

GUTKIN, B.

Economic efficiency is the main criterion. Avt.transp. 43
no.11:8-10 N '65. (MIRA 18:12)

1. Direktor 5-y avtobazy Mostorgtransa.

LOMACHENKOV, S.Ye., inzh.; GUTKIN, B.G., kand. tekhn. nauk; SHAGURIN, K.A., otv. red.; ACHKINADZE, Sh.D., inzh., red.; KRASLAVSKIY, G.M., tekhn. red.

[Portable electric spark systems; work of the Research Branch of the State Planning Institute of the Ministry of Transportation Machinery Manufacture] Perenosnye elektroiskrovye ustanovki; opyt raboty NIF GPI MTrM. Leningrad, 1952, 11 p. (Informatsionno-tekhnicheskii listok, no.23(36.)) (MIRA 14:7)

1. Leningradskiy dom nauchno-tekhnicheskoy propagandy. 2. Glavnyy inzhener Leningradskogo doma nauchno-tekhnicheskoy propagandy (for Shagurin) (Metals--Hardening) (Electric apparatus and appliances)

GUTKIN, B.G.; VISHNITSKIY, A.L.; GUSEV, V.N., laureat Stalinskoy premii, redaktor.

[Control systems for electric spark and electrolytic-mechanical tools] Regulirovaniye rezhima raboty elektroiskrovyykh i anodno-mekhanicheskikh stankov. Pod red. laureata Stalinskikh premii V.N.Guseva. Moskva, Gos. nauchno-tekhn. izd-vo mashinostroit. lit-ry, 1952. 41 p.

(MLRA 6:8)

(Electric controllers)

GUTKIN, B.G.

SOV/1404

25(1)

PHASE I BOOK EXPLOITATION

Levinson, Ye. M., B. G. Gutkin, A. P. Dyatchenko, and Ye. I. Vladimirov

Polucheniye polostey i otverstii v metalle elektroskrovym sposobom (Electrospark Method of Cutting Cavities and Holes in Metals) Moscow, Mashgis, 1952. 95 p. (Series: Bibliotekha elektrotehnologa, No. 4) 6,000 copies printed.

Ed. (Title page): Gusev, V. N., Laureate of the Stalin Prize, Engineer; Ed. (Inside book): Popilov, L. Ya., Engineer; Tech. Ed.: Sakoleva, L. V.; Managing Ed. for Literature on Machine-Building Technology (Leningrad Division, Mashgis): Nikitin, P. S., Engineer.

PURPOSE: This booklet is intended for technologists working in the field of electrical metalworking processes and for skilled workers.

COVERAGE: The booklet presents basic principles of the electrospark machining of holes and cavities in metals. Information on electrospark equipment is given and some examples of the applications of electrospark machining methods are presented. The following personalities were awarded Stalin prizes for their contributions to the development of electromachining methods: B. R. Lazarenko, N. I. Lazarenko, and V. N. Gusev. For the purpose of introducing and promoting electromachining methods, the Leningrad branch of Mashgis (State Scientific

Card 1/3

3

PHASE I BOOK EXPLOITATION 938

Gutkin, B.G., Candidate of Technical Sciences

Avtomatizatsiya elektroiskrovykh i anodno-mekhanicheskikh stankov
(Automation of Electrospark Electrolytic Machine Tools) Moscow,
Mashgiz, 1952. 226 p. 8,000 copies printed.

Reviewers: Gusev, V.N., Engineer, Laureate of the Stalin Prize, and
Levinson, Ye.M., Engineer.; Ed.: Lomachenkov, S.Ye., Engineer;
Tech. Ed.: Pol'skaya. R.G.; Managing Ed. for literature on the
technology of machine building (Leningrad Division, Mashgiz):
Nikitin, F.S., Engineer.

PURPOSE: This book is intended for engineers and technicians working
in the field of electromachining of metals, and for students of
vuzes and tekhnikums.

COVERAGE: The book deals with various problems of automatic control
of electrospark and electrolytic machine tools. Devices used for
automatic control of various processes, safety devices, and design
features of automatic electrospark and electrolytic machine tools

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Automation of Electrosark Electrolytic Machine Tools 938
are described. No personalities are mentioned. There are
13 Soviet references.

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Card 2/5

GUTKIN B. G.

Regeleinrichtungen Fur Elektrofundenund Anodenmechanische Werkzeugmaschinen. Von B.G. Gutkin Und GUTKIN, B. G. Be lin, Technik, 1954.

43 P. Diagr., Table.

Translation From The Russian, Regulyatory Reshima Raboty Elektroiskovykh I Anodnomekhani Cheskich Stankov, Leningrad (N. D.)

SO: N/5
663.5
.G9

GUTKIN, B.G.

Apparatus for automatic control of the current density in
an electroplating bath. B. G. Gutkin. U.S.S.R. 107,050.
Aug. 25, 1957. The wiring and auxiliary instrument for
automatic control of c.d. are described. M. Hirsch.

2

JR

GUTKIN, B.G.

LIVSHITS, A.L. kandidat tekhnicheskikh nauk; GUTKIN, B.G., kandidat tekhnicheskikh nauk, retsenzent; UVAROVA, A.F., tekhnicheskii redaktor.

[Electric erosion treatment of metals] Elektroeroziionnaia obrabotka metallov. Moskva, Gos.nauchno-tekhn.izd-vo, mashinostroit. lit-ry, 1957. 117 p. (MLRA 10:6)
(Metal cutting) (Metals--Hardening)

BOGORAD, Lev Yakovlevich; GUTKIN, Ben'yamin Girshevich; SHOBİK, L.Ye.,
inzh., ved. red.; SHREYDER, A.V., kand. tekhn.nauk, red.;
PAUTIN, N.V., inzh., red.; SOROKINA, T.M., tekhn. red.

[Wear resistant chromizing with periodic current reversal] Iz-
nosostoikoe khromirovanie pri periodicheskom izmenenii naprav-
leniia toka. Moskva, Filial Vses. in-ta nauchn. i tekhn. in-
formatsii, 1958. 23 p. (Peredovoi nauchno-tekhnicheskii i
proizvodstvennyi opyt. Tema 13. No.M-58-245/25) (MIRA 16:3)
(Chromium plating)

GRISHIN, Valerian Maksimovich, inzh.; GUTKIN, Ben'yamin Girshevich, kand. tekhn. nauk; LIVSHITS, Abram Lazarevich, kand. tekhn. nauk; YAKHIMOVICH, Dmitriy Fedorovich, inzh.; BRYANTSEVA, V.P., inzh., red.; SOROKINA, T.M., tekhn. red.

[Dimensional electric spark machining of metals] Razmernaia elektroerozionnaia obrabotka metallov. Moskva, Filial Vses. in-ta nauchn. i tekhn.informatsii, 1958. 88 p. (Peredovoi nauchno-tekhnicheskii i proizvodstvennyi opyt. Tema 8. No.M-58-6/1) (MIRA 16:2)

(Electric metal cutting)

POPILOV, Lev Yakovlevich, LEVINSON, Yevgeniy Maksimovich,; GUTKIN, B.G.,
kand. tekhn. nauk, retsenzent,; KOSMACHEV, I.G., inzh., red.;
BORODULINA, I.A., red. izd-va,; LEYKINA, T.L., red. izd-va.

[Electric metal-machining processes; a survey of foreign
technology] Elektricheskie metody obrabotki metallov; obzor
zarubezhnoi tekhniki. Moskva, Gos. nauchno-tekhn. izd-vo
mashinostroit. lit-ry, 1958. 145 p. (MIRA 11:11)
(Electric cutting machinery)

GUTKIN, B.G.; PODLAZOV, S.S.; YEVSEYEV, V.V.

"Spark-erosion machining of metals" by A.L. Livshits. Reviewed by
B.G.Gutkin, S.S. Podlazov, V.V. Evseev. Stan. i instr. 29 no.10:
44-45 0 '58. (MIRA 11:11)

1. Nachal'nik sektora elektroobrabotki metallov Leningradskogo
filiala Vsesoyuznogo teplotekhnicheskogo instituta im. F. Dzerzhinskogo
(for Gutkin). 2. Nachal'nik osobogo konstruktorakogo byuro Eksperi-
mental'nogo nauchno-issledovatel'skogo instituta metallorazhushchikh
stankov (for Podlazov). 3. Starshiy inzhener laboratorii rezaniya
Leningradskogo Kirovskogo zavoda (for Yevseyev).
(Electric metal cutting)
(Livshits, A.L.)

GUTKIN, Ben'yamin Girshevich; GRIGORCHUK, Igor' Petrovich; POPILOV, L.Ya.,
red.; VARKOVETSKAYA, A.I., red.izd-va; SPERANSKAYA, O.V., tekhn.red.

[Electric spark machining of metals] Elektrokontaktnaia obrabotka
metallov. Pod obshchei red. L.IA.Popilova. Moskva, Gos.nauchno-
tekhn.izd-vo mashinostroit.lit-ry, 1960. 46 p. (Bibliotekha
elektrotekhnologa i ul'trazvukovika, no.5). (MIRA 14:6)
(Electric metal cutting)

PHASE I BOOK EXPLOITATION: SOV/3901

Novoye v elektricheskoy i ultrazvukovoy obrabotke materialov (New Developments in Electrical and Ultrasonic Machining of Materials) [Leningrad], Lenizdat, 1959. 261 p. 5,000 copies printed.

Ed. (title page). L.Ya. Popilov, Ed. (inside book): S.I. Borshchevskaya; Tech. Ed.: P.S. Sharmov.

PURPOSE: This book is intended for technical personnel and production workers.

CONTENTS: This is a collection of 20 articles presented at the Third All-Union Conference of the Scientific and Technical Society of the Machine Industry on Electrical and Ultrasonic Machining of Metals, held in Leningrad. The articles deal with the latest achievements in the field of electrical and ultrasonic machining of metals. New methods of machining presently being developed are described. References follow several of the articles.

Livshits, A.L., S.S. Podlazarov, A.I. Travers, and A.I. Anonov. Some Problems in the Technology and Design of Machines for Electroerosion Machining of Metals 87

Rozhnov, I.S. Electric-Pulse Generators of Unipolar Pulses for Electroerosion Machining of Metals 109

Mashukhin, L.Ya. Electrical-Pulse Machining of Forging-Die Grooves 115

Ryabinok, A.O. Intensity of Metal Removal and Surface Quality in Electrolytic Machining of Carburized 134

Dikushin, G.A. Selection of Process Regimes in Electrolytic Gear-Machining 145

Getkin, B.O. Electric-Resistance Machining of Metals 151

Yanogorodskiy, I.Z. New Uses of Heating in Electrolytes 157

Mikhaylov V.A. Cleaning and Degreasing of Parts and Intensification of Electroplating with the Aid of Ultrasonics 174

Gorshchakov, M.S. Technique of Ultrasonic Machining of Carbide Dies 183

Ustinov, V.V. Production of Magnetostrictive Transducers for Ultrasonic Machines for Machining Carburized 199

Mezhovskiy, B.N. Ultrasonic Machining of Parts Made of Ceramic Materials 203

Mondrus, D.B. Ultrasonic Units Developed by OES KTO 211

Kumbol'dt, M.N. Spot Welding with the Use of Ultrasonics 235

Rabizov, O.I., and B.Ya. Mikhailov. Methods of Ultrasonic Analysis and Inspection 244

AVAILABLE: Library of Congress (CJ 1191 .P 63)

Card 3/3
VK 74/76
8-12-80

GUTKIN, B.G.

The EAK automatic electric spark machine for stamping parts. Biul.
tekhn.-ekon.inform. no.7:48-49 '61. (MIRA 14:8)
(Marking devices)

GUTKIN, Ben'yamin Girshevich, kand. tekhn. nauk; FYATISOTNIKOV, A.I.,
red.; FREGER, D.P., red. izd-va; GVIRTS, V.L., tekhn. red.

[The ERM semiautomatic electric-spark cutting machine for
machining the cone of atomizers]Elektroiskrovoi poluavtomat
ERM dlia obrabotki konusa raspylitelei. Leningrad, 1962. 13 p.
(Leningradskii dom nauchno-tekhnicheskoi propagandy. Obmen pe-
redovym opytom. Seriya: Elektricheskie metody obrabotki mate-
rialov, no.4) (MIRA 15:8)

(Electric cutting machinery)

38710
S/193/62/000/006/002/002
A004/A101

1.1110

AUTHOR: Gutkin, B. G. Candidate of Technical Sciences

TITLE: 3PM (ERM) electrospark semi-automatic for machining the working cone of sprayers

PERIODICAL: Byulleten' tekhniko-ekonomicheskoy informatsii, no. 6, 1962, 31 - 35

TEXT: The author reports on the ERM electrospark semi-automatic which has been developed at a plant (Abstracter's note: no name given) and is intended for the electrospark grinding and lapping of working cones of sprayers and nozzle holders of diesel engines. He presents a functional diagram of the machine and gives a description of its operation. The workpiece is rotated by a belt-drive. A characteristic feature of the electric diagram of the semi-automatic is the utilization of a special programming device characterized by simplicity and dependability. The author describes in detail the electric system of the machine and its units and presents the following technical data: input power, w = 300; (maximum) electrode voltage, v = 110; (maximum) current between electrodes, amp = 0.9; (maximum) capacitance between electrodes, f = 2; (maximum) deposition depth of

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ERM (ERM) electrospark....

S/193/62/000/006/002/002
A001/A101

the sprayer working cone, mm - 60; angle of taper of the working cone - up to 90°; electrode tool diameter, mm - 1-2; electric motors; electrode tool feed motor - MH-250 (MN-250); main drive motor - ~~207~~ - 11/2 (AcL-11/2); machining cycle on each condition, sec. - from 2 to 120; total machining time, min - from 1 to 6; class of surface finish after machining (according to GOST 2789-51) - 8; machining accuracy (maximum permissible play of the sprayer working cone relative to the fitting office for the needle) μ - 5; overall dimensions, mm - 540 x 420 x 1,490; weight, kg - 200. The working fluid in which the electrospark machining takes place consists of transformer oil (50%) and lighting kerosene (50%). During two-shift work a section of 10 ERM machines will set free 48 workers and save 27,600 rubles annually. There are 2 figures.

Card 2/2

GUTKIN, B.M.

Machine for the production of sanitary tissues. Bum. prom. 38
no.li:29 N '63.

Roller felt dryers instead of drying cylinders. Ibid.:29
(MIRA 17:1)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tsellyulozno-
bumazhnoy promyshlennosti.

YEFANOV, A.G., inzhener; GUTKIN, B.M., kandidat tekhnicheskikh nauk;
REYNGOL'D, Yu.B.

Use of magnetic amplifiers in electric drives. Elektrichestvo
no.2:9-14 F '56. (MLRA 9:5)

1. TsKB "Elektroprivod" Ministerstvo elektropromyshlennosti.
(Magnetic amplifiers) (Electric driving)

БУКИН, Б. М.
BUKIN, B. M.

"A Control Apparatus With Thyatron Rectifiers," pp 76-86, 111

Abst: The article examines the circuits and control apparatus developed by the TsKB (Central Design Bureau) 'Elektroprivod,' and testing in experimental-production installations of rectified current drive in 1954-1956.

SOURCE: Raboty MER SSSR po Mekhan. i Avtomatizatsii Narodn. Khoz. (Work of the Ministry of the Electrical Engineering Industry USSR on Mechanization and Automation in the National Economy), Part 3, Moscow, TsBTI, 1956

Sum 1854

ETTINGER, Ye.L., kandidat tekhnicheskikh nauk; ~~WOTKIN, B.M.~~ kandidat tekhnicheskikh nauk; Borodavchenko, P.M., inzhener.

Present-day systems of rectifier drives. Elektrichestvo no.9:
32-38 S '56. (MLRA 9:11)

1. Tsentral'noye konstruktorskoye byuro "Elektroprivod" Ministerstva elektropromyshlennosti.
(Mercury-arc rectifiers)

GUTKIN, B.M., kandidat tekhnicheskikh nauk; ETTINGER, Ye.L., kandidat tekhnicheskikh nauk.

Peak choke for regulating electronic instruments. Vest.elektroprom.
27 no.1:26-32 Ja '56. (MIRA 9:6)
(Electronic apparatus and appliances)(Electric controllers)

ETTINGER, Ye.L., kandidat tekhnicheskikh nauk; ~~GUTKIN, B.M., kandidat tekhnicheskikh nauk;~~ BORODAVCHENKO, P.M.

Modern arrangements of rectifier electric drives. Elektrichestvo
no.1:60-66 Ja '57. (MLRA 10:2)

1. Tsentral'noye knstruktorskoye byuro "Elektroprivod" Ministerstva
elektropromyshlennosti.
(Electric driving)

GUTKIN, E.M., kand.tekhn.nauk

D.C. drive with ionic excitation. Elektrichestvo no.11:14-22
N '61. (MIRA 14:11)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut elektromekhaniki.
(Electric driving)

GUTKIN, Boris Mironovich; SILAYEV, E.F., red.

[Direct current drives with ignitrons] Ionnyi privod
postoiannogo toka. Moskva, Energiia, 1965. 455 p.
(MIRA 18:7)

Методы анализа устойчивости работы автономных инверторов

Study of steady periodic modes of an autonomous inverter.
Электротехника 36 no.8:31-37 Ag 1965. (MIRA 1969)

GUTKIN, E.

USSR/ Miscellaneous

Card 1/1 Pub. 89 - 28/28

Authors : Klyukachev, V.; Gol'dreer, I.; Roginskiy, V.; Piltakyan, A.; and
 Gutkin, E.

Title : Exchange of experiments

Periodical : Radio 4, pages 48, 53, and 63, Apr 1955

Abstract : The following subjects and items are briefly discussed and described: A two-voltage rectifier used for rectification of the 300-320 and 130-150 volt plate circuits in a cathode-ray tube; electronic compensators for stabilizing power feeds; the use of the 6ZhZP pentode as an amplifier; the semi-duplex operation during amateur radio communications; and the contest of amateur radio clubs in establishing radio communication with Experimental Arctic Stations No. 3, and No. 4. Circuit diagrams; graphs; tables.

Institution :

Submitted :

AID P - 4330

Subject : USSR/Radio
Card 1/1 Pub. 89 - 4/14
Author : Gutkin, E. (UB5TsE)
Title : KV and UKV Transmitter
Periodical : Radio, 1, 26-29, Ja 1956
Abstract : The design and performance of this transmitter as used in telegraph and telephone operations at the radio station UB5TsE are described in detail. The standardized parts of the equipment are referred to by types. A table gives data on the wires used. Two figures illustrate the layout and mounting of the transmitter.
Institution : None
Submitted : No date

GUTKIN, E.I.

Eliminating antenna "doubling" in the television transmitter. Tekh.
kino i telev. 4 no.4:67-70 Ap '60. (MIRA 13:9)

1..Luganskiy televizionnyy tsentr.
(Television--Transmitters and transmission)

GUTKIN, E.I., inzh.; YESHCHENKO, A.T., inzh.; STRATINEVSKIY, N.I., inzh.

Increase in the power of the TRSA-56 relay transmitter. Vest. svyazi 23
no.1:15-17 Ja '63. (MIRA 16:3)

(Radio relay systems)

GUTKIN, E.I.

Improvement of UI-1C preamplifiers. Vest. svyazi 24 no.3:10-11
Mr '64. (MIRA 17:4)

1. Starshyy inzhener Luganskogo televizionnogo tsentra.

GUTKIN, G.M., inzhener.

Developing a more efficient design for weak-current ship cables.
Sudostroenie 22 no.8:13-14 Ag '56. (MLRA 9:10)

(Electric cables) (Electricity on ships)

GUTKIN, I.; KROL', A.

Schools of culture in the mechanization schools. Prof.-tekh.
obr. 18 no.8:20-21 Ag '61. (MIRA 14:9)
(Student activities)

MARKIN, V. F., kand. tekhn. nauk; ~~CHIKIN, I. I., inzh.~~; EGSTUE, A. G.,
kand. tekhn. nauk; SHIPRIN, Ye. L., inzh.

Effect of unsettled heat exchange on the regulation process
of gas turbine systems. Teploenergetika 10 no.3:38-42 Mr '63.
(MIRA 16:4)

1. Moskovskiy energeticheskiy institut i zavod "Ekonomayzer".

(Gas turbines)

GUTKIN, I.I.

USSR/Nuclear Physics - Structure and Properties of Nuclei.

C-4

Abs Jour : Ref Zhur - Fizika, No 1, 1958, 452

Author : Demirkhanov, R.A., Gutkin, I.I., Dorokhov, V.V.
Inst : -
Title : Mass of the Isotope He³.

Orig Pub : Atomn. energiya, 1957, 2, No 5, 469-470

Abstract : A mass-spectroscopic determination was made of the mass of the isotope He³, in a mixture of helium isotopes enriched with He³ to 99.5%, using a setup previously described (Referat Zhur Fizika, 1957, No 4, 8706). The mass was measured in the doublets H³ -- He³ and HD³ -- He³. The results of the measurements were checked against the HD -- H³ doublet. The mass scale was calibrated against the spectrum N¹⁴ H -- N¹⁴ H₂ -- N¹⁴ H₃. The value obtained for the mass of He³ is 3.016970 ± 2 atomic units of mass. The data of this

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USSR/Nuclear Physics - Structure and Properties of Nuclei.

Abs Jour : Ref Zhur - Fizika, No 1, 1958, 452

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work were used to calculate the energy values for the reaction $D(d,n) He^3$, $D(p, \gamma) He^3$, and $He(d,p) He^4$, which equal 3.275 ± 0.004 , 5.501 ± 0.003 , and 18.336 ± 0.005 Mev respectively.

Card 2/2

GUTKIN, I.A., inzh.; SHIFRIN, Ye.L., inzh.; GOL'DZAND, L.D., inzh.;
KIRAKOSYANTS, G.A., kand.tekhn.nauk.

Hydraulic system of control and protection of the OSPT-1150 turbine
pump. Energomashinostroenie 9 no.9:11-14 S '63. (MIRA 16:10)

S/096/63/000/003/006/010
E194/E455

AUTHORS: Markin, V.F., Candidate of Technical Sciences,
Gutkin, I.A., Engineer, Kostyuk, A.G., Candidate of Technical
Sciences, Shifrin, Ye.L., Engineer

TITLE: The influence of transient heat-exchange on the
process of regulating gas-turbine sets

PERIODICAL: Teploenergetika, no.3, 1963, 38-42

TEXT: In governing a gas turbine it is not the amount of gas
flow which is regulated (as is the case in a steam turbine) but
the amount of heat applied to the flow. Under steady-state
conditions a steady temperature distribution is achieved between
the various parts of the gas duct and the gas flowing through it.
However, under transient conditions, the gas duct may either give
up heat to the gas or extract heat from it, thus temporarily
modifying the influence of the regulator. This effect can be of
considerable practical significance. The differential equation
for a gas-turbine regenerator is derived in the form

$$\frac{d\theta}{dz} = \frac{\mu}{\tau_{\mu}} + \frac{\theta}{\tau_{\theta}} + \frac{\nu}{\tau_{\nu}} + \frac{p}{\tau_p} \quad (8)$$

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The influence of transient ...

where $\theta = \Delta T_e / T_{e0}$; $\mu = \Delta B / B_0$; $\nu = \Delta G / G_0$; $\rho = \Delta \epsilon / \epsilon_0$;
 T_e - air temperature beyond regenerator, °K; B - rate of fuel
consumption; G - rate of air consumption, ϵ - compression ratio.
This equation was used to calculate the effect when a turbine
picks up load and it is shown that because of transient cooling in
the regenerator the temporary loss of output is greater than it
otherwise would be. The problem cannot be overcome by increasing
the regulator speed but a solution may be achieved by temporary
over-regulation. The device used by the "Ekonomayzer" Works to
achieve such temporary over-regulation of a gas turbine type
ГТУ-6 (GTU-6) is then described. In basic principle there is
only one fuel-control valve, which over-travels in the first
stage of the transient process and gradually returns to the
correct setting. Two servo-motors are used in the regulator.
Comparative test results on a gas turbine type GTU-6 with the
normal regulator and with this special one are quoted for cases
of picking up and throwing off 100% load. There is a
substantial improvement in performance with the new regulator.
The use of temporary over-regulation avoids the need to alter the
Card 2/3

The influence of transient ...

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E194/E455

static characteristics of the regulation system; perfection has not yet been achieved but further improvement is possible. It should be noted that a regenerator does not always distort the transient process, but only in such cases when at different loads the temperature gradient between the regenerator wall and gas changes markedly. The greatest change occurs in gas turbines in which a compressor of flat characteristic runs at approximately constant speed. The main criterion in assessing the probable influence of the regenerator on the transient process is the gas temperature beyond the turbine. The more this changes on change of load the greater the influence of the regenerator on the transient process. There are 5 figures.

ASSOCIATION: Moskovskiy energeticheskiy institut - zavod
"Ekonomayzer" (Moscow Power Engineering Institute -
"Ekonomayzer" Works)

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GUTKIN, I.N.

C-4

USSR/Nuclear Physics - Structure and Properties of Nuclei

Abs Jour : Ref Zhur - Fizika, No 1, 1958, 453

Author : Demirkhanov, R.A., Gutkin, I.N., Dorokhov, V.V.

Inst : -

Title : Masses of the Isotopes C^{13} , N^{14} , and N^{15} .

Orig Pub : Atomm. energiya, 1957, 2, No 6, 544-551

Abstract : Results are reported on new mass-spectrographic measurements of the masses of C^{13} , N^{14} , and N^{15} . It is shown that there exists "an internal agreement" for the values of the masses of these isotopes, obtained from various systems of doublets. The measurements were performed under conditions that exclude the systematic errors. A procedure is given for a precision adjustment of the ion-optical system. For the masses of C^{13} , N^{14} , and N^{15} , the values obtained were $13.007491 \pm 3 \times 10^{-6}$, $14.007527 \pm 4 \times 10^{-6}$ and $15.004890 \pm 5 \times 10^{-6}$ atomic units of mass respectively, which is in good agreement with the values

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USSR/Nuclear Physics - Structure and Properties of Nuclei.

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Abs Jour : Ref Zhur - Fizika, No 1, 1958, 453

published in recent times by Nier and his associates. These data are high compared with the average values, obtained from nuclear reactions as the result of a statistical analysis. The discrepancy in these values is attributed to the inaccuracy of the measurement of the values of Q , used to calculate the masses of

${}^1_0\text{H}$, D , He^4 , and C^{12} , as well as of the isotopes C^{13} , N^{14} , and N^{15} .

Card 2/2

GUTKIN, I.V.

Introducing the 2V460 jig-boring machine. Biul.tekh.-ekon.
inform.Gos.nauch.-issl.inst.nauch.i tekhn.inform. 18
no.11:25-26 N '65. (MIRA 18:12)

GUTKIN, I. Ye.

Impact extrusion of steering knuckles for GAZ-63 automobiles.
Kuz.-shtam. proizv. no.4:15-18 Ap '61. (MIRA 14:3)
(Extrusion(Metals))
(Automobiles—Steering gear)

GUTKIN, K.A., kand.med.nauk, zaslyzhennyy vrach respubliky.
SAMSONOV, V.A., kand.med.nauk (Petrozavodsk)

Giant mixed tumor (fibromyoma in a cystoma) of the round ligament of
the uterus. Akush. i gin. 34 no.4:102-103 JI-Ag '58 (MIRA 11:9)

1. Iz ginekologicheskogo i patologoanatomicheskogo otdeleniy
Respublikanskoy bol'nitsy (glavnyy vrach L.T. Filimonova) Ministerstva
zdravookhraneniya i sotsial'nogo obespecheniya Kazakhskoy ASSR.

(PELVIC SUPPORTING STRUCTURES, neoplasms
mesothelioma of round ligament (Rus))

(MESOTHELIOMA, case reports
round ligament (Rus))

KORIN, D. L., kand. med. nauk; SMOLIN, V. V.; GUTKIN, Kh. G.

Injury of the ureters and kidneys in retrograde pyelography.
Urologia no.3:11-14 '61. (MIRA 14:12)

1. Iz gospi'tal'noy khirurgicheskoy kliniki (zav. - prof. G. D. Obraztsov) i fakul'tetskoy khirurgicheskoy kliniki (zav. - prof. I. D. Korabel'nikov) Chelyabinskogo meditsinskogo instituta.

(KIDNEYS--RADIOGRAPHY)
(KIDNEYS--WOUNDS AND INJURIES)
(URETERS--WOUNDS AND INJURIES)

GUTKIN, Kh.G.; KUZNETSOV, V.I.

Total substitution of the ureter with a segment of the small intestine. Urologia no.6:58-59'62. (MIRA 16:7)

1. Iz khirurgicheskogo otdeleniya (zav. V.I.Pol'tsverger) 2-oy dorozhnoy bol'nitsy Yuzhno-Ural'skoy zheleznoy dorogi.
(URETERS—SURGERY) (SURGERY, PLASTIC)

GUTKIN, Kh.G.

Parental hypernephroma with thrombosis of the "I" renal vein.
Vop. onk. 3 no.11:105-107 '62. (MIRA 17:6)

1. Iz khirurgicheskogo otdeleniya 2-y Berozhncy bol'nitsy
Yuzhno-Ural'skoy zheleznoy dorogi (zav. - V.I. Pel'tsverger,
glavnyy vrach - T.M. Ovchinnikova).

GUTKIN, L.

"New trends in the development of electrification of railroads in the United States; on the pages of the American press."

p.44 (Transportno Delo, Vol. 10, no. 3, 1958, Sofia, Bulgaria)

Monthly Index of East European Accessions (EEAI) LC, Vol. 7, No. 8, August 1958

GUTKIN, L. S.

PA 19T31

USSR/Demodulators

Sep 1946

Frequency changers

"Relationships between Diode Detection and Frequency Conversion and Amplitudes of Incoming Signal and Heterodyne," L. S. Gutkin, Candidate of Mech Sci, 19 pp

"Radiotekhnika" Vol I, No 6

A calculation procedure is presented which makes possible an analytical determination of the relationships between detection parameters and the amplitude of the incoming signal (for detection) and the amplitude of the heterodyne signal (for frequency conversion).

19T31

GURNEY, L. J.

PA 20767

USSR/Radio Receivers, Superregenerative Dec 1946
Radio Interference

"Interference Effect in Superregenerative Receivers,"
L. S. Gorkin, Candidate of Mechanical Sciences, 23 pr
"Radiotekhnika" Vol I, No 9

Results of a theoretical investigation on the performance of a superregenerator acted upon by oscillatory interference and aperiodic interference. The selectivity of a superregenerative receiver operating under varying conditions and different laws of circuit attenuation is analyzed. The influence of fluctuational and impulse interference on the superregenerator is examined, and a general comparative estimation of the interference probability in a superregenerative receiver is given.

20767

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Effect of interference on super-regenerative reception.
 II. Effect of random noise. (LITVIN, L. S. *Radiotekhnika*, 2 (No. 4) 24-45 (1947) *In Russian*. A mathematical analysis is given of the signal/noise deterioration in a super-regenerative receiver when compared with a normal receiver having similar characteristics. The normal receiver is equipped with a narrow low-pass a.f. filter with a cut-off at the highest modulation frequency. Two methods used to determine the thermal noise of the input circuit agree well. The valve noise is calculated, and it is shown that the signal/noise is always lower (down to 1:2 in extreme case) than in a normal receiver, but remains unaffected by linear or non-linear quenching operation.

ASB 31A METALLURGICAL LITERATURE CLASSIFICATION

GUTKIN, L. S.

Gutkin, L. S., "Theory of Superregenerative Receivers"

Moscow Lower Engineering Institute internal photo. (LII,)

SO: Radiotekhnika, No. 3, 1948; (W-27801, 14 Sept. 1953)

Journal of Technical Physics
USSR, Vol. 18, No. 5, 1948

El'tsin, I.A. (Scientific Research Physics Institute, Moscow State University), The disk method for the determination of dielectric penetrability and the tangent of the angle of loss, 657-64

"A rigorous theory for the case of a thin disk placed in the center of a tuned Lecher system. The formulas that are obtained are used to calculate the dielectric permeability and loss (for wave length of 336 cm) for different dielectrics."

Gutkin, L.S., Basic relations for diode frequency conversion, 614-38

"Basic relationships in diode frequency conversion are derived on the basis of results of the general theory of frequency transformation. The conditions for obtaining maximum amplification are analyzed on the basis of loading the converter with a single and double contour filter. The action of noise is analyzed and conditions of minimal noise production are investigated."

Source: C.T.R.S.P.K., Vol. 1, No. 5

GUTKIN, L. S.

USSR/Radio Receivers, Super-
regenerative
Radio Interference

Jan/Feb 49

7
"Effect of Interference on a Superregenerative
Receiver," L. S. Gutkin, Cand Tech Sci, ~~15~~ 17

"Radiotekh" Vol ~~17~~ 18, No. 1.

Considers action of impulse interference, consist-
ing of single and periodic impulses, on super-
regenerative receiver. Proves that superregenera-
tive receiver has better noise-limiter action
during impulse interference than ordinary receiver.
Makes general conclusion on noise-limiter action

36/49T103

GUTKIN, L. S.

GUTKIN, L. S. -- "Theory and Design of Detectors in Radio-Receiving Equipment."
Sub 28 Apr 52, Moscow Order of Lenin Power Engineering Institute
V. V. Molotov (Dissertation for the Degree of Doctor in Technical Sciences)

SO: Vechernaya Moskva January-December 1952

GUTKIN, L.S.

Preobrazovanie sverkhvysokikh chastot
i detektirovanie (Transformation of superhigh frequencies
and detection) Moskva, Gosenergoizdat, 1953. 415 p.

SO: Monthly List of Russian Accessions, Vol. 7, No. 5, August 1954

Gutkin, L.S.

3000

621.335.2 : 621.370.23
3137. THE EFFECT OF ELECTRON TRANSIT TIME IN
DIODE DETECTORS AND FREQUENCY CHANGERS.

L.S. Gutkin and A.M. Kuz'min
Radio Engng., Vol. 10, No. 14-16 (1955). In Russian. *Ch. 2*

Assuming parallel electrodes (true in the case of "piggy-back" diodes and almost true for cylindrical diodes with very short anode-cathode gaps) and neglecting electrode inductances and capacitances (which are usually absorbed by the external circuit), formulae are derived for detector current and input conductance for the first application and for conversion gain and noise factor for the second application. It is then shown how these alter at frequencies where electron transit time can no longer be neglected. The effect is of loss of gain and increase of noise, but the same laws are still valid, with new values for parameters such as internal impedance and input admittance. For the vicinity of the upper frequency limit, experimental determination of operating conditions is considered to be preferable to the analytical method described.

A. L. Kuz'min

PS

GUTKIN, L. S.
GUTKIN, L. S.

"Determination of Nominal Power Amplification of Linear and Quasilinear
Quadripoles." pp 72-78, 111

Abst: The general formula for rated power amplification of a network is
derived; specific cases -- common-cathode amplifier and common-grid amplifier
-- are examined.

SOURCE: Trudy Moskovskogo Energeticheskogo In-ta im. V. M. Molotova (Works of
the Moscow Energetics Institute imeni V. M. Molotov), No 21 -- Radio
Engineering, Moscow-Leningrad, Gosenergoizdat, 1956

Sum 1854

GUTKIN, L.S.

USSR / Radio Physics, Reception of Radio Waves.

I-7

Abs Jour : Izv. Zhur - Fizika No 3, 1957, No 7336

Author : Gutkin, L.S.

Title : Transients in the Detection of Weak Signals

Orig Pub : Radiotekhnika i elektronika, 1956, 1, No 4, 433-437

Abstract : The transients in the detection of weak signals are analyzed. A formula is derived for the distortion of the envelope of a pulse of arbitrary shape.

Card : 1/1

- 51 -

SUBJECT
AUTHOR
TITLE
PERIODICAL

USSR / PHYSICS
GUTKIN, L.S.

CARD 1 / 2

PA - 1215

The Interaction between Signal and Noise in an Inert Detector.
Radiotechnika, 11, fasc. 2, 43-53 (1956)
Publ. 2 / 1956 reviewed 8 / 1956

Here the simultaneous detection of the voltages of the signal and of the noise through a linear inert detector is discussed.

General relations: The voltage acting at the input of the detector is the sum of the momentary values of the voltages of the noise and of the signal. Because of the inertia of the detector the resistance of capacity must be low not only for the high-frequency- but also for the low frequency components of the current spectrum. Therefore, also the voltage at the RC-load of the detector must be constant. For this voltage a formula is derived by means of which the result of detection may be determined both if a signal is given and also if there is no signal.

The detection of noise: The last mentioned formula is specialized for the case with lacking noise, i.e. with vanishing voltage u_{sig} , it is several

times transformed and illustrated by means of a diagram. A further formula shows the increase of the rectified voltage on the occasion of transition from an inertialess to an inert detector. Next, a formula for the simultaneous detection of a harmonic signal and of noise is given. In view of the fact that this equation can be solved analytically only in the case of a very high or very low value of the ratio (signal/noise), these two limit-

Radiotechnika, 11, fasc. 2, 43-53 (1956) CARD 2 / 2

PA - 1215

ing cases are the first to be dealt with. In the case of very low values of this ratio the useful effect of detection in the inert and inertialess detector is proportional to the square of the ratio (signal/noise) at the input of the detector. In the case of any value of this ratio, the basic equation must be solved numerically. On this occasion the absolute amount of the rectified voltage in the inert detector is higher, and the ratio of this voltage to the noise voltage is lower than the corresponding quantities in the inertialess detector.

There follow deliberations concerning the constancy of the voltage at the RC-load, the input resistance of the detector for the voltages of the noise, and concerning the case with modulated signal. On this occasion the following conclusions result: a) With $a \gg 1$ (a denotes the ratio signal/noise) an inert detector furnishes the same result as an inertialess one, because for the signal the detector is practically without inertia. b) With $a \ll 1$ the amplitude $U_{m\Omega}$ of the modulated voltage depends, as in

the case of the inertialess detector, quadratically on the ratio (voltage U_{om} of the modulated signal at the input/voltage U_R) of the noise, but the absolute amount of $U_{m\Omega}$ is higher.

INSTITUTION:

SUBJECT USSR / PHYSICS
 AUTHOR GUTKIN, L.S.
 TITLE The Interaction of Signal and Noise in an Inert Detector.
 PERIODICAL Radiotekhnika, 11, fasc. 3, 51-62 (1956)
 Publ. 3 / 1956 reviewed 9 / 1956

CARD 1 / 2

PA - 1236

This is the conclusion of a previous work published under the same title in fasc. 2, p. 43 of this year's edition.

7. The ratio between signal and noise at the output of the detector:
General relations: In the most interesting case, namely that in which the ratio (signal / noise) is low ($a < 1$), the influence exercised by the signal upon the noise voltage $U_{R\Omega}$ may in first approximation be neglected. Besides,

$U_{R\Omega}$ in that case depends comparatively little on the amplitude of the signal. It is therefore possible to proceed from a scheme in which the voltage at the load consists of a constant component u_0 and a weak fluctuation component u_{\sim} . The equivalence scheme of the detector for the determination of u_{\sim} and the method for the determination of the inside resistance R_{i0} of this detector are discussed. $R_{i0} = \Delta U_0 / \Delta I_0$ is found; here ΔI_0 denotes the modification of the constant component of the current caused by a slight modification of the constant voltage ΔU_0 . For very inert detectors the following approximate relation is valid: Amperage of the low frequency component $i_{nf} =$ amperage i_{knf} of the low frequency component at $u_{\sim} = 0 + \varphi_0 \cdot u_{\sim}$.

Radiotechnika, 11, fasc. 3, 51-62 (1956) CARD 2 / 2

PA - 1236

Here $\varphi_0 = 1/R_{i0}$. There follows the determination of R_{i0} ; in the case of an inert detector it is larger than in the case of an inertialess detector, and this difference increases with increasing parameter. Next, the amperage i_{knf} and the correlation function of this low frequency component, and, following this, the voltage of the noise on the charge of the detector are determined. The output band ΔF_E being equal the voltage of the noise at the output of an inert detector is considerably larger already at $SR > 10$ than in the case of an inertialess detector. In conclusion, the ratio between signal and noise at the output of the detector is ascertained. Now ΔF_E and $\Delta F'_E$ denote the breadth of the output band in the case of an inert and an inertialess detector respectively. In the case of $\Delta F_E = \Delta F'_E$ the ratio (noise / signal) is considerably higher than in the case of an inertialess detector only at $SR > 100$. The relations found by this work were checked by experiment; experimental results were found to agree well with theory.

INSTITUTION:

GUTKIN, L. S.

RECEPTION

"Use of Low-Frequency Equivalents for the Analysis of Transients Occurring in Diode Detection," by L. S. Gutkin and O. S. Chentsova, Radiotekhnika, No 6, June 1957, pp 31-44.

A method is proposed for the analysis of transients in a system consisting of a high frequency amplifier and a diode detector, whereby it is possible to determine relatively easily results that take into account the transients in the system of resonant circuits of the system of amplifier resonant circuits that feed the detector, for various types of resonant circuits and for various variations of the envelope of the input signals. The method is based on a linearization of the processes occurring upon detection, and on the replacement of the detector as well as of the system of driving resonant circuits, with low-frequency equivalence.

Card 1/1

- 32 -

GUTKIN, L.S.

CIRCUITS

"Generalization of the Theory of Diode Detection of Weak Signals"
by L. S. Gutkin, Elektrosvyaz, No 11, November 1957, pp 47-51.

The author derives a single equivalent detector circuit, which holds for the regulation of the detection of weak unmodulated, amplitude-modulated, and pulse signals, and also for small noise voltage for a sum of signal and noise. Examples of application of this circuit to the calculation of several types of signals are given.

Card: 1/1

-7-

AUTHOR: Gutkin, I.S.

109-8-7/17

TITLE: Analysis of the detection of amplitude-modulated signals by the method of low frequency analogues. (Analiz detektirovaniya amplitudno-modulirovannykh kolebaniy metodom nizkochastotnykh ekvivalentov)

PERIODICAL: Radiotekhnika i Elektronika, 1957, Vol. II, Nr 8, pp.1012-1026 (USSR)

ABSTRACT: The system considered consists of a tuned output circuit, a rectifier and a load (see Fig.1). It is pointed out that the analysis of such systems is usually carried out without considering the effect of the modulation envelope on their performance. This can be done by describing the system by equations 10:

$$\left. \begin{aligned} dI_{\Sigma} &= S_{1d} dU_1 + g_{1d} dU_{\Sigma} , \\ dI_1 &= g_{2d} dU_1 + S_{2d} dU_{\Sigma} , \end{aligned} \right\}$$

where U_1 is the input voltage, I_1 is the magnitude of the first input harmonic and U_{Σ} and I_{Σ} are the load voltage and current respectively (see Fig.1), and the

Card 1/3

109-8-7/17

Analysis of the detection of amplitude-modulated signals by the method of low frequency analogues.

parameters S_{1d} , g_{1d} , S_{2d} and g_{2d} are defined by equations 11. The input admittance of the system is then defined by equation 15:

$$Y_{BX\Omega} = \frac{\Delta^* I_1}{\Delta^* U_1}$$

where $\Delta^* I$ and $\Delta^* U$ are the complex current and voltage amplitudes of the input envelope. $Y_{BX\Omega}$ is referred to as the input admittance of the detector for the deviations of the envelope (see Fig.2). Expressions for $Y_{BX\Omega}$ can be easily evaluated and it is shown that for a double-tuned amplifier they are in the form of equation 25, (p.1016), and for a single tuned amplifier they are given by equation 29 (p.1017). Thus the full input impedance of a detector connected to a resonant amplifier can be determined if the internal parameters of a detector (S_{1d} , g_{1d} , S_{2d} and g_{2d}) are known. The analysis is carried out for the case of

Card 2/3

109-8- 7/17

Analysis of the detection of amplitude-modulated signals by the method of low frequency analogues.

small signals and it is shown that the input admittance is equal to the standard input conductance of the detector. In a linear detector the input admittance is no longer equal to its standard input conductance (see Figs. 14 and 16), and in this case the presence of the detector can lead to a decrease of the bandwidth of the system. Similar effects can be observed with an exponential detector. For this case the actual input conductance is in the form shown in Figs. 16 and 17. There are 17 figures and 3 references, all of which are Slavic.

SUBMITTED: December 27, 1956.

AVAILABLE: Library of Congress.

Card 3/3

AUTHOR
TITLE

GUTKIN L.S., Regular Member of Society, CHENTSOVA O.S. ~~XXXXXXXXXX~~
Analysis of the Transition Processes in the Case of Diode Detection According to the Method of Audio-Frequency Equivalents.
(Analiz perekhodnykh protsessov pri diodnom detekirovani metodom nizkochastotnykh ekvivalentov-Russian)

PERIODICAL

Radiotekhnika, 1957, Vol 12, Nr 6, pp 31 - 44 (U.S.S.R.)

ABSTRACT

A method for the analysis of the transition processes in a high-frequency-amplifier-diode detector system is given. By means of this method relatively simple results can be obtained and the transition processes in the system of the amplifier circuit, which feed the detector, are taken into account in the case of various types of these circuits as well as of various rules governing modification of the envelope curves of the initial signal. This method is based on a linearization of the processes occurring on the occasion of detection, then on the replacement of the detector as well as of the system of feeding circuits by audio-frequency equivalents. The authors show that the audio-frequency equivalent of the selection system must meet the following two demands: 1. It must have a transmission coefficient which is similar to the complex transmission coefficient for the envelope curves of the selection system in the case of idle motion i.e. without regard to detector reaction. 2. It must have an initial resistance which is similar to the initial resistance for the envelope curves of the selection system. The parameters of an audio-frequency equivalent

Card 1/2

Analysis of the Transition Processes in the Case of ~~XXXXXXXX~~
Diode Detection According to the Method of Audio-Frequency Equi-
valents.

with a two-circuit filter are determined as examples
(18 illustrations and 6 Slavic references).

ASSOCIATION Not Given.
PRESENTED BY
SUBMITTED 14.6.1956
AVAILABLE Library of Congress.
Card 2/2

GUTKIN, L. S.

AUTHORS: Gutkin, L. S., Real Member of the Society, and 108-11-6/10
Chentsova, O. S.

TITLE: Transition-Processes in the "High Frequency-Amplifier-Detector"
System (Perekhodnyye protsessy v sisteme "usilitel' vysokoy chasto-
ty-detektor").

PERIODICAL: Radiotekhnika, 1957, Vol. 12, Nr 11, pp. 50-61 (USSR).

ABSTRACT: With reference to the earlier work of the authors (reference 1)
and the in this work established method of low frequency-equivalents
is adapted for the analysis of the transition-processes in the most
common schemes. The indicated method allows to take into considera-
tion the influence of the transition-processes in a system feeding
the detector under various variation-rules of the envelope curve of
the input signal. Examined are: a tuned resonance-circuit, a untuned
resonance-circuit and two coupled circuits.
There are 19 figures and 5 references, 5 of which are Slavic.

SUBMITTED: June 14, 1956.

Card 1/2

Transition-Processes in the "High Frequency-Amplifier-Detector" (Cont.) 108-11-6/10

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi
im. A.S. Popova (Scientific-technical Society of Radio Engineer-
ing and Electrical Communications im. A.S. Popov)

AVAILABLE: Library of Congress

Card 2/2

GUTKIN, L.S.

Noise factor and sensibility of superregenerators. Nauch.dokl.
vys.shkoly; radiotekh. i elektron.no.1:176-181 ' 58.
(MIRA 12:1)

1. Kafedra radiopriyemnykh ustroystv Moskovskogo energetiche-
skogo instituta.
(Radio--Receivers and reception)

6(4)

SOV/108-13-11-13/15

AUTHOR:

Gutkin, L. S.

TITLE:

On the Article by V. Ya. Khevrolin "On the Theory of the Super-Regenerative Receiver Operating in a Linear Domain" (Po povodu stat'i V. Ya. Khevrolina "K teorii superregeneratora, rabotayushchego v lineynom rezhime")

PERIODICAL:

Radiotekhnika, 1958, Vol 13, Nr 11, pp 75-78 (USSR)

ABSTRACT:

This is a letter to the editor. In his article (Ref 1) V. Ya. Khevrolin declares that the papers by L. S. Gutkin and M. K. Belkin contain errors in connection with the determination of the conditions for the stability of the amplification of the super-regenerative receiver. It is shown in this letter that this is not the case and that Khevrolin himself committed errors. Thus, the errors alleged to have been committed by Gutkin have, in reality, been committed by Khevrolin himself. There are 2 Soviet references.

Card 1/1

1(1); 6(4); 9(0)

PHASE I BOOK EXPLOITATION

SOV/3257

Gutkin, Lev Solomonovich

Printsipy radioupravleniya bespilotnymi ob"yektami (Principles of the Radio Control of Pilotless Objects) Moscow, Izd-vo "Sovetskoye Radio," 1959. 383 p. Errata slip inserted. No. of copies printed not given.

Eds.: V.I. Shamshur and A.A. Kokushkin; Tech. Eds.: K.P. Boronin and B.V. Smurov.

PURPOSE: This book is intended for radio engineers and students of advanced courses in radio. It may also be useful to specialists interested in the radio control of guided missiles.

COVERAGE: The author outlines the principles of the radio control of guided missiles, e.g., rockets, airborne torpedoes, bombs, etc. General characteristics of controlled missiles and various methods of guidance and control are described (i.e., self-guidance, homing, remote control and combined control). Basic factors affecting the accuracy and range of radio control systems are analyzed. According to the author, while the information contained in the book is 10 to 15 years old, it is based on material not subject

Card 1/7

Principles of the Radio (Cont.)

SOV/3257

to rapid change, i.e., basic equipment and general principles of control. Latest data on control systems for guided missiles were for obvious reasons not available to the author. The present book serves only as an introduction to this problem. Numerical data and examples apply to equipment used in World War II and are included only for purposes of illustration. Certain problems are treated only briefly or not at all. These include dynamics of flight, stability and quality of regulation, problems of jet technique, control of long-distance rockets, and proximity fuses. The manuscript was prepared in 1954; in 1958 small additions were introduced concerning the development of the intercontinental ballistic rocket in the USSR, corrected values of aircraft speeds, a short history of radio control based on the book by A.V. Khramov "Ocherk istorii razvitiya avtomatiki v SSSR" (AN SSSR 1956), and additions to the list of references. There are 25 references: 15 Soviet (10 are translations), 9 English, and 1 German.

TABLE OF CONTENTS:

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Ch. I. General Characteristics of Guided Missiles and Methods of Control	9
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SOLOV'YEV, I.V. [translator]; GUTKIN, L.S., prof., red.; FRIDMAN, V.Ya.,
red.; GRIBOVA, M.P., tekhn.red.

[Reception of signals in the presence of noise; collection of
articles] Priem signalov pri nalichii shuma; sbornik statei.
Moskva, Izd-vo inostr.lit-ry, 1960. 342 p. Translated from
the English. (MIRA 14:1)
(Radio--Noise) (Radio--Receivers and reception)

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77562
SOV/108-15-2-7/12

AUTHOR: Gutkin, I. S.

TITLE: Some Relationships in Optimal Systems of Signal Detection (To Be Continued)

PERIODICAL: Radiotekhnika, 1960, Vol 15, Nr 2, pp 47-57 (USSR)

ABSTRACT: The paper analyzes various aspects of signal detection in the presence of white noise. Approximate expressions for determining the sensitivity of optimal detecting systems are derived. The signal $x(t)$ and the noise $n(t)$ at the receiver input are represented by $y(t) = x(t) + n(t)$. When the oscillation $y(t)$ is received there is a probability $P_y(x)$ that the signal $x(t)$ is transmitted. An optimal receiver evaluates $P_y(x)$ for all possible signals x and selects the signal for which $P_y(x)$ is a maximum. Three types of signals are considered: (1) an exactly known signal; (2) a signal with a random phase; and (3) a slow

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Some Relationships In Optimal Systems of
Signal Detection (To Be Continued)

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SOV/198-15-2-7/12

fluctuating signal with amplitude distribution according to the Raleigh law. The binary detection is considered first. Here the presence or absence of the signal has to be determined against a noise-background. Thereby two types of errors are possible; (1) the false alarm, i.e., indication of signal presence while only the noise is acting; (2) the signal omission, i.e., indication of signal absence, while actually at the input is the sum of signal and noise. The probabilities of these errors are noted as P_{fa} and P_{so} , respectively. They are defined for an exactly known signal by the following expressions:

$$P_{fa} = \sqrt{\frac{N_0}{4\pi E_1}} \int_0^{\infty} e^{-\frac{N_1}{4E_1} y^2} dy, \quad (1)$$

$$P_{so} = 1 - \sqrt{\frac{N_0}{4\pi E_1}} \int_0^{\infty} e^{-\frac{N_1}{4E_1} \left(y - \frac{2E_1}{N_0}\right)^2} dy, \quad (2)$$

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repeated on the
next reel.*

Some Relationships in Optimal Systems of
Signal Detection (To Be Continued)

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SOV/106-15-2-7/12

$$\alpha = \frac{E_1}{N_0} + \beta \quad (3)$$

Here N_0 is the specific noise power given as

$$N_0 = \frac{\overline{n^2(t)}}{\Delta f} \quad (4)$$

where $n^2(t)$ is the average square of the noise voltage at entrance to the receiver; Δf is the passband within limits of which N_0 is being determined; E_1 is the specific signal energy. When the signal $x(t) = U_m \cos(\omega t + \psi)$ is acting during the observation time T , E_1 may be written as

$$E_1 = \frac{U_m^2 T}{2} \quad (5)$$

where β is a threshold coefficient, which may be eliminated for the considered relationships. Assuming $P_{fa} \leq 0.1$

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Some Relationships in Optimal Systems of
Signal Detection (To Be Continued)

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SOV/108-15-2-7/12

and $P_{so} \leq 0.1$ the following expression is obtained
after transformations of Eq. (1), (2), and (3):

$$\frac{E_s}{N_0} = (a + b)^2, \quad (6)$$

where

$$a = \sqrt{\ln \frac{1}{P_{fa}} - 1.4}, \quad (7a)$$

$$b = \sqrt{\ln \frac{1}{P_{so}} - 1.4}. \quad (7b)$$

A comparison of the approximate Eq. (6) with the exact results obtained from Eq. (1), (2), and (3) shows that the errors introduced by expression (6) do not exceed 0.5 db and tend to zero asymptotically when $P_{fa} \rightarrow 0$ and $P_{so} \rightarrow 0$. In case of a signal with a random phase the exact expressions for P_{fa} and P_{so} are transformed under the same assumption as above. In the thus

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obtained Eq. (9)

$$\frac{E_s}{N_0} = (a' + b)^2 \quad (9)$$

b is defined by Eq. (7b) and a' is

$$a' = \sqrt{\ln \frac{1}{P_{fa}}} \quad (10)$$

The error introduced by Eq. (9) does not exceed 0.5 db and tends to zero asymptotically when $P_{fa} \rightarrow 0$ and $P_{so} \rightarrow 0$. For the fluctuating signal the following exact expression

$$\frac{E_{us}}{N_0} = \frac{\ln \frac{1}{P_{fa}}}{\ln \frac{1}{P_{so}}} = 1, \quad (11)$$

where

$$P_{so} = 1 - P_{fa} \quad (12)$$

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shows the probability of correct signal detection when there is actually a signal at the input; E_{as} is the average specific energy of the fluctuating signal at the receiver input. Comparing Eq. (6), (9), and (11), the following basic conclusions may be drawn: (1) When $P_{fa} \leq 0.1$ and $P_{so} \leq 0.1$ the energy required for detection of a signal with a random phase exceeds the energy required for detection of a signal with a random phase exceeds the energy required for detection of an exactly known signal by no more than 2 db. When $P_{fa} = 10^{-2}$ and $P_{so} = 10^{-2}$ the difference does not exceed 1.1 db. Consequently, no considerable amount of signal energy can be saved by taking into account the signal phase; (2) When $P_{so} = 0.63$, then $E_{as} = E_1$; i.e., the average energy required for the detection of a fluctuating signal exceeds the energy required for the detection of a signal of known amplitude. The difference increases sharply as P_{so} decreases. The case of

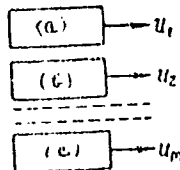
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multichannel detection is illustrated on Fig. 1.

Fig. 1. (a) 1st channel;
(b) 2nd channel; (c) m-th
channel.



The signal $x(t)$ is either present in one of the channels or absent in all channels. The following problems are considered; (a) detection only, i.e., to determine whether the signal $x(t)$ is present at the entrance of any of the m-channels; (b) recognition only, i.e., when the presence of $x(t)$ is known, so as to determine in which channel the signal is present; and (c) detection and recognition, combining (1) (2).

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(a) Detection only. For a signal exactly known, assuming $P_{fa} \leq 0.1$ and $P_{so} \leq 0.1$, the following expression is obtained:

$$\frac{E}{N_s} = (a + b)^2 + 0.5 \ln m, \quad (16')$$

where a and b are given by Eq. (7a) and (7b); E is the signal energy required for the m -th alternative detection ($m > 1$). For a signal with a random phase, under the above assumptions, the corresponding expression is:

$$\frac{E}{N_s} = (a' + b) + 0.5 \ln m + 1, \quad (18)$$

where a' and b are defined by Eq. (10) and (7b), respectively. Comparing Eq. (16') and (18), it is seen that the signal with a random phase requires only a little more energy than the exactly known signal (the difference does not exceed 2db. (b) Recognition. After transformation of the expression for an exactly

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known signal and under the assumption that the probability of distortion $P_{dis} \ll 0.1$, the following expression is obtained:

$$\frac{E}{N_0} = 2 \ln \frac{1}{P_{dis}} + \ln(m-1) - 2.8. \quad (20)$$

P_{dis} is the probability of distortion, i.e., that the signal will not be attributed to the channel in which the signal is actually present. When $P_{dis} \ll 0.1$ Eq. (20) introduces an error not exceeding 1 db. Under the same assumption of $P_{dis} \ll 1$ it may be considered that Eq. (20) is valid also for a signal with a random phase. (c) Detection and recognition. An optimum reception system is shown on Fig. 2

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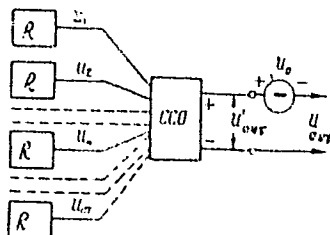


Fig. 2.

Here R_1, R_2, \dots, R_m are optimal receivers of the corresponding channels. The output of any receiver, for instance of R_k is proportional to $P_y(x_k)$

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where C is a constant of equal magnitude for all channels. The voltage u_0 is constant and corresponds to the probability that there is only noise present. The block CCO performs two functions: (a) it compares the voltages u_1, \dots, u_m , one against the other, and it determines the largest of them. Consequently, it determines also the channel with the highest output voltage; (b) it supplies an output voltage u'_{out} equal to the largest u_k . The total output of the system is then

$$u_s = CP_s(x_s). \quad (21)$$

When $u_{out} \leq 0$, it is considered that there is no signal in any of the m channels. When $u_{out} > 0$ it is considered that the signal is present in the channel K having the largest u_k . It is shown that expression

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For the signal-to-noise ratio in an n-channel system may be obtained from corresponding expressions of a one-channel system by substituting P_{fa}/m for P_{fa} .

Changes in the form of the detector characteristic do not affect the sensitivity of the above system, provided the threshold u_0 is changed correspondingly.

Therefore, the system shown on Fig. 2 may be used for optimal reception of various signal types.

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TO: GUTKIN, L.S.