

On a Starting-Up Circuit of a Converter Induction Motor 161 - 1958

can be successfully used in two-phase converter motors. In a three-phase motor it is only applicable subject to certain restrictions, as it leads to a distortion of the magnetization curve. 4. The suggested circuit can be of interest under certain conditions, as it is simple and economical. There are five Soviet references. The publication of this article was recommended by the Kafedra elektricheskogo transporta Moskovskogo energeticheskogo instituta (Chair of Electric Transportation at the Moscow Institute of Power Engineering).

ASSOCIATION: Kafedra elektricheskogo transporta Moskovskogo energeticheskogo instituta (Chair of Electric Transportation at the Moscow Institute of Power Engineering); Kafedra elektrotekhniki Moskovskogo vyshego tekhnicheskogo uchiliща im. Baumana (Chair of Electrical Engineering at the Moscow Higher School of Technology imeni Baumana)

SUBMITTED: January 21, 1958

Card 3 of 4

NEKRASOV, Oleg Alekseyevich, kand.tekhn.nauk, starshiy nauchnyy

~~sovetskii~~ .

Frequency regulation of asynchronous driving motors. Izv. vys.
ucheb. zav.; elektromekh. 1 no.6:77-89 '58. (MIRA 11:?)

1. Kafedra elektricheskogo transporta Moskovskogo energeticheskogo
instituta.
(Electric locomotives) (Electric motors, Inc.)

8(6)

AUTHOR:

~~SECRET~~
Nekrasov, Oleg Alekseyevich, Candidate of S.V., 161-58-2-27, 50
Technical Sciences, Senior Scientific Worker, Chair of
Electric Transportation, Moscow Power Engineering Institute

TITLE:

On the Current Supply of Mine Transportation Locomotives for Condenser
Electric Engines (Ob elektrosnabzhenii rudnichnoy otkatki pri
kondensatornykh elektrovozakh)

PERIODICAL:

Nauchnyye doklady vysashchey shkoly. Elektromekhanika i avtomatika,
1958, Nr 2, pp 217 - 222 ("SSR")

ABSTRACT:

The energy-supply system of the transportation with a single-phase current and condenser locomotives shows some peculiarities which consist of an asymmetric load on the train-transformers and in increased difficulties to protect the system against short-circuit currents. These questions are now treated briefly, i.e. on the basis of the author's elaborations and practical experience gained in the transportation by means of electric engines KE-2. The calculations were applied to these locomotives (Ref 1). The results of these calculations are given here. Admissible transformers loads are investigated and calculations of a system for minimum voltage at the

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On the Current Supply of Mine Transportation Means for SSV 't1-1' Electric
Condenser Electric Engines

collector are performed. The system for short-circuit currents is calculated; the reactance protection of a short-circuit current is investigated and it is demonstrated that it is the best means of simplifying and reducing costs of the current-supply system. There are 2 figures and 4 Soviet references.

ASSOCIATION: Katedra elektricheskogo transporta Moskovskogo energeticheskogo instituta (Chair of Electric Transportation at the Moscow Power Engineering Institute)

SUBMITTED March 11, 1988

Card 2/2

8(5), 12(3)

AUTHORS:

Nekrasov, Oleg Alekseyevich, Candidate of SOV/161-58-4-13/28
Technical Sciences, Senior Scientific Associate of the Chair,
Rokus, Grigorij Gavrilovich, Assistant

TITLE:

On the Condenser-auxiliary-machines of Alternating Current
Locomotives With Rectifiers (O kondensatornykh vspomogatel'nykh
mashinakh elektrovozov peremennogo toka s vypryanitelyami)

PERIODICAL:

Nauchnyye doklady vysshey shkoly. Elektromekhanika i avtomatika,
1958, Nr 4, pp 150 - 160 (USSR)

ABSTRACT:

In electro-locomotive construction in the USSR, asynchronous
condenser-motors and three phase induction motors (fed from a
phase splitter (Ref 3)) are used for driving the auxiliary units
of alternating current locomotives with the industrial frequency.
Some results are given here of the examination of auxiliary
condenser motors, in order to determine the most economical,
reliable, and simple circuit diagram. The following units belong
to these auxiliary machines: Motor-ventilators, motor-compressors,
motor-cooling water pumps and motor-generators of the control
circuits. The working conditions of these auxiliary motors of the
single-phase direct-current locomotives are very difficult. On the
current take-off devices of the locomotives, voltage fluctuations

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On the Condenser-auxiliary-machines of Alternating Current SOW/161-58-4-17/28
Locomotives With Rectifiers

of the nominal value are allowed within the limit of from 0.75-1.1, and the range of outside temperature is limited between $+40^{\circ}$ - -50° Celsius. The examination carried out here showed that the installed power of the condensers requires a system of auxiliary condenser-motors and a hydraulic drive of the compressors for starting from the cold, since no switched-off condensers are available if all motors are working. Applied to the electro-locomotive of the NC-type, it is shown in table 1 that this allows reducing the total capacity by 2.2 times, at simultaneous improving the starting properties of all motors. At the same time, the compressors are protected against increased wear during starting at voltages coming close to the nominal voltages. The circuit diagram developed here is illustrated and described on an example in figure 2. The examination showed that with the mentioned circuit diagram and drive respectively, any motor can be started and stopped, independent of the condition of the other motors. When starting all motors in succession, all contactors close with the exception of one. With the circuit diagram for the condenser-motors of the electro-locomotive of the NO-type, 8 contactors must be switched-off by 8 relays, for starting all auxiliary motors. The

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On the Condenser-auxiliary-machines of Alternating Current Locomotives With Rectifiers SOV/161-58-4-19/28

circuit is simple and reliable. The control circuit can also be simple and reliable, especially in the case of contactless relays being used. There are 5 figures, 1 table, and 9 Soviet references.

ASSOCIATION: 1) Kafedra elektricheskogo transporta Moskovskogo energeticheskogo instituta (Chair for Electrical Transportation at the Moscow Institute of Power Engineering), 2) Kafedra teplovogo kontrolya i avtomatiki Moskovskogo energeticheskogo instituta (Chair for Heat Control and Automation at the Moscow Institute of Power Engineering) (1. Nekrasov; 2. Rekus)

SUBMITTED: August 2, 1958

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8(5), 8(2), 12(3)

SCV 105 59-5-8 29

AUTHORS: Nekrasov, O. A. Candidate of Technical Sciences, Chikhin, A. Ya,
Engineer

TITLE: Self-regulation of Diesel Locomotive Generators Using Magnetic
Amplifiers (O samoregulirovaniye тепловозных генераторов с
использованием магнитных усилителей)

PERIODICAL: Elektrichestvo, 1959, № 5, pp 31-36 (USSR)

ABSTRACT: In connection with the production of new heavy Diesel locomotives in the USSR, great attention is being paid to the problem of self-regulation of generators with the use of magnetic amplifiers. On Diesel locomotives the generator excitation is produced by direct current exciters. It is shown here that the use of a synchronous exciter instead of the direct-current exciter greatly reduces the spreading of self-regulation, and offers a possibility of reducing the amplifying coefficient and the capacity of the system for the automatic regulation of the capacity of the Diesel engine and of the generator. But the stability of the automatic regulation is also affected by other factors. The problem of stability with the use of a synchronous

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Self-regulation of Diesel Locomotive Generators Using Magnetic Amplifiers SOV'IC 59 5-8 29

exciter is investigated here and the analytical correlations between the properties of self-regulation and the properties of the individual building groups in the wiring are determined in a general form. This general correlation is ascertained by means of an example for a specific case combination of certain building groups. A method of obtaining this correlation is not given here. The results obtained are then generalized. On the basis of these give a number of some variants of wirings and combinations of building groups of the regulating systems for the generators of Diesel locomotives were investigated theoretically and in practice. The regulation of the system at a reduced number of revolutions of the prime mover and the calculation of the necessary prime mover torque for various building groups were also carried out. The method of the general correlation given here. The experimental control in the laboratory is described. The general correlations given for systems of self-regulation of generators for Diesel locomotives with the use of magnetic amplifiers make it possible to investigate wirings, and to carry out technical calculations of stationary operating conditions. The correlations obtained can also be

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SOV/105-59-5-8/29
Self-regulation of Diesel Locomotive Generators Using Magnetic Amplifiers

used for other drives in a generator-d.c.motor system. There are 6 figures and 3 references, 1 of which is Soviet.

ASSOCIATION: Moskovskiy energeticheskiy institut (Moscow Power Engineering Institute)

SUBMITTED: January 31, 1959

Card 3/3

NEKRASOV, O.A.

S/271/63/000/001/017/047
D413/D308

AUTHORS: Nekrasov, O.A. and Shikhin, A.Ya.

TITLE: On the calculation of operating range for automatic control systems for diesel locomotive electric transmissions

PERIODICALS: Refraktivnyy zhurnal. Avtomatika, telemekhanika i vychislitel'naya tekhnika, no. 1, 1963, 45 abstract 1A248 (Tr. Nauch. energ. in-ta, no. 37, 1961, 75-85)

TEXT: A description is given of a graphic-analytical method for calculating the required variation of magnetizing force \mathcal{E}_M to drive the DC split-pole exciter used on Soviet diesel locomotives to achieve generator self-regulation for constant diesel power. A certain range of variation of magnetizing force is necessary to compensate for a considerable spread in self-regulation characteristics, and is secured by the systems of automatic control of power and current. The calculation is based on the technical data of the machines, exciter circuit diagrams of the diesel locomotive and families of

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D413/D308

On the calculation ...

exciter load curves. These curves are obtained with the generator exciter windings both hot and cold, for a number of independent exciter winding current I_1 with one fixed value of shunt exciter winding current I_s . Using the exciter load curves, a plot of exciter voltage against magnetizing force U_g (Φ) is constructed (for a given value of I_s and generator exciter winding impedance). The actual self-regulation characteristic is derived graphically by finding the intersection points of the curve of exciter voltage against magnetizing force (constructed from the exciter load curves) and the curve of magnetizing force against exciter volts obtained by considering the exciter circuit diagram. An example of the calculation is given. Self-regulation characteristics obtained in practice are stated to have agreed with the calculated one to an accuracy of about 5%. 4 figures. 1 reference.

[Abstracter's note: Complete translation]

Card 2/2

NEKRASOV, Oleg Alekseyevich, kand.tekhn.nauk, starshiy nauchnyy se-
trudnik; GURIN, Nikolay Nikolayevich, inzh.

Utilization of the power of asynchronous short-circuited ma-
chines operating under conditions deviating from nominal.
Izv. vys. ucheb. zav.; elektromekh. 6 no.8:9.6-951 '63.

(MINA 10:9)

1. Tsentral'nyy nauchno-issledovatel'skiy institut Minister-
stva putey soobshcheniya.

TIFHMENEV, B.N., doktor tekhn.nauk, IZOSIMOV, A.V., kand.ekonom.nauk,
NEVRASOV, O.A., kand.tekhn.nauk; LAPIN, V.B., inzh.

Technical and economic comparison of methods for joining a.c. and d.c.
electrified railroad districts. Trudy TSNII MPS no.256:108-122 '63.
(MIRA 16:6)
'Electric railroads)

NEKRASOV, O. A., kand. tekhn. nauk; SHEVCHENKO, V. V., kand tekhn nauk;
REKUS, G. S., kand. tekhn. nauk

Calculation of the heating of asynchronous machines using
a thermal parameter method. Izv vyz ucheb zav; energ 7
no. 1:40-46 Ja '64. (MIRA 17:5)

1. Moskovskiy khimiko-tehnologicheskiy institut. Predstavlena
kafedroy elekrotekhniki i elektroniki.

NEKRASOV, O.A., kand.tekhn.nauk; NOVIKOV, V.Ye., inzh.

Results of the traction and power tests of the experimental VL20
electric locomotive. Trudy TSNII MPS no.286:5-34 '65.

(MIRA 18:8)

NEKRASOV, O.A., kand.tekhn.nauk

Comparing the traction and power characteristics of a.c. multiple-unit trains with collector motors and with rectifier type traction.
Trudy TSNII MPS no.286:71-82 '65.

(MIRA 18:8)

NEKRASOV, O.A., kand.tekhn.nauk; GORIN, N.N., kand.tekhn.nauk

Auxiliary a.c. motors. Trudy TSNII MPS no.286:103-117 '65.

(MIRA 18:8)

NEKRASOV, Oleg, Aleksseyevich, kand. tekhn. nauk, ANDERS, Vitaliy Ivanovich,
assistant

Compensation of the current of an idle three-phase magnetic amplifier.
Izv. vys. ucheb. zav., elektromekh. 8 no.5:573-579 '65. (MIRA 18:7)

I. Rukov. ditej laboratori elektronodvizhnogo sostava TSentral'nogo
nauchno-issledovatel'skogo instituta Ministerstva putey soobshcheniya
'for Nekrasov O. I. na fakultete elektroteknicheskogo transporta Moskovskogo
energeticheskogo universiteta 'for Anders'.

MALYSHEV, V.S., gornyy inzhener.; NEKRASOV, O.P., gornyy inzhener.; RYTIKOV, K.M.,
gornyy inzhener.

Systems of mining thin, flat skarn deposits. Gor. zhur. no.2:14-18
F '57.
(MLRA 10:4)

1. Dzhenichkinskoye rudoupravleniya.
(Mining engineering) (Silicates)

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(MCR) 1526

ALL INFORMATION CONTAINED
HEREIN IS UNCLASSIFIED
EXCEPT AS NOTED

NEKRASOV, P.A., Akademik [deceased]; TYUTYUNNIKOV, A.I.

Experience in using T.S.Mal'tsev's method for shallow tillage heavy loam soils. Trudy MIMESKH 4 no.2:3-35 '59. (MIHA 15:4)
(Tillage) (Mal'tsev, T.S.)

14
The action of potassium and calcium ions upon the fatigued muscle. I. The action of potassium and calcium ions upon the curve of fatigue with indirect stimulation of muscle. I. A. Nekrasov. *Zhur. fiz. khim.* 11, S. 8-10. 1937. (See also 31) In frog muscle nerve preps were fatigued by elec stimulation and then exposed to Ringer solns contg various amt's of KCl and CaCl₂ (0.050-0.080-0.104% each). Control exps with unfatigued muscles were made. K⁺ and Ca²⁺ in increased concn produced in fatigued muscles strongly marked recovery. The K⁺ effect was transitory and followed a more prolonged depression, while the recovery effect by Ca²⁺ was more slowly attained, was much more lasting and the total

activity was greater than in the control unfatigued muscle. This effect is not explained by the washing out of fatigue products as shown in control exps. The recovery effect is produced by removal of K⁺ or Ca²⁺ 1.5-2.0 times that in ordinary Ringer soln. In lower concn, Ca²⁺ produces the greater effect, while in higher concn, the effect of K⁺ is more marked. The usual effect manifests itself in two phases: a rapid rise of the curve with a subsequent fall, rapid with K⁺ and gradual with Ca²⁺. Occasionally 3 phases were observed initial fall, followed by a rapid rise and then by a gradual decline. Increased concn of K⁺ acts upon the muscle fatigued in the same general way as upon the fatigued muscle, only the initial positive phase is either weak or missing followed by depression of function which is the basic phase. Ca²⁺ acting on the unfatigued muscle either produces no effect or depresses the contractions without any subsequent increase, and causes in the later stages a retardation of the fatigue stage. The strong similarity of the action of Ca²⁺ upon muscle and of the action of sympathetic nervous system is emphasized. II. The action of potassium and calcium ions upon the fatigue curve of muscle in asphyxiation and direct stimulation. *Zhur. fiz. khim.* 13, 735. 1939. (German 73)
In these exps the muscles were first subjected to asphyxiation by immersing in Ringer soln contg KCN instead of the KCl (0.002 M) and were then treated with increased concn of KCl or CaCl₂ in Ringer soln still contg the above concn of KCN. The controls were treated with Ringer-KCN only. In some exps

the Ca effect was compared in KCN-treated preps with the effect upon muscles subjected to an oxygenated Ringer soln. without KCN. In the caps, with direct stimulation normal and curarized muscles were compared. The preliminary treatment with KCN not only did not diminish the ion effects upon the nerve-stimulated muscle, but actually increased them. The basic character and phases of the effects of these ions remain the same as in the normal fatigued muscle, except that the initial drop in activity is uniformly lacking. This initial phase is evidently related to the oxidative processes in the muscle. The K and Ca effects upon the directly stimulated normal, not curarized, muscle are in general the same as upon nerve-stimulated muscle. In the curarized fatigued muscle the effects are different. Ca⁺⁺ produced a transient, slowly increasing diminution of contractions which then gradually abates, so that the amplitude of the contractions reaches that of the control muscle; the K⁺ under the same conditions produces its usual biphasic effect of initial stimulation followed by depression of the contractions. The character of the curves of the unfatigued muscles is in general the same as that with the fatigued preps., only the effects are weaker and require higher concns. of the two ions and more prolonged exposure to them. The K-treated muscle performs less work and is more rapidly fatigued than the control, while the muscle treated with Ca, even before the onset of fatigue, compares well with the control or exceeds it in this respect. These data are correlated with the known physiol. effects of K⁺ and Ca⁺⁺ upon membrane permeability and potentials, irritability and chronaxie and of K⁺ upon viscosity and contractility of muscle.

W. A. Verhaeg

Analysis of the action of the sympathetic nervous system
and of potassium and calcium salts on the skeletal muscles
I. The action of the normal sympathetic system and of
potassium and calcium salts on muscle poisoned with
monooiodoacetic acid P. A. Nekrasov et al.
U.S.S.R. No. 20, 817, 27 (1949) (Chemical Abstracts 1950, 44,
1163). A muscle fatigued and poisoned with $\text{C}_6\text{H}_4\text{IO}_2\text{Na}$
fails to react to the stimulation of the sympathetic system or to
potassium and K salts in concentrations producing
normal contraction. Calcium salts were taken as the only
substance which can activate the muscle. It was found that
the muscle can react to the stimulation of the sympathetic system

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analysis of the action of the sympathetic nervous system
and of salts of potassium and calcium on the skeletal

muscles. II. The effect of salts on muscles possessed by
monoiodoacetic acid under various conditions of transfer
of the stimulus from the nerve to the muscle. P. A.
Nekrasov and R. P. Chivzov. *Zh. Fiziol.* 1938, 13, No.
5, 311-21. (in Russian). *Biochem. Z.* 1938, 310, No.
1, 4-33. ¹⁴⁴⁸ Studies on the effect of potassium
and from frogs indicated that the failure of salts of calcium and
KCl, as well as of the so-called "active" salts of potassium
to produce any effect on muscles possessed by a reflex, is due
not to any influence of the salts on the structure of the
nerve fibers, but rather to the fact that the fibers are
connected with the muscle and not with the muscle itself.
A. V. M. and
stimulus.

Changes in the gaseous metabolism as an indication of fatigue in long continued physical work. I. Changes in the gaseous metabolism while moving or standing with a load. A. H. Lowman, P. A. Dehany, N. S. Shachter, V. D. Shulman and V. S. Lardé. *J. Physiol.* 138, 31-38, 1958. The respiration rate of subjects during long duration fatiguing movements with a load remained unaltered throughout the period. The same subjects during the control period, however, showed a decrease in the rate in the initial period of work and a rise at completion of the tasks. With static work, there was no increase in the gaseous metabolism. II. Changes in the gaseous metabolism during the lifting of metal bars and the polishing of metal. A. H. Lowman, N. S. Shachter, P. A. Dehany and V. D. Shulman. *J. Physiol.* 138, 39-44, 1958. II. 1958.

CP

The action of blood serum on fatigued muscles. I
P. A. Nekrasov and N. V. Nekrasova. J. Physiol.
U.S.S.R. 21, 519-51 (1930). Chem. Zentralbl. 1930, II
1627, ref. C.A. 23, 2500P. - When a few drops of blood
from the frog was placed on a fatigued muscle, a
temporary restoration of contraction appeared. The
effect was similar to that of adrenaline and Ca. Poisoning
of the muscle with KCN made the effect more pronounced.
This effect can be explained neither by the sugar nor the
salt contained in the serum. The active factor in the
serum is comparatively stable, since it is destroyed only
after long heating.

6 A
The action of blood serum on fatigued muscles. II
The action of serums from different animals on the fa-
tigued muscle when applied in different ways. N. V.
Nekrasova and P. A. Nekrasov. *J. Physiol.* (S. S. R.)
24, 1015-31 (1939). *Chem. Zbl.* 1939, I, 2017, cf. C. A.
33, 2745, 34, 5139. The active agent of the serum which
revives the fatigued muscle occurs in different species in
the frog, rabbit, cat, dog and man. The serum is more

effective when applied by perfusion than by external
application. The active principle still remains in serum
which has been stored 2 days, in that through which CO₂
has been bubbled for 1-2 hrs., and in that which has
been heated, even in slightly alk. soln. Boiling
for 10-15 min. completely destroys the active principle.
M. G. Moore

The action of blood sera on fatigued muscles. III.
The effect of the sera of venous and arterial blood, and the
influence of labor on the serum effect. P. A. Nezhoda
and N. V. Nezheva. *J. Physiol. U.S.S.R.* 27 (1962). Serum ob-
tained from the venous blood of dogs and rabbits is less ac-
tive in stimulating fatigued frog muscle than is the serum
of arterial blood. The serum of human blood, taken after
slight labor, is more active than when taken at rest. After
hard labor all the serum activity is lost. It is suggested
that the substances responsible for the activation are ad-
sorbed from arterial blood as it passes through the capil-
laries. S. A. Kurnik

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NEKRASOV, P.A., prof.; ZEMSKAYA, Ye.I., assistant

Influences from the receptors of the nerve trunks on the spinal
motor reflexes. Sbor. tverd. Kursk. gos. med. inst. no. 13:280-286
'58. (MIRA 14:3)

1. Is kafedry fisiologii (sav. - prof. P.A.Nekrasov) Kurskogo
gosudarstvennogo meditsinskogo instituta. (REFLEXES)
(RECEPTORS (NEUROLOGY))

NEKRAZOV, P.A.

Physiology of the receptors of the peripheral nerve trunks. Fiziol.
zhur. 47 no.9:1105-1113 9 '61. (MG A 14:9)

. From the Department of Physiology, Medical Institute, Kursk.
(RECEPTORS (NEUROLOGY))

NEKRASOV, P. Ya. (Kiyev, 74, ul. Verbovaya, d. 2b.)

A case of angioblastoma of the mediastinum. Nov. chir. arkh. 5:123-124
S-0 '58. (MIRA 12:1)

1. Kafedra onkologii (zav. - prof. I.T. Shevchenko) Kiyevskogo instituta
usovershenstvovaniya vrachey.
('EDIASTINUM--TUMORS')

LESECHENKO, P.I. (Kiyev, ul. Vorovskogo, d.14, kv.14); NEKRASOV, P.Ya.

Diagnosis and treatment of melanomas of the rectum. Nov.khir.arkh.
no.5:95-97 S-0 '99. (MIRA 13:3)

1. Kafedra onkologii (zavedyushchii - prof. I.T. Shevchenko) Kiyev-
skogo instituta usovremenizovaniya vrachey.
(MELANOMA) (RECTUM--TUMORS)

POKROVSKIY, S.A. (Kiyev, ul. Tolstogo, d.7, kv.1); SEMENOVA, A.M.;
NEKRASOV, P.Ya.

Radiotherapy in malignant bone tumors. Nov. zhir. arkh. no.2:
89-96 Mr-Ap '60. (MIRA 14:11)

1. Kiyevskiy nauchno-issledovatel'skiy rentgeno-radiologicheskiy
i onkologicheskiy institut.
(BONES--CANCER) (RADIOTHERAPY)

VOLIN, Ye.I. (Kiev, Tsvetnoy blu, kv.17); NIKONOV, I.Ya.; LITVINOV, V.P.; LOBINA, Z.F.

X-ray, radio and surgical method for treating internally or externally located cancer. Klin. khir. no.3:12-19 1961.

1. Radio-khirurgicheskiy otdei. (zav. - zаслуженный деятель науки, prof. I.T.Shevchenko) kievskogo nauchno-issledovatel'skogo radiologicheskogo i onkologicheskogo instituta.

NEKRASOV, Roman Mikhaylovich; ALYAB'YEV, V.I., red.; MIKHAYLOVA, L.G.,
red. izd-va; VDOVINA, V.M., tekhn. red.

[Rigging of skidding and loading equipment] Montazh trelevochno-
pogruzochnogo oborudovaniia; prakticheskoe rukovodstvo. Moskva,
Goslesbumizdat, 1961. 130 p. (MIRA 16:2)
(Lumbering)

AMERICAN V. V.I., KING. (Hannibal) - 1960, U.S.A.

...quintal of wood from the forest and 100 ft. of timber
large by 12 in. - small. - W. 25 ac. 14 - 1/2. 12.

(Lumbering—activity)

PERFILOV, M.A.; ALYAB'YEV, V.I.; NEKRASOV, R.M.; GRECHISHNIKOV, V.V.;
MAZHIN, G.K.; FEDOROV, N.S., otv. red.; KALININA, L.M., red.
izd-va; SHIBKOVA, R.Ye., tekhn. red.

[Album of auxiliary skidding and loading equipment] Al'bum
vespomogatel'nogo trelevchno-pogruzochnogo oborudovaniia. Mo-
skva, Goslesbumizdat, 1962. 119 p. (MIRA 16:4)
'Lumber—Transportation)

ALVAN MCKEE, 70, LIVING IN NEW YORK CITY; ALVAN, JR.
~~ALVAN MCKEE~~, 38, NEW YORK CITY,

[Can always be identified here by his name or by his
three- letter code. In my opinion he is a breakaway type
individual who has lost contact with his former
Soviet supporters. He seems to be a very intelligent
man, but I don't know if he is reliable. He is
interested in politics, particularly the Soviet Union, and
he has been writing to me for some time now. He is
not a member of the KGB, but he may be.

NEFRASOV, Roman Mikhaylovich; ALYABEEV, V.I., red.

(Assembly of equipment at cutovers. Kontakt ogranichenie
na lesosekakh. 2. Izd. Moscow, Leningrad, 1942.
247 p.)

ALYAB'YEV, V.I., kand.tekhn.nauk, MASHIN, G.K., inzh., NEKRASOV, R.N., inzh.,
TIMOFEEV, L.G., inzh.

The new TPU-4 Ysniiye skidding and loading equipment. Mekh.i avtom.
proizv. 14 no.5:32-35 My '60. (MIRA 14:2)
(Lumbering-Machinery)

MERKASOV, S. A.

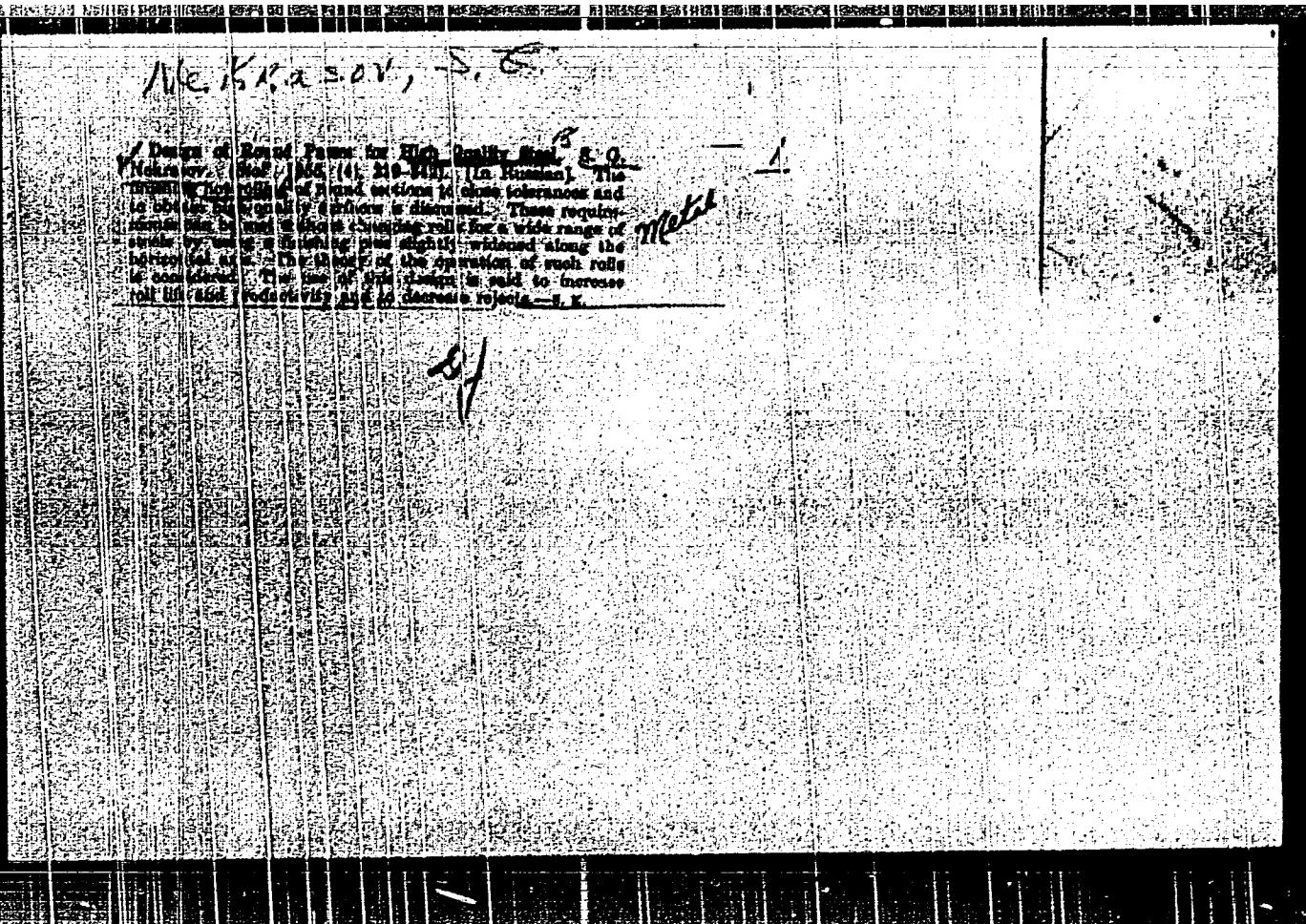
USSR/Moscow/Leningrad--Machine construction

Card 1/1

Author : Merkashov, S. A., engineer
Title : About methods of projection without making a copy
Periodical : Vest. mash. 34/3, 101, Mar/1954
Abstract : The VMP-1 apparatus is intended for direct manifolding of drawings from pencil originals, for photographic copying without changing the scale, and for mechanized chemical copying of drawings. Much time is saved by this apparatus. Drawings.
Institution :
Submitted :

MURASOV, Sergey Afanas'yevich; KUZNETSOVA, N.I., red.; GALICHENKOVA,
A.N., red.

[Manual for inspection commissions of the plant-factory and local
committees] V pomoshch' revisionnym komissiam PZMK. [Moskva] Isd-
vo VTsSPS Profisdat, 1957. 47 p.
(Trade unions)



SHURALEV, M.V., inzhener, NEKRASOV, S.G.

Rolling of square bar steel with sharp edges. Stal' 16 no.11:997-
999 N '56.
(MIRA 10:1)

1. Zlatoustovskiy metallurgicheskiy zavod.
(Rolling (Metalwork))

130-9-13/21

AUTHORS: Shuralev, M.V. (Eng.) and Nekrasov, S.G. (Calibration

TITLE: Operation of a 600 Mill according to a New Schedule.
(Rabota stana 600 po novomu grafiku)

PERIODICAL: Metallurg, 1957, Nr 9, II.27-28 (USSR)

ABSTRACT: The 600 mm roll diameter mill at the Zlatoustovsk metallurgical works rolls rounds of carbon and alloy steel 90 to 150 mm in diameter from 170 x 170 and 190 x 190 mm square billets weighing 520 to 720 kg. The mill consists of four three-high stands with two continuous furnaces. The rolling schedule and pass designs were recently revised, leading to higher productivity on account of more uniform loading of the stands and working with overlay. The setting and control of the mill was facilitated by the use of separate stands for producing the starting square billets, and separate furnaces were also used for different sizes. An annual economy of about 500,000 roubles has been effected. Pass designs and rolling schedules for the old and revised systems are given. There are 3 figures.

ASSOCIATION: Zlatoust Metallurgical Works (Zlatoustovskiy
Metallurgicheskiy Zavod)

AVAILABLE: Library of Congress.
Card 1/1

AUTHORS: Shuralev, M.V., and Nekrasov, S.G., Engineers.

TITLE: Determination of Spread during Rolling (Oprudeneniye ushireniya pri rokatke)

PERIODICAL: *Stal'*, 1958, no.1, pp. 57 - 60 (USSR).

ABSTRACT: Four methods of calculating spread in rolling (Refs. 1, 2, 3 and 5) were checked by comparing the calculated results with those actually obtained on rolling on three different mills. Characteristic data on mills are given in Table 1. The experiments were carried out as follows: a) templets were cut off from various strips after passes at the same setting of the rolls; b) the temperature of the strips was determined by an optimal pyrometer; c) transverse dimension of cold templets, perimeters of templets and their cross-sectional areas were measured and d) the spread was also calculated by the above four methods and the determined and calculated results compared. The comparison is given in Table 2. The results obtained by the calculations differed from the experimental results, so that all methods of calculating require some experimentally determined correcting coefficients. Therefore, it would be advantageous to use for practical purposes the most simple formulae, introducing into them the corresponding experimental coefficients. Such formula was obtained by the authors

Ca:d1/2

Determination of Spread during Rolling

17-1-1-24

(Formula 6) based on S.N. Petrov's formula (Ref.6). The formula proposed is suitable for determining spread in roll passes and on a smooth roll. A comparison of results calculated using the above formula with the actual spread (Table 2) indicated that a good agreement was obtained. It is stated in the editorial note that the use of the proposed formula under conditions of other works requires a preliminary experimental check of correcting coefficient m for various passes. There are 2 tables, 1 figure and 6 Russian references.

ASSOCIATION: Zlatoust Metallurgical Works (Zlatoust' vskiy metalurgicheskiy zavod)

AVAILABLE: Library of Congress
Card 2/2

SOV/133/58-9-17/29

AUTHORS: Shuralev, M. V., ~~Maxrasov, S. G.~~ (Engineers) and Azarenko, B. S. (Cand.Tech.Science)

TITLE: Review of the Book of A. A. Protasov and F. F. Zuyev, "Calibration of Rolls for Rolling High Speed Cutting Steel" Retsonziya na knigu A. A. Protasova i F. F. Zuyeva, "Kalibrovka valkov dlya prokatki bystrorezhushchey stali")

PERIODICAL: Stal', 1958, Nr 9, p. 825-827 (USSR)

ABSTRACT: The book was published by Metallurgizdat in 1956. The review is favourable.

ASSOCIATION: Zlatoustovskiy metallurgicheskiy zavod, VTU im Baumana (Zlatoust Metallurgical Works and MVTU im Baumana)

Card 1/1

NEKRASOV, S.O., inzh.

Improved grooving for punching die shapes no. 3. Izv.vys.ucheb.zav.;
chern.mat. no.11:145-147 N 158. (MIRA 1211)

1. Zlateoustkiy metallurgicheskiy zavod. Rekomendovano kufadroy
obrabotki metallov dvoleniyem Sibirskego metallurgicheskogo instituta.
(Rolls (Iron mills))

SOV/133-59-1-13/23

AUTHORS: Shuralev, M.V. and Nekrasov, S.G.

TITLE: Roll-pass Designing and Rolling of Shaped Profiles from Alloy Steels (Kalibrovka i prokatka fasonnykh profiley iz legirovannoy stali)

PERIODICAL: Stal', 1959, Nr 1, pp 58 - 63 (USSR)

ABSTRACT: Rolling of shaped economical profiles (channel beams PS-102, PS-103 and PS-120) from alloy steels (1Kh18N9T, 30KhGSA and Kh17N2) (Figure 1, Table 1) which are supplied to consumers instead of strip resulted in a 20-30% economy in the consumption of metal and simplified the manufacturing of finished parts. The rolling is done on a three-stand mill 400. Billets are heated in a two-zone continuous furnace with bottom heating. The dimensions of roll passes are given in Tables 2 and 3 and Figures 2 and 4. Some special features of rolling alloy steels are discussed. It is pointed out that for steel 1Kh18N9T the permissible angles of grip are 2-3° lower than for carbon steels which is explained by a higher resistance to deformation of this steel at the rolling temperature. Steels 1Kh18N9T and Kh17N2 are strongly spreading during rolling. Therefore, in designing roll passes for these steels, the limitation of spread should be smaller than

Card1/2

SOV/133-59-1-13/23

Roll-pass Designing and Rolling of Shaped Profiles from Alloy Steels

for carbon steels. In designing finishing passes an increased shrinkage of alloy steel (particularly 1Kh18N9T) should be taken into consideration. There are 6 figures and 4 tables.

Card2/2

. 25(1)

SOV 148-59-1-14 1;

AUTHOR: Nekrasov, S.G., Engineer

TITLE: Computation of Height Deformation in Non-Uniform Rolling . С
расчёте высотной деформации при неравномерном отжатии.

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy - Chernaya metallurgiya,
1959, Nr 1, pp 121-126 (USSR)

ABSTRACT: Average reduction for computing deformation of metal in groove
rolling was determined by the method of shifted volume suggest-
ed by I.Ya. Tarnovskiy [Ref 1, 2]. Complicated calculation
was the basic deficiency of this method. The author presents
a formula: $\frac{1}{\eta} = \frac{h_0}{h_1} = \frac{\omega_0}{\omega_1}$, where η is the average height

coefficient of deformation; h_0 and h_1 are the initial and final
average heights of the strip, and ω_0 and ω_1 are the initial
and final cross-section surfaces of the strip. This formula
serves to compute height deformation in non-uniform absolute
and relative reduction by the width of the deformed strip,
without preliminary equalization of absolute reduction. The
proposed method can be used to compute height deformation in

Card 1/2

SOV 146-52-1-14 19

Computation of Height Deformation in Non-Uniform Rolling

rolling with different-shaped grooves.

There are 5 sets of diagrams, 3 tables and 13 viet references

ASSOCIATION: Zlatoust'skiy metal'noe zavod (Zlatoust Metalurgical Plant)

SUBMITTED: August 20, 1958

Card 2/2

S/137/60/000/011/018/043
A006/A001

Translation from: Referativnyy zhurnal, Metallurgiya, 1960, No. 11, p. 117.
261⁴⁴

AUTHOR: Nekrasov, S.O.

TITLE: Rolling of High-Speed Steel at the Zlatoust Metallurgical Plant

PERIODICAL: Tr. Mezhvuz. nauchno-tekh. konferentsii na temu: "Sovrem.dostizh. prokatn. proiz-va", Vol. 2, Leningrad, 1959, pp. 220 - 227

TEXT: An ingot, weighing with the riser 200 kg, is rolled to a blank of 78 x 78 mm on a 620 mm three-high mill after heating for 10 hours up to 1,170 - 1,200°C (grade P-18 (R-18)) or to 1,150 - 1,180°C (grade P 9 (R9)) with twice preheating. Grooving of the rolls includes 9 box-, 8 rhombic- and 2 square grooves. R18 steel is rolled in 19 passes with a mean coefficient of extension equal to 1.15. R9 steel is rolled in 15 passes with a mean coefficient of extension equal to 1.19. The effective yield is 76.5 - 77.5%. The blank is rolled to a finished shape after preheating to the same temperature, for 2 hours

Card 1/2

S/137/60/000/011/018/043
A006/A001

Rolling of High-Speed Steel at the Zlatoust Metallurgical Plant

30 minutes in the case of 78 x 78 mm sections and for 1 hour 50 minutes at 30 x 30 mm sections with an extension coefficient up to 1.63 in oval grooves and 1.45 in square grooves. The temperature at the end of rolling process is 980°C.

P.O. ✓
—

Translator's note: This is the full translation of the original Russian abstract.

Card 2/2

SHURALEV, M.V. ; NEKRASOV, S.G., kalibrovshchik

Charge in the grooving of no.4 stamp strips. Metallurg 4 no.3:26-27
Mr '59. (MIRA 12:4)

1. Zamestitel' glavnogo inzhenera Zlatoustovskogo metallurgicheskogo
zavod (for Shuralev). 2. Zlatoustovskiy metallurgicheskiy zavod (for
Nekrasov).
(Rolling mills)

A - 21

AUTHOR Nekrasov,

TITLE Rolling of new E-profiles by cold forming.

PERIODICAL Referaty, st. 1, Nauk. organiz., 1970, No. 1, 1970, 1139
"Tr. Konferentsii Tekhnicheskogo proizvoda" (Transl. of "Soviet Metalworking, Metallurgicalization", 1970)

TEXT Data on grooving and rolling of profile flanges E-type channel type are given. Rolling of profile flanges is carried out in four cold forming passes from billets of carbon steel, grade X 45, Kr 40M and 3KFGA (30Kh13A). The coefficient of narrowing of the billet for the end temperature of rolling 980 - 1,038° was 1,14 for steel Kr 40M and 1,15 for steel 3KFGA. The grooving for profiles P1-P2 and P3-P4 is given. It turns out that for grooving shaped profiles from high-alloyed steels it is necessary to take into account the deterioration of metal gripping which is lower than for carbon steel, the higher value of strain rigidity, shrinkage, and spread.

Abstracter's note Complete translation.

A. D. A. V.

Card 1/1

二三九

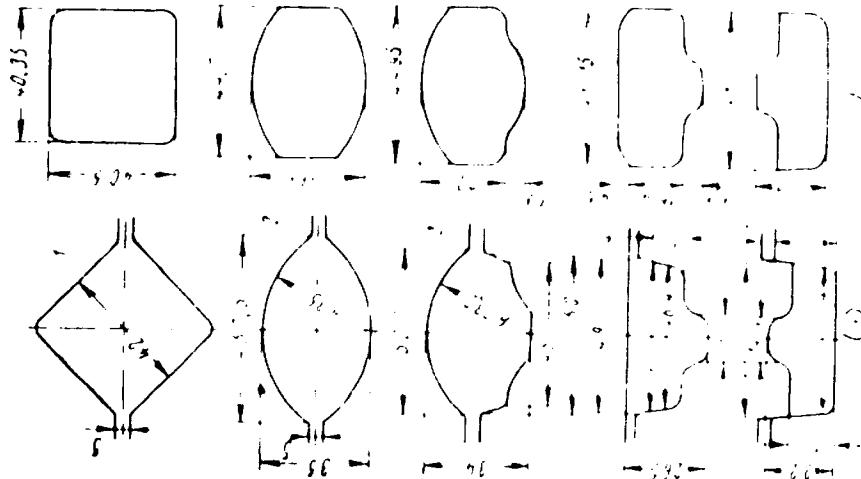
AUTHOR : *Chapman, M. V., and others*
TITLE: *Refrigerant-12 and its mixtures with R-13*
PERIODICAL: *Monatsh. Chem.*, No. 1, 1937 (1938)

ABSTRACT: K. Zinn and M. L. Tuck have proposed (Zinn and Tuck, 1971) a model for the diffusion of a gas in a rotating fluid. The model is based on the KINEMATIC APPROXIMATION (see Fig. 1). The solution is reduced to that passed from a square cylinder rotating at a constant angular velocity ω in a fluid which rotates about its center. The following problems are presented: (1) a stationary cylinder of finite length is rotated in a fluid; (2) a cylinder of finite length is rotated in a fluid with finite viscosity; (3) a cylinder of finite length is rotated in air. The solution is obtained for three shaped I-beam bases (see Fig. 2) and for a circular base. The cylinder is rotated in a square fluid. (1) The cylinder of finite length is a semielliptical cylinder (see Fig. 3); (2) the cylinder of finite length is a semielliptical cylinder (see Fig. 4); (3) the cylinder of finite length is an I-beam base with a top elliptical part (see Fig. 5).

... was not used. It was noted that the
heat shield had been partially broken off the
airframe at the attachment point to the
airframe. The heat shield was attached to the
body of the aircraft after (or prior to) separation
and did not appear to have been damaged or
showed signs of being impacted by the ground or
other aircraft. The heat shield was
approximately 14 inches long and 10 inches wide.

None

REVERSE SIDE - CARD 3 OF 4



Card 3 of 4

FIGURE 1
PS-1000

R (List all countries involved)

Permit me to add a few comments to your question.
A. In the exchange of information between the two governments
of the United States and the Soviet Union, there has been a
tendency to assume that the other side is fully informed about
our policies and our intentions. This is not true. We have
not told the Soviets (or anyone else) what our policy is in
() Asia. We have not told them what our policy is in
Europe. We have not told them what our policy is in
Latin America. We have not told them what our policy is in
Africa. These are the major areas of uncertainty.

ASSOCIATION: Zaire, Libya, Mengistu, etc., etc.

CIA-1

NEKRASOV, S.Q.

Calculating the horizontal projection of the contact area
in oval groove rolling. Izv.vys.ucheb.zav.; chern.net.
no.6:88-94 '60. (MIRA 13:7)

1. Zlatoustovskiy metallurgicheskiy zavod.
(Rolling(Metalwork))

S 14870 000 01 36 1 0 0
A161 A171

AUTHOR: Nekrasov, S. G.

TITLE: The grooving of straightening machine rolls for rolled bars.

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya metalurgiya,
no. 12, 1960, 77 - 83

TEXT: Rapid and nonuniform wear of square roll grooves is the reason why most metallurgical plants use grooves with a curved outline for round bar steel. Three kinds of groove are discussed - 1) Of geometrically true half-circle shape (without divergence); 2) Circular with divergence (width at the base along the straight line); 3) Two-radius profile (Fig. 1). The article includes the calculation formulas (final formulas and their derivation). Information is given on round grooves used at the Zaporozhstal' Metallurgical Plant (Fig. 6) and their features and dimensions. The calculation range of the grooves is determined by their holding capacity, which diminishes with increasing the space between metal and groove sides, and there is a critical α value (α_{cr}) that is calculated with the formula

$$\alpha_{cr} > \frac{D_{min}}{2} \cdot (\sqrt{2K} - 1)$$

Cari 1.5

C H A P T E R

A. T. H.

The first virtue of straightening machine fiber.

where D_{min} is the minimum trile diameter to be considered, θ is the angle of the groove, and K - the "universal factor" dependent on the type of bearing. The empirically determined optimum angle values θ and the universal factor K are given in the 40×10^3 range. Straightening trials were conducted at the Zlatoust Plant at different times. In 1950, it was found (and it is fairly true) the size of the fit and the value of the universal factor K depend on the work diameter. The value was the smallest and K the largest for the largest diameter of bearing in the bearing assembly. The next largest diameter had a second groove with (without divergence). Straightening trials were conducted with kinematics.

$\lambda \in \mathbb{C}, \mu$ for μ a parameter in \mathbb{C} or \mathbb{R})

Higher K factors reflect a loss of material from the cutting tool pass through the passes several times. Wear is measured in microns per meter above 15 mm, i.e. the minimum wear rate. The "K factor" is the "saliency factor" and the minimum wear is $W = K \cdot M^{\alpha}$, calculated for the case obtained with two-ball test procedure. The K factor is determined by test:

Carrie

S/140/700/100,000-1770
A161/A171

The grooving of straightening machine rolls ...

at $r = \frac{D_{\max} + D_{\min}}{2}$ the χ is < 1.6 for diameters 25 - 60 mm, and < 1.7 for diameters up to 60 mm; above 60 mm; at $r = \frac{D_{\min}}{2}$ it is < 1.7 for diameters up to 60 mm, for diameters above 60 mm. Both these limits of groove width are given by the plant to the plant; the "univ. facility" limit is $\chi = \frac{D_{\max} - D_{\min}}{D_{\max}}$. Two-radius groove rolls wear slower and more uniformly than three-radius groove rolls, and do not loose the holding capacity during operation campaign. An example of two-radius groove calculation is given for 26 - 44 mm diameter at $\chi = 15^\circ$: 1) Groove depth and radius $R = 7.5$, $B = 1.1 D_{\max} = 1.1 \cdot 44 = 48.4$ mm; $r = \frac{D_{\max}}{2} = \frac{44}{2} = 22$ mm. ✓
 $R = \frac{0.25 \cdot B^2 + r^2 - B \cdot r \sin \chi}{2r_m - B \sin \chi} = \frac{0.25 \cdot 48.4^2 + 22^2 - 48.4 \cdot 22 \cdot 0.707}{2 \cdot 22 - 48.4 \cdot 0.707} = 72.4$ mm.

$$r = \frac{D_{\max}}{2} = \frac{44}{2} = 22 \text{ mm.}$$

$$2) \text{Groove depth } H = r + \sqrt{(B-r)^2 - (R-r_m)^2 \sin^2 \chi} - (R-r_m) \cos \chi = 17 + \sqrt{(72.4-22)^2 - (72.4-22)^2 \cdot 0.707^2} - (72.4-22) \cdot 0.707 = 27.6 \text{ mm.}$$

There are 6 figures.

Card 3/5

The grooving of straight and saddle rails...

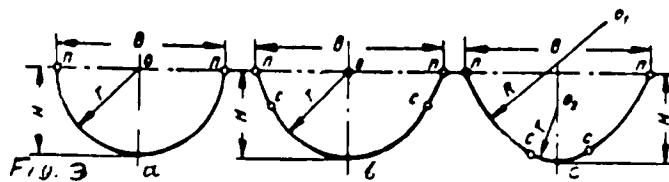
186, 210
A 161 217

ASSOCIATION: Zlatoustivskij metallopreryabnyj zavod (Zlatoust Metal Forming Plant)

SUBMITTED: April 17, 1952

213.

Legend: a - circular;
b - with liverwort;
c - tree-fern.



Carri 1/5

NEFRASOV, S. V.

Design of improved thin-walled square - oval system of profiles for aircraft alloy steels. Izdatelstvo avia. promst. tekhnicheskoy literatury

Izdatelstvo metalurgicheskoy literatury
(VNIIM)

NEKRASOV, S.G., inzh.

Design of rectangular grooves for the rolling of carbon and alloyed
steel. Stal' no.6:541-542 Je '61. (MIRA 14:5)

1. Zlatoustovskiy metallurgicheskiy zavod.
(Rolls (Iron mills))

2/17/86 10:45 AM
AAT/AM

AUTHOR: Shuralev, M.V., Chief Engineer Deputy, Nefmas v., S.M.

TITLE: Economical Alloyed Steel Sections

PUBLICATION: Metallurg, 1961, No. 4, pp. 21 - .*

TEXT: New economical sections are now being rolled in the three-stand mill No. 2 at the Zlatoust Metallurgical Plant (Figure 1). The sections are made of 20^{kg} (20Kh3MVP) and 30^{kg} (30KhGSA) alloyed steel. Each section has 10 closed passes: passes 1 - 5 on stand No. I; pass 6 on stand II; passes 7 - 8 on stand III (Figure 2). A rectangular strip is used as initial material for the rolling of shaped sections obtained from a ribbed groove with rounded edges (Figure 3), so that the initial strip width can be altered during rolling, when switching over from one section to another one, and the thickness of the strip can also be controlled. Each of the 7 sections shown in Figure 4 is obtained from a ribbed groove designed for rolling with limited widening. When designing the grooves in the rolls of stand III it was taken into account that due to the limited widening the strip jams in the closed pass and tends to turn laterally. Therefore the closed passes of the pre-finishing grooves were arranged on the left, stand I/II.

3124 3124 3124
Axx(Axx)

Economical Alloyed Steel Sections

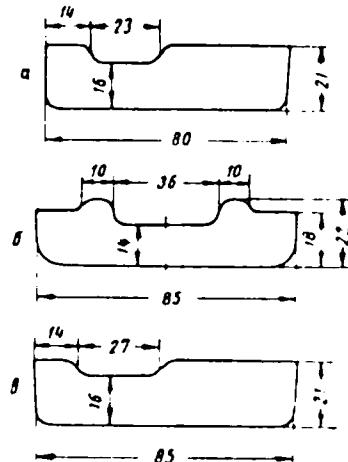
roll and those of finishing grooves on the lower roll. This arrangement makes the strip bend downwards. To prevent this the lower forged steel wires are placed into the closed passes of the lower roll. The described arrangement of grooves requires no new set of rolls only for stand III, and the boring of a ribbed groove in the new set of rolls only for stand III. Roll changing is only necessary for stand III when switching over to the method of economical rolling of sections. To determine the nature of strip deformation and the filling of grooves during the rolling of the strips, templets were taken from strips of the intermediate passes. When rolling section a) (Figure 1) of 20Kh3MVP steel the strip showed lateral bulging when entering the ribbed groove. The bulging was not fully eliminated by the end of the groove. When rolling a rectangular strip in the first stand at a rate of 1000 mm/min, reduction in length of the peaks of sections was observed. At the same time uniform compression over the width of the groove was equal to 10 mm at the center and 6 mm at the edges. The final shaping of peaks is performed in the second stand at a rate of 1000 mm/min. When rolling sections a) and b) (Figure 1) the strip enters the ribbed groove with the metal in agreement with calculations. Data concerning the rolling of economical sections are presented in the table below. The cost of the described sections yields 22% savings of expenditure on material and

Economical Alloyed Steel Sections

8/130/61/300/004/TY 3/1961
AU06/AU01

Reduces labor-consuming machining operations when manufacturing machine parts.

Figure 1: Economical sections; a - -01 (GK-01); b - GK-09; c - GK-014

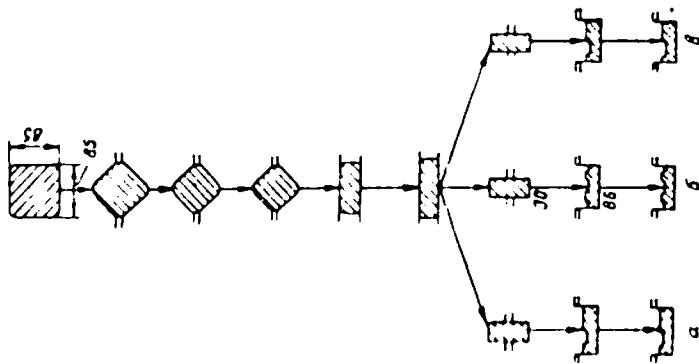


Card 3/8

Economical Alloyed Steel Sections

S/130/61/000/0-4/MC3/01
AC06/AOC:

Figure 2: Schematic diagram of rolling sections; a - GK-01; b - GK-09;
c - GK-014

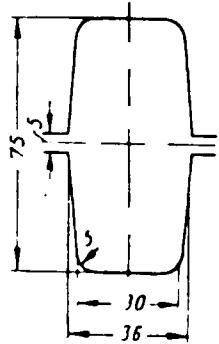


Card 4/8

Economical Alloyed Steel Sections

S/13/61/00/004/003/10-
A006/A001

Figure 3: Design of a ribbed groove



Card 5/8

Economical Alloyed Steel Sections

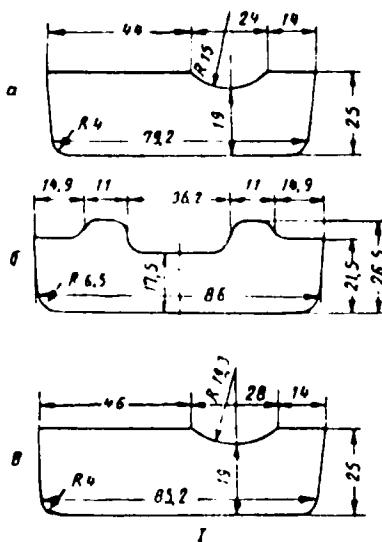
Figure 4: Design of

grooves for sections

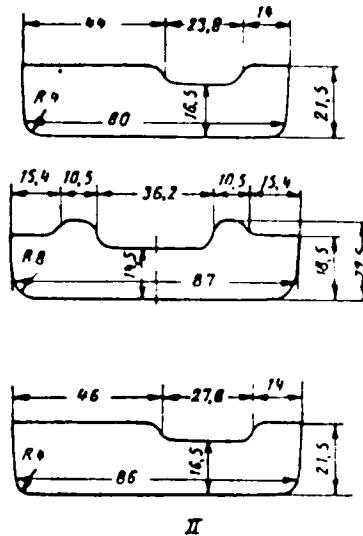
a - GK-01; b - GK-09;

c - GK-014; I) pass a

; II) pass 3



S/130/61/000/004/003/005
A006/A001



Card 6/8

Economical Alloyed Steel Sections

Table:

Analysis of calibrating sections GK-01,
GK-09 and GK-014

a) Strip dimensions

b) Side of square

c) Cross sectional surface of strip in mm²

d) Coefficient of reduction in length

e) Square

f) Smooth

g) Rib

h) Shaped

Коды Standard	Профиль	Groove shape	Height	Width	Coef. Red.	Material	Weight	Section	Коэффициент	
									Гладкий	Совершенно гладкий
blank										
	Заготовка		85	7100						
I	1 Р Квадрат	-	78	54 11 22 20 40						
I	2 Тоже	-	70	4820 1 21 24 - 50						
I	3 >	-	70	4680 1 0 3 15 - 30						
I	4 Гладкий 50	78	-	3650 1 28 19 - 20						
I	5 Тоже	30	89	- 2550 1 43 18 - 45						
II	6 g Ребро	77	30	- 2300 1 11 5 - 30						GK-01
II	7 h Фасон- ный	25	79	- 1880 1 22 13 50						GK-01
III	8 Тоже 121,5 80	80	- 1600 1 17 7 - 45							
I	5 Гладкий 30	89	- 2550 1 43 18 - 45							GK-09
II	6 Ребро 83	30	- 2480 1 03 11 - 0							GK-09
II	7 Фасон- ный 26,5 86	86	- 1835 1 35 14 - 45							GK-09
III	8 Тоже 22,5 87	87	- 1530 1 2 8 - 20							
I	5 Гладкий 30	89	- 2550 1 43 18 - 45							GK-014
II	6 Ребро 83	30	- 2480 1 03 11 - 0							GK-014
II	7 Фасон- ный 25 85	85	- 2030 1 22 13 50							GK-014
III	8 Тоже 121,5 86	86	- 1700 1 19 7 - 45							

Card 7/8

Economical Alloyed Steel Sections

S/130/61/000/004/003/005
A006/A001

There are 4 figures and 1 table.

ASSOCIATIONS: Zlatoustovskiy metallurgicheskiy zavod (Zlatoust Metallurgical Plant) (Shuralev); Sibirskiy metallurgicheskiy institut (Siberian Metallurgical Institute) (Nekrasov)

Card 3,3

3/130/61/707-3/11/1976
A806/A111

AUTHORS: Shuralev, M. V.; Nekrasov, S. G.; Galega, S. G.

TITLE: The new economical ГК-06 (ГК-6) shaped section

PERIODICAL: Metallurg. no. 1, 1981, 23-24

TEXT: A new economical (ГК-06) shaped section made of alloyed 3M415 (E7415) and 30ХГСА (30KhGSA) steel was assimilated at the Zlatoust Metallurgical Plant. The section is rolled on a medium-grade "40хNr.2" mill which consists of four three-high stands arranged in a line. The 85 mm square blanks are heated in a continuous furnace and rolled into finished sections in 8 passes: the first four passes on stand I, three on stand II and the finishing pass on stand III. The section is shaped in one semi-closed groove with large cutting edges and 3 closed beam-type grooves with constant position of joints. All section grooves were designed for operation with reduced spread thus promoting the precise formation of the shaped section. The closed grooves are placed on the lower rolls since due to the reduced spread the strip may jam in the closed grooves and bind with the roll. The dimensions of the rolling diameter are almost equal in order to prevent excessive increase of the lower roll load and weakening

Card 1/2

3/130/61/OK-06/16/A. M. 17

A006/A101

The new economical OK-06 (OK-06) shaped section

of the upper roll. Binding of the lower roll is avoided by the use of forged steel guide fixtures placed into the closed grooves. Experimental and industrial rolling of the OK-06 shape has shown that if the stands are correctly set-up, satisfactory filling of the grooves with metal is assured, the finished sections possess the dimensions required and a satisfactory surface quality. The use of OK-06 sections instead of rolled strips in machinebuilding saves about 3% of alloyed metal and reduces labor consuming mechanical operations when manufacturing machine parts. There are 3 figures and 1 table.

ASSOCIATION: Zlatoustovskiy metallurgicheskiy zavod (Zlatoust Metallurgical Plant); Sibirskiy metallurgicheskiy institut (Siberian Metallurgical Institute)

Card 2/2

NEKRASOV, S.G.

Resistances in rolling with standard grooves. Izv.vys.ucheb.zav.;
chern.met. 5 no.4:91-101 '62. (MIRA 15:5)

1. Sibirskiy metallurgicheskiy institut.
(Rolling (Metalwork))

NEKRASOV, S.G.

Calculating the horizontal projection of the contact area in
rolling with plain grooves. Izv. vys. ucheb. zav.; chern. met.
6 no.4:88-97 '63. (MIA 16:5)

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(Rolling (Metalwork)—Graphic methods)

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Designing the next in the heat oval planishing groove for
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"APPROVED FOR RELEASE: Wednesday, June 21, 2000

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NEPKAROV, T.N.

Moving to the right, nose slat track following the horizontal
movement of the aircraft. Launch study LTA no. 410148 '81.
(MIRA 17:0)

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L 1294-66 EWT(d)/EED-2/EWP(1)
ACCESSION NR: AR5007329

IJP(c) BB/GG
UR /0271/65/000/001/B044/B044
681.142.62

SOURCE: Ref. zh. Avtomatika, telemekhanika i vychislitel'naya tekhnika.
Sv. t., Abs. 1B253

AUTHOR: Yefremov, V. D.⁴⁴; Nekrasov, S. P.⁴⁴

TITLE: Code converters based on a current-distribution principle

CITED SOURCE: Uch. zap. aspirantov i soискателей. Leningr. politekh. in-t.⁴⁴
Elektroizmerit. tekhn. i avtomatika. L., 1963, 72-78

TOPIC TAGS: code converter, binary decimal converter

TRANSLATION: Several code converters constructed on a current-distribution principle and using square-loop ferrites are described. A circuit for converting binary code into "1 out of 2" code is presented. In the binary system of coding, the signal in the trunk corresponds to 1, the absence of a signal, to 0. In the "1 out of 2" code, a signal in one trunk means 1, in another trunk, it means 0. The circuit operation is described. A circuit for converting three digits of the "1 out

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of 2" code into a "1 out of 8" code is explained. The above circuits permit designing the converters of a binary number into any number system having base 2^n . A conversion circuit of one digit of a "2 out of 5" code into a "1 out of 10" code is considered, as is a circuit for conversion of the cyclic Gray code into a "1 out of 2" code. The conversion algorithm is presented, and operation is explained. Also, a binary-decimal converter is considered which includes a control device that coordinates the operation of various components, a counter that checks the moment of finishing the conversion, and decimal and binary resistors; the converter operation is described. A circuit is given of one digit of the decimal register which permits doubling of the stored number. A structural diagram of a decimal-binary converter is presented. A circuit of one digit of the decimal register which permits division of the stored number by 2 is presented.

Bibl. 2, figs. 8.

SUB CODE: DP

ENCL: 00

mfr
Card 2/2

...MURALEV, M.V., ~~operator~~

operator of 1600-ton ingot mill according to a new flow chart.
Metallurgist 27-108-12.

1. Same as in previous statement (intouzovetskogo metallurgicheskogo zavoda - na lev.), i.e. (inener-sistemnykh zavodov tsvetkovykh metallurgicheskikh zavodov - na desno).

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S. S. Nekrasov. Vestnik Mashinostroyeniya. Bulletin of
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production of cog wheel cutters and three-sided cut-
ters. Composition of wax molding material used is
indicated. Optimum conditions of casting were de-
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Technika otlivki rezinushchikh instrumentov metodom voskowych modeli.
(Vestn. Mash., 1950, no. 11, p. 46-53)

Precision casting of cutting tools by wax model method.

SIC: 373.9*

SC: Manufacturing and Mechanical Engineering in the Soviet Union, Library of
Congress, 1953.

U.S.A. I. S.

"Karmala" (a racing track located near the village of Karmala, 10 km. N.E. of Tashkent)

Burned-out hardened raceways (Tashkent, 1970)

Dec. 1970

Soviet manufacturer and engineer at the Ministry of Defense of the USSR, D.C.

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 4. Pipe, Steel
 7. Workability of cold-rolled pipes made of steel ShKh 15. Podshinnikov, N.O., 1951.
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axial significance of specific cutting stresses. *Journal of Materials*, 10, 101-106.

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