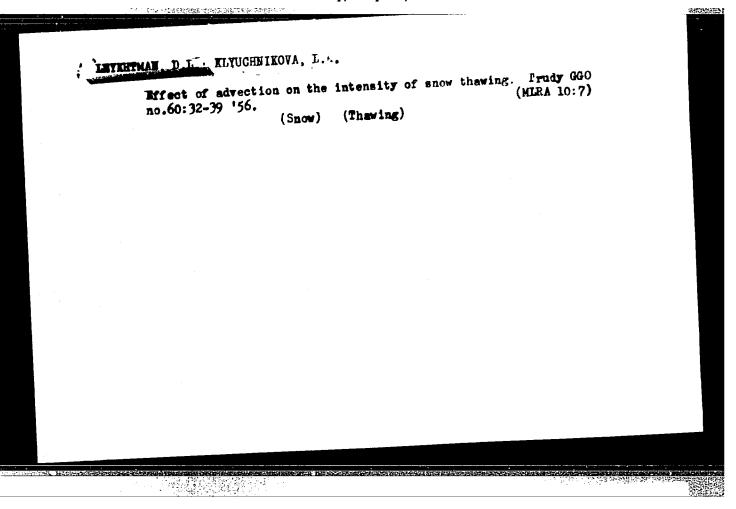
LEYKHTLING, K.A.; SMORGON, L.S., nauchnyy sotrudnik

Wear resistance of saws with bits. Trudy VSNIPILezdrev no.10:27(MIRA 18:10)
32 164.

1. Nachal'nik laboratorii stankov i instrumentov Vostochno-Sibirskogo nauchno-issledovatel'skogo i proyektnogo instituta lesnoy i derevoobrabatyvayushchey promyshlennosti (for Leykhtling).



## LEYKIN, A., inzh.

Expenditure of power in moving grain by chain conveyors with sunk scrapers. Muk. elev. prom. 28 no.1:14-15 Ja 162.

(MIRA 16:7)

1. Vsesoyuznyy nauchno-issledovatel'skiy i eksperimental'no-konstruktorskiy institut prodovel'stvennogo mashinostroyeniya. (Grain-Handling machinery)

DEMSKIY, A., ingh.; TAMAROV, Ye., inzh.; KALASHNIKOV, N., inzh.; SHISKIN, N., inzh.; LEYKIN, A., inzh.; IL'UEMINI, I., inzh.

New machines for mills and elevators. Mak.-elev. prom. 28 no.9: (MIRA 15:10) 22-26 S 162.

1. Gor'kovskiy mashinostroitel'nyy savod im. Vorob'yeva (for Demskiy, Tamarov, Kalashnikov, Shishkin). 2. Vsesoyusny, nauchno-issledovatel' skiy i eksperimental'no- konstruktorskiy institut prodovol'stvennogo mashinostroyeniya (for Leykin). 3. Khar'kovskava mashinoisnytatel' naya stantsiya.

(Grain-handling machine)

# IEYKIN, A.; IL'YEMINI, I.

Screw conveyor-loader for grain. Muk.-elev. prom. 29 no.3:24-25 (mira 16:9)
Mr 163.

1. Vsesoyuznyy nauchno-issledovatel skiy i eksperimental no-konstruktorskiy institut prodovol stvennogo mashinostroyeniya (for Leykin). 2. Khar kovskaya mashinoispytatel naya stantsiya (for Is yemini).

CHARNYY, M.; LEYKIN, A. The new All-Union State Standard for belt bucket conveyors

for grain and flour. Muk.-elev. prom. 29 no.9:26-27 S 163.

1. Vsesoyuznyy nauchno-issledovatel'skiy i eksperimental'no-konstruktorskiy institut prodovol stvennogo mashinostroyeniya.

TARASEVICH, Yuriy Sergeyevich; FUKS, I.I., inzh., retsenzent; LEYKIN, A.M., inzh., red.; SOROKA, M.S., red.izd-va; RUDENSKIY, Ya.V., tekhn.red.

[Designing dies for cold pressing] Konstruirovanie shtampov dlia kholodnoi shtampovki. Kiev, Gos. nauchno-tekhn. izd-vo mashinostroit. lit-ry, 1958. 187 p. (MIRA 12:2) (Dies (Metalworking)) (Metals--Cold working)

Card 1/2

117-58-5-6/24 Leykin, A.M., Engineer AUTHOR: Dies in Multispindle .utomatic Presses (Shtampy k mnogoshpindel'nym pressam-avtomatam) TITLE: Mashinostroitel', 1958, Nr 5, pp 17-21 (USSR) PERIODICAL: Constructional features of dies for multi-spindle presses are different from those of ordinary dies. Figure 1 shows a con-ABSTRACT: venient form of the lower part of die; the length of the die correspondends to the width of the table of the press, while the distance between retaining bolts must correspond with the grooves of the table. To the extent as the dies are installed on one press and function at the same stroke of one slide, they must be strictly of the same height. Blanks are cut out from a strip either on ordinary presses or on automatic presses. A typical shearing die is shown in figure 2 with the corresponding matrix. The first extrusion of a flat blank is done by means of the die shown in figure 3. The matrix consists of a bushing which can be centered in relation to the punch. On lowering the punch the part is extruded to the desired shape. After the first operation the part is picked up

APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R0009297200

by tongues and placed in position for the following operation.

Dies in Multispindle utomatic Presses

117-58-5-6/24

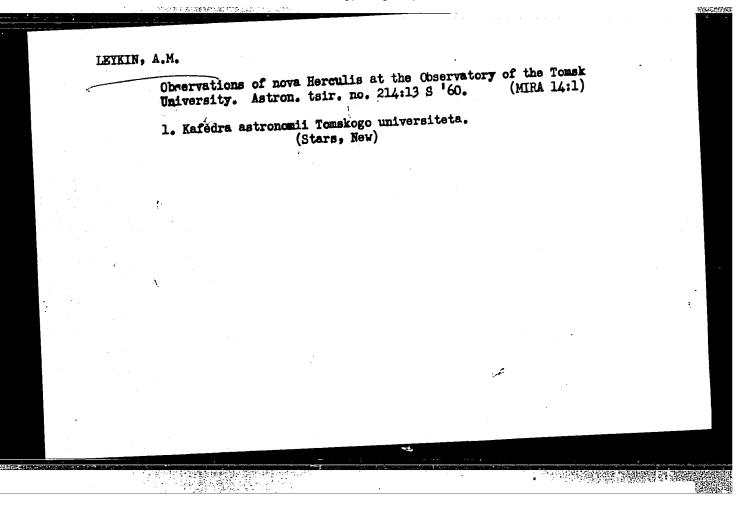
Figure 4 shows a typical die for the consecutive extrusion; this die differs from the preceding one only in the construction of the lower part. Figure 5 shows the precess of extrusion at the beginning of the operation (a) and at the end (b). Figure 6 shows the position of the extruded part on the next die designed to cut the flanges. Figure 7 shows the die forming the bottom of the part and calibration of the flange, as being the next operation in the cycle. The following bead rolling operation is done by a die as is shown in figure 8. For the punching of holes, two types of dies can be used, the difference of construction depending on whether the waste is evacuated through the upper or the lower part of the die, as is shown in figures 9 and 10. There are 10 figures.

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1. Dies-Construction



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	1964	SACE AND 10
LEYKIN, A. S. DECEASED		
SPRAY PAINTING		

Cand, Tech. Sci.

LEYKIH, A. S.

Dissertation: "Distribution of stresses in the crankpins of aviation

Scientific Council of the Central Sci-Res. Inst. of Aircraft Engine Building imeni

P. I. Baranov

### SO Vecheryaya Moskva Sum 71

LEYKIN, A. S., and SERENSEN, S. V.

"Studies of the Distribution of Stresses in Crankshafts of Airplane Engines."

SO: Izvestiya Akademii Nauk SSSR, Otdeleniye Tekhnicheskikh Nauk, No 3, pp 451-476, 1950.

### LEYKIN, A-S. USSR/Miscellaneous --- machine construction Card 1/1 Leikin, A. S., Cand. in Tech. Sciences Author Concentration of strains and calculation of the strength of a shaft Title with a transverse opening Vest. mash. 34/3, 3-14, Mar/1954 Periodical Transverse openings in shafts, because of the high concentration of strains which they cause, are often a source of breaking. The questions Abstract which have to be considered are the relation of the distribution of strains in hollow shafts with transverse openings during bending or twisting, to the effect of the thickness of the walls of the shaft, size of openings and their angle as compared with the shaft and nature of the edges of the openings. Results of experiments are given along with computations of strength and strains. Twelve Russian references, one dated 1952. Tables and graphs. Institution Submitted

LeyKIN,

PHASE I BOOK EXPLOITATION

sov/3472

Akademiya nauk SSSR. Institut mashinovedeniya

Problemy prochnosti v mashinostroyenii, vyp. 4 (Strength Problems in Mechanical Engineering, No. 4) Moscow, Izd-vo AN SSSR, 1959. 122 p. Errata slip inserted. 2,300 copies printed.

Ed.: N.I. Prigorovskiy, Doctor of Technical Sciences, Professor; Ed. of Publishing House: G.B. Gorshkov; Tech. Ed.: Yu.V. Rylina; Editorial Board: S.V. Serensen, Academician, USSR (Chairman), F.M. Dimentberg, Doctor of Technical Sciences, V.O. Kononenko, F.M. Dimentberg, Doctor of Technical Sciences, S.V. Pinegin, Doctor of Technical Doctor of Technical Sciences, S.V. Pinegin, Doctor of Technical Sciences, Professor, D.N. Reshetov, Doctor of Technical Sciences, Professor, G.V. Uzhik, Doctor of Technical Sciences, Professor, and R.M. Shneyderovich, Candidate of Technical Sciences.

PURPOSE: This collection of articles is intended for scientists and engineers concerned with plastic deformation.

COVERAGE: This collection of 6 articles by different authors gives the results of investigations carried out by the Institut mashino-

Card 1/3

Strength Problems (Cont.)

sov/3472

vedeniya AN SSSR (Institute of Machine Science, Academy of Sciences, USSR). The foreword was written by N.I. Prigorovskiy, Professor, Doctor of Technical Sciences, editor of the collection. The collection of articles is the second of a series and discusses the problem of tensile and compressive stresses, elasticity, deformations under loading, and the calculation and analysis of stresses. The authors emphasize advanced methods of analysis and report on experimental results. References follow each article.

TABLE OF CONTENTS:

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Foreword

Shneyderovich, R.M. [Candidate of Technical Sciences]. Elastic and Plastic Deformations of Beam and Frame Constructions

The method described is based on variable parameters of plasticity. Rods, beams, and frames are discussed.

Shishorina, O.I. Experimental Verification of the Superposition Method for Solving Stress Concentration Problems 47

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Leykin, A.S. Stress Concentration in Fillets Symmetric Shafts Under Bending and Torsional	s in Stepped Axial- Stresses 61
Vasil'yev, A.A. Stresses in the Blade of a Blade Turbine	Hydraulic Adjustable-
Ugodchikov, A.G. Stress Concentrations in T	ightly-Fitted Parts 100
Khurshudov, G.Kh. Stresses in Plate-Shaped l Crossbars	Frames Connected by
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### "APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000929720

E I NOCK EFFORMATION SOV/NAS abtorreductive Convince of Naturally Convince of Strungth of conv. 1979. 199 p. Errain Bellocus; Considery; Pedi. Mai. S. S. S. Salkin. Occabory; Pedi. Mai. S. S. S. Salkin. Occabors and estimates on construction:	onier. mis col inte of Section in Serengia of a sectivity. The alsectivity of the occupation attes and combants at the end column	n pracoliti ar dystan utti dariodically ta ia a Compressible	tanati Tanati		7 7 7	h A		1
FRAME I NOCK EXPLOSATION BOY/NALS FRAME IN NOCK EXPLOSATION BOY/NALS FROM NAME AND A DESCRIPTION OF STRUCTURE	OFFIGURE The book continued to preficient; mass otherstice search and of mediate contraction of the prepared under the direction of the interpret mode to the search of th	PART II. DIRANGS AND CALCHIANTES OF SHEEDTH AND EXTERNITY Exception, T. O. Marinel Vibrations of a Scalinear System with Particle Variable Pareneters Balatti, T. T. Problem of the Stability of a Flate in a Compressible Take June	Preschers, I. M., and Quastry, A. A. Deflacting Force in a Florible Sease Comes by the Forces of Tabelians Grober, W. A. Asymptotic between Studying Konstationary Thurst con- Graphy W. A. Asymptotic between Studying Konstationary Thurst con- Graphy M. A. Asymptotic Devices Problems of Siligaty Seri and Non- Vernings, A. R. Analogy Between Problems of Siligaty Seri and Non- Vernings, A. R. Analogy Between Services of Warners Pricessa	miltimaly leaded (tremlar Plates of Varying immunosity, St. D., Calculation of Symmetrically Looked Support Christian Plates by the Method of Initial Parameters Christian by the Method of Initial Parameters Spherical Confederations of Eventual Pressures in Spherical Confederations	Mainin, B. E., Calculation of Greep of Notating Recentionally Enated Tidology of Varying Thibiness  Paskin, Yorkes. Fractice of Calculating Parameters of Notating Dison During Flastic-Blastic Deformation  Recentered by B. H., Spatic-Liastic Deforming of a Bess of Circulat Recentering, B. H., Spatic-Liastic Deformation of a Bess of Circulat Recentering in M., Spatic-Liastic Deforming of a Bess of Circulat Recentering in M., Spatic-Liastic Deforming of a Bess of Circulat Recentering in M., Spatic-Liastic Deforming of a Bess of Circulat	painter, B. P., Putipe of Compressor Risks Laytin, A. B. Brudy of the Extribution of Stresses in Fir Tree Type 1974 of Publics Risks in Pranton and Bonding Obseringer, T. F. F., Study of the Extribution of Purces in Fir Tree	Rephotor, D. F., and Z. M. Jertha. Chiculations on Contact Rigidity In Reching Construction Transferor, A. D. One Characteristic of a Milp Line APLIABLE: Library of Congress	- Abilian
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AUTHOR: Leykin, A. S. (Moscow) SOV/179-59-3-33/45

TITLE: The Distribution of Stresses in Bending a Multi-tooth Coupling of Equal Hardness (Raspredeleniye usiliy priizgibe mnogozubykh soyedineniy postoyannoy zhestkosti)

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Mekhanika i mashinostroyeniye, 1959, Nr 3, pp 179-183 (USSR)

ABSTRACT: A case is described when a herringbone type lock (Fig 1) serves as a coupling device for joining the vane assembly and disc of a turbine. The diagram showing a distribution of stresses is shown in Fig 2. When the distribution of reactive forces due to stresses are defined as Eq (1.1) (where t 7 step distance between teeth, b - width of the locking ring), then the bending moment can be expressed as Eqs (1.2) and (1.3) (where x - length of the locking coupling, be bending arm of a tooth). The condition of a joined action is defined by Eqs (1.4) and (1.5), where E - modulus of elasticity, \( \mu \) - Poisson coefficient, I - axial moment of coupling inertia, \( \wideharmony \times \times \times \) and \( \chi \) - coefficients of the tooth's pliability \( \wideharmony \times \times \times \times \) and \( \chi \) - coefficients of the tooth's pliability

SOV/179-59-3-33/ $^4$ 5 The Distribution of Stresses in Bending a Multi-tooth Coupling of

Equal Hardness integration, N  $\leqslant$  0.2 M/x (Fig 2), the index  $\Pi$  denotes the vane shaft and  $\Pi$  - coupling ring of the disc. condition of equilibrium of forces is expressed by Eq (1.6). Thus, the expression (1.7) is obtained from Eqs (1.2), (1.3), (1.5) and (1.6). The general solution of the problem can be found from Eq (2.3) which is obtained from Eq (1.5) for the conditions (2.1) and The formulae (2.4) define the distribution of forces p(x) and p(x) when the formula (2.5), found experimentally, can be applied. Then, its solution can be determined as Eqs (2.6), (2.7) and (2.8). The bending moments of both the shaft vane and the coupling ring of the disc can be expressed as Eq (2.9) which, when Eq (2.6) is included, can be written as Eq (2.10) The relations (3.3)  $(+ = M_{\prod}(x) \text{ and } - = M_{\bigwedge}(x)).$ to (3.8) can be defined for the conditions (3.1) and (3.2), where x - angle of deflection of the cross-section x = 0 of the coupling ring. The formulae in this work were Card 2/3 verified experimentally. Fig 3 illustrates the moment

sov/179-59-3-33/45

The Distribution of Stresses in Bending a Multi-tooth Coupling of Equal Hardness

of bending M, K = M, K (x)/M related to the coupling ring of the lock x = x/x as obtained for the 5-teeth lock. Good agreement between the experimental results (circles) and the theoretical ones (curves) can be seen from this figure. There are 3 figures and 3 Soviet references.

SUBMITTED: November 8, 1958

Card 3/3

83320

8/179/60/000/04/019/027 E191/E181

Leykin, A.S. (Moscow)

On the Overall Non-Uniformity in the Distribution of Stresses in the Roots of Blades Van Turbo-Machinery Stresses in the Refeat of the Blade Profile Associated with the Effect of the Blade Profile AUTHOR: TITLE:

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk. Mekhanika i mashinostroveniye. 1960. No 4. nauk, Mekhanika i mashinostroyeniye, 1960, No 4, pp 149-153

TEXT:

The strength of turbine blade roots is substantially of strength of turbine blade roots is substantially of stress concentration. The strength of turbine blade stress concentration of stress distribution of stress but also by the curved profiled part causes a sources but also by the root and the profiled part causes a connection between the root and the profiled part of stress distribution. Substantial overall non-uniformity of stress distribution. connection between the root and the prolited part causes a substantial overall non-uniformity of stress distribution. substantial overall non-uniformity of stress distribution. Failures in blade roots are usually fatigue failures and start at the point of the root where this non-uniformity is greatest. rallures in place roots are usually latigue lallures and start the point of the root where this non-uniformity is greatest the point of the root where this non-uniformity is greatest the the point of the root where this non-uniformity is greatest the latest of the effect of stresses due to the stresses of section is independent of the effect of stresses due thanks of section is independent of the effect of stresses.

It was round in previous investigations that the ellect of the to the effect of stresses due to change of section is independent of the ellect of stresses due to the forces at the contact points between the higher root and the difference at the contact points between the higher root and the difference at the contact points between the higher root and the difference at the contact points between the higher root and the difference at the contact points between the higher root and the difference at the contact points between the higher root and the difference at the contact points between the forces at the contact points between the difference at change of section is independent of the effect of stresses and the disc. the forces at the contact points between the blade root and the disc.

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**LEASE:** Monday, July 31, 2000 CIA-RDP86-00513R0009297

83320

s/179/60/000,604/019/027 E191/E181

On the Overall Non-Uniformity in the Distribution of Stresses in the Roots of Blades in Turbo-Machinery Associated with the Effect

For this reason, strain gauge tests were carried out with enlarged metal models of blade profiles integral with rectangular blocks simulating the roots. The models were loaded in tension and bending. The blade portion was of uniform cross-section. In most of the models, an intermediate flange was formed between the blade of the models, an intermediate flange was formed between the blade of the models. and the root portions. The different models were distinguished by and the root portions. The different models were distinguished different relative stiffnesses of the blade and root portions. The ratio of the profile chord to the width of the root was maintained in the narrow interval between 0.85 and 0.96, the blade of the profile shape of the blade and root was maintained in the narrow interval between 0.85 and 0.96, characteristic of actual designs. The profile shape of the blade was described by the angles of the tangents to the profile contour near the leading and trailing edges and the angles of the tangent to the mean profile line. The position of the blade in relation to the root was characterised by the angle between the blade chord and the plane of symmetry of the root. The section of the blade root in which the stress distribution is sought lies at a variable Card 2/4

83320

S/179/60/000 604/019/027 E191/E181

On the Overall Non-Uniformity in the Distribution of Stresses in the Roots of Blades in Turbo-Machinery Associated with the Effect of the Blade Profile

distance from the beginning of the blade section. The ratios of the cross-sectional areas and section moduli of the blade and the the cross-sectional areas and section moduli of the blade and the root were further parameters. The stresses were measured with root were further parameters. The results of the measurements show strain gauges of 3 mm base. The results of the measurements show that peak stress factors just exceeding 2.0 exist in the root. that peak stress factor sportion in the middle of the Very near the top face of the root portion in the middle of the very stress that meaning the stress nearly vanishes. Two stress peaks blade profile, the stress nearly vanishes. Two stress peaks blade factors of tension and bending on the stress distribution are the effects of tension and bending on the stress distribution are very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar. The experiments have yielded families of curves very similar the maximum peak stress factor to each of the main relating the maximum peak stress factor to each of the main formulae empirically summarizes the tests. The peak stress of formulae empirically summarizes the tests. The peak stress factors are related to each of the geometric parameters of the blade profile and the root section.

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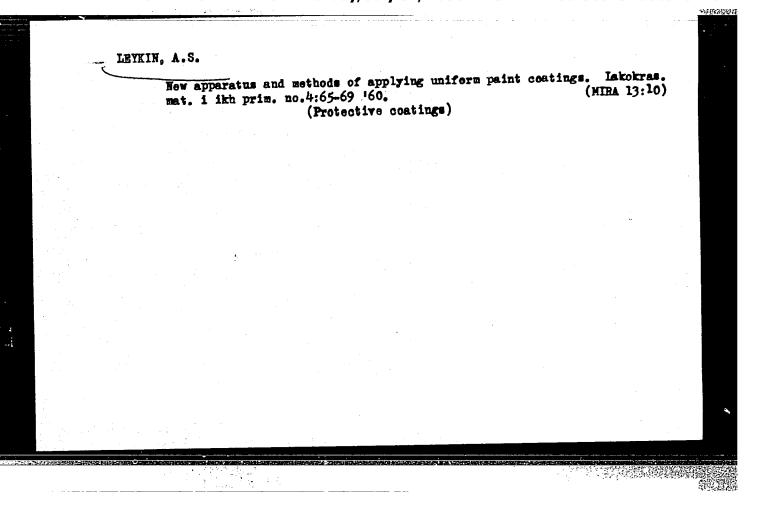
83320 \$/179/60/000/04/019/027 E191/E181

On the Overall Non-Uniformity in the Distribution of Stresses in the Roots of Blades in Turbo-Machinery Associated with the Effect of the Blade Profile

There are 5 figures and 2 Soviet references.

SUBMITTED: July 11, 1959

Card 4/4



CIA-RDP86-00513R0009297200 **APPROVED FOR RELEASE: Monday, July 31, 2000** 

3/122/60/000/005/004/017 A161/A130

AUTHOR:

Leykin, A. S., Candidate of Technical Sciences

TITLE:

Stress concentration in prankshaft fillets

PERIODICAL: Vestnik mashinostroyeniya, no. 5, 1960, 20-25

Data existing in literature are too limited for accurate evaluation of stresses and strength of crankshafts. Stress concentration at bending and TEXT: torsion has been studied in experiments with large single-crank metal models (neck diameter 200 mm), and a calculation method is suggested. Strain on the fillet was measured with wire tensiometers and an induction tensiometer, and the main strain sense preliminarily determined by brittle varnish method. A crank specimen and shafts with barrel-shaped bores were examined. The article includes a part of experimental data. The suggested method for calculating the stress concentration in fillets consists in the following procedure. The stress concentration factors are first determined for initial sheft, and then corrected for the given parameters of a real shaft. For the case of bending in the crank plane, the concentration factor (%) as is first calculated for the fillet of analogous crankshaft but with zero overlapping of necks and an optimum distance to the weight-reducing bore

Card 1/5

5/122/60/000/005/004/017

Stress concentration in crankshaft fillets

in the adjacent web (L = L\*): (κε) Δ = 0 = (κε) Δ = 0 (βε) b (βσ) a

where  $d(\alpha_0)_{\Delta} = 0$  is the concentration factor  $(\alpha_0)_{\Delta} = 0$  for a snaft with  $\frac{b}{d} = 1.6$  and  $d(\beta_0)_{\Delta} = 0$ , determined depending on  $\beta_0$  by Fig. 3 a;  $(\beta_0)_{\Delta}$  and  $(\beta_0)_{$ concentration in the shaft fillet, taken from Fig. 3 b and c. If the weightreducing bore is eccentrical, a factor must be introduced into the right part of the equation (4), ( $\alpha_e$ ) depending on the relations  $\frac{d}{d}$  and  $\frac{d}{d}$ . Next, the ( $\beta_c$ ) and the equation (4), correction factors characterizing the effect of the necks overlapping and the distance to the home in the address to the home in the address to the home. the distance to the bore in the adjacent web are calculated;  $(\beta_6)\Delta$  is found with

where  $(\beta_6)_{\Delta}$  is the  $(\beta_6)_{\Delta}$  factor for analogous crank with  $\frac{1}{d}=1.6$ , from Fig. 5a; and  $(\xi)_b$  - correction factor depending on  $\frac{1}{d}$ , from Fig. 5 b. Before finding  $(\xi)_L$ , and  $(\xi)_b$  - correction factor depending on  $\frac{1}{d}$ , from Fig. 5 b. Before finding  $(\xi)_L$ , the optimum distance to the bore in adjacent neck  $\frac{1}{r}$  must be found in Fig. 6 a. the optimum distance to the bore is  $(\beta_6)_L$  factor is found from Fig. 6 b if the real distance to the bore is larger than optimum (i.e.,  $\frac{1}{L^*} > 1$ ), and from Fig. 6 c if it is below 1. Experilarger than optimum (i.e.,  $\frac{1}{L^*} > 1$ ), and from Fig. 6 c if it is below 1. (B6) = 1 - (E6) = [ 1 - (B6) & ].

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Stress concentration in crankshaft fillets

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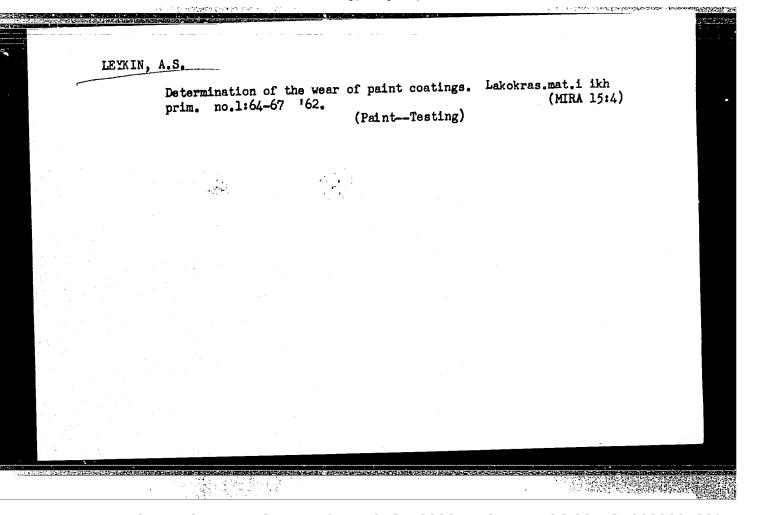
mental data of Ref. 7 (W. C. Gadd, T. C. van Degrift, A Short Gage-Length Extensometer and its Application to the Study of Crankshaft Stress, "J. of Applied Mechanics", March 1942, v. 9, no. 1) were also utilized for plotting the curves (Fig. 6). Finally the stress concentration in the fillet of the real crankshaft at bending in the crank plane is calculated with the formula

In the case of barrel-shaped bores,  $d_1$  must be replaced by  $d_2$  in the calculation of the stress concentration factor  $(\mathcal{A}_7)$  for torsion. It is first to be found for stepped axisymmetrical shaft with same  $\frac{1}{d}$  and  $\frac{1}{d}$  as in the sought-for crank and  $\frac{1}{d} = 2$ . The formula for tangential stress doncentration factor in the sought-for shaft at torsion is

 $\alpha_{\hat{l}} = (\alpha_{\hat{l}})_{o} (\beta_{\hat{l}})_{b} (\beta_{\hat{l}})_{h} (\beta_{\hat{l}})_{\Delta} \qquad (7)$  Factors to the formula (7) are given in (Fig. 8). The formulae (3) and (6) originate from author's previous works listed in bibliographic references. A practical calculation example is included. There are 9 figures and 7 references: 6 Soviet-bloc and 1 non-Soviet bloc. The reference to the English-language publication is cited in text.

Card 3/5

# Perchlorovinyl-cement compositions for the painting and waterproofing of structural surfaces. Lakokras.mat.i lkh prim. no.1:36-41 161. (MIRA 14:4) (Building materials) (Paint materials)



41894

5/740/62/000/009/001/002 E191/E135

26.212

TITLE:

Leykin, A.S. AUTHOR:

Non-stationary thermal elasto-plastic stresses in a hollow cylinder with a surface temperature varying

exponentially with time

Akademiya nauk SSSR: Institut mashinovedeniya. SOURCE:

Problemy prochnosti v mashinostroyenii. no.9, 1962.

57-72

The problem of non-steady-state heat conduction is solved for the hollow cylinder under boundary conditions expressed TEXT: as arbitrary exponential polynomials, which take into account the possible lag of the beginning of temperature variation at the colder surface of the body. Initially, the infinite hollow cylinder has a stationary temperature field, wherein the temperature varies logarithmically with the radius. A varying temperature gas flow inside and a cooling air flow outside create surface temperature variations following different exponential laws. On the assumption of purely radial heat flow, the heat conduction equation and the initial and boundary conditions are formulated. Card 1/4

S/740/62/000/009/001/002 Non-stationary thermal elasto- ... E191/E135

A Laplace transformation with respect to time is applied to the difference between the variable temperature and the initial temperature of the cycle. An ordinary differential equation is obtained for the transform, whose solution is given in a general form using Bessel functions. The solution for the temperature is derived by an inverse Laplace transformation. The ratio of the difference between the actual and initial temperatures to the largest temperature increment on the inner (hot) surface is written down. Simplification of the expressions in a special case is discussed. The thermo-elastic stresses are derived using the general equations of the theory of elasticity on the assumption that neither Young's modulus nor the coefficient of thermal expansion are dependent on the radius. The thernal stresses in the elasto-plastic region are derived by an approximate method on the assumption that the effective Poisson's ratio has the value of 0.5. This assumption has been shown earlier by R.S.Kinasoshvili (Raschet na prochnost' diskov turbomashin. "Stress analysis of discs in turbo-machinery", Oborongiz, 1954) to agree well with observations of elasto-plastic deformations of turbine discs at Card 2/4

S/740/62/00C/009/001/002 E191/E135

Non-stationary thermal elasto- ...

high temperatures. The hollow cylinder is divided into several concentric tubes, each with a constant effective Young's modulus. An elastic analysis is applied first. For a given instant in the heating or cooling cycle, the stress values are cound at the mean radii of the tubes from the known temperature distribution along the radius and from graphs giving the variation of Young's modulus and the thermal expansion coefficient with temperature. Some auxiliary integrals and functions are computed by combining graphical and analytical methods. These enter into the expressions for the principal stresses, from which the equivalent "octahedral" normal stress is computed. If the equivalent stress exceeds the yield stress, the strain is first derived from the "elastic" stress, then the true stress corresponding to the above strain is found from the stress-strain curve measured in pure tension and, finally, the secant modulus is computed. With this secant modulus, the principal stresses and equivalent stress are derived again until the approximation process converges. A numerical example applies the analysis to conditions similar

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Non-stationary thermal elasto- ...

S/740/62/000/009/001/002 E191/E135

to those in gas turbine blade tests. The temperature changes most rapidly at the start of the heating (cooling) cycle. The highest equivalent stress is reached after six seconds of heating. Its "elastic" value is  $54~\rm kg/mm^2$  and the true "plastic" value is  $25~\rm kg/mm^2$  at a longitudinal strain of 0.005. There are 8 figures.

Card 4/4

IEYKIN, A.S., kend. tekhn. nauk; VINOGRADOV, B.R., inah.

Study of hydration and hardening processes of emulsified

Study of hydration and hardening processes of emulsified

(MIRA 17:9)

(MIRA 17:9)

LEYKIN, A.S., kand.tekhn.nauk; PESEL'NIK, V.Ye., kand.tekhn.nauk

Protective coatings for air-entrained silicate slabs of exterior walls.

(MIRA 16:2)

Stori. mat. 9 no.2:15-16 F \*63.

(Sand-lime products) (Protective coatings) (Walls)

LEYKIN, A.S., kand.tekhn.nauk

Stress distribution caused by the bending of herringbone joints of turbomachine blades. Vest.mashinostr. 44 no.1:22-31 Ja '64. (MIRA 17:4)

5/0122/64/000/003/0026/0032

ACCESSION NR: APLO26245

patesers weak realist thou

AUTHOR: Leykin, A. S. (Candidate of technical sciences)

TITLE: Construction methods to improve strength of christmas tree locks in turbine blades under variable loads

SOURCE: Vestnik mashinostroyeniya, no. 3, 1964, 26-32

TOPIC TAGS: christmas tree lock, turbine blade, rotor disk, stress concentration, vibration damping, nomuniform stress distribution

ABSTRACT: Different ways of improving the strength of christmas tree locks joining turbine blades to the rotor disk have been discussed. To reduce the local stress on the trough (space between teeth) of the lock the radius of curvature is increased and the surface of the tooth is beveled. This lowers the coefficient of stress concentration by 20-29%. An attempt is made to redistribute the reaction force on the lock teeth by making the coefficient of linear expansion & of the disk material larger than & of the blade material. A nominal clearance & is suggested in a 6-5 pair of christmas tree lock teeth to hold the coefficient of reaction force nomuniformity below a given level. It is shown that the clearance

Card 1/2

## ACCESSION NR: APLO262L5

o expresses the difference in dimension between the tooth pitch of the disk and the blade roots, at working temperatures, relative to the unit length of the christmas-tree lock profile line. To minimize nomuniform stress distributions the parameter \( \begin{align\*} & = \L/b \) is increased (b = blade chord, L = distance from top of lock surface to the first trough). To improve rotor blade vibration damping in the blade-lock coupling, the addition of a band of rods is suggested on the blade-to-joint coupling rack, or a split root for the rotor blades. The adverse effects caused by such damping techniques are discussed, in particular when they create local stress concentration in blade roots or the lock. Orig. art. has: 6 equations and 6 figures.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 20Apr64

ENCL: 00

SUB CODE: MD

NO REF SOV: 005

OTHER: 002

Card 2/2

IEYKIN, A.S., kand. tekhn. nauk

Strength calculation of shaped parts by extreme reduced effective stresses. Vest. mashinostr. 44 no.8:9-16 Ag 164.

(MIRA 17:9)

TO ASSET FOR THE STREET WINTERS SEED TO SEE A - E5510N M : AT4046185 AUTHOR: Blinnik, B. S., Leykin, A. S. TIPLE: The design of working turbine clades with the fellowers The second secon TODAY TAGS: turbine blade, turbine leade design blade contlut, turnine blade awarkact; The authors note that it is but to be seen the catalitys of gas turbines. and the company of th of a felt weiges independent extimation of the stresses in the flankers of endiable at given lift for computation to the reduction of negative allowante tergent onto flanges recapse of the Cord 1/3

L 14956-65

ACCESSION NR: AT4046185

or awing of the disk and blades under the eiters to be eitritizal forces and femcerature. The increase in allowance as a result of temperature expansion is to allow described. It is now to accomplish to the end of the

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there is anywhere the model of  $\Delta_{ij}$  . The relations of was a substance of the structures of

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ASSOCIATION: None

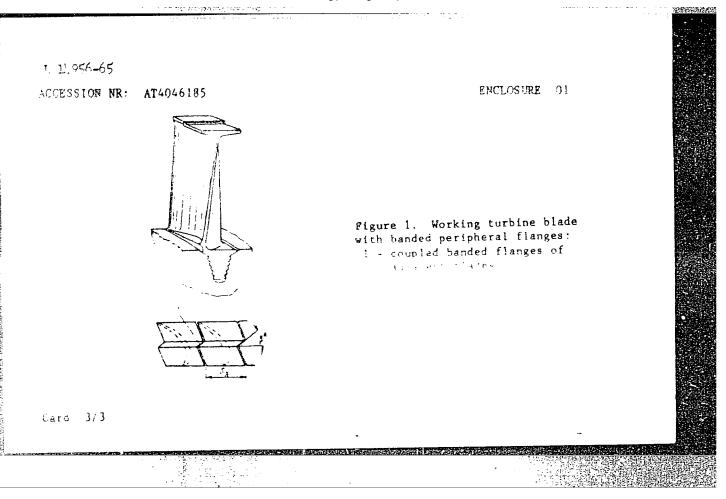
SUEMITTED: 15Apr64 ENCL: 01 SUB CODE: PR

NO REF SOV: 005 OTHER: 002

Card - - - - 2/3

## "APPROVED FOR RELEASE: Monday, July 31, 2000

## CIA-RDP86-00513R000929720



ENDERSON AGE OF EWE REPORT OF THE RESERVE OF THE STORY OF A. ESSION NR: AT4C46191 -5 0000 F4 000 001 00217-0258 AUTHOR: Leykin, A. S. TIPLE: Stress concentration and relative stress distribution factors in the tis mone locking mechanisms of turbine blades SOURCE: Prochrost' i dinamika aviatsionnv\*kh dvigatelev (Durability and dynamics of direraft engines); sbornik statey, no. 1. Mest w. Izd-vo Mashinostroyenive. 1964. 277-288 TOPIC TAGS: turbine blade, turbine blade coupling, turbine blade stress, fishbone catch ABSTRACT: The author notes that the fatigue character of the majority of failures observed in the fishbone-type locking devices which are used to couple the blades to the disks in turbines requires a careful investigation of the concentration and distribution of stresses on the surfaces of the joint element reesses particularly under hending conditions . A combar of proprieseral studies of era concentration and distribution, primarics using the polarization-obtical and for situations of tension of the ending of the end obticized mountaint article, the author crist word case one wealth of a study jets Card 1/4 \_

L 24415-65 ACCESSION NR: AT4046191

stress concentration and distribution on the surfaces of the recesses or depressions of locking devices of the fishbone type under the effect of both bending and stretching. These results were obtained by the author on the basis of previous enderiments (A. S. Leykin, Isslede Janive rashredeleriya haprvayheriy v velochov\*kh ovako lonatok turbin pri rasivazovom podzel koje o vodeky\* prodocesti material-. sunstruktsiy. Izd. AN SSSR, Modeling and also termine there applementary experiments using the tensiometric method on large, flat, metal models with elastic deformation of the materials. In a manner applicable to the ratios of the geometric dimensions characteristic of fishbone locking mechanisms, general formulae are proposed for dimensionless factors of stress concentration and relative ation as a function of the last, geometric parameters of the lock or retentime coupling joint. The formulae are simple in form and provide the degree of racy required for practical engineering calculations. Figure 1 of the Enclosto shows diagrams of the force interaction of the elements of a fishbone-type \* 3 coint of the type considered in this application for an interior lience of stretin- Committee (with neeliminary viscous), and for a tree action and property of a. Increase in stresses of the wirthles of the receases of the fishbone-type

Card 2/4

L 24415-65

ACCESSION NR: AT4046191

the teeth. Some numerical recommendations are given. Orig. art. has: 7 figures

and 33 formulas.

ASSOCIATION: None

SUEMITTED: 15Apr64

ENCL: 01

SUB CODE: PR

NO REF SOV: 007

OTHER: 001

Card 3/4

LEYKIN, A.S., kand, tekhn, mank

Method of applying paint with the PIRP I device. Shore informable. WHINSM no.15:44-46 162.

Method of determining the wear resistance of lacquered and painted surfaces. Ibid.:54-55

Using emulsion polymer dement as a protective coating for cellular concrete. Ibid.:59-65

(MIRA 18:3)

A CONTROL OF THE CONT	23
SOURCE CODE: UR/0122/66/000/011/0007/0011	
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o (Postor of technical sciences)	
UTHOR: Leykin, A. S. (Doctor of technical sciences)	l
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ABSTRACT: Optimization of stress distribution in the total nonuniformity of the sources of local stress concentration at lowering the local stress concentration of the sources of local stress concentration at lowering the local stress distribution is lowered, by a stress distribution, by disposition of the stress distribution is lowered, by a stress distribution to the stress in the concentration zones, and stress the total nonuniformity of greatest stress in the concentration.	
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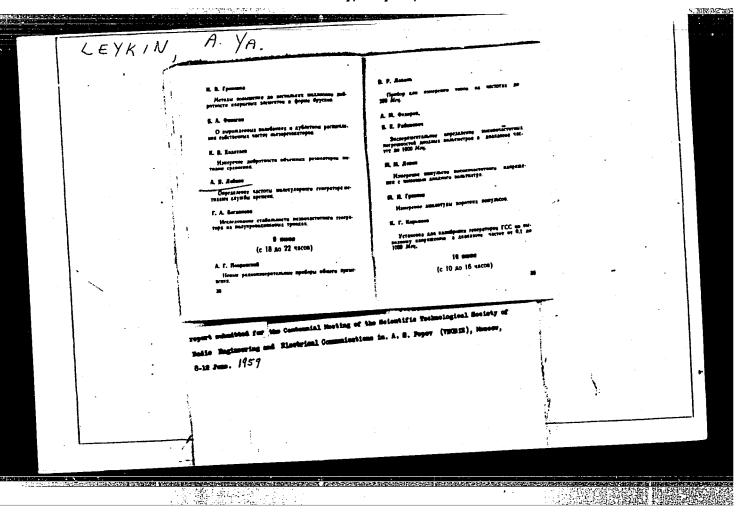
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ERYZZHEV, L.D.; BURDUN, G.D.; LEYKIN, A.Ya.; OKHOTINA, S.M.; SIMKIN, G.S.;
SHPAN'ON, P.A.

Precise determination of the units of time and frequency by means of atomic constants. Ism. tekh. no.3:3-9 My-Je '55.

(Time measurements)

LEYK	,	Referry nauchno-tastedovatel'skikh rabot; sbornik Mo. 2 (Scientific Research Abstracts; Collection of Articles, Nr 2) Moscow, Standartgir, 1958. 139 p. 1,000 copies printed.  Additional Soposoring Agency: USSR. Komitet standartov, mer 1 Immerial'nyth priborov.	Ed.: S. V. Reshetins; Tech. Ed.: W. A. Kondret'reve. FURFORE: These reports are intended for scientists, researchers, and engineers engaged in developing standards, measures, and gages for the Various industries.	COVERAGE: The volume contains 128 reports on standards of managed and and control. The reports were yrapared by scientists of mattrices of the Komite's series with antitutes of the Komite's transactory met i insertiel hydrical properties in the particle paths institute are: Wall's wall was managed by a standards, when the particle paths institute are: Wall's wall was a particle paths institute as a series of the particle paths institute are: Wall's word and was a particle paths institute of the branch of the institute of wastern institute of the relation of this institute of wastern institute of the comitation of this institute in wastern institute of the comitation of this institute in wastern institute of the comitation	Prequency Service  Prequency Service  Artem Year, Ye.V. (VNIPTHI). ISCh-1 and ISCh-2 Type Instruments  (for Integral Comparison of Electric Geolilation Prequencies  (for Integral Comparison of Electric Geolilation Prequency  Verabrut. A.D. and Y.K. Budin [Docessed] (VNIM). Automatic  Verabrut. A.D. and Y.K. Budin [Docessed] (VNIM). Automatic  Tators	Pality_Q.N. (VNIPTRI). Standard Frequency Note: 100 cm. Short-purposes) for Frequency Transmission Through a High-power Short-purposes) for Frequency Transmission Through a High-power Short-grant LD. A.Ys. Leykin, I.V. Baulin, and Ye.Z. Orlow Bryzhey. LD. A.Ys. Leykin, I.V. Baulin, and Ye.Z. Orlow Absorption Lines and Strength Requirements (Dolinakly, Ye.F., Candidate Gradness and Strength Requirements (Dolinakly, Ye.F., Candidate of Technical Soloncos)  Savirsky F.S., and I.A. Zakharov (Sverdlovsk Branch of VNIM), Card 11,77 and I.A. Zakharov (Sverdlovsk Branch of VNIM), Card 11,77 and I.A. Zakharov (Sverdlovsk Branch of VNIM).	by a voltage to 1 microvolt and by the reco



sov/115-59-7-20/33

8(3), 9(3) AUTHOR:

Leykin, A.Ya.

TITLE:

The Experimental Investigation of a Molecular Generator

PERIODICAL:

Izmeritel'naya tekhnika, 1959, Nr 7, pp 41-44 (USSR)

ABSTRACT:

In 1956 and 1957, the Khar'kovskiy gosudarstvennyy institut mer i izmeritel nykh priborov (Khar kov State Institute of Measures and Measuring Instruments) built a number of masers (molocular generators). The results of investigating these masers are presented in this article. In two maser models, developed by N.G. Basov (Ref.1) at FIAN SSSR imeni P.N. Lebedev, several design changes were introduced, while their electrical parameters were kept. A grid with long channels (1.3-1.5 mm at a diameter of 0.05 mm) was used as a beam source. A very even tuning of the resonator was achieved by a system consisting of a thin and thick rod as shown in fig.1. Two generators were mounted in one common vacuum housing as this was done in one of the FIAN masers. The oscillation amplitude was measured by means of a device, whose block diagram is represented in fig.2. Measurements were made concerning oscillation amplitude dependences on the resonator tuning (the ammonia

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SOV/115-59-7-20/33

The Experimental Investigation of a Molecular Generator

pressure in the source was kept equal to p = 2 mm mercury column and the voltage at the quadrupole capacitor U ~ 32 kv), on the ammonia pressure in the beam source (with mean tuning and U  $\simeq$  32 kv) and on the voltage of the quadrupole capacitor (P = 2 mm mercury column. The pressure in the beam source was measured by a U-shaped mercury pressure gage. Frequency changes in the maser under investigation during retuning of its resonator were determined by comparing the frequency difference between two masers. The results of these measurements, presented in fig.3, show that the oscillation amplitude changes as a function of the resonator tuning according to electric load. With an ammonia pressure increase in the beam source, the oscillation amplitude increases and decreases after reaching its peak. Further, the oscillation frequency was investigated by means of a measuring unit as shown in the block diagram, fig.4. The author also investigated the relative stability of maser frequencies. The resonator Q-factor were  $Q_1-8,000$  and  $Q_2-5,000$  respectively. The cooling system was filled with liquid nitrogen one hour prior to the begin of the measurements. Fig.5 a, contains results of frequency change measurements

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SOV/115-59-7-20/33

The Experimental Investigation of a Molecular Generator

of the oscillator with ammonia pressure increasing from 1.5 to 5 mm mercury column. Fig.5 b shows the voltage change at the focusing electrodes from 20 to 30 kv for three fixed tuning ranges. The investigations show that the described maser has a highly constant frequency and good operational qualities. For obtaining the one or other absolute frequency value, the ammonia pressure should be changed for tuning the resonator. The accuracy of reproducing absolute frequency values by a maser using this method, depending on different factors, will be investigated in the future. A.I. Samoilovich participated in design of the maser model. M.I. Klyus joined in assembling the maser. Ye.Z. Orlov assisted in recording the measuring results. There are 4 graphs, 2 block diagrams, 1 diagram and 5 references, 3 of which are Soviet and 2 American.

Card 3/3

SOV/115-59-8-23/33

25(1) AUTHOR:

Leykin, A. Ya.

TITLE:

A System of Comparing the Frequency of a Maser With

a Quartz Standard

PERIODICAL: Izmeritel naya tekhnika, 1959, Nr 8, pp 43 - 44

(USSR)

ABSTRACT:

At the Kharkovskiy gosudarstvennyy institut mer i izmeritel nykh priborov -KhGIMIP- (Khar'kov State Institute of Measures and Measuring Instruments), a special device was designed and built for comparing the maser frequency with the frequency of a highstability quartz generator. The frequency of the quartz reference generator at KhGIMIP is 60 kc. Increasing this frequency to that of the maser (23170 Mc) requires a great frequency multiplication and is connected with considerable difficulties. The author describes the application of an auxiliary quartz generator having a frequency of 3.1 Mc. The author describes this device briefly. Its block diagram is shown in Figure 1. The signal with a frequency of 1.3 Mc from the quartz generator is mixed with the signal of the maser after multiplication by 7,700

Card 1/2

A System of Comparing the Frequency of a Maser With a Quartz

times. By means of the described device comparisons of the maser frequency with the quartz reference getable the author presents the results of one measuring series which were obtained with unchanged tusing of the maser. The table shows that the mean amounts to ~1x10 frequency measurements also the unstability of the quartz reference generation. For simplifying the measuring process and elirator, a second version of the frequency comparison figure 2. It is different from the first version by gain factor of 700 and a mixer. I. V. Baulin built orlow participated in the construction and investigation of the entire comparison system. There is 1 table and 1 block diagram.

Card 2/2

.5/033/60/037/03/020/027 E032/E514

3.9000

Bryzzhev, L.D., Leykin, A.Ya. and Sopel'nikov, M.D.

**AUTHORS:** TITLE:

A Determination of the Frequency of a Molecular Generator and of the Irregularities in the Earth's Rotation

PERIODICAL: Astronomicheskiy zhurnal, 1960, Vol 37, Nr 3,

pp 579-583 (USSR)

The molecular generator employing a beam of ammonia molecules at the Khar'kov State Institute of Measures ABSTRACT:

and Measuring Instruments was described by Leykin in Ref 3. Systematic measurements of the frequency of this generator were begun in February, 1958. Regular comparisons of its frequency in the UT-1 and UT-2 systems of astronomical time were also carried out. The molecular generator in the above standard does not function continuously and is only "switched on" for a

time necessary for the comparison with quartz generators. It was therefore necessary to have continuously running clocks in order to determine the frequency in the

astronomical time system. KKh, clocks were used for this purpose. These clocks are employed by the All-Union

Card 1/3 this purpose.

5/033/60/037/03/020/027 E032/E514

A Determination of the Frequency of a Molecular Generator and of the Irregularities in the Earth's Rotation

Time Service and the All-Union Scientific Research Institute for Physicotechnical and Radiotechnical Measurements who publish monthly corrections to these clocks in the bulletin "Standard Time". Moreover, daily time signals transmitted by the GBZ-10<sup>h</sup> Station (England) are also used in the determination of these corrections. These are further corrected in accordance with the data supplied by the Greenwich Observatory. The frequency of the generator in the KKh, clocks was daily compared with the frequency of the molecular generator. A preliminary value for the frequency of the molecular generator, based on the data supplied by the time services of the Soviet Union and Great Britain, is now reported to be 23 870 129.395 kc/s + 0.012 kc/s. Data on the irregularities in the Earth's rotation in 1958 were obtained from the determination of the Card 2/3 frequency of the molecular generator in astronomical

s/033/60/037/03/020/027 E032/E514

A Determination of the Frequency of a Molecular Generator and of the Irregularities in the Earth's Rotation

systems of time. It was found that the amplitude and phase of seasonal irregularities in the Earth's rotation during 1958 were practically the same as those in 1955-1956. The latter were obtained with the aid of the caesium standard. It is argued that the results obtained show that irregularities in the Earth's rotation can be determined with the aid of the molecular generator to the same accuracy as with the caesium

There are 3 figures and 5 references, 2 of which are Soviet, 1 French and 2 English.

ASSOCIATION: Khar'kovskiy gosudarstvennyy in-t mer i izmeritel'nykh priborov (Khar'kov State Institute of Measures and Measuring Instruments)

SUBMITTED: October 6, 1959

Card 3/3

POLULYAKH, Konstantin Stepanovich: IEYKIN, A.Ya., retsenzent; SKORIK, Ye.T., retsenzent; SHVETCKIY, 3.I., retsenzent; TSARENKO, V.T., otv. red.; TRET'YAKUVA, A.N., red.; ALEKSANDROVA, G.P., tekhn. red.

[Electronic resonance measuring devices] Elektronnye rezonansnye izmeritel'nye pribory. Khar'kov, Izd-vo Khar'kovskogo gos. univ. im.A.M.Gor'kogo, 1961. 138 p. (MIRA 14:12) (Electronic measurements) (Radio measurements)

30159 S/609/61/000/003/008/008 D039/D112

9,2582 (also 1163)

AUTHOR: Leykin, A. Ya

TITLE: A molecular standard of time and frequency

SOURCE: Akademiya nauk Ukrains'koyi RSR. Organizatsionnyy komitet pc

provedeniyu Mezhdunarodnogo geofizicheskogo goda. Mezhdunarodnyy geofizicheskiy god; informatsionnyy byulleten', no. 3, 1961,

82-87

TEXT: The paper describes a molecular standard of time and frequency developed by the Khar'kovskiy gosudarstvennyy institut mer i izmeritel nykh priborov (Khar'kov State Institute of Measures and Measuring Instruments). The basis of this device is a molecular generator, operating on a beam of ammonia molecules which was developed by N. G. Basov and A. M. Prokhorov. The paper also gives the methods of reproducing the frequency of the molecular standard; the first results of comparisons of the frequency of the molecular generator with that of quartz generator No 3 of the Khar'kov State Institute of Measures and Measuring Instruments, which have been regularly conducted since February 5, 1958, and results of determination of the frequency of the molecular generator within the UT-1 and UT-2 astronomic time systems.

V

Card 1/5

30159 \$/609/61/000/003/008/008 D039/D112

A molecular standard of time ...

The electrical parameters of the new molecular generator are the same as those of the molecular generator of the Fizicheskiy institut AN SSSR im. P. N. Lebedeva (Physics Institute of the AS USSR im. P. N. Lebedev) which is mentioned in the paper of N. G. Basov (Ref. 3 "Pribory i tekhnika eksperimenta", t. 1, 1957, s. 71). A grid with long holes, the production technology of which was proposed by A. I. Samoylovich, was used in the beam source. The resonator of the molecular generator has a mechanical two-stage (rough and smooth) tuning system for smooth tuning within a small range. The tuning method was based on the fact that the dependence of the generator's frequency on the ammonia pressure in the molecular bear source is higher by one order than its dependence on the voltage on the quadrupole capacitor. The resoluting power of the tuning method was rated as being of the order of 3 ° 10 ° . As comparison of the molecular generator and the quartz generator was complicated by the great difference in the frequencies of both devices, a comparator with an auxiliary high-stability quartz (enerator, frequency amplifiers and counters, was developed. On the basis of the counter recordings, the value of the quartz generator frequency with respect to the frequency of the molecular generator was found from the formula

Card 2/5

30159 S/609/61/000/003/008/008 D039/D112

A molecular standard of time ...

$$f_{st_d} = \frac{f_{mol\ gen} + F_2 - 700F_1}{238\ 700}$$

where f std is the frequency of the quartz generator of the standard frequency in hundreds of kilocycles: f the frequency of the molecular generator;  $F_1$  and  $F_2$  the beat frequencies. The quartz generator used for comparison with the molecular generator has been operating without interruption since 1950. Its mean quadratic variation per 24 hours is of the order of 6 · 10-10. It is used as the standard clock (KKh3) of the Sluzhba vremeni Sovetskogo Soyuza (Time Service of the Soviet Union). The measurements were conducted with two molecular generators, the mean quadratic deviation of whose difference frequency from the mean deviation was established. Apart from this, the frequency of the quartz generator is determined every day by the reception of time signals transmitted by various stations including the GBR. This makes it possible to determine the frequency of the molecular generator in the same time system in which the signals are transmitted. Since the UT-1 and UT-2 time systems are associated with the speed of the

Card 3/5

A molecular standard of time

30159 \$/609/61/000/003/008/008 D039/D112

Earth's rotation, and since the frequency of the molecular generator is constant and independent from the Earth's rotation, variations in the rotation speed of the Earth can be found by such comparisons. The first results of measuring the molecular generator frequency within the UT-1 and UT-2 systems are given. The results show that in spring 1958 there was no usual decrease in the rotation speed of the Earth, which agrees with the data given in the report of Wm. Markowitz read at the X Astronomical Conference, In conclusion, the author thanks L. D. Bryzzhev for his valuable advice and his participation in the discussion of the results, and Ye. Z. Orlov, A. I. Samoylovich, I. V. Baulin and M. I. Klyus, who helped in the construction of the molecular generator, the development of the comparator and in conducting the comparisons. There are 4 figures and 6 references: 3 Soviet-bloc and 3 non-Soviet-bloc. The three references to English-language publications read as follows: L. Essen, I. V. L. Parry, The Caesium Resonator as a Standard of Frequency and Time, Phil. Trans. Roy. Soc. L., Sec. A, No 973, vol. 250, p. 45, 1957.; L. Essen, I. V. L. Parry, Wm. Markowitz, R. C. Hall, Variation in the Speed of Rotation of the Earth Since June 1955, Nature, vol. 181, p. 1054, 1958.; I. P. Gordon, H. I. Zieger, C. H. Townes, The Maser - New Type

Card 4/5

5/169/62/000/002/001/072 D228/D301

AUTHORS: Sopel'nikov, M. D., Leykin, A. Ya. and Bryzzhev, L. D.

TITLE: Determining the irregularity of the earth's rotation by means of a molecular time and frequency standard

PERIODICAL: Referativnyy zhurnal, Geofizika, no. 2, 1962, 3, abstract 2A1 (Mezhdunar. geofiz. god, Inform. byul.,

no. 4, 1961, 29-32)

TEXT: The results are described for determining the irregularity of the earth's rotation by means of a molecular generator, introduced into the time and frequency work of the Khar'kovskiy gosudarstvennyy institut mer i izmeritel'nykh priborov (Khar'kov State Institute of Measures and Measuring Instruments) from February 1958. The magnitude of the irregular and seasonal changes in the length of a day is cited, and corrections are given for the transition from UT-1 time to UT-2 time for the interval March 1958 -March 1959. / Abstracter's note: Complete translation. /

Card 1/1

CIA-RDP86-00513R0009297200 APPROVED FOR RELEASE: Monday, July 31, 2000

S/115/63/000/002/005/008 E202/E492

AUTHORS:

Leykin, A.Ya., Orlov, Ye.Z.

TITLE:

Coincidence of frequency values in molecular

generators of similar constructions

PERIODICAL: Izmeritel'naya tekhnika, no.2, 1963, 46-48

The authors used four identically constructed molecular generators contained in pairs in one general vacuum shell. aggregate was supplied with electronic equipment which tuned the frequency of the generator according to the minimum changes in the pressure of ammonia in the source of the molecular beam and compared this molecular frequency with that of quartz generators. The pressure of Details of preliminary tuning are given. ammonia was so chosen that the amplitude of generation was at its maximum. In order to determine the effect of the voltage on the quadrupole condenser, the beat frequency was measured between the two molecular generators. At the same time the voltage on the quadrupole condenser of one generator was fixed at 35 kV, while that of the other varied from 22 to 37 kV. The measurements have shown that changes in voltage of 15 kV cause frequency changes of Simultaneous frequency measurements on the standard 70 c/s.

Coincidence of frequency ...

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quartz generator and the molecular generators were carried out for a period of three weeks; each molecular generator was tuned and the difference between the standard and molecular generators measured. Approximately 10 to 12 measurements were taken on each of the molecular generators. The results of these measurements show that the mean arithmetic deviation of frequencies of the individual generators was of the order of about 0.1 while the mean quadratic deviation was of the order of  $1 \times 10^{-9}$ . It was concluded that using this method of tuning, it is possible to attain a frequency with a mean quadratic error of  $1 \times 10^{-9}$ . It is stated that when subjected to the above procedure, molecular generators may be operating with the same frequency accuracy as that which is ascribed to the standard generator. There are 5 tables.

Card 2/2

VALITOV, R.A. Prinimali uchastiys: LEYKIN. A.Ya.; SIDORENKO, B.C.;
KUKOLEVA, T.V., red.; BEDIRIDIT, V..., tekhn. red.

[Radio-engineering measurements] Radiotekhnicheskie izmerenia. Moskva, Sovetskoe radio, 1963. 631 p.

(Radio measurements)

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BENDERSKIY, S.N., kand.tekhn. nauk; BURSIAN, V.R., prof., kand.

tekhn. nauk; VASIL'YEV, P.N., inzh.; DORFMAN, E.Ye., inzh.;

ZHURAVLEV, V.F., kand. tekhn. nauk; KESTEL'MAN, V.N.,

inzh.; KRUGLOV, A.N., dots., kand. tekhn. nauk; KUKIBNYY,

A.A., dots., kand.tekhn. nauk; LEVACHEV, N.A., dots., kand.

tekhn. nauk; LEYKIN, A.Ya., inzh.; NAREMSKIY, N.K., dots.,

kand. tekhn. nauk; PLATONOV, P.N., prof., doktor tekhn.

nauk; SOKOLOV, A.Ya., prof., doktor tekhn. nauk; KUTSENKO,

K.I., kand. tekhn. nauk, dots., retsenzent; VEREMEYENKO,

Ye.I., inzh., retsenzent; KOVTUN, A.P., inzh., retsenzent;

SEMENYUK, A.I., retsenzent; KASHCHEYEV, I.P., inzh.,

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[Conveying and reloading machinery for the overall mechanization of the food industries] Transportiruiushchie i peregruzochnye mashiny dlia kompleksnoi mekhanizatsii pishchevykh proizvodstv. Moskva, Pishchevaia promyshlennost¹, 1964.
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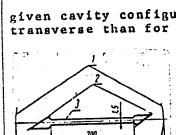
4. Zaveduyushchiy laboratoriyey Vsesoyuznogo nauchno-issledovatel'skogo instituta zerna i produktov ego pererabotki (for Pal'tsev).

IVANOV, A.I.; LEYKIN, A.Ya.; KHUVES, E.S.; CHERNYY, M.S.; KLEYMAN, L.M., red.

[Machines for overall mechanization of grain loading and unloading operations] Mashiny dlia kompleksnoi mekhanizatsii pogruzochno-razgruzochnykh rabot s zernom. Moskva, Kolos, 1964. 230 p. (MIRA 18:9)

EWI(1)/EEC(k)=2/T/EWP(k)IJP(c) UR/0115/66/000/009/0028/0030 SOURCE CODE: AP6032005 Leykin, A. Ya.; Samoylovich, A. I.; Solov'yev, V. S. AUTHOR: ORG: none TITLE: A stable cw gas laser 15 SOURCE: Izmeritel'naya tekhnika, no. 9, 1966, 28-30 TOPIC TAGS: cw laser, gas laser, methology ABSTRACT: A stable, single-frequency, dc-excited He-Ne laser has been developed by the Kharkov Institute of Measures and Measuring Instruments for use in metrology. Because of the required single-frequency characteristic, the amplifying medium is designed to damp both higher-order oscillations and extraneous longitudinal modes; emission is confined to the  $\text{TEM}_{q\,0\,0}$  type of oscillations. This provides for a minimum of 4-5 axial modes being generated simultaneously within the Doppler width of the 3s2-2p4 line. The damping of all the longitudinal modes except those at line center is accomplished by specifying losses which are introduced into the resonator cavity by various elements. The resonator cavity (Fig. 1) contains a small-diameter capillary (1.5 mm) for the Card 1/3 UDC: 621.375.9

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given cavity configuration which insures losses ten times higher for transverse than for basic oscillations. The 300-mm discharge gap

Fig. 1. Resonator cavity configuration

1 - Mirrors; 2 - Brewster windows; 3 - capillary.

insures emission conditions for only one longitudinal type of oscillations at the given gain of 12%-13% and a pumping level only slightly exceeding threshold. The resonator cavity is formed by spherical mirrors with dimensions  $R_1=R_2=580$  mm. A stable output power of

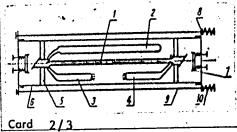
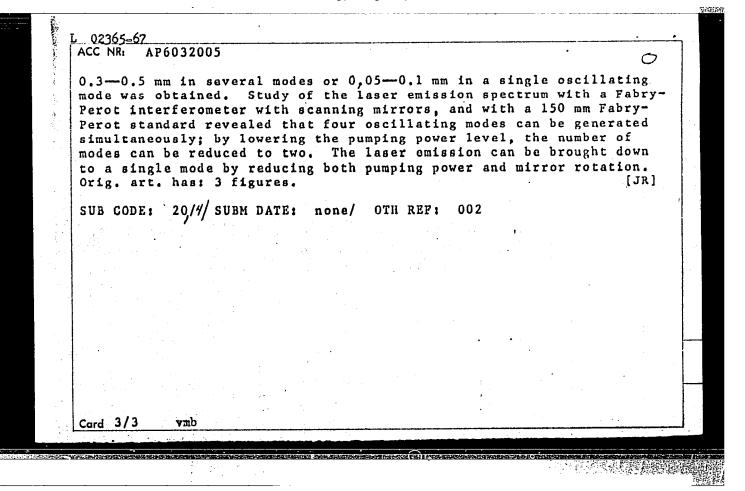


Fig. 2. Laser configuration

1 - Discharge tube; 2 - reserve tube; 3 and 4 - cathode and anode tubes; 5 - holders; 6 - quartz tube; 7 - mirror holders; 8 - end flanges; 9 - steel couplers; 10 - springs

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MAIYUGIN, V.N., red.; MASLOV, N.A., red. [deceased]; USPENSKIY, V.V.,

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