [illegible]). Consequently, when compressing obtuse, wedge-shaped bodies with no friction being present the relation [illegible] at failure point should be $p = \sigma_s(2 + \gamma)$ [illegible]

Card1/5

On Contact Strength of Rea. Materials SOV/

yield stress as affected by the stres
of the material. Similarly, for a
$p = c_d(1 + \gamma)$ when no friction is
$p = c_d(1.3 + \gamma)$ when there is friction
contact, where
Figure 1 gives the
the specimens made
of 10 mm length and
vertical angle
based on the smaller
based on the
at the
relation be
the case $\gamma = 0$.
It is seen that
theoretical
γ

Card2/5

as the strain increases, i.e. there is a further strain hardening; this may be explained by the fact that the specimens begin to buckle (as shown in Figure [illegible]) for $\varepsilon > 30\%$; this buckling evidently counteracts the hardening effect.

The experiments with specimens of $\gamma = 30°$ and $\gamma = 45°$ in which the buckling of the resisting surface was removed by a grinding wheel show that in these cases the experimental points coincide with the theoretical relation. These points are encircled in Figure [illegible].

Similar experiments with specimens of grey cast iron (specimen I: Brinell hardness H_B = [illegible] and σ_d = 99.5 - 102.5 kg/mm^2, specimen II: H_B = 222 and σ_d = 94.5 - 99 kg/mm^2) are represented by the graphs in Figure [illegible] which are seen to coincide with the straight line $p = \sigma_d(1.3 + \gamma)$ (line a) or to be contained between that line and the line b representing the relation $p = \sigma_d(1 + \gamma)$.

Card3/5 Finally, some experiments were carried out with specimens

made of the Dan coal mixed with cement. The results are given in Figure 4.

In order to check the validity of Eq. (1) for a large range of angles γ some experiments were carried out with punches (see Figure 5) made of Dan coal and cement which were forced into a block of the same material. The relation between the depth of the penetration h and the force on the punch P is given in Figure 6. It can be seen that for $h/d > 1$ there is a little change in the force required to increase the penetration which suggests that h/d is the deciding parameter. In Figure 6 this ratio is taken as the base against which the pressure on the punch (in kg/mm^2) is plotted for various diameters of the punch. It appears that pressure required to force a punch into the material does not depend on the diameter of the punch. For

Card4/5

On Contact Strength of Real Materials SOV/[illegible]-14/29

h/d > 1 , the graph is a straight line and this may be explained simply as the effect of three-dimensional strain hardening of the material.
Results of the experiments carried out on non-symmetrical specimens are given in Figure 10, which also shows the geometry of the specimens.
There are 10 figures and 2 Soviet references.

1. Plasticity--Theory
4. Materials--Test methods

Card 5/5

KISHVARI, M., student V kursa; NEKRASOV, S.S., dotsent, kand.tekhn.nauk

Clamping devices with liquid plastic. Nauch. rab. stud. GNSC MGI no.7:186-193 1959. (MIRA 14:5)
(Machines tools—Attachments)
(Plastics)

NEMRAsOV, S.S., doktor tekhnicheskikh nauk

Dependence of the force of cutting on the strength of wood.
Izv. TSKHA no.3:226-231 '61. (MIRA 14:9)
(Woodworking)

NEKRASOV, S.S.; OFENGENDEN, N.Ye.

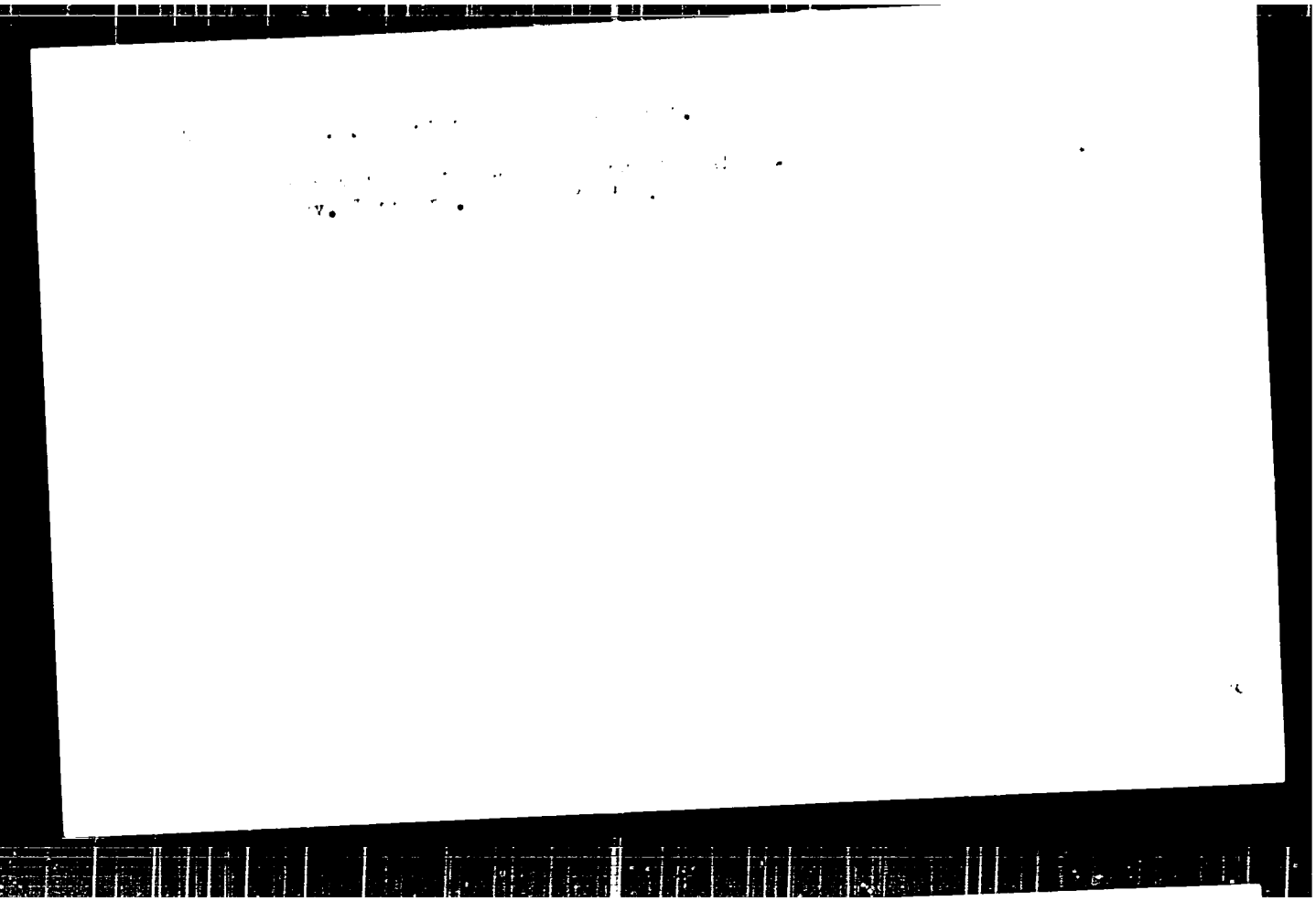
Investigating the wear resistance of plastics, cast basalt and rubber in an abrasive liquid mixture. Plast.massy no.11:34-36 '61. (MIRA 14:10)

(Plastics—Testing)

MSKRASOV, S.S., doktor tekhn.nauk, prof.

Determining the magnitude of the breaking load in cutting plastic and brittle materials. Izv. VSKHA no.2: [illegible] '62. (MIRA 15:6)

(Metal cutting)



APPROVED FOR RELEASE: Wednesday, June 21, 2000 CIA-RDP86-00513R001136

S/0122/64/000/003/0068/0071

ACCESSION NR: AP4026250

AUTHORS: Nekrasov, S. S. (Professor); Vitliyemov, V. D. (Engineer)

TITLE: Investigation of machining with vaporized liquid cooling

SOURCE: Vestnik mashinostroyeniya, no. 3, 1964, 68-71

TOPIC TAGS: machining cooling method, coolant supply, vaporized liquid cooling, spray cooling, steel R18, steel 45, tool bit, lathe 1A62

ABSTRACT: The effects of nozzle shape, nozzle diameter, method of application (from above and from below), compressed air pressure, and coolant flow rate on the cooling properties of a vaporized liquid during machining were investigated experimentally using a tool bit of steel R18 to cut samples of steel 45. The nozzle shape shown in Fig. 1 of the Enclosure was investigated. It was found that: a) the diverging nozzle (c) gave the coolest spray and working temperature; b) the work temperature decreased as the coolant flow rate was increased to 40 gm/m^3 of compressed air (at 4 kg/cm^2) and remained constant above that; c) a throat diameter of 1.5 mm was optimum for the geometry and operating pressure. Using this "optimum" nozzle, tool wear was measured for machining without cooling, cooling by pouring the coolant, spraying from above, and spraying from below.

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ACCESSION NR: AP4026250

It was found that spraying from above caused least tool wear but resulted in catastrophic tool failure faster than spraying from below. By changing the air supply pressure and specific coolant flow rate it was found that the work temperature decreased with increasing supply pressure but that the effect of increased coolant flow rate became negligible after a certain flow rate was reached. This flow rate varied for different conditions but was below ≈ 200 gm/hr for all conditions considered. Orig. art. has: 7 figures

ASSOCIATION: Timiryazevskaya sel'skokhozyaystvennaya akademiya (Timiryazevo Agricultural Academy)

SUBMITTED: 00 DATE ACQ: 20Apr64 ENCL: 01

SUB CODE: IE NO REF SOV: 000 OTHER: 000

Card 2/3

ACCESSION NR: AP4026250

ENCLOSURE: 01

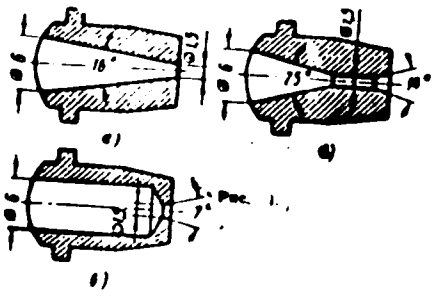


Fig. 1 Experimental nozzles
a- converging, b- cylindrical, c- diverging

NEKRASOV, T.K.; KHAST, D., redaktor; LAVRENT'YEVA, tekhnicheskiy redaktor

[Rural motion-picture operators] Sel'skie kinomekhaniki. Moskva, Gos. izd-vo kul'turno-prosvetitel'noi lit-ry, 1954. 19 p. [Microfilm] (MLRA 8:7)

(Motion-picture projection)

NIKRASOV, T.P.

"Diclinism" of the Lapland pine. Bot.zhur. 39 no.4:579-583 Jl-Ag '54.
(MLRA 7:10)

1. Zapadno-Sibirskiy filial Akademii nauk SSSR, Novosibirsk.
(Scotch pine)

AUTHOR: Nekras[illegible], V.A.

TITLE: The Catalytic [illegible] n-Hexane [illegible]

PERIODICAL: [illegible] [illegible] [illegible], Nr [illegible], [illegible] (USSR)

ABSTRACT: The [illegible]rination was carried out in the vap[illegible] phase by means of various [illegible] catalysts. The best result was obtained with a Mg[illegible] catalyst [illegible]. The catalysates were subjected to fractional distillation in a vacuum column. The var[illegible] are given. The [illegible]rination in the presence of alloys [illegible] was [illegible] studied. It has been shown that an alloy of [illegible] mole-% Mg [illegible] and [illegible] mole-% [illegible] is the most effective catalyst. There are [illegible] graphs and [illegible] references, [illegible] and [illegible] English.

The Catalytic Chlorination of n-Hexane and n-Heptane SOV/63-4-3-24/31

ASSOCIATION: Krymskiy sel'skokhozyaystvennyy institut imeni M.I. Kalinina (Crimean Agricultural Institute imeni M.I. Kalinin)

SUBMITTED: December 29, 1958

Card 2/2

NIKRASOV, V.A., insh.

Calculating the number of cycles in the winning of milled peat.
Torf. prom. 35 no.3:10-11 '58. (MIRA 11:5)

1. Varegovskoye torfopredpriyatiye.
(Peat)

DEYEV, M.Ya., master; YELCHEV, G.A., slesar'; SNIGIREV, F.I., slesar'; NEKRASOV, V.G., slesar'; NAD'KIN, N.A., mashinist elektrovoza; OSHIVALOV, A.V., mashinist elektrovoza; PANCHENKO, P.M., mashinist elektrovoza.

Brush-holder units must be improved. Elek.i tepl.tiaga 2 no.4:6-7 Ap '58. (MIRA 12:3)

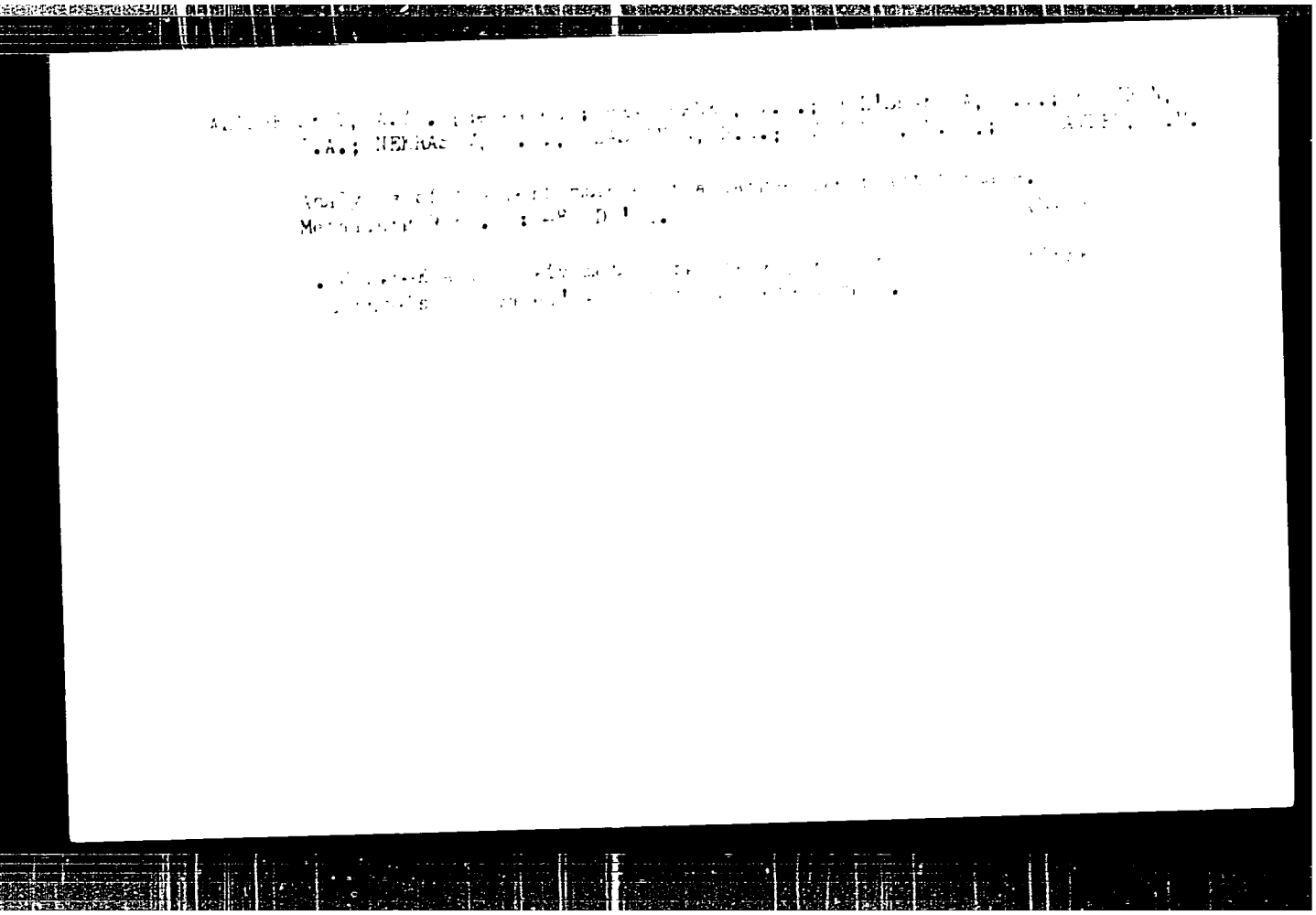
1. Elektromashinnyy tsekh depo Zlatoust Yuzhno-Ural'skoy dorogi (for Deyev). 2. Depo Zlatoust-Yuzhno-Ural'skoy dorogi (for all except Deyev).

(Electric brushes) (Electric railway motors)

NEKRASOV, V.G., inzh.; YAMPOL'SKIY, T.S., inzh.

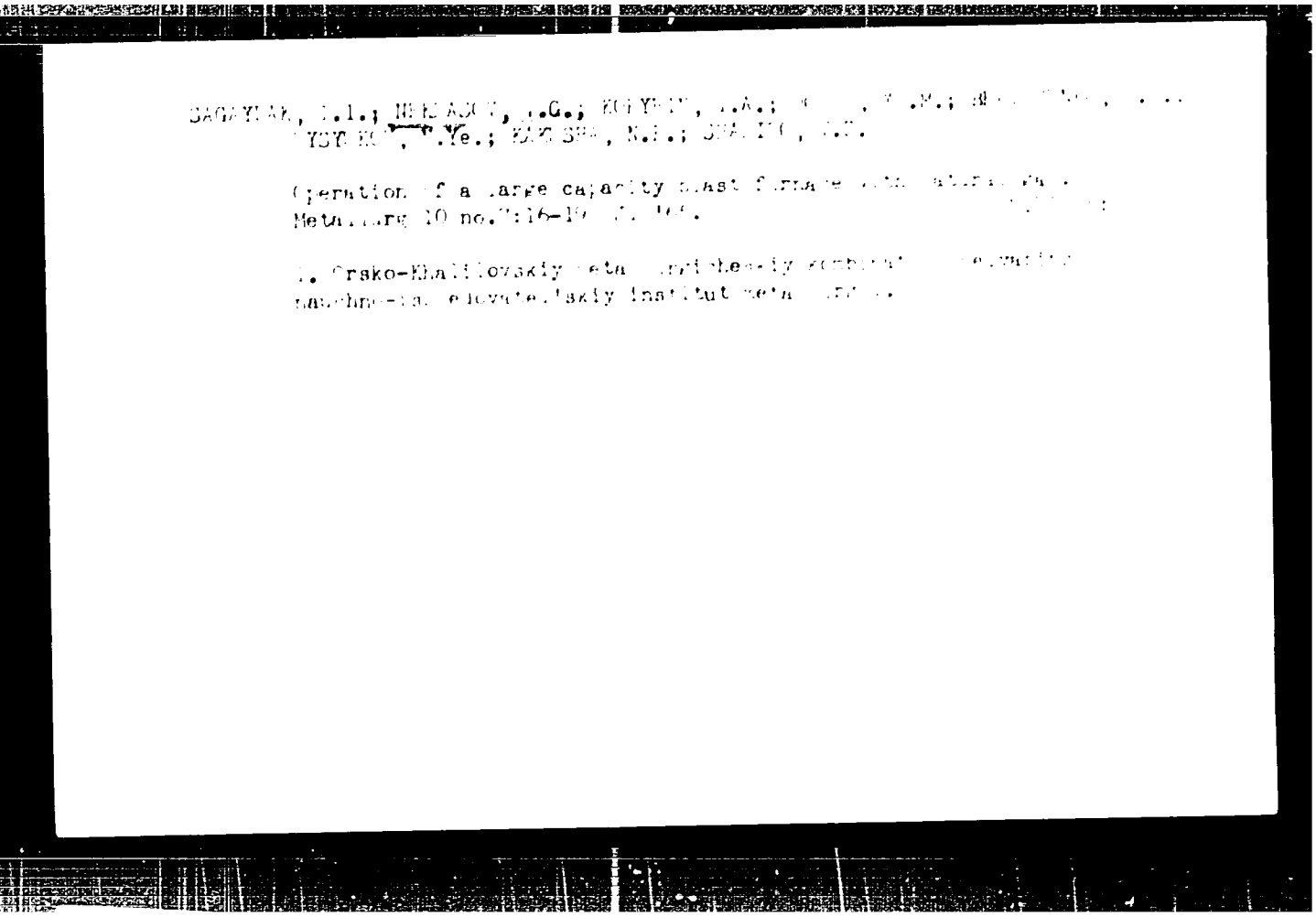
Using precast reinforced concrete construction elements in building cooling towers with ventilating systems. Prom.stroi. 38 no.1:31-34 '60. (MIRA 13:5)

1. Trest Mosstroy No.4 (for Nekrasov). 2. Giprotis (for Yampol'skiy). (Cooling towers) (Precast concrete construction)



NEKRASOV, V.G.; OLISOV, A.A.; SHAPIRO, V.Z.

Introducing blast pipes with heat-res [illegible]
inform.Gos.nauch.-issl.inst.nauch.i tekh. [illegible]



PLAKS, A.V., inzhener; NEKRASOV, V.I., inzhener.

Differential protection for electric locomotives. Zhel. dor. transp. 38 no.11:64-66 N '56. (MLRA 9:12)

(Electric locomotives)

32(3)

SOV/112-59-5-9110

Translation from: Referativnyy zhurnal. Elektrotekhnika, 1959, Nr 5, p 100 (USSR)

AUTHOR: Dunenkov, V. L., Nekrasov, V. I., Plaks, A. V., Sheleshkov, K. K. and Yarchuk, A. Ya.

TITLE: Investigation of Electrical Equipment of Type N8 Electric Locomotive

PERIODICAL: Sb. Leningr. in-ta inzh. zh.-d. transp., 1957, Nr 155, pp 29-44

ABSTRACT: To introduce final corrections, the scheme of a type N8 electric locomotive had been tested under various conditions before serial manufacturing of the locomotive was started. Under regenerative braking conditions, the current reached 2,000 amp. On the section where the sub-stations had no inverter equipment, the contact-wire voltage reached 4,200 v with NB-406 traction motors operating normally. Investigation of the transients accompanying the transition to series connection showed that sometimes under regenerative conditions, the residual EMF of traction motors is so combined with the contact-wire voltage that voltages up to 5,100-6,000 v appear on the motor brushes. This caused flashovers from energized motor parts and

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Investigation of Electrical Equipment of Type N8 Electric Locomotive

equipment to ground. To eliminate such overvoltages, it was suggested that the motors next to ground be short-circuited. To eliminate burning of contacts of the braking switch under transient conditions, it was recommended that two contactors be used for breaking the traction-motor field circuit when regeneration is cut off. Tests of a new laminated-core D-4 relay showed that it provides a satisfactory differential protection of the power circuit. Buffer protection, under traction conditions, is realized by introducing starting resistors; its operating time is 0.1-0.2 sec, the motor current being reduced to one-third of its value. Investigation of the functioning of the protective system under regenerative conditions permitted setting a course for solving this important problem. Forced ventilation is recommended for improving the operating conditions of "fekhral" resistors. Detailed investigations of air exchange within the locomotive body permitted providing some recommendations on how to improve the ventilating system. Bibliography: 3 items.

V.N.K.

Card 2/2

32(3) SOV/112-59-5-9109

Translation from: Referativnyy zhurnal. Elektrotekhnika, 1959, Nr 5, p 100 (USSR)

AUTHOR: [redacted]

TITLE: Investigation of an Electromechanical Induction-Motor-Driven Energy Accumulator for Traction Purposes

PERIODICAL: Sb. Leningr. in-ta inzh. zh.-d. transp., 1957, Nr 155, pp 45-60

ABSTRACT: An electromechanical energy accumulator, "gyrobus," can be expediently used in a metropolitan transport system and in such industries where process-determined train stops can be used for energy storing. The electromechanical energy accumulator has the following advantages over the conventional storage battery: (1) lower operating expense due to elimination of acid (or alkali) equipment; (2) saving on critical metals, lead and nickel; (3) quick charging, a few minutes; (4) simplification of charging stations, thanks to the use of AC machinery. The electromechanical accumulator has the following disadvantages: (1) limited section length determined by the

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SOV/112-59-5-9109

Investigation of an Electromechanical Induction-Motor-Driven Energy

energy stored at a feeding station; (2) increase in vehicle weight by 10-12% (3) higher specific energy consumption by the vehicle; (4) need, in some cases, for a hydrogen medium to decrease flywheel friction losses and to cool the accelerating motor. Results of an investigation of an induction-motor-driven electromechanical accumulator mounted on a 10-ton-capacity truck are submitted. The tests were conducted at the "Krasnyy proletariy" plant Moscow, in 1956; they showed the expediency of using the electromechanical accumulator for metropolitan short-run transportation and for those cases where specific conditions require elimination of the contact wire.
Bibliography: 3 items.

V.N.K.

Card 2/2

DUNENKOV, V.L.; NEKRASOV, V.I.; PLAKS, A.V.; SHELESHKOV, K.K.; YARCHUK, A.Ya.
(Leningrad)

Investigation of some parts of the electric equipment of M8 electric locomotives. Elek.i tepl.tiaga no.[illegible] '57. (MIRA 10:11)

(Electric locomotives)

NEKRASOV, V.I. (Leningrad); POPOV, I.M. (Leningrad); ESTLING, A.A. (Leningrad)

Modeling method used for investigating dynamics of electric trains. Elek. i tepl. tiaga 2 no.9:10-13 S '58. (MIRA 11:10)
(Electric railroads--Dynamics--Trains)

RABINOVICH, A.A., inzh.; NEKRASOV, V.I., inzh.; PLAKS, A.V., inzh. (Leningrad

Broadening the field of using railroad motorcar trains. Zhel. dor. transp. 40 no.12:48-51 D '58. (MIRA 12:3)

1.Glavnyy konstruktor zavoda "Dinamo" imeni S.M. Kirova.
(Railroad motorcars)

NEKRASOV, V.I., inzh.; CHERKASOV, Ye.B., inzh.; PEREVOZCHIKOV, S.N., inzh.

MT-16 narrow-gauge diesel-electric locomotive using single-phase current of industrial frequency. Sbor.LIIZHT no.159:92-105 '58. (MIRA 12:2)

(Diesel locomotives)

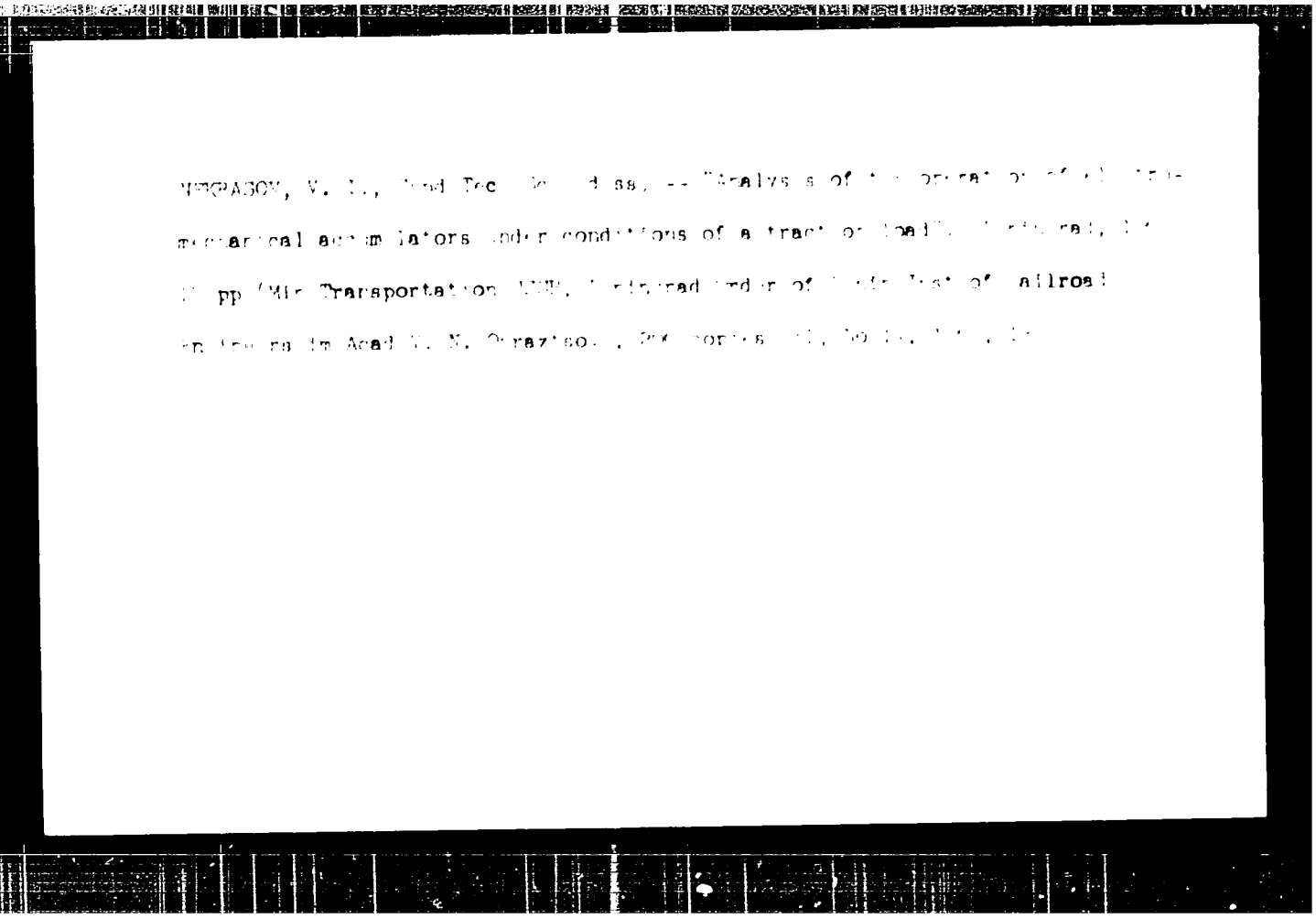
NEKRASOV, V.I., inzh.

Investigating physical processes of self-excitation in asynchronous generators with the aid of vector diagrams. Sbor. LIIZHT no.159:128-141 '58. (MIRA 12:2)
(Electric generators)

NEKRASOV, V.I., inzh.

Using batteries for electric traction. Sbor.LIIZHT no.167:23-44 '59. (MIRA 13:5)

(Electric railroads--Equipment and supplies)
(Storage batteries)



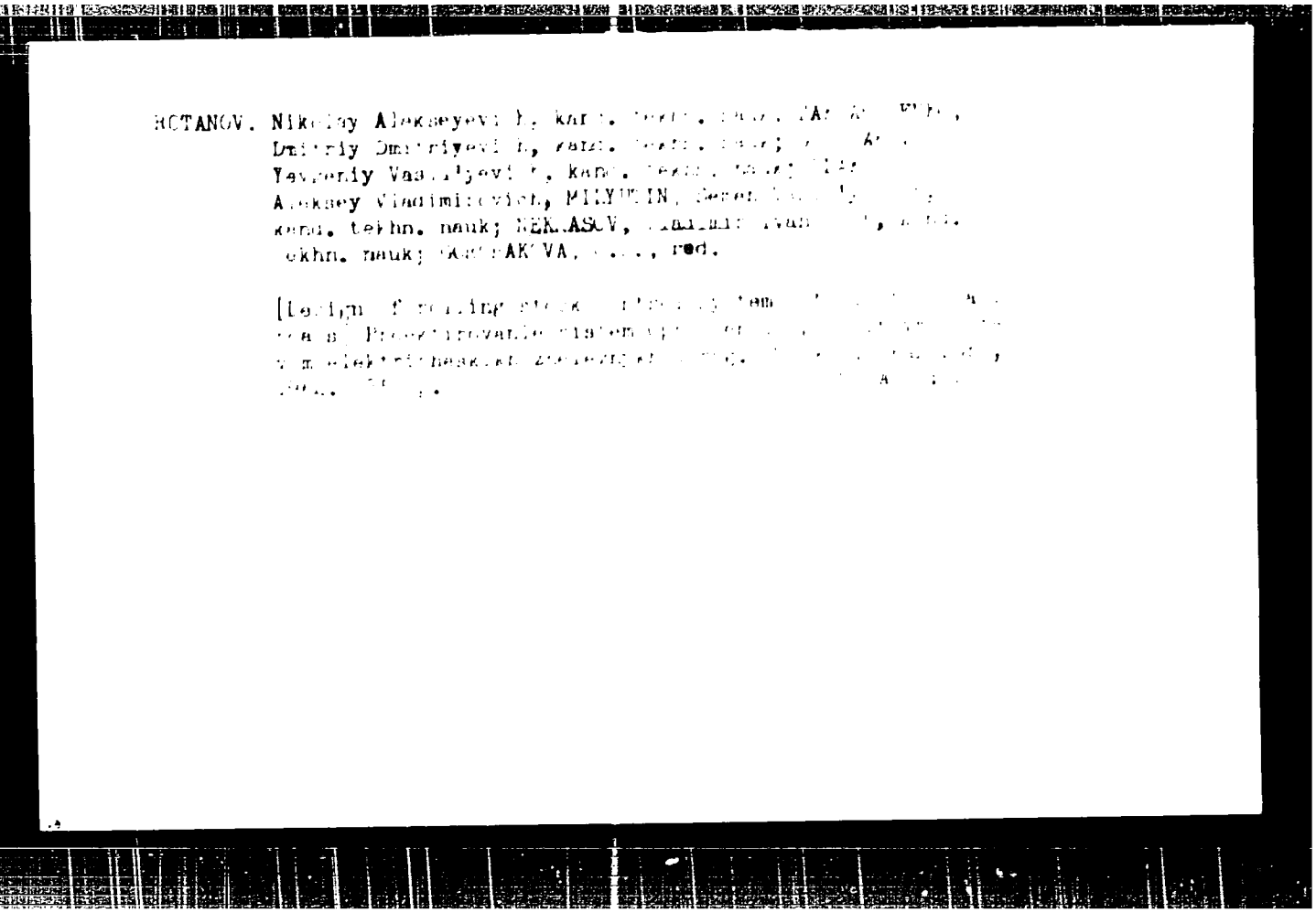
ZAKHARCHENKO, D.D., kand. tekhn. nauk; NEKRASOV, V.I., kand. tekhn. nauk; PLAKS, A.V., kand. tekhn. nauk, dots.; PRIVALOV, V.V., kand.tekhn. nauk; TREYMUNDT, N.D., kand. tekhn. nauk; VISIN, N.G., kand. tekhn.nauk, retsenzent; KUCHMA, K.G., kand. tekhn. nauk, retsenzent; FAMINSKIY, G.V., kand. tekhn.nauk, retsenzent; KALININ, V.K., kand. tekhn. nauk, red.; VOROTNIKOVA, L.P., tekhn. red.

[Automation of electric rolling stock control systems] Avtomatizatsiia sistem upravleniia elektricheskim podvizhnym sostavom. Moskva, Transzheldorizdat, 1963. 214 p. (MIRA 16:7)
(Electric railroads--Electronic equipment)

NEKRASOV, V.I., kand.tekh.nauk, MAKLAKOV, T.I., inzh.

Investigating the performance of the auxiliary machines of the EP-
01 electric train. Vest. VNII MPS 22 no.8:8-13 '63. (MIRA 17:2)

1. Leningradskiy institut inzhenerov zheleznodorozhnogo transporta.



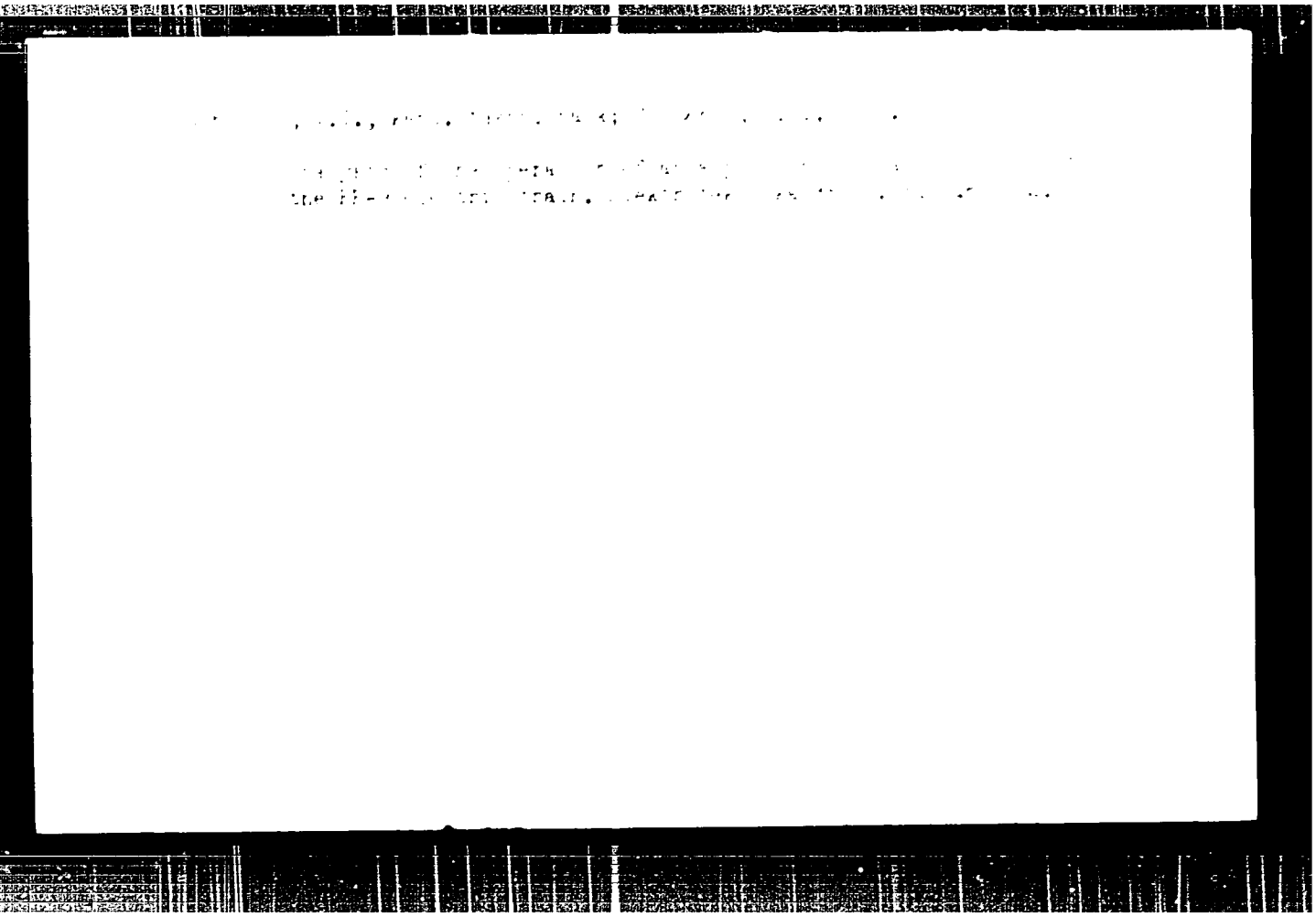
ROTANOV, Nikolay Alekseyevich, kand. [illegible]; [illegible]
Dmitriy Dmitriyevich, kand. [illegible]; [illegible]
Yevgeniy Vasil'yevich, kand. [illegible]; [illegible]
Alekseyev Vladimirovich, MILYUTIN, [illegible]
kand. tekhn. nauk; NEKRASOV, [illegible]
tekhn. nauk; [illegible], red.

[illegible]

GLAZOV, D.N., doktsent; MEKHANOV, V.I., [illegible]

Determination of the principal [illegible]
for underground main line locomotives [illegible]
Sbor. nauch. trud. Kem. gor. in-ta. [illegible]

1. Gorno-elektromekhanicheskiy fakul'tet [illegible]
institute.



L 31702-66

ACC NR: AP6021335 SOURCE CODE: UR/0144/66/000/003/0260/0270

AUTHOR: Nekrasov, Vladimir Ivanovich (Candidate of technical sciences; Chief science associate) 34 B

ORG: Department of Electric Locomotives, Leningrad Institute of Railway Transport Engineers (Kafedra elektricheskoy tyagi Leningradskogo instituta inzhenerov zheleznodorozhnogo transporta)

TITLE: Use of continuous-action electronic machines for the investigation of transient processes in the power circuits of electric locomotives

SOURCE: IVUZ. Elektromekhanika, no. 3, 1966, 260-270

TOPIC TAGS: electric motor, locomotive, locomotive engineering

ABSTRACT: The transient processes considered in the power circuits of electric locomotives are those due principally to sudden voltage surges on the terminals of the driving motors and to short circuits. Transients also occur when the energy states of the power circuits are varied. Such transients occur about 1000 times faster than any variation in train speed. Since the drive motors are the main components of the power circuits, methods are presented for simulating drive motor operation. After giving initial equations and their relationships, the author discusses the simulation of eddy currents, reactions of the armature, adhesion, and switching of the drive motors. A complete block diagram of the drive-motor switching model used to investigate the transient processes is shown. Orig. art. has: 8 figures and 19 formulas. [JPRS]

SUB CODE: 13, 09 / SUBM DATE: 22Jul63 / ORIG REF: 005

UDC: 621.333.+621.3.011

Card 1/1 GP

NEKRASOV, V I

PRAVDIN, L.F.; NEKRASOV, V.I.

Natural grafting in conifers. Bot.zhur. 38 no.6:874-878 N-D '53.
(MLRA 7:1)

1. Institut lesa Akademii nauk SSSR, Moskva.
(Coniferae) (Grafting)

NEKRASOV, V. I.

NEKRASOV, V. I.: "The effect of [illegible] water-temperature treatment of the seed of forest plants on seedling growth". Moscow, 1955. Acad Sci USSR. Inst of Forestry. (Dissertations for the Degree of Candidate of Biological Science)

SO: Knizhnaya letopis', No. 52, 24 December, 1955. Moscow.

AUTHOR: None Given

TITLE: Acclimatization of the Tulip Tree in the USSR (Akklimatizatsiya tyul'pannogo dereva v SSSR)

PERIODICAL: Priroda, 1958, Nr 5, pp 93-94 (USSR)

ABSTRACT: The tulip tree, Liriodendron tulipifera L. of the Magnoliaceae family, originating in North America, is cultivated in small amounts for ornamental and scientific purposes in the USSR, in the Caucasus, Crimea and southern parts of the Ukraine. It is not found in the north parts of the country due to severe winters. L. Chibiras, I. Dzniaukshtas and V. Nekrasov of the Institut lesa AN SSSR (The USSR Academy of Sciences' Forest Institute) have described these trees which are of special importance with respect to selection problems. Professor A.A. Lypa (Kiyev) relates interesting details about the history of the tulip tree in Russia. The oldest and largest tulip tree still existing in the USSR near the settlement Golovinka in the Lazarev district of the Krasnodar Kray on the Black-Sea shore of the Caucasus was planted in the [illegible]. In 1956 it was 25 m high, had a circumference of [illegible] m and a crown of 25 x 27 m. There are [illegible] tops.

AVAILABLE: Library of Congress

Card 1/1 1. Tulip tree - Growth 2. Plants - USSR

NEKRASOV, V.I.

Conference on problems of forest [illegible]. Izv. [illegible].
biol. no.5:[illegible] S-O '[illegible].
(THIS BRIDGING)

AUTH RS: Chib ras, L., Izniauskas tas, Nauras and eras.V.,
(Moskva

TITLE: A Rare Lime-Tree Redkaya lipa

PERIODICAL: Prir da, Nr FF

ABSTRACT: There is a rare specimen f a big-leaved lime tree Tilia platyphy s f. laciniata . Koch fig. in the park f the dairy technical school "Be. vederis" in the Lithuanian Vil'ki District. t has kinds of leaves i.e. pinnately lobed, entire-margined and intermediate stages. The tree has trunks emerging from a common base and with a diameter of the tree top of m. The change of the leaves seems to be a true mutation. Seeds are gathered from each branch separately in order to prove this hypothesis. The same will be done by way of vegetative propagation. The phenomenon of pinnately lobed lime tree leaves has also been recorded in other individual trees of other parks in the Lithuanian Republic. There are

Card 1/2

A Rare Lime-Tree

AUTHOR: Litovskiy nauchno-issledovatel'skiy institut lesnogo khozyaystva /Kaunas (The Lithuanian Scientific Research Institute of the Forest Economy /Kaunas) Institut lesa Akademii nauk SSSR /Moskva (The Forest Institute AS USSR /Moskva)

Trees--Lithuania

Card 2/2

PRAVDIN, L.F.; NEKRASOV, V.I.; NIKONCHUK, V.N.; VOTINTSEV, A.M.

Problems of floating larch. Trudy Inst. lesa 45:145-165 '58. (MIRA 11:11)

(Larch) (Lumber--Transportation)

NEKRASOV, Valeriy Ivanovich; PRAVDIN, L.F., prof., doktor biolog.nauk, otv.red.; TIKHOMIROVA, Ye.V., red.izd-va; UL'YANOVA, O.G., tekhn.red.

[Pre-sowing cultivation of forest-tree seeds at low temperatures] Predposevnaia obrabotka semian lesnykh drevesnykh porod ponizhennymi temperaturami. Moskva, Izd-vo Akad.nauk SSSR, 1960. 105 p. (MIRA 13:7)
(Trees)

NEKRASOV, V.I.

Program for studying the genetic nature of forest tree varieties under acclimatization. Izv.Sib.otd.AN SSSR no.[illegible] '60. (MIRA 13:7)

1. Institut lesa i drevesiny Sibirskogo otdeleniya AN SSSR.
(Trees)

YEMEL'YANOV, Yu.M.; NEKRASOV, V.I.

Abnormal growth of arboraceous vegetation in the region of the fall of the Tunguska meteorite. Dokl. AN SSSR 135 no.5:1266-1269 D '60. (MIRA 13:12)

1. Moskovskiy gosudarstvennyy universitet im.M.V.Lomonosova i Glavnyy botanicheskiy sad AN SSSR. Predstavleno akademikom V.N. Sukachevym.

(Podkamennaya Tunguska Valley--Meteorites)
(Growth (Plants)) (Trees)

NEKRASOV, V.I.; SMIRNOVA, N.G.

X-ray method for studying the development of seeds of introduced woody plants. Biul.glav.bot.sada no.43:47-52 '61. (MIRA 15:2)

1. Glavnyy botanicheskiy sad AN SSSR.
(Woody plants) (Seeds)

S/026/62/000/002/004/004
D036/D113

AUTHORS: Nekrasov, V.I., Candidate of Biological Sciences (Moscow), and Yemel'yanov, Yu M., Candidate of Chemical Sciences (Moscow)

TITLE: Did the Tunguska catastrophe affect forest growth ?

PERIODICAL: Priroda, no 2, 1962, 102-105

TEXT: The authors discuss changes in forest growth in the area where the Tunguska meteorite fell. In 1958, an expedition of the Komitet po meteoritam AN SSSR (Committee on Meteorites of the AS USSR) under K.P. Florenskiy found that in the impact area the mean annual growth of the trees in diameter increased from 0 4-2 0 mm before the fall of the meteorite to 6-10 mm afterwards, a rate of growth which is still being maintained. This increase was observed both in young trees which sprung up after 1908, and in the surviving trees To establish whether this accelerated growth was due to improved vegetation conditions caused by the fall of the meteorite or to the

Card 1/2

S/026/62/000/002/004/004
D036/D113

Did the Tunguska . . .

fertilizing action of the meteoric substance itself, an expedition of the Sibirskoye otdeleniye AN SSSR (Siberian Branch of the AS USSR) under G.F. Plekhanov and V Koshelev, set up in 1960, planted test trees at various distances from the point of impact After the fall of the meteorite, the coniferous trees were replaced by their own kind. There are no deforested areas now, except for those due to soil destruction The new plantations are irregularly dispersed, they contain no more than 700-1200 trunks per 1 ha, the trunks are very regularly distributed and there are no signs of dying-off. Forty- to fifty-year-old trees of large and medium thickness were found to have grown to heights of 17-22 m as compared with the 7-8 m normal under analogous conditions The central part of the area of forest destroyed by the meteorite is now occupied by trees with class II and even class I bonitet, and the peripheral areas by trees of class III bonitet; normally, the forests of this zone have class IV and V bonitets, rarely class III. The mean annual growth in diameter of trees suffering damage to the base of the trunk by burning was 5.0 mm, 2-4 years after the fall of the meteorite as compared with 1 2 mm before. Further investigation is required to establish the causes of the described phenomena There are 3 figures and 2 Soviet references

Card 2/2

KRASOV, V. I.; VARTAZAROVA, L. S.; BORODINA, N. A.

Occurrence of a monoclinous inflorescence in an introduced Japanese white birch. Bot. zhur. 48 no.3:436-440 Mr '63. (MIRA 16:4)

1. Glavnyy botanicheskiy sad AN SSSR, Moskva.

(Birch) (Inflorescence) (Abnormalities(Plants))

YEMEL'YANOV, Yu.M.; NEKRASOV, V.I.

Radiophotography of wood from the area affected by the fall of the Tunguska meteorite. Dokl. AN SSSR 148 no.6:1418-1421 F '63. (MIRA 16:3)

1. Moskovskiy gosudarstvennyy universitet im. M.V.Lomonosova i Glavnyy botanicheskiy sad AN SSSR. Predstavleno akademikom V.N. Sukachevym.

(Podkamennaya Tunguska Valley--Meteorites) (Wood)
(Autoradiography)

NEKRASOV, V.I.

Use of additional pollination for increasing the number of viable seeds of the spruce Picea canadensis Britt. Biul. Glav. bot. sada no.42:54-57 '61. (MIRA 17:3)

1. Glavnyy botanicheskiy sad AN SSSR.

NEKRASOV, V.I.

Problems of the study of seeds in the introduction of woody plants. Biul. Glav. bot. sada no.50:12-18 '63. (MIRA 17:1)

1. Glavnyy botanicheskiy sad AN SSSR.

NEKRASOV, V.I.; KNYAZEVA, O.M.; SMIRNOVA, N.G.

Germination of the pollen introduced woody plants. Biul.Glav.bot.sad no.52:76-79 '64. (MIRA 17.4)

1. Glavnyy botanicheskiy sad AN SSSR.

EKRASOV, V.I.; SMIRNOVA, N.G.

Seed productivity and quality of seeds of some introduced woody plants and shrubs. Biul.Glav.bot.sada no. 48:11-17 '63.
(MIRA 17:5)

1. Glavnyy botanicheskiy sad AN SSSR.

NEKRASOV, V.I.; YEMEL'YANOV, Yu.M.

Studying forest growth in connection with the problem of the Tunguska meteorite. Meteoritika no.24:[illegible] '64. (MIRA 17:5

NEKRASOV, Valeriy Ivanovich; MYAKUSHKOV, V., red.; POLOZHENTSEVA, T.S., mlad. red.

[Trees change their addresses] Derev'ia meniaiut adresa. Moskva, Mysl', 1965. 101 p. (MIRA 18:4)

NEKRASOV, V.I., kand.biol.sg.nauk

Study and production of seeds of introduced plants, seminar-conference in Moscow. Vest.AN SSSR 35 no.8:100-102 Ag '65.

(MIRA 18:8)

L 15788-66 EWT(m)/ETC(f)/EWG(m)/EPF(n)-2 WW

ACCESSION NR: AT5023162 UR/2892/65/000/004/0133/0136

AUTHOR: Gudkov, A. N.; Kolobashkin, V. M.; Nekrasov, V. I.; Ushakova, N. P.

TITLE: The geographical distribution of nuclear reactors

SOURCE: Moscow. Inzhenerno-fizicheskiy institut. Voprosy dozimetrii i zashchity ot izlucheniy, no. 4, 1965, 133-136

TOPIC TAGS: nuclear reactor, economic geography, air pollution control, atomic energy plant equipment

ABSTRACT: The article presents the results of a review of Russian and foreign literature for the period from 1957 to 1964. It is intended to serve as an aid in the study of the distribution of harmful contaminants in the earth's atmosphere. A figure shows the rise in the power of atomic power reactors for the period 1951-1967 (including those presumed to be in operation). Another figure shows the change in the maximum thermal capacity of atomic energy, research, and transport reactors. An exponential relationship is proposed to predict the rise

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L 15788-66

ACCESSION RN: AT5023162

in the capacity of atomic plants. Orig. art. has: 1 formula and 4 figures

ASSOCIATION: None

SUBMITTED: 00 ENCL: 00 SUB CODE: 18,13

NR REF SOV: 001 OTHER: 013

Card 2/2

NEKRASOV, Vladimir Konstantinovich

Postroika avtomobil'nykh dorog. [Construction of automobile roads]. Moskva, Dorizdat, 1947. 329 p. illus.
"Rekomendyemaia literatura": p. 326-327. DLC: TE5.N4

SO: Soviet Transportation and Communications, A Bibliography, Library of Congress, Reference Department, Washington, 1952, Unclassified.

NEKRASOV, Vladimir Konstantinovich.

Stroitel stovo i eksploatatsiia gorodskikh dorog. [Construction and exploitation of city roads]. Utverzhdeno v kachestve uchebnika dlia uchashchikhsia tekhnikumov po spetsial nosti "Gorodskoe dorozhnoe stroitel stove." Moskva, Izd-vo Ministerstva kommunal'nogo khoziaistva RSFSR, 1949. 266p. illus.
Bibliography: p. [264]

DLC: TE250.N36

SO: Soviet Transportations and Communications, A Bibliography, Library of Congress Reference Department, Washington, 1952, Unclassfied

NEKRASOV, Vladimir Konstantinovich

Estimates and accounts in the railroad construction industry; a textbook
Moskva, Trizdat, 1951. 20 p. (52-15965)

TE183.N4

ANOKHIN,A.I., doktor tekhnicheskikh nauk,prof.[deceased]; BORODACHEV,I.P. kand. tekhnicheskikh nauk; BROMBERG, professor, VASIL'YEV,A.A., laureat Stalinskoy premii; PETERS, kandidat tekhnicheskikh nauk; POLOSIN-NIKITIN,S.M., kandidat tekhnicheskikh nauk; PRUSSAK,B.N., inzhener; RITOV,M.N., inzhener; FEYNBERG,G.M., inzhener; ESTRIN, M.I., inzhener; ALEKSEYEV,A.P., inzhener; BIRULYA,A.K., professor, doktor tekhnicheskikh nauk; BOLDAKOV,Ye.V., doktor tekhnicheskikh nauk;BOCHIN,V.A., laureat Stalinskoy premii,inzhener; VOLKOV,M.I., professor; GIBSHMAN,Ye.Ye., professor, doktor.technicheskikh nauk; DONCHENKO,V.G., dotsent, kandidat tekhnicheskikh nauk; ZHURAVLEV,A.Ya., laureat Stalinskoy premii; IVANOV,N.N., laureat Stalinskikh premii, professor, doktor tekhnicheskikh nauk; KUVASOV,A.S., inzhener; NEKRASOV, V.K., kandidat tekhnicheskikh nauk; POLOSIN-NIKITIN,S.M., dotsent, kandidat tekhnicheskikh nauk; KHLEBNIKOV,Ye.L., laureat Stalinskoy premii, professor; ORNATSKIY,N.V., doktor technicheskikh nauk, professor, redaktor; VOSKRESENSKIY,N.N., redaktor; KOVALIKHINA,N.F., tekhnicheskiy redaktor

[Manual for highway engineers; road building machinery] Spravochnik inzhenera dorozhnika; dorozhno-stroitel'nye mashiny. Moskva, Izd-vo dorozhno-tekhn. lit-ry. Gushosdora MVD SSSR, 1952. 698 p. [Microfilm] (MLRA 9:2)

(Road machinery)

NEKRASOV, Vladimir Konstantinovich; RITOV, M.N.; TOVSTOLUZHSKIY, N.I.

[Highway engineer's reference book] Spravochnik tekhnika-doroshnika. Izd.2., perer.i dop. Moskva, Izd-vo doroshno-tekhn. lit-ry, 1953. 591 p.
(MLRA 6:10)
(Road construction)

NEKRASOV, Vladimir Konstantinovich; SOBOLEV, S.S., professor, redaktor; CHVANOV, V.G., redaktor; KOVALIKHINA, N.F., tekhnicheskiy redaktor

[Erosion control and use of roadside gullies] Ukreplenie i ispol'-zovanie pridorozhnykh ovragov. Pod red. prof. S.S.Sobeleva. Moskva, Nauchn.-tekhn. izd-vo avtotransportnoi lit-ry, 1954. 59 p. (MLRA 8:3)
(Roadside improvement) (Erosion)

NEKRASOV, V.; VULIS, D.

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(Road construction)

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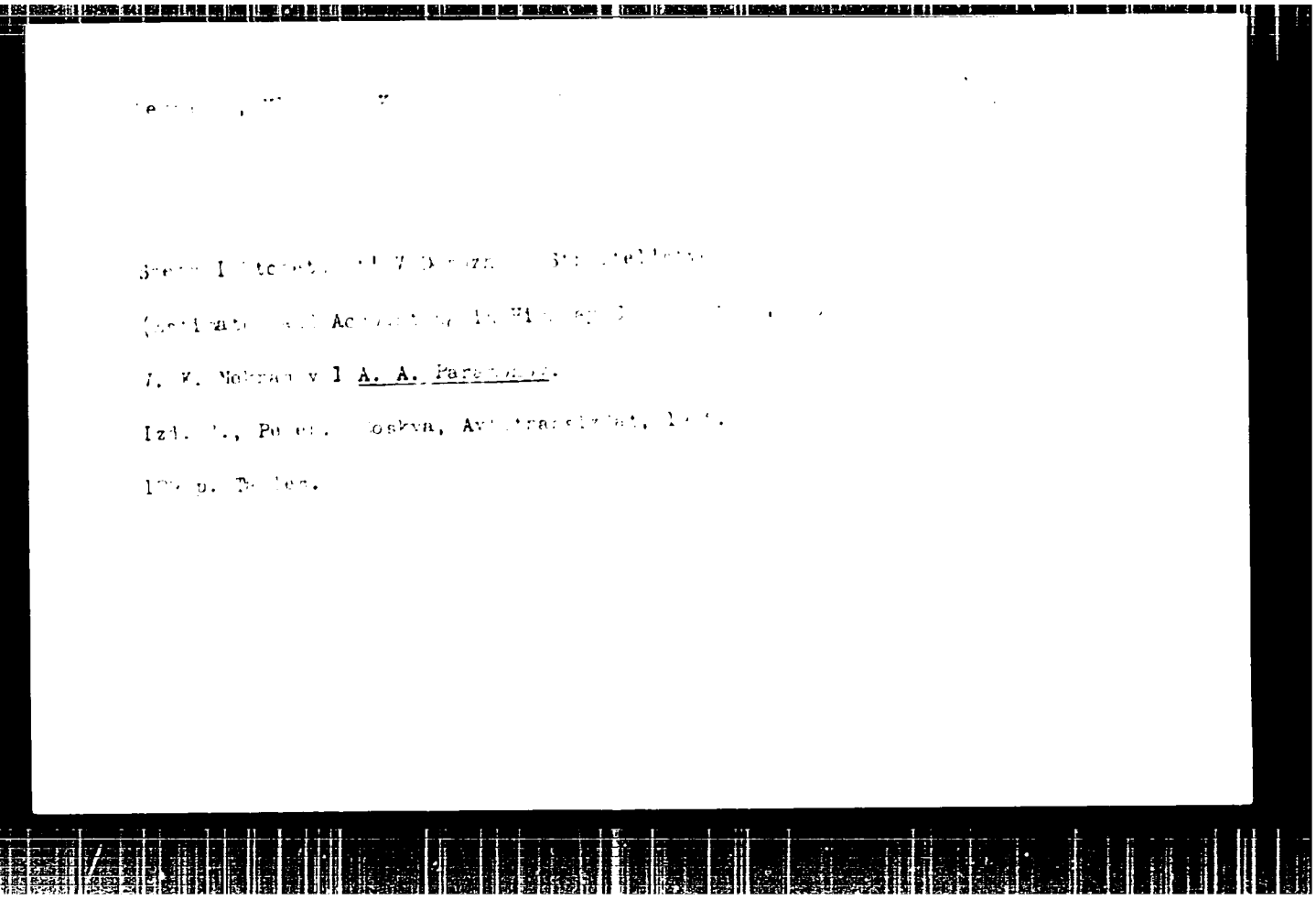

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