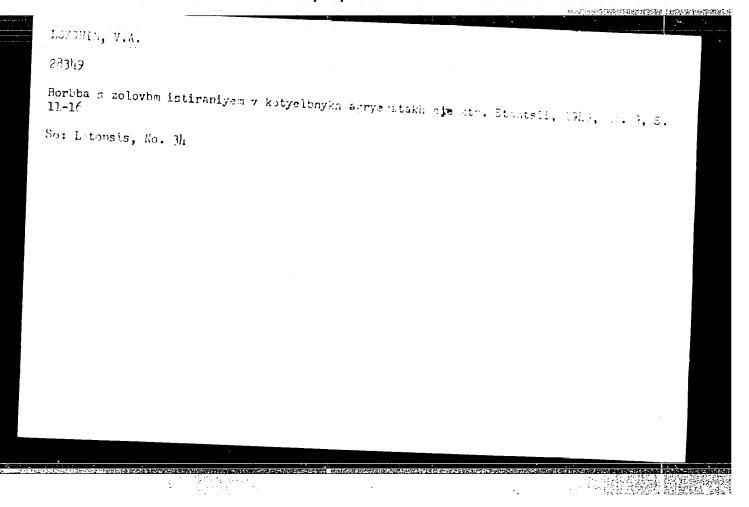
<del>Ammin</del> j v. n.		, rå 1/#53	
	USSR/Boilers Surfaces - Heating	Jul 1947	
	"Reducing Ash Wear of Boiler Heat V. A. Lokshin, 6 pp	ing Surfaces,"	
	"Izv VTI" No 7		
	Discusses the nature and method of computing general wear, local wear, reduction of general wear, and prevention of local damage.		
		14T53	



LONDIES, T. A. : LIL', V. J.: Y.MORCI, L. A.

Steam Boilers

Increasing the work reliability of high-pressure boilers. Rab. energ. 2 no. 3, 1952.

Monthly List of Russian Accessions, Library of Congress, May 1952. UNGLASSIFIED

3	LOKSHIN.	Ū A
4.	*************	. K 21. a

- 2. USSR (600)
- 4. Steam Boilers Efficiencies
- 7. Examining the effect of operating factors on the circulation in a high-pressure boiler. Izv. VTI 21 no.10, 1952.

9. Monthly List of Russian Accessions, Library of Congress, January 1953, Unclassified.

Versvitskiy, I.B., Krol' L.B., and Lokshin, V.A., "The Operation of Injection Regulators in Superheating High-pressure Steam," Elektricheskiye stantsii /Electric Power Stations/, 1953, No 8, Pages 3-8.

### "APPROVED FOR RELEASE: 06/20/2000

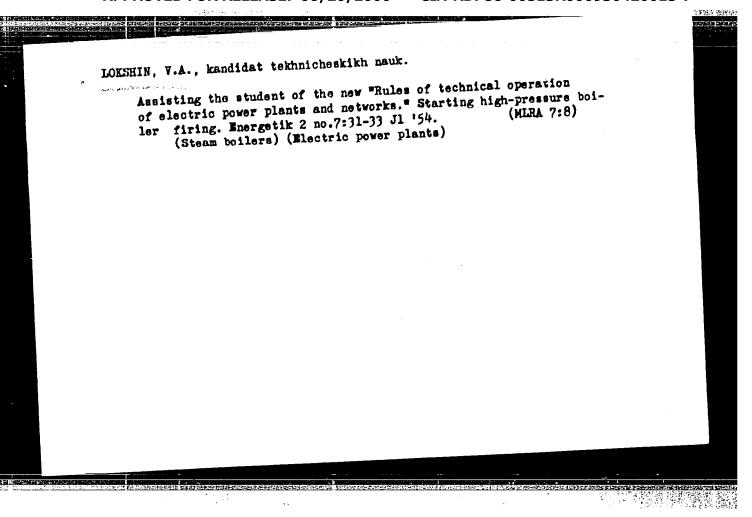
### CIA-RDP86-00513R000930420015-7

Fuel Abstracts
Juno 1954;
Steam Raising and
Steam Engines

V h556. OPHOTION OF BOSH PROCESS GRAP FOR STANDARD AND A CONTROL OF THE STANDARD AND A CONTROL OF

IOKSHIN. V.A. kandidat tekhnicheskikh nauk; TALDYKIN, K.M.,
inshener.

Operational inspection of cleaning heating surfaces of furnaces
by steam-blast. Elek.sta. 24 no.12:16-20 D '53. (MIRA 6:12)
(Furnaces)



LOKSHIN, V.A.

AID P - 682

Subject

: USSR/Engineering

Card 1/1

Pub. 29 - 17/24

Author

: Lokshin, V. A., Kand. of Tech. Sci.

Title

: Firing of high pressure boilers

Periodical

: Energetik, 7, 31-33, J1 1954

Abstract

The initial firing of high pressure boilers is discussed, particularly in reference to importance of cooling of rapidly heated convectional and radiant types of superheaters, economizers, tubing and other elements of the boiler. Specific precautionary measures are recommended for each boiler part designed for normal circulation of

heating and cooling media.

Institution:

None

Submitted

No date

### "APPROVED FOR RELEASE: 06/20/2000

### CIA-RDP86-00513R000930420015-7

# LOKSHIN, V. A.

AID P - 730

Subject : USSR/Electricity

Card 1/1

Pub. 29 - 23/26

Author

: Lokshin, V. A.

Title

**《** : Dimensions of balls used in the coal pulverizing

ball mills

Periodical: Energetik, 9, 35-36, S 1954

Abstract

In reply to a reader's question, the author gives a brief explanation concerning the selection of ball sizes.

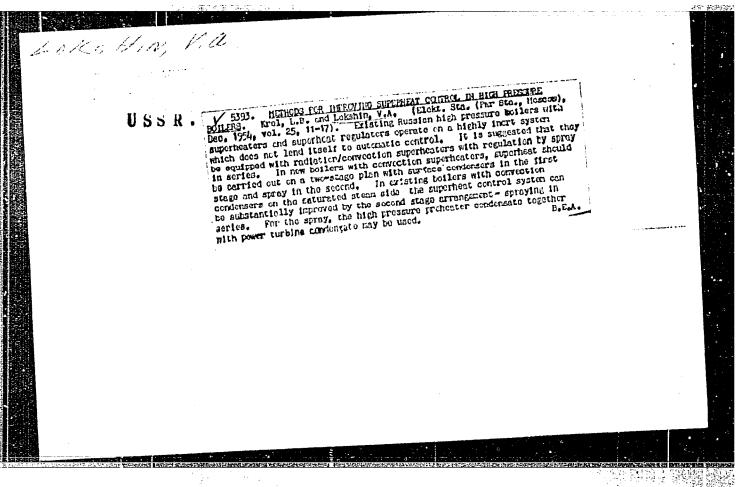
Institution:

None

Submitted

: No date

CIA-RDP86-00513R000930420015-7" APPROVED FOR RELEASE: 06/20/2000



LALAYANTS, A.M., redaktor; ABRAMYAN, A.A., redaktor; GUBERMAN, I.D., redaktor, DOKUNIN, A.V., redaktor; ZASADYCH, B.I., redaktor; IVANENKO, G.I., redaktor; LETOV, H.A., redaktor; MELAMED, Z.M., redaktor; LIVSHITS, I.I., LOKSHIN, V.A., redaktor; MONIN, G.I., redaktor; SUMCHENKO, V.A., redaktor; TOPCHIYEV, A.V., redaktor; SHEVALDIN, A.S., redaktor; SIROVA, V.A., redaktor; ANDREYEV, G.G., tekhnicheskiy redaktor; PROZOROVSKAYA, V.L., tekhnicheskiy redaktor.

[Materials and equipment used in the coal industry; a reference mammal]
Materialy i oborudovanie, primeniaemye v ugol'noi promyshlennosti;
spravochnik. Moskva, Ugletekhizdat. Vol.1.[Materials] Materialy. Pt.2.

(MIRA 9:5)
1955. 544 p.

(Coal mines and mining--Equipment and supplies)

LALAYANTS, A.M., redaktor; ABRAMYAN, A.A., redaktor; GRIBERMAN, I.D., redaktor; DONUKIN, A.V., redaktor; ZASAUTCH, B.I., redaktor; IVANENKO, G.I., redaktor; LETOV, M.A., redaktor; TOKININ, V.A., redaktor; redaktor; LIVSHITS, I.I., redaktor; LOKSHIN, V.A., redaktor; MONIN, G.I., redaktor; EDMCHENKO, V.A., redaktor; TOKINEV, A.V., redaktor; SHEVALDIN, A.S., redaktor; SUROVA, V.A., redaktor; AIDRETEV, G.G., tekhnicheskiy redaktor; PROZOHOVSKAYA, V.L., AIDRETEV, G.G., tekhnicheskiy redaktor; PROZOHOVSKAYA, V.L., tekhnicheskiy redaktor.

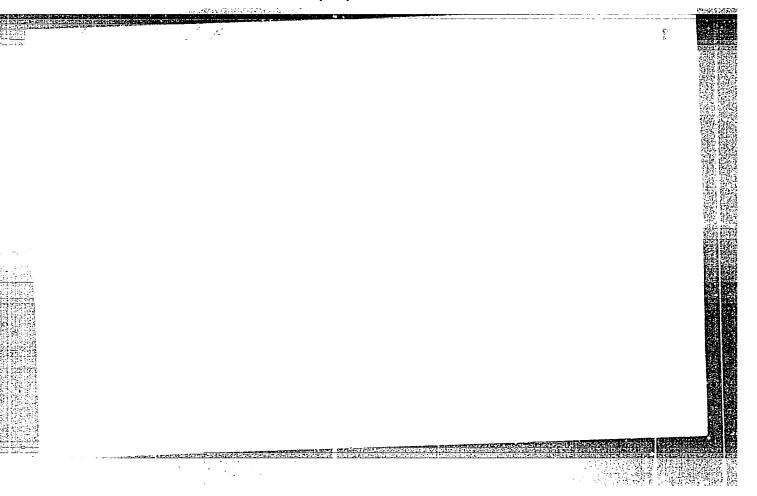
[Material and equipment used in the coal industry] Materialy in oborudovanie, primeniaemye vugol'noy promyshlennosti; spravochnik vobrudovanie, primeniaemye vugol'noy promyshlennosti; spravochnik vostva, Ugletekhizdat, Vol.1 [Material—Mholesale prices in effect as of July 1, 1955] Materialy. Pt. 1.1955. 786 p. — Obtpwye teeny, vedenye s 1 iiulia 1955. g. 192 p. [Microfilm] (MLRA 9:1) (Coal mining machinery) (Coal mines and mining)

LONSHIN, V.1)-

LALAYANTS, A.M., glavnyy redaktor; AMRAMYAN, A.A., otvetstvennyy redaktor; GUHERMAN, I.D., redaktor; DOKUKIN, A.V., redaktor; ZASADYCH, B.I., redaktor; LETOV, N.A., otvetstvennyy redaktor; LIVSHITS, I.I., redaktor; LOKSHIN. V.A., redaktor; MELAMED, Z.M., redaktor; MONIN, G.I., redaktor; SUMCHENKO, V.A., redaktor. TOPCHIYEV, A.B., redaktor. tor; SHEVALDIN, A.S., redaktor; YEGURNOV, G.P., redaktor; LYUBIMOV, N.G., redaktor izdatel stva; ANDREYEV, G.G., tekhnicheskiy redaktor; PROZOROVSKAYA, V.L., tekhnicheskiy redaktor.

[ Material and equipment used in the coal industry; a reference manual] Materialy i oborudovanie, primeniaemye v ugol noi pro-mushlennosti; spravochnik. Moskva, Ugletekhizdat. Vol.2. [Equipment] Oborudovanie. Pt.1. 1956. 455 P.

(Coal mines and mining-Equipment and supplies)



CHARRICIGIN, V. G. (Engr.) and LORDHIN, V. A. (Cand. Tran. Sei.)

"Results of Experimental Investigation of the Influence of Non-Uniformity of Reat Exchange wound the Perimeter of a Horizontal Steam Raising Tabu."

report presented at sei. and tech. session on Heat Amelange during Change of Aggregate State of Matter (by Comm. on High Steam Conflictions, Peter Inst. Ad USSI and Thermal Engineering Inst., AS UST, SSR, Mev. 19-28 Sep 57.

All-Union Thermo-Technical Inst.

LEWELL, L.A. LONSHIN, VA

IAIAYANTS, A.M., redsktor; ARRAMYAN, A.A., redsktor; GUBERMAN, I.D., redsktor; DOKUKIN, A.V., redsktor; ZASADYOH, B.I., redsktor; LETOV, H.A., redsktor; LIVSHINS, I.I., redsktor; LOUSHIN, V.A., redsktor; MELAMED, Z.M., redsktor; MIN, G.I., redsktor; SUMCHEMO, V.A.; TOPCHIYEV, A.V., redsktor; SHEVALDIN, A.S., redsktor; TEGURNOV, G.P., redsktor; LYUBIMOV, N.G., redsktor izdstel'stwa; PROZOROVSKAYA, V.L., tekhnicheskiy redsktor

[Materials and equipment used in the coal industry; a reference manual] Materialy i oborudovanie, primeniaemye v ugol'noi promyshlennosti; spravochnik. Moskva, Ügletekhizdat. Vol.2. [Equipment] Oborudovanie. Pt.2. 1957. 485 p. (MIRA 10:9)

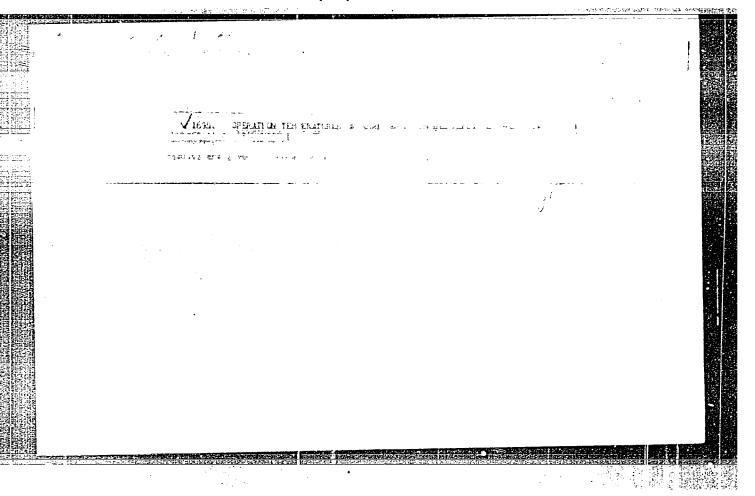
(Goal mining machinery)

IAIAYANTS, A.M., glavnyy red.; ABRAMYAN, A.A., red.; CUBRRMAN, I.D., red.;
DOKUKIN, A.V., red.; ZASADYCH, B.I., red.; LETOV, N.A., red.;
LIVSHITS, I.I.; LOKSHIN, V.A.; MELAMED, Z.M.; MONIN, G.I.; SUMCHENKO,
V.A.; TOPCHIYEV, A.V.; SHEVALDIN, A.S.; YEGURNOV, G.P., red.;
LYUBIMOV, N.G., red.izd-va; PROZOROVSKAYA, V.L., tekhn.red.

[Materials and equipment used in the coal industry; a handbook]
Materialy i oborudovanie, primeniaemye v ugol'noi promyshlennosti;
spravochnik. Moskva, Ugletekhizdat. Vol.2. [Equipment] Oborudovanie.

(MIRA 11:2)
Pt.3. 1957. 655 p.

(Coal mines and mining—Equipment and supplies)



AUTHOR:

LONSAIN, V.A., Candidates of Technical Shvarts A.L. and Lokshin, V.A., Candidates of Technical

Sciences (All-Union Thermotechnical Institute).

TITIE:

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Eksperimental'noye issledovaniye dvizhushchikh naporov pri opusknom dvizhenii parovdyanoy smesi v vertikal nykh trubakh pri davleniyakh do 180 at.)

PERIODICAL: "Teploenergetika" (Thermal Power), 1957, Vol. 4, No. 6,

pp. 12 - 17 (U.S.S.R.)

ABSTRACT:

A recent investigation into the reversal of circulation in a multitube circuit with natural circulation at a pressure of 12 atm. makes it possible to represent the circulation characteristics of the tubes in the left quadrant of the circulation diagram. This left quadrant corresponds to a negative flow of water and has two branches. The righthand branch is a continuation of the circulation characteristic of the tubes in the region of small positive water flows and corresponds to downward movement of water combined with upward movement of steam. The left branch of this quadrant is the circulation characteristic corresponding to downward movement of the steam-water mixture when both phases are moving in the same direction.

Until now experimental data for the construction of the branch of the circulation characteristic corresponding to

Card 1/7

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

downward movement of the mixture was limited to tests carried out in the Central Boiler and Turbine Institute by D.F. Peterson and O.M. Baldina in 1937 at a pressure of 10 atm. with high steam contents in the mixture.

The present work is mainly devoted to the determination of so-called useful heads corresponding to this lefthand branch of the circulation characteristic over the pressure range of the circulation characteristic over the pressure range of the structure of the downward study the special features of the structure of the downward flow of steam-water mixture and to determine the limiting speed of circulation with downward movement of the water (at which a bubble remains stationary and above which both liquid and gaseous components move together). This critical circulation speed approximately characterises the beginning of the left branch of the circulation characteristic of the tube in the left hand quadrant of the circulation diagram.

The experimental rig is described. It is connected to two steam mains, one at a pressure of 300 atm. and a temperature of 600 °C and the other at 130 atm. and 500 °C. The water was prepared by condensing part of the steam delivered to the rig in a special steam cooler with an output of 3 tons/h.

After leaving the cooler the condensate passed into a contact heater of the flow type where it was heated by steam to the necessary temperature. Appropriate controls are

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

After throttling, the steam-water mixture passed to separators from which the water passed to coolers and then on to the condensate tank whilst the steam was discharged into the atmosphere. The rig was modified during different stages of the work. In the first stage the useful heads were determined during downward flow in a pipe of 42/29 mm dia. on two independent sections located one below the other. The next stage included a new experimental section of diameter 70/55 mm for determination of useful heads of downward flow, having independent tapping of pressure drop on two parallel differential manometers. The limiting speed of steady downward flow of the mixture was determined on two glass, water-air models of 26 and 55 mm diameter. Air from a compressor at a pressure of 280 atm. was supplied to the pipe through a nozzle, the quantity of water delivered to the tube was adjusted so that the air bubbles remain stationary.

Two runs were made to determine the heat loss through the insulation of the rig to the surrounding medium and one to determine the heat absorption from the surrounding medium for the calorimeter-cooler. The steps that were taken to ensure

card 3/7

639

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

accuracy of the results are described.

The working-up of the experimental data on the moving heads consisted of determination of the speed of circulation, of the referred speed of the steam and of the total resistance with downward movement of the steam-water mixture, which we called the negative useful moving head, by analogy with rising movement. This terminology is advisable because in the circulation diagram the values of the useful heads and 'negative' useful heads are laid out on one and the same ordinate axis and in the latter case the heads correspond to negative flow of water, i.e. the downward flow.
Formulae are given for the rate of circulation, the

enthalpy, and the negative useful moving heads.

Tests to determine the useful heads of downward flow of a steam-water mixture in a pipe of 29 mm internal diameter were carried out at pressures of 35, 100, 140 and 180 atm. and circulation speeds of 0.3, 0.5, 0.75, 1 and 1.5 metres/sec in the range of flows with the steam content of the mixture from 0 to 0.97 by volume; also on a pipe of internal diameter 55 mm at pressures of 35 and 100 atm. at circulation speeds of 0.3, 0.5, 0.6 and 0.7 metres/sec when the pressure is 35 atm. with the same range of steam content. Experimental data on the useful head of downward flow for

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

the 29 mm pipe at p = 140 atm. is given in Fig. 4 and the corresponding figures for 55 mm tube at 100 atm. in Fig. 5. These figures show that, as with rising motion of the steamwater mixture, there are two regions of the relationship between the useful head and the referred steam speed at constant

For small values of referred steam speed there is a sharp increase in the useful head with the referred speed, then the curve bends over and becomes flatter. This reflects the nature of the relationship between the volume and weight steam contents However, unlike the case of rising movement of steam water mixture with downward movement there is an intersection of the curves of negative useful moving heads relating to different speeds of circulation.

The experimental data obtained make possible for the first time the construction of the left branch of the circulation characteristic of the left hand quadrant of the circulation diagram over the pressure range from medium to super-high. By way of example, Fig. 6 gives curves of these characteristics for tubes with an internal diameter of 29 mm at a pressure of 100 atm.

A mathematical expression is given that represents the results

Card 5/7

APPROVED FOR RELEASE: 06/20/2000

CIA-RDP86-00513R000930420015-7"

Experimental investigation of moving heads during downward movement of a steem-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

of tests on the determination of enthalpy (i.e. steam content) at the centre of the downward flow. The relationship is also plotted on graphs in Figs. 7 and 8 for 29 mm tubes at 35 and 100 atm., respectively.

The tests carried out on samples taken from the central part of the downward flow made it possible to establish that at low and moderate steam contents the centre of the downward flow is free of bubbles. In a flow of steam-water mixture moving downwards in a vertical tube the centre is the place with a maximum concentration of steam bubbles. Only at large volume steam contents in the central part of the flow is the steam content equal to the total steam content of the mixture.

Determination of the critical speed of circulation for downward flow of a two-phase mixture, corresponding to the gas bubbles being stationary, was carried out on air water models of 26 and 48 mm diameter. For both diameters of pipe the speed was the same and for larger bubbles was 0.2 metres/sec and for small bubbles (3 - 5 mm dia.) 0.16 m/sec, which is in satisfactory agreement with published data. The rate of downward flow of water at which the bubbles remain stationary is close to the rate at which bubbles rise in the tube in still water. At water speeds somewhat above the critical value the rate of movement of bubbles was determined by measuring the time required for bubbles of a definite size to pass between upper

Card 6/7

Experimental investigation of moving heads during downward movement of a steam-water mixture in vertical tubes at pressures up to 180 atm. (Cont.)

and lower marks on the tube. The tests were carried out for single bubbles and for groups of bubbles and the results are given on Fig. 9. The graphs show that at circulation speeds less than 0.4 m/sec there is sluggish carry-over of bubbles and therefore even a small quantity of steam entering the tube causes it to have a large true steam content which in a contour with natural circulation can interrupt downward flow of mixture in the tube. Therefore, although the steady rate of circulation of flow in a downward tube in which a mixture of given steam content is flowing is determined by the circulation characteristic of the tube and the magnitude of the useful head of the given circuit, it may be concluded that steady downward flow of the mixture is hardly likely to occur at circulation speeds less than 0.4 m/sec (at low and medium pressures). This speed should be established more accurately for high and superhigh pressure steam-water mixtures.

9 figures, 2 Russian literature references.

Card 7/7

Temperature conditions for horizontal steam generating tubes under extra high pressures. Teploenergetika 4 no.9:58-63 S '57.
1. Vsesoyuznyy tenlotekanicheskiy institut. (Boilers)

LUKSHIN, V. F

96-1-1/31

AUTHORS: Chakrygin, V.G., Engineer and Lokshin, V.A., Candidate of Technical Sciences.

TITLE: Temperature Conditions of Operation of Vertical Steam-

generating Tubes at Super-high and Super-critical Pressures with Downward Flow (Temperaturnyy rezhim raboty vertikal'nykh paroobrazuyushchikh trub pri sverkhvysokikh i sverkhkriticheskikh davleniyakh i opusknom dvizhenii potoka)

PERIODICAL: Teploenergetika, 1958, vol.5, No.1, pp. 3 - 8 (USSR).

ABSTRACT: In the design of large boilers it is convenient to use tubes with downward flow; the hydrodynamics of downward flow of steam-water mixtures has been studied in detail in previous works. (Refs.2, 3). An expression is derived for the heat transfer coefficient under conditions of boiling of the steamwater mixture for the case of absence of a liquid film on the heating surface. Tests were made on a tube of an internal diameter 29 mm at pressures of 140 - 246 atm., with heat-flow rates up to 390 000 kcal/m²hr. The super-high-pressure expermental rig is illustrated diagrammatically in Fig.1. The rig and the experimental procedure are fully described in Teplo. energetika, 1957, no.9.

The method of working out the test results is explained. Fig. gives the results of tests at pressures of 140, 160 and 100 an

96-1-1/3

Temperature Conditions of Operation of vertical Steam-generation Tubes at Super-high and Super-critical Pressures with Downward

with a heat-flow rate of 230 000 kcal/m²hr. Until the boil: point is reached, at a messure of 180 atm., the wall tempe at misses and all the same at t rises gradually with the flow temperature, but when surface boiling occurs the wall temperature is constant for a given pressure. An expression is given for the mean lines of the graph in Fig. 2. The influence of the heat-flow rate on the operational temperature

tures of the tube at a pressure of 180 atm. are shown in Fig. The stepwise increase in wall temperature with increasing flo rate will be noted: similar results were obtained at a pressure of 200 atm., as shown in Fig.4. In a certain range of operating conditions, a greater flow-rate of medium corresponds to a lower heat transfer coefficient. The results of tests at 210 atm. are generally the same as those at 200 atm. Tests at 220 atm., with heat transfer rates of 140 000 and 390 000 kcal/m2hr are represented in Fig. 5. Some results at a super-critical pressure (230 atm.) are given in Fig.6. When pressure, heat transfer rate and mass rate of flow are constant the points lie near straight lines. There were no deviations Card2/5 from the general relationships in the region of second-order

Temperature Conditions of Operation of Vertical Steam-generating Tubes at Super-high and Super-critical Pressures with Downward Flow.

phase transition. Calculated values of metal temperature are also given in Fig.6; the agreement between the calculated and experimental temperatures is satisfactory. Similar experimental results were obtained at a pressure of 246 atm. The experimental data is then analysed, revealing a number of regions of different internal cooling conditions. Below the boiling point, there are three regions: convective heat exchange in a turbulent flow of a single-phase liquid; surface boiling of liquid at a pressure below 210 atm; and surface-film boiling of liquid at pressures above 210 atm. (Fig. 5). Four characteristic zones were observed in the boiling range: a region of normal boiling with bubbles; a region of "developed" boiling in the absence of a liquid film on the heating surface; a region of conditions with varying wall temperatures; and a region of film-wise boiling of liquid near the boiling point. The conditions pertaining to these various regions are discussed. Each of the heat exchange regions corresponds to a certain operational temperature of the tube and attention must be paid to those conditions which can lead to disturbance of normal cooling of the metal. Film-wise boiling with variable wall

Card3/5

96-1-1/31

Temperature Conditions of Operation of Vertical Steam-generating Tubes at Super-high and Super-critical Pressures with Downward Flow.

temperatures is a dangerous condition. At super-critical pressures, heat transfer from the wall to the liquid takes place in a single-phase flow, the wall temperature changing smoothly with change of enthalpy. Comparative tube wall temperatures for various pressures, as determined experimentally, are given in Fig. 9. For the given conditions the highest wall temperatures are reached below the boiling point at a pressure of 220 atm. Practical conclusions drawn from the results are that heated tubes with downward flow can operate reliably over a wide range of conditions at super-high and super-critical pressures. Heating and evaporative surfaces can be used with downward flow at pressures of 140 - 200 atm., heat-flow rates of less than 400 000 kcal/m hr and mass flow-rates greater than 850 kg/m sec. For the heating surfaces of supr-critical-pressure boilers in the region of phase transition, even at high heat transfer rates (up to 300 000 kcal/m hr), tubes may be made of pearlitic steels for downward flow with a mass flow-rate of the order of 500 kg/m sec.

Card4/5 There are 9 figures and 5 Slavic references.

Temperature Conditions of Operation of Vertical Steam-generating Tubes at Super-high and Super-critical Pressures with Downward Flow.

ASSOCIATION:

All-Union Thermo-technical Institute (Vsesoyuznyy Teplotekhnicheskiy Institut)

上。1955年1873年1967年

AVAILABLE:

Library of Congress.

Card 5/5

AUTHOR:

Lokshin, V.A. (Cand. Tech. Sci.)

SOV/96-58-10-23/25

TITLE:

On calculating the temperature of matal in radiation tubes of superheaters (K raschetu temperatury metalla trub radiatsionnykh paroperegrevateley.)

PERIODICAL: Teploenergetika, 1958, No.10. pp. 88-89 (USSR)

ABSTRACT:

As steam conditions increase, radiation super-heaters are becoming more widely used. These heating surfaces are sensitive to disturbances in thermal conditions, particularly those likely to accur when the boiler is working under a fluctuating load. The external temperatures of the tubes then vary considerably whilst the internal temperature remains constant. Measurements have shown that the temperature of the outer surface of tubes in a main radiation superheater may reach 580°C; the corresponding temperature in the intermediate radiation superheater exceeds 600°C, and the temperature difference across the wall of the metal is 100°C. It is, therefore, very important to determine the temperature on the outside of the tubes of radiation super-heaters, but the standard method of calculation accepts a mean metal temperature as a basis for selecting the type of metal and for strength determinations. Unfortunately, there are not sufficient data for making strength calculations on tubes with allowance for variable thermal stresses; more work needs to be done on this subject. The maximum stresses may occur on the external surfaces of tubes; in such cases the external temperature

Card 1/2

On calculating the temperature of metal in radiation tubes of super-heaters.

SOV/96-58-10-23/25

must be known for calculations of mechanical strength. A formula is given for calculating the outside temperature of tubes. It can lead to values 50°C higher than the standard formula, but should be used in the selection of metal for the tubes. For the time being, wall thickness determinations should be based on a mean temperature. There are 5 Soviet referencess:

Card 2/2

501/96--59--3--15/21

AUTHORS: Shvarts, A.L., Candidate of Technical Sciences and

Lokshin, V.A., Candidate of Technical Sciences

TITLE: A Method of Determining True Volumetric Steam Contents

and Hydraulic Resistances from Experimental Values of Effective Circulatory Pressures (Metod opredeleniya istinnykh ob"yemnykh parosoderzhaniy i gidravlicheskikh

soprotivleniy iz eksperimental nykh znacheniy

poleznykh dvizhushchikh naporov)

PERIODICAL: Teploenergetika, 1959, Nr 3, pp 72-75 (USSR)

ABSTRACT: A good deal of experimental data is now available about

effective circulatory pressures in vertical tubes over the pressure range of 10-220 atm. The data can provide ways of using measured values of these pressures to give at least an approximate value of the hydraulic resistances and true steam contents over a wide range of pressure. To this end published works about direct measurements of true steam and gas contents are first analysed. The results of A.A.Armand are plotted in Fig.1 in the form

results of A.A.Armand are plotted in Fig.1 in the form of a relationship between the true gas content and the volumetric gas content for a water/air mixture in a

Card 1/3 vertical tube. It will be seen that over most of the

SOV/96--59-3-15/21

A Method of Determining True Volumetric Steam Contents and Hydraulic Resistances from Experimental Values of Effective Circulatory Pressures

> range the graph is a straight line. This graph does not cover the range of small flows and accordingly the results of Schwarz, which covers such conditions, have been recalculated in the same coordinates and are plotted in Fig.2. It follows from this graph that for high steam contents the relationship is also approximately linear over most of the range. The departures from linearity are discussed in some detail. By means of formula (2) the lower boundary of linearity may be determined. In selecting a method to determine true steam contents from the pressure values, it is necessary to select a coordinate system which gives a similar straight-line relationship for the hydraulic friction losses, at least to a first approximation, The method of determining friction losses is then explained and, by way of example, data of the Central Boiler-Turbine Institute on effective circulatory pressures are

Card 2/3

50V/96--59--3--15/21

A Method of Determining True Volumetric Steam Contents and Hydraulic Resistances from Experimental Values of Effective Circulatory Pressure

plotted in Fig.3 and 4. Then an expression is derived for the pressures and its use is explained. There are 4 figures and 5 references of which 4 are Soviet and 1 German.

ASSOCIATION: Vsesoyuznyy teplotekhnicheskiy institut (All-Union Thermo-Technical Institute)

Card 3/3

BIL', V.S., kand. tekhn. nauk; LOKSHIN, V.A.

Comparative investigation into the effect of temperature fluctuations on the reliability of welded joints of economizer pipes. Teploenergetika 6 no.12:68-71 D 159. (MIRA 13:3)

1. Vsesoyuznyy teplotekhnicheskiy institut. (Boilers)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

SOV/96-59-8-20/27

Lokshin, V.A., Shvarts, A.L., Candidates of Technical AUTHORS:

Sciences

The Calculation of Driving Heads and Hydraulic Resistances TITLE:

During the Motion of a Steam-Water Mixture in Vertical

Rising Tubes

Teploenergetika 1959, Nr 8, pp 73-77 (USSR) PERIODICAL:

ABSTRACT: The previous article by the same authors published in Teploenergetika 1959, Nr 3, described a method of calcula-

ting true volumetric steam contents and hydraulic resistances from experimental values of useful driving pressures. The method was used to work up experimental data on useful driving pressures within the pressure range of 11 - 220 atm with tube diameters of 25.5 - 56 mm. Curves of the total useful head as a function of steam velocity referred to total tube section were constructed for each series of tests with volumetric steam contents less than 0.91. The method used in the previous article was applied to each series of tests to determine the values of the constants C

in equation (6) of the previous article. The values of C

Card 1/4

507/96-59-8-20/27

The Calculation of Driving Heads and Hydraulic Resistances During the Motion of a Steam-Water Mixture in Vertical Rising Tubes

so obtained were used to determine values of true steam content, which were plotted as function of volumetric flow steam content. An example of the procedure is given and the corresponding curve is plotted in Fig 1 for a pressure of 32 atm and tube diameter of 55.9 mm. Calculations were made of the total driving head: determinations could then be made of the friction losses, and curves were plotted of friction loss as function of flow rate, as exemplified in Figs 2 and 3. This linear relationship may be expressed by formula (1) which includes a coefficient A. To give a better idea of the influences of tube diameter and pressure on the values of C and A. curves of these coefficients as functions of pressure are plotted in Figs 4 and 5; test points are also plotted. It will be seen from Fig 4 that the relationship between C and the pressure is not a simple one. The curves of Fig 5 show that the frictional loss formula currently used is not valid at very high pressures, particularly when tubes are of small diameter. The procedure to be adopted when the volumetric Card 2/4 steam content is greater than 0.91 is discussed, and a

SOV/96-59-8-20/27

The Calculation of Driving Heads and Hydraulic Resistances During the Motion of a Steam-Water Mixture in Vertical Rising Tubes

> typical curve of true steam content as a function of volumetric steam content for a pressure of 62 atm is given in Fig 6. True steam velocity as a function of mixture velocity for a pressure of 62 atm is plotted in Fig 7. Further numerical examples are worked out, and it is concluded that a formula similar to equation (8) may be used in all cases of motion of a steam-water mixture in vertical rising pipes to determine the value of the true steam content. The constant  ${\bf C}$  in this formula may be taken from the nomogram in Fig 9. Finally, equation (9) is given for calculations of useful driving heads total driving heads and hydraulic resistances during motion in a vertical rising tube of steam-water mixtures of various steam contents at pressures up to the sub-critical. In equation (9) the coefficient C is determined from the nomogram of Fig 9 and the coefficient A from Fig 5, depending on the mixture pressure. Limitations on the use of the nomogram are explained. Values

Card 3/4 of useful driving heads calculated by means of the nomogram

SOV/96-59-8-20/27

The Calculation of Driving Heads and Hydraulic Resistances During the Motion of a Steam-Water Mixture in Vertical Rising Tubes

were found to be in good agreement with experimental values, as will be seen from the graph in Fig 10, which relates to a pressure of 111.5 atm and tube diameter of 25.5 mm. There are 10 figures and 3 Soviet references.

ASSOCIATION: Vsesoyuznyy teplotekhnicheskiy institut (The All-Union Thermo-Technical Institute)

Card 4/4

والأوافاع المتستند للحالم فالمتدارية أراي المراواة فوالمعاود المتاويس والماقالة أقالها

IOKSHIN, V.A., kand.tekhn.nauk; MOISEYEV, G.I., inzh.; PAVLENKO, L.I., inzh.;
TALDYKIN, K.M., inzh.; VARICHEV, V.A., inzh.

Thermal conditions during the operation of high-pressure radiation
wall-type superheaters. Elek.sta. 30 no.1:21-26 Ja \*59.

(MIRA 12:3)

(Superheaters)

LOKSHIN, V.A., kand. tekhn. nauk; TALDYKIN, K.M., inzh.

Temperatures in the strengtheners of boilers. Elek sta. 30 no.2:78
F '59.

(Boilers)

LOKSHIN, V.A., kand.tekhn.nauk; PAVLENKO, L.I., inzh.; TALDYKIN, K.N., inzh.;
TARAVKOV, S.S., inzh.

Temperature conditions in the operation of air preheaters with a high degree of air heating. Elek.sta. 32 no.4:24-28 Ap 161.

(Air preheaters)

LOKSHIN, V.A., kand.tekhn.nauk; PAVLENKO, L.I., inzh.; TALDYKIN, K.M., inzh.

Thermal characteristics of radiation-convectional steam
superheaters. Energomashinostroenie 7 no.5:7-9 My '61.

(MIRA 14:8)

(Superheaters)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

SHNEYEROVA, R.I., inzh.; SHVARTS, A.L., kand.tekhn.nauk; MIROPOL'SKIY, Z.L., kand.tekhn.nauk; LOKSHIN, V.A., kand.tekhn.nauk

Experimental study of the real steam contents and useful heads in tilted pipes. Teploenergetika 8 mo.4:63-67 Ap '61.

1. Energeticheskiy institut AN SSSR 1 Vsesoyusnyy teplotekhnicheskiy

(Boilers)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

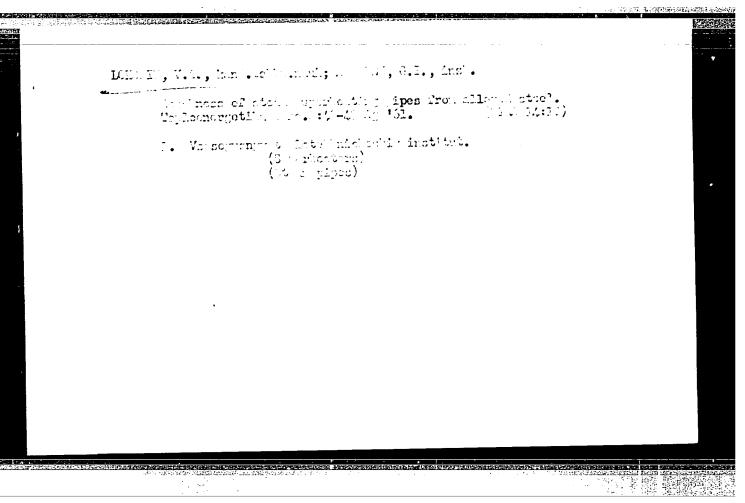
"探話舞蹈"的舞舞舞舞舞

Results of testing the GTU-600-1.5 plate regenerator.

Teploenergetika 8 no.5:11-17 My '61. (MIRA 14:8)

1. Yuzhnoye otdeleniye Gosudarstvennogo tresta po organizatsii i ratsionalizatsii elektrostantsiy; Khar'kovskiy tekhnologicheskiy institut i Dneproenergo. (Gas turbines)

	<b>发展的数数型</b>
P. M. Marketter C. S. Marketter and C. S. Marketter and C. M. Marketter and C. M.	
KLITIN, N.P., inzh.; LOKSHIN, V.A., kand.tekhn.nauk  Heat transfer and resistance of finned bundles. Teploenergetik 8 no.7:53-57 Jl '61.  1. Vsesoyuznyy teplotekhnicheskiy institut. (Gas turbines) (Air preheaters)	A
COLUMN TO THE PARTY OF THE PART	



LOKSHIN, V.A., kand.tekhn.nauk; PAVLENKO, L.I., inzh.; TakaVkOV, S.S., inzh.

Testing of a small economizer for boilers fired with anthracite fines under a system of upward gas flow. Teploenergetika 9 no.5:10-15 My '62. (MIRA 15:4)

1. Vsesoyuznyy teplotekhnicheskiy institut i Rostovenergo. (Boilers--Testing)

TULIN, S.N., inzh.; LOKSHIN, V.A., kand. tekhn. nauk

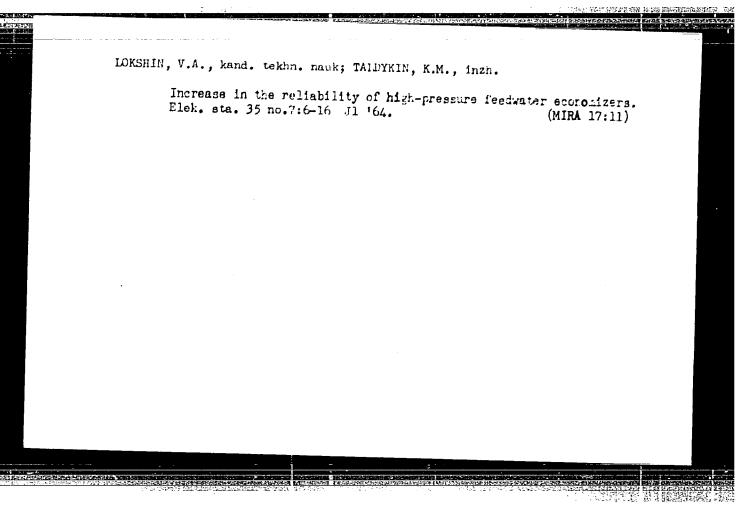
Experimental check of generalized design formulas of tubes with wire ribbing, Vest. elektroprom. 34 no.7:35-39 Jl 163. (MIRA 16:8)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

KLITIN, N.P., inzh.; LOKCHIN, V.A., kand. tekhn. nauk

Heat transfer and resistance of longitudinall; ribbed pipes.
Teploenergetika 11 no.5:79-83 My'64. (MIRA 17:5)

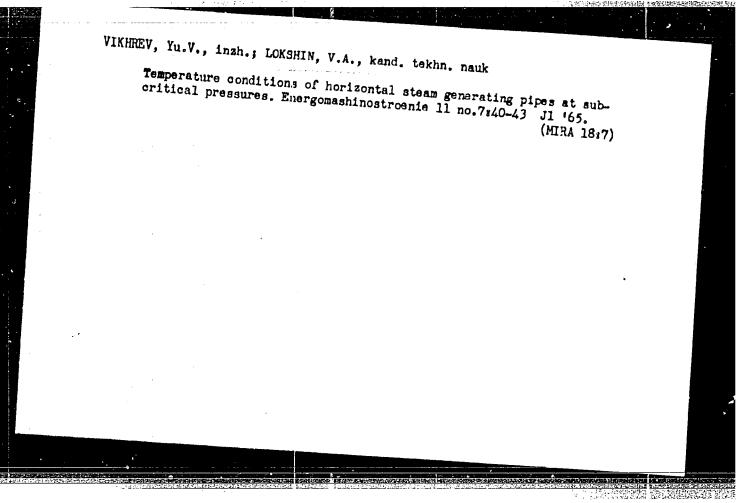
1. Vsesoyuznyy teplotekhnicheskiy institut.



SHNEYEROVA, R.I., inzh.; SHVARTS, A.L., kand. tekhn. nauk; MIROPOL'SKIY, Z.L., kand. tekhn. nauk; LOKSHIN, V.A., kand. tekhn. nauk

Hydraulic resistance in the upward motion of a steam and water mixture in inclined pipes. Teploenergetika 11 no.7:24-26 (MIRA 17:8)

l. Vsesoyuznyy nauchno-issledovateliskiy teplotekhnicheskiy institut i Energet cheskiy institut im. Krzhizhanovskogo AN SSSR.



VIKHREV, Yu.V., inzh., diesertant; LOKSHIN, V.A., kand. tekhn. nauk

Experimental study of temperature conditions in herizontal
steam generating pipes at supercritical pressures. Teploenergetika 11 no.12:79-82 D \*64 (MIRA 18:2)

1. Vsescyuznyy teplotekhnicheskiy institut.

MCSEYEV, C. a. kund.tekhn.nauk; 1625AlN, V.A., kand.tekhn.nauk; FiMeN, V.M.,

St. Ag of an experimental double-alght radiation superneater structure.

Elek. sta. 36 no.8:9-13 Ag 165.

(MIRA 12:9)

FERNYAKO, B.A., inzh.; LORSHIN, V.S., send. tekin. zauk

Study of heat transfer from a asseten whi. We an ein ein student stream.

Toplomergetika 11 no.9:52-60 5 164.

1. Vsesoyuznyy toplotekimieneskiy institut.

LIPETS, A.U., inzh.; LAFA, Yu.I., inzh.; FOMINA, V.N., inzh.; LOKSHIN, V.A., kand. tekhn. nauk

Aerodynamic resistances of compact checkerboard tube clusters.
Teploenergetika 12 no.6:32-34 Je 65. (MIRA 18:9)

1. ZiO i Vsesoyuznyy nauchno-issledovateliskiy teplotekhnicheskiy institut.

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

LIPETS, A.U., Inzh.; ZHOLUDOV, Ya.S., inzh.; LOKSHIN, V.A., kand. tekhn. nauk; ANTONOV, A.Ya.

Use of pipes with interral longitudinal fins in an intermediate superheater. Teploenergetika 12 no.8:23-27 Ag '65. (MIRA 18:9)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

TULIT, W.H., inwh.; LOKSHIN, W.A., F.nd. tekhn. nauk; BATENIN, B.A., innh.; DANILOV, I.A., inzh.

Industrial tests of a cooling unit with aluminum tubes designed by the All-Union Scientific Research Institute for Metallurgical Machines. Elek. sta. 36 no.9:8-12 S 165. (MIRA 18:9)

VGROB'YEV, G.A.; NANIY, V.P.; GEGESHIDZE, G.A.; LIPETS, A.U.;
LOKSHIN, V.A.; ANTONOV, A.Ya.; GEL'TMAN, A.E.; IL'INA, L.V.;
RUBIN, V.B.

Inventions. Energ. 1 elektrotekh. prom. no. 4:50 0-D '65.
(MIRA 19:1)

L 03766-67 EWT(m)/EWP(t)/ETI/EWP(k) IJP(c) JD/WW/HW/JG

ACC NR: AR6029496

SOURCE CODE: UR/0137/66/000/006/D036/D036 4/C

AUTHOR: Donskoy, A. V.; Kostygov, A. S.; Klitin, N. P.; Lokshin, V. A., Stepanov, A. V.

TITLE: Production of longitudinally ribbed pipe from molten metal and the investigation of thermal and manufacturing properties of the pipe

SOURCE: Ref. zh. Metallurgiya, Abs. 6D251

REF SOURCE: Uch. zap. Leningr. gos. ped. in-ta im. A. I. Gertsena, no. 265, 1965, 12-32

TOPIC TAGS: pipe, ribbed pipe, convective heat exchange

ABSTRACT: Longitudinally-ribbed pipes produced from molten metal by the A. V. Stepanov method possess a combination of properties which in a number of cases, makes them suitable for use in the production of heat-exchange equipment. The convective heat exchange in clusters of longitudinal pipe has a pattern identical to internal heat exchange in channels during longitudinal joining. The production technology of longitudinally ribbed pipes is discussed in detail. Orig. art. has:

14 figures. L. Kochenova. [Translation of abstract]

[AM]

SUB CODE: 13/

UDC: 621, 771. 35

COKEHIM, Y. B.

AKOL'ZIN, L.Ye.; BOROZDOV, I.A.; BEDILO, V.Ye.; TERESHKIN, F.N. Prinimali uchastiye: BELYAYEV, F.R.; BEREZHNOY, N.V.; BUBYR', V.A.; VARSHAVSKIY, I.N.; DUDKO, V.P.; YERSHOV, V.S.; DUGHN, Ye.V.; DUKALOV, M.F.; IVANOV, P.S.; KONAREVA, V.F.; MONIN, M.I.; MOGILKO, A.P.; PANCHENKO, A.I.; POKALYUKOV, S.N.; PRIKHOD'KO, N.D.; RUBIN, I.A.; SIDOREHKO, P.A.; TYUTYUNIK, Ya.I.; KHMEL'NITSKIY, L.Ya.; BONDAR', V.I.; KRIVTSOV, A.T.; LOKSHIN, V.D.; SOFIYENKO, N.P. RABINKOVA, L.K., red.izd-va; BOLDYREVA, Z.A., tekhn.red.

[Types of mine cross section] Tipovye secheniis gornykh vyrabotok. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po gornomu delu. Vol.4. [Cross section of mines supported by a sectional reinforced-concrete lining of URP-11 panels for 1-, 2- and 3-ton railroad cars] Secheniia vyrabotok, zakreplennykh sbornoi zhelezobetonnoi krep'iu iz plit URP-II, dlia 1-, 2- i 3-tonnykh vagonetok. 1960. 278 p. (MIRA 13:12)

1. Khar'kov. Gosudarstvennyy proyektnyy institut Yuzhgiproshakht. (Mine timbering)

Methodology for the approximate calculation of induced resistances of dipoles. Radiotekhnika 17 no.11:23-29 N '62. (MIFA 15:11)

(Antennas (Electronics))

9,1700

S/108/62/017/011/003/007 D413/D308

AUTHOR:

Lokshin, V.L. and Yampol'skiy, V.G.

TITLE:

an approximation technique for calculating mutual

impedances of <del>vibrators</del>

PERIODICAL:

Radiotekhnika, v. 17, no. 11, 1962, 23-29.

The precise formulas for the mutual impedance are too complex for use in design calculations on multi-element arrays, while the published curves only cover a few of the cases needed in practice. The authors present a new approximation to the general formula, and compare the results from it with accurate calculations for various cases. The new formula appears to give good agreement for the resistive component of mutual impedance provided the vibrators are not much longer than full-wave and whatever the distance between them: the reactive component is not accurately given when the separation is less than  $\lambda/2$ , since the basis of the approximation breaks down, but a correction can be developed to take account of this. There are 11 figures.

SUBMITTED:

January 3, 1962

Card 1/1

LOXSHIN, V.S., polkovnik zapssa; PARKOV, V.P., polkovnik;
MUHAVTEV, A.I., red.

[A wonderful alloy] Chudosmyi splav. Poskva, Voem. izdvo M-va oboromy SSSR, 1965. 414 p. (MIRA 18:3)

LOESHIN, V.Sh., redaktor; POLOSINA, A.S., tekhnicheskiy redaktor

[Four-speed draw works for drilling; technical conditions for checking in for major repairs and for returning after repairs] Lebedki chetyrekh-skorostnye dlia bureniis; tekhnicheskie usloviia na sdachu v kapital'-nyi remont i na postavku posle remonta. Vedomstvennaia normal' Ministerstva M567-56. [Moskva] 1.v. (MLRA 9:12)

1. Russia (1923- U.S.S.R.) Ministerstvo neftyancy promyshlennosti. (Oil well drilling--Equipment and supplies)

[TV02-4x6 5/8 and TV03-4x6 5/8 internal release pipe grabs; technical specifications for delivery] Trubolovki vnutrennie

[TV02-4x6 5/8 and TV03-4x6 5/8 internal release state of technical specifications for delivery] Trubolovki vnutrennie osvobozhdaiushchiesia TV02--4x6 5/8 i TV03-4x6 5/8; tekhnicheskie usloviia na postavku. [Moskva, 1957] 5 p. (Vedomstvennaia normal' Ministerstva N811-56)

1. Russia (1923- U.S.S.R.) Ministerstvo neftyancy promyshelnnosti. (Oil wells--Equipment and supplies)

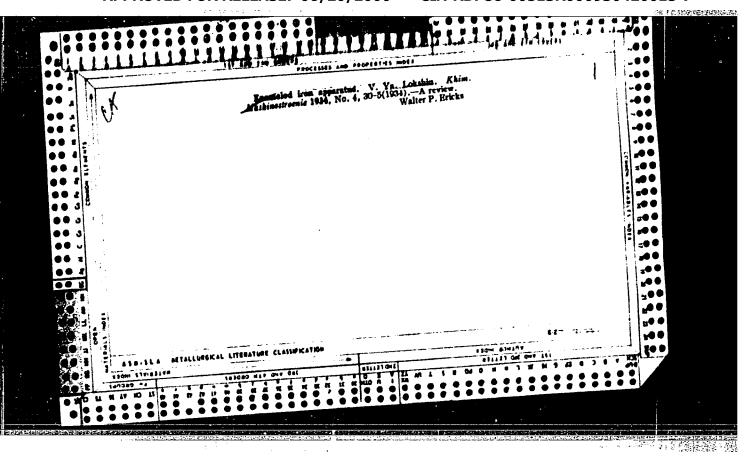
Le KShin, V.Sh., red.; KHLEENIKOVA, L.A., tekhn.red.

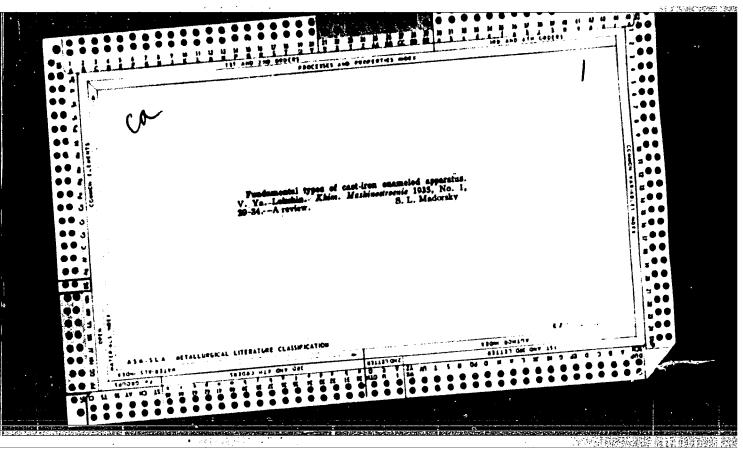
[Supplementary gear box for the LF2M windlass] Demul'tiplikator lebeki LF2M; tekhnicheskie usloviia na sdachu w kapital'nyi remont i na postawku posle remonta. [Moskva, 1957] 6 p. (Vedomstvennaia normal' Ministerstva N809-56) (MIRA 11:1)

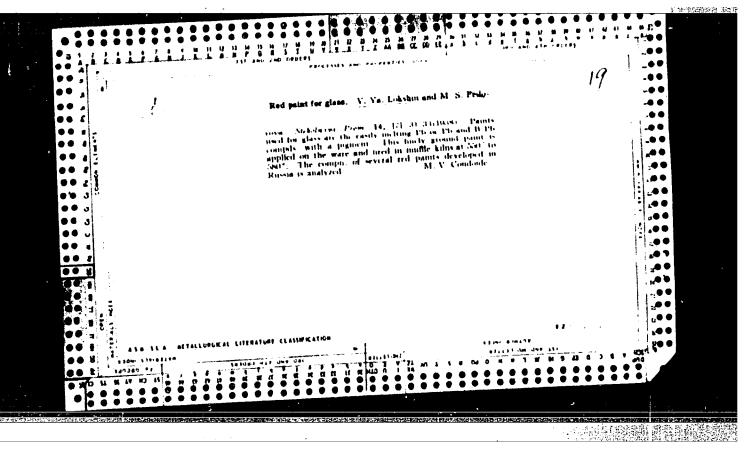
1. Russia (1923- U.S.S.R.) Ministerstvo neftyanoy promyshlennosti. (Windlass)

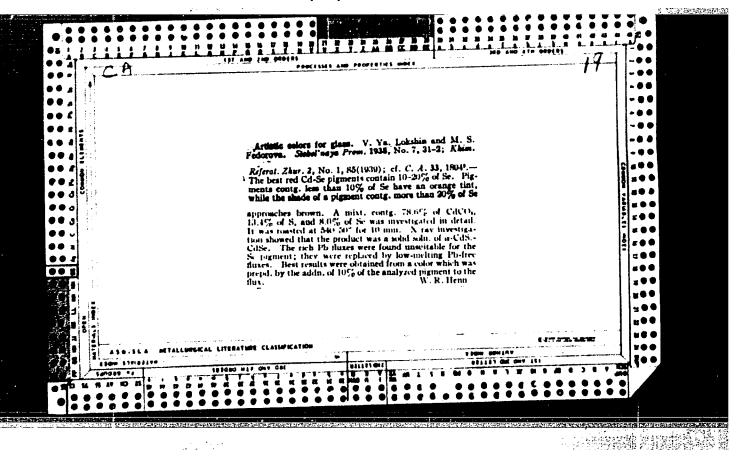
"APPROVED FOR RELEASE: 06/20/2000

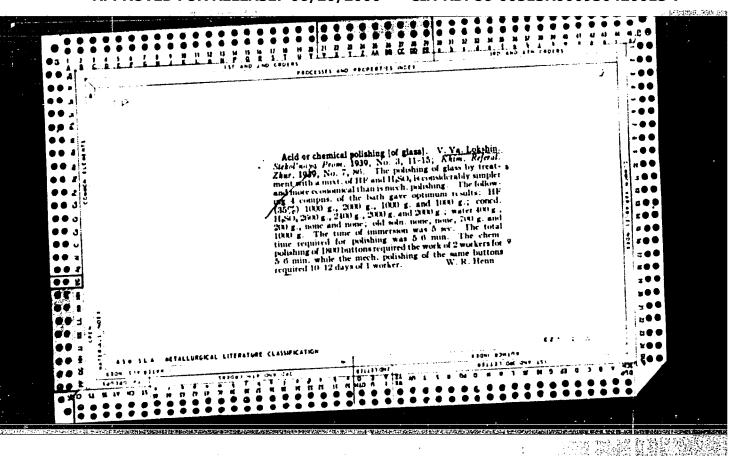
CIA-RDP86-00513R000930420015-7

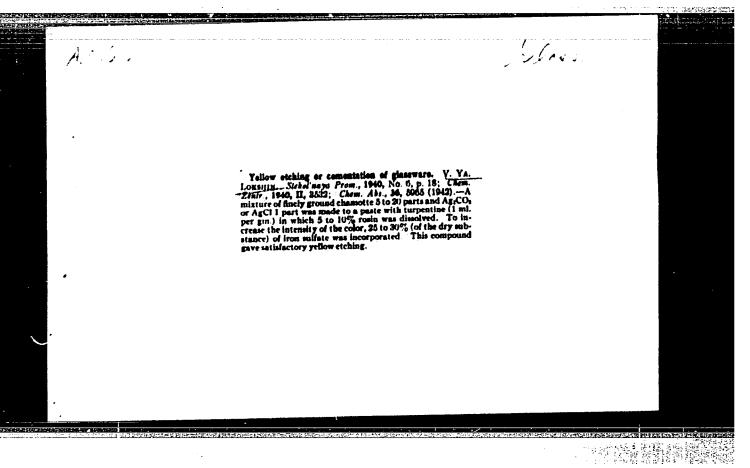












Techniques of enameling metal articles RSFSR, 1951. 342 p. (52-37712)

TS700.16

1. Enamel and enameling. 2. Cast-iron. 3. Sheet-steel.

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"

### CIA-RDP86-00513R000930420015-7 "APPROVED FOR RELEASE: 06/20/2000

7658. LOKSHIN, V. YA. -- Uproshchennyy metod opredeleniya płavkosti emaley, M., promstroyizdat, 1954. 12 s. s chert. 22 sm. (M-VO Prom-Sti Stroit. Materialov SSSR. Tekhn. Sovet I Tekhn. Upr. Tsentr. Byuro Tekhn.

Informataii. Inform. Soobsheheniya). 600 ekz. Bespl. --nvt. ukazan

na oborote tit. L. -- (55-3201)

666,26

SO: Knizhnaya Letopsis', Vol. 7, 1955

LOKSHIN, V YA.

LOKSHIN, V.Ya., kandidat tekhnicheskikh nauk; RAYNIS, I.S., redaktor;

MEL'NIKOVA, N.V., tekhnicheskiy redaktor

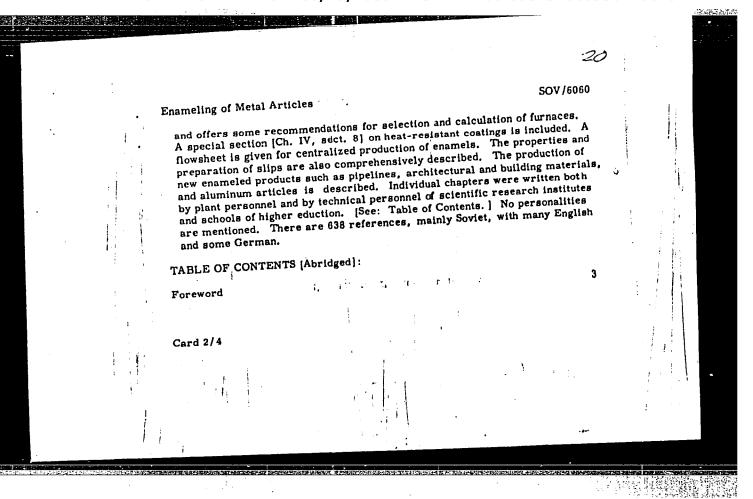
[Technology of enemeling metal parts] Tekhnologiia emalirovaniia metallicheskikh izdelli. Izd. 2-e, dop. Hoskva, Gos. izd-vo mestnoi promyshl. ESFSR, 1955. 422 p. (MLHA 8:8)

(Enamel and enameling)

		LOKSH			Li Steato i kormatina, 1950, Nr 12, pp 41-48 (USSE)	manuscration (Leangery obligates (Exception of the contents of		
--	--	-------	--	--	---	--	--	--

Foregresses on Bassals and Reial Bassaling  P. G. Paudah, Lartypity genederstweapy universites (Latina State of Translatory) reperted on the investigation of finites prize smearis (for constitutions) and for constitution of chantal companies of the including reports only in the including companies of the including reports of the prize of the companies of	
and and the second seco	SCALEN COMES PERSONAL DRIVER TO SERVICE PROPERTY.

# PHASE I BOOK EXPLOITATION PHASE I BOOK EXPLOITATION SOV/8060 Vargin, V. V., Professor, ed. Emalirovaniye metallicheskikh izdeliy (Enameling of Metal Articles). Moscow, Imashgiz, 1962, 546 p. Errata silp inserted. 7500 copies printed. Reviewer: A. S. Ragozin, Engineer; Ed.: M. V. Serebryakova, Engineer; Eds. of Publishing House: I. A. Borodulina, A. I. Varkovetskaya, and T. L. Leyof Publishing House: I. A. Borodulina, A. I. Varkovetskaya, and T. L. Leyof Publishing House: I. A. Borodulina, Mangig Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: L. V. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Literature on Machinkina; Tech. Ed.: M. V. Schechtinina; Managing Ed. (or Liter



THE PROPERTY OF THE PROPERTY O			NOT DESCRIPTION
	13		,
. Enameling of Metal Articles	7/6060		
PART I. ENAMELING TECHNOLOGY	5		
Ch. I. Raw Materials and Batch Preparation (V. Ya. Senderovich)  Ch. II. Melting of Enamels (V. A. Kuzyak, V. V. Vargin, and V. P. Vaulin)	23		
Ch. III. Grinding of Enamels and Slip Preparation (L. D. Svirskiy.	93		
PART II. THE TECHNOLOGY OF ENAMELING METAL ARTICL.  Ch. IV. Enameling of Steel Articles (N. S. Smirnov, N. N. Zelenskiy, Ye. M. Oshurkov, B. Z. Pevzner, Ye. A. Antonova, V. V. Ye. M. Oshurkov, B. Z. Pevzner, Ye. A. Antonova, V. V. Luchinskiy, V. P. Vaulin, L. V. Purin, V. V. Vargin, M. M. Karabachinskaya, A. A. Appen, and V. Ya. Lokshin.		<b>1</b>	
Card 3/4			
		•	

	·			
•			8	**
	•	Enameling of Metal Articles ( ' .)	SOV/8060	į
		Ch. V. Enameling of Cast Iron Articles (V. Ya. Lokshin) V. P. Vat G. A. Kudryavtseva, and V. E. Mishel*)	ulin, 352	, ,
		Ch. VI. Enameling of Aluminum Articles (M. V. Serebryakova)	422	
		Ch. VII. Enameling of Articles of Nonferrous and Precious Metals (L. L. Gutorova)	440	
		Ch. VIII. Control of Enameling Production (V. V. Vargin, M. V. Serebryakova, and G. P. Smirnova)	457	
		Ch. IX. Industrial Hygiene and Safety Engineering (B. Z. Pevzner)	494	
		Appendix (V. E. Mishel')	515	
	/	References	529	
		AVAILABLE: Library of Congress SUBJECT: Metals and Metallurgy	BN/pw/jk 10-31-62	
	:	Card 4/4	10-31-02	2
				:
				· •
Profession and the	estruction value			

ACCESSION NR: AP3012256 S/0125/65

\$/0125/63/000/011/0095/0095

AUTHOR: Lokshin, V. Ye.; Puzrin, L. C.

TITLE: Electron beam welding of thick metal parts

SOURCE: Avtomaticheskaya svarka, no. 11, 1963, 95

TOPIC TAGS: electron beam welding, thick metal welding, 1Kh18N9T stainless steel, AISI 321 steel, heavy section welding

ABSTRACT: Specimens of 1Kh18N9T [AISI 321] stainless steel 100 mm thick were electron-be m welded at the In: titut elektrosvarki im. Ye. O. Paton (Electric 'elding Institute). The parts were held together without a gap and welded from both sides. Welding equipment was a U-3 electron-beam welder, a U-146 electron cun, and an OB-449 power source. Because of the high concentration of energy, the welding required a minimum powder of only 19 kw, which in two-pass are welding is only sufficient for faining metal parts 15—18 mm thick. The heat-affected zone of the electron-beam weld was very narrow.

Card 1/2

ACCESSION NR: AP3012256
ASSOCIATION: none
SUBMITTED; 00 DATE ACQ: 02Dec63 ENCL: 00
SUB CODE: NL NO REF SOV: 000 OTHER: 000

ACCESSION NR: AP4004595

8/0020/63/153/004/0810/0811

AUTHOR: Lokshin, V. Ye.; Puzrin, L. G.

TITLE: Some data on weld formation in electron beam welding

SOURCE: AN SSSR. Doklady\*, v. 153, no. 4, 1963, 810-811

TOPIC TAGS: electron beam welding, weld formation, weld shape, electron beam pressure, molten metal pressure, welding

ABSTRACT: By the use of electron beam welding, welds with an extremely low form coefficient (less than 1/10) and a relatively large depth of penetration can be achieved. It has been assumed that the electron beam pressure permits a depth of penetration of several dozen mm, but a simple calculation proves this to be wrong. Thus, the electron beam pressure is at least one or two orders of magnitude lower than the ferrostatic molten metal pressure in the welding crater. The assumption that the depth of penetration is achieved because of the evaporation of metal in the zone heated by the electron beam is also wrong, since when a metal plate is melted by the electron beam, a fillet weld with reinforcement is formed. The authors therefore measured the pressure developing during electron beam welding by special experiments using scales attached to an induction coil in a vacuum chamber. When carbon steel was welded at 10 kv, 80 ma, 65 m/hour and optimal focusing, the pressure was 430 mg.; at the same time, the rated pressure of the electron beam was Cord 1/2

### ACCESSION NR: AP4004595

only 2.8 mg. This shows that the pressure on the molten metal during electron beam welding is commensurate with the molten metal pressure in the welding vessel and that the pressure of the electrons is insignificant. Other experiments showed that the overall pressure varies directly with the density of the electron beam. Orig. art. has: 1 figure.

ASSOCIATION: Institut elektrosvarki im. Ye. O. Patona, Akademiya nauk USSR (Institute of Electric Welding, Academy of Sciences Ukr SSR)

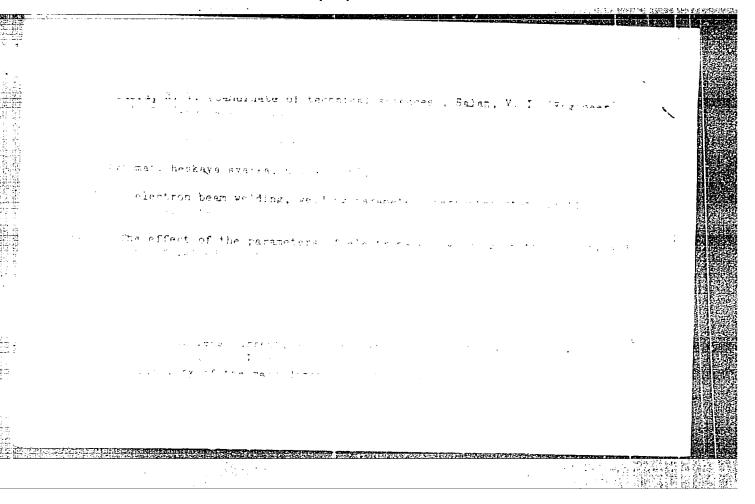
SUBMITTED: 08June63 DATE ACQ: 24Dec63

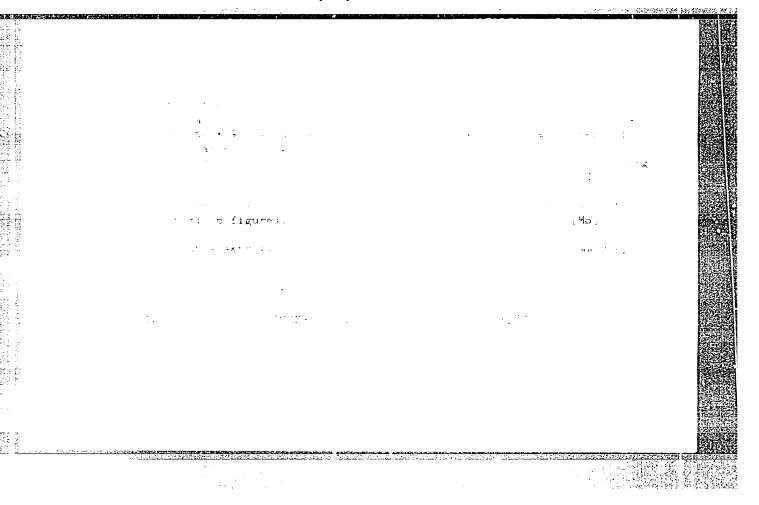
ENCL: 00

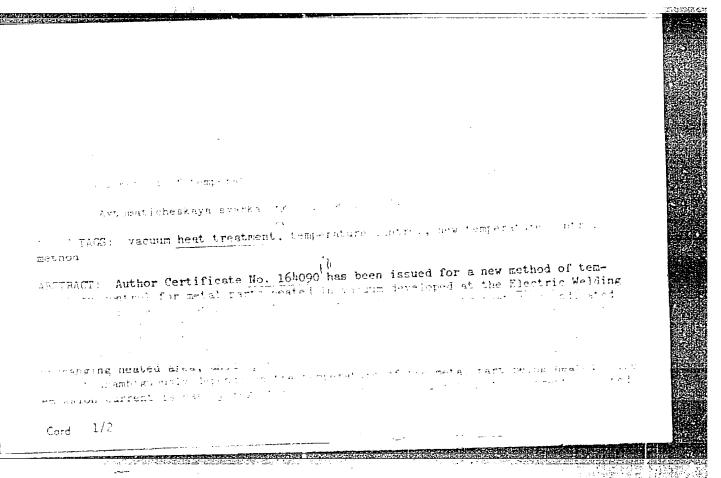
SUB CODE: ML

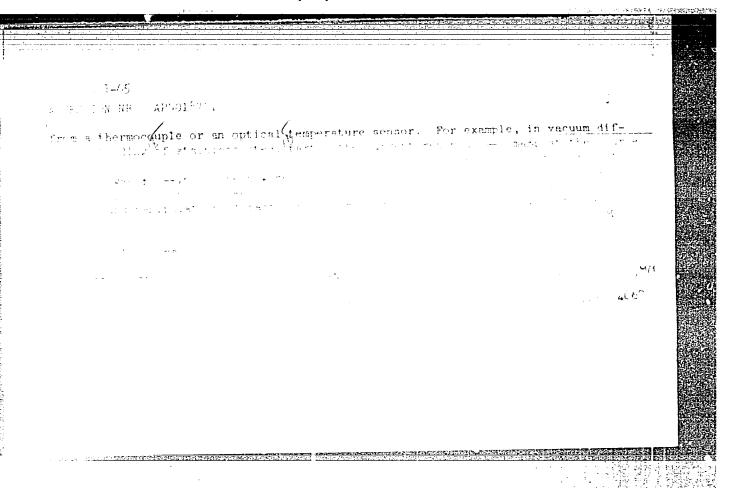
NO REF SOV: 001

OTHER: 001









Stabilization of electron beam wolding conditions. Avion, svan. 18 no.4 23-27 in 165. (VIBS 1847)

1. Institut elektrosvarki imeni batona 48 UkrCCR,

AUTHOR: Lokshin, V. Yu., Engineer.

122-2-6/23

TITIE:

An automatic production line for the manufacture of chiseltype ploughshares. (Avtomaticheskaya liniya dlya proiz-

vodstva dolotoobraznykh lemekhov)

"Vestnik Mashinostroyeniya" (Engineering Journal), PERIODICAL:

1957, No.2, pp. 36 - 43 (U.S.S.R.)

ABSTRACT: A production line recently erected at the Altaisk Plant for Agricultural Muchinery (Altaiskiy Zavod Selskokhozyaystvennogo Mashinostroyeniya) for manufacturing 1.1 million ploughshares per year is described. The apparent simplicity of the component is outweighed by its complex space geometry and absence of references bases. The blanks are cut from a special hot rolled recurrent section to eliminate the machining of the share chisel. The finish machining is carried out before bending the profile to simplify the grinding whilst the variable radius and helical curve have not yet been formed. The profile is then bent hot to eliminate springback. The production line consists of several divisions with intermediate storage to ensure flexibility. The new specially developed recurrent section is shown. The profile is cut, blanked, pierced and marked by press work. Machining consists of counter-boring of three holes, grinding of the working surface

Card 1/3

An automatic production line for the manufacture of chisel-type ploughshares. (Cont.) 122-2-6/23

and sharpening of the cutting edge and heel. The grinding and sharpening are performed on a special seven-spindle grinding mill constructed of standard units. The edge and heel sharpening require one spindle each, the grinding of the working surface (performed by the wheel face inclined at 40°) four spindles, and the grinding of the back, one spindle. The subsequent hot operations involve bending in a hydraulic press and heat treatment. The heating operations are performed by induction, at 2 500 cps. for bending and tempering and at 8 000 c.p.s. for quenching. Abrasive liquid cleaning for appearance is carried out with one part of silica sand in four parts of water under 4 kg/cm2 pressure. The layout of the production line is described. The mechanisms specially designed to ensure accurate automatic setting up of the grinding and sharpening operations are illustrated semi-diagrammatically. In sharpening the cutting edge, a weight loading is adopted, so that the grinding wheel follows the blank. The heating and finishing operations are entirely automatic. The use of automatic controls for all operations obviates the need for 100% inspection and a 2-3% sampling is practised. The automatic line reduces the labour cost to one quarter compared Card 2/3 with present day continuous production. The removal of press

and the second of the second o

An automatic production line for the manufacture of chisel-type ploughshares. (Cont.) 122-2-6/23 shop waste requires further mechanisation.

Card 3/3 There are 12 figures, including 4 photographs.

AVAILABLE: Library of Congress

Logstill, v. lu

122-2-1/33

Vlasov, S.N. and Lokshin, V.Yu., Engineers AUTHORS:

Experience with the Setting-up of Automatic Production TITLE:

Lines (Opyt otladki avtomaticheskikh liniy)

PERIODICAL: Vestnik Mashinostroyeniya, 1958, No. 2, pp. 3-6 (USSR)

The familiarisation stage in setting to work automatic ABSTRACT: production lines as experienced at the First National Ball Bearing Plant (1GPZ) and the "Altaysel'mash" ploughshare factory has proved to be of the same duration as the design and construction stage. The cost of blanks amounts to 40-60% of the total production cost and so the supply of blanks with minimum allowances is a major consideration. Thus, the introduction of blanks for ploughshares cut from a special "periodic" profile yielded an annual saving of 1.5 million roubles. Generally, the introduction of advanced mthods, in spite of higher first cost, is advantageous. Examples are: induction heating for the overall heat treatment of the ploughshares and the extensive use of centreless grinding in the ball race production line. The highest quality and consistency of cutting tools and abrasive wheels is essential. Nonuniform grinding wheels can reduce the utilisation of multi-spindle automatic machines from 85 to 50%. The configuration Cardl/3 of the automatic production line and its sub-division into

122-2-1/33

Experience with the Setting-up of Automatic Production Lines

several self-contained sections with adequate storage between them is the next most important element. The introduction of magazine chutes in the ploughshare production line has increased its utilisation by 10%. The combination of storage between sections in series and the provision of parallel sections has made it possible to achieve in the ball bearing plant a util-Transporter instalisation exceeding 70% from its very start. lations with a storage capacity ensuring independent working of the subsequent sections for at least 20 minutes have proved their value. In the original design of the ball-bearing and ploughshare production lines, the servicing and maintenance of equipment did not receive sufficient attention. The wear resistance of components in the transporter installations has been inadequate. All rapidly wearing assemblies must be easily accessible and interchangeable. Reliable lubrication needs thorough attention. Standardisation of typical units can be taken to considerable length. All creative groups should be drawn in to assist during setting to work. Initial faults due to manufacturing or assembly errors are revealed early and are easily remedied. They are not repeated. More profound design errors basically due to inadequate wear resistance or stiffness Card2/3 reappear and are best dealt with in groups and not immediately

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420015-7"