ESTEROV, Ya.Kh., inzh.; PUGACHEV, V.I., inzh.

Practices in blasting holes on steep slopes. Transp.stroi. 14 no.12:6-7 D 164. (MIRA 19:1)

ESTERNOVICH, V.O., inzh.

Rubbor linings in feeding units used in molding bricks instead of the spraying process. Rats. i izobr. predl. v stroi. no.5:58-59 158.

(MIRA 11:6)

1. Proyektno-konstruktorskoy byuro Nauchno-issledovetel skogo instituta streitel noy keramiki, Moskva, Vekovaya ul., d. No.18/12. (Brickmaking)

AUTHOR: Esterzon, M.A.

121-2-7/20

TITLE:

Improvement of the dimensional stability of a cutting tool by the method of elastic compensation (Povysheniye razmernoy stoykosti rezhushvhego instrumenta metodom uprugoy kompensatsii.)

PERIODICAL: "Stanki i Instrument" (Machine Tools and Tools), 1957, No.2, pp. 24 - 28 (U.S.S.R.)

In metal cutting, especially turning, the cutting endur-ABSTRACT: ance of the tool considerably exceeds its endurance limitation due to the gradual shift in the mean dimension. Although the random scatter also increases as the cutting proceeds, the compensation of the shift of the mean dimensions can considerably increase the practical tool endurance. This compensation can be accomplished on the basis of the number of machined components or the cutting time or by feeding back the result of direct measurement of the component dimension. It can also be carried out by making use of the change in the cutting force which takes place with the blunting of the tool. Research work carried out by the VNII Tool Research Institute has led to the design of a toolholder based on a new principle of the increase in the total cutting force component situated in the plane of the tool planform. This total component can 1/3

Improvement of the dimensional stability of a cutting tool by the method of elastic compensation. (Cont.) 121-2-7/20 be further resolved into the axial (parallel with the main spindle) and radial components. Of these, the radial force always causes springing back in its own direction but the axial force can be made to advance or withdraw the cutting edge according to the geometry of the elastic deformations of the tool holder. The practical condition which ensures that the compensating tool holder does not increase the scatter between the components, is that the change in the component size under the effect of the radial force component does not exceed twice the change under the axial component. Thus elastic compensation of the systematic error can be accomplished without increasing the scatter, either when the dimentional wear factor is small or when the effect of the wear

illustrated. The prismatic tool carrying the cutting tips is supported against the radial and tangential cutting forces by separate pins. These pins butt against tapered stops. The axial force tries to turn the tool about on axis passing through the stops. This causes the tool to press against a public which deforms a leaf spring, whose stiffness can be

on the axial force is large. This cours with a large planform angle of the tool. A variable stiffness tool holder is

Improvement of the dimensional stability of a cutting tool by the method of elastic compensation. (Cont.) 121-2-7/20 adjusted by screws. Histograms of cutting dimensions resulting from an ordinary tool holder and a compensating tool holder in cutting mild steel are compared at a cutting speed of 60 m/min feed of 0.238 mm/rev. and depth of cut of 2 mm. A dimension skim of a compensating tool holder developed from the experiments reported is given, together with a formula for the initial adjustment of the negative stiffness.

The re are 8 figures, including 2 photographs, 5 graphs and 2 Slavic references.

AVAILABLE:

ESTERZON, M.A., inzhener. Calculating dimensional stability of cutting tools. Vest. mash. 37 no.7:63-66 Jl 157. (MIRA 10:8)

(Cutting tools)

ESTERZON, M.A.; PETROV, K.P.

Cutting-tool equipment used on the turning section of automatic gear-machining line. Stan.i instr. 30 no.3:7-10 Mr '59. (MIRA 12:3) (Gear-cutting machines)

TEMCHIN, G.I.[deceased]; YULIKOV, M.I., kand. tekhn. nauk, retsenzent; ESTERZON, M.A., kand. tekhn. nauk, red.; SEMENCHENKO, V.A., red.1zd-va; MODEL', B.I., tekhn. red.; DEMKINA, N.F., tekhn. red.

[Multitool adjustments; theory and design] Mnogoinstrumentnye naladki; teoriia i raschet. Izd.2., ispr. Moskva, Mashgiz, 1963. 542 p. (MIRA 16:12) (Metal cutting)

IVANOV, B.N., kand. tekhn. nauk; ESTERZON, Yu.Ya.

Industrial testing of the device for automatic measurement of sheet length. Art. i prib. no.4:75-77 C-D *64 (MIRA 1802)

ETIGIN, M.G.; REVENKO, I.F.

Economic work at the Donetsk and the Makeevka metallurgical plants. Metallurg 10 no.12:39-40 D '65.

(MIRA 18:12)

KOLTON, A.Yu., kand. tekhn. nauk; UMIKOV, I.N., inzh., ETINBERG, I.E., kand. tekhn. nauk

Basic principles of the establishment of new nomenclature on large Kaplan and Francis-type hydraulic turbines. [Trudy] LMZ no.10:39-52 '64. (MIRA 18:12)

TADZHIYEV, Kamil Fadzhiyevith; ETINGE, Ye., dots., red.; MANSURC, Kh.Kh., prof., red.; BATUROVA, L., red.

[Operative and postoperative complications in the treatment of mitral stenosis and their control] Operatsicance i posleoperatsicance oslowheniis pri lechenii mitralinego stenoza i boriba s nimi. Dushanbe, Irfon, 1965. 249 p. (EIRA 18:11)

ETINGOF, M.I.

Active control of parts having discontinuous surfaces. Izm.tekh.

(MIRA 18:12)

no.10:3-6 0 165.

SAMEONON, COU.; ETIMOTO, YESD. Supermitted of verticus components of platomycle as the feet gel-filtration method through 0.25 approve and cobar ometric titration. Antiblotik: 10 no. 35:27-319 No. 166. 1. landagradakly khimiko-farmetserticheskly in filmite

LYUBIMOVA, T.F.; KANEVSKIY, B.Z.; ETKIN, V.S.

Study of signal limiting in a regenerative frequency converter. (M Radiotekhnika 20 no.5:70-75 My 165. (MIRA 18:10)

1. Deystvitel'nyye chleny Nauchno-takhnicheukogo obshchestva radio-tekhniki i elektrosvyazi imeni Popova.

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NEKRASOV, V.I. (Leningrad); POPOV, I.M. (Leningrad); ESTLING, A.A. (Leningrad)

Modeling method used for investigating dynamics of electric trains. Elek. i tepl. tiaga 2 no.9:10-13 S '58. (MIRA 11:10) (Electric railroads-Dynamics-Trains)
```

POPOV, I.M.; ESTLING, A.A. (Leningrad)

Investigating the dynamics of electric locomotives at high speeds. Elek.i tepl.tiaga 3 no.10:35-37 0 '59. (MIRA 13:2)

(Electric locomotives—Dynamics)

POPOV, I.M., inzh.; CHERKASOV, Ye, B., inzh.; ESTLING, A.A., inzh.

Dynamic testing of models of electric rolling stock. Sbor.LIIZHT no.167:67-77 '59.

(Blectric railroads-Rolling stock)

ESTLING, A.A., insh.

Selecting the parameters of hydraulic shock absorbers for cars.

Shor. LIIZHT no.168:209-220 *60. (MIRA 13:10)

(Railroads--Cars--Shock absorbers)

CHELNOKOV, I.I., doktor tekhn.nauk, prof.; ESTLING, A.A., inzh.

Selecting the design diagrams for determining the frequency
of the natural vibrations of railroad cars. Sbor.trud.LIIZHT
on.183:3-28 '62.

(Railroads--Cars-Vibration) (Car springs--Testing)

VISHNYAKOV, B.I., inzh.; ESTLING, A.A., inzh.

Methods of testing vibration dampers for passenger cars. Sbor.

(MIRA 16:2)

trud.LIIZHT no.183:69-94 *62.

(Damping (Mechanics)) (Railroads—Passenger cars—Vibration)

```
CHELNOKOV, I.I., doktor tekhn. nauk, prof.; VISHNYAMOV, B.I., inzh.; GARBUZOV, V.M., inzh.; ESTLING, A.A., kand. tekhn.nauk; DOLMATOV, A.A., kand. tekhn. nauk, retsenment; SARANTSEV, Yu.S., inzh., red.; USENKO, L.A., tekhn. red.

[Vibration dampers for railroad cars] Gasiteli kolebanii vagonov. [By] I.I.Chelnokov i dr. Moskva, Transzheldorizdat, 1963. 175 p.

(Railroads—Cars—Vibration) (Damping (Mechanics))
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CHELNOKOV, I.I., dr. tekhn. nauk, prof.; ESTLING, A.A., kand. tekhn. nauk

Selecting the necessary number of vibration dampers and their
distribution on the truck of passenger cars. Sbor. trud.
LIIZHT no.215:3-19 164. (MIRA 17:12)

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-

CIA-RDP86-00513R00041222

BRAILOVSKIY, A.Ye., kand. tekhn. nauk, dotsent; FSTLING, A.A., kand. tekhn. nauk

Determining the parameters of vibration dampers for cars by nomograms. Sbor. trud. LIIZHT no.215:87-98 '64. (MIRA 17:12)

MAKOVICKY, L.; namestnik poverenika zdravotnictva; KSTOK, S. poverenictvo zdravotnictva.

Considerations on the development of public health in Slovakia in the Czechoslovakian People's Democracy. Cesk. zdravot. 5 no.12: 672-682 Dec 57.

(PUBLIC HEALTH,
in Czech. (Cz))

RUSNAK, M.; ESTOK, S.

The development of child care in Slovakia during the past 10 years. Cesk. pediat. 20 no.6:453-461 Ja'65.

1. Oddelenie starostlivosti o zenu a dieta Poverenictva SNR pre zdravotnictvo a Slovensky ustav zdravotnickej statistiky, Bratislava.

ENT (m)/ENG(m)/ENP(t)/ENP(b) IJP(c) RVM/JD/RM S/0289/64/000/003/0085/0090 42930-65 ACCESSION NR: AP5009427

AUTHOR: Chernyak, A.S.; Esmont, Ye. M.

TITLE: Adsorption of germanium from weakly alkaline solutions

SOURCE: AN SSSR. Sibirskoye oddeleniye. Izvestiya. Seriaya khimicheskikh nauk, no. 3, 1964, 85-90

TOPIC TAGS: germanium adsorption, germanium refining, anion exchange resin

ABSTRACT: The article reports the results of laboratory and large-scale investigations into the recovery of germanium by anion-exchangers from waters containing 100 to 800 mg/m³, and presents data on the control of the adsorption process by means of the radioisotope Ge71. The weekly basic anion exchangers EDE-10p and AN-2f were used in the recovery, both static and dynamic conditions being studied. In the latter case, most complete recovery was achieved at a flow rate of water of 1 to 2 ml/min/cm2 through the exchanger. Desorption was performed under dynamic conditions with sulfuric acid and sodium hydroxide solutions; the latter gave better results. The recovery of germanium was 70.4%, but this relatively low yield was due to the low concentration of germanium in the water. A reduction of NaOH concentration in the eluate to 5% will Card 1/2

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ESTRETCHER, Karol

Eugeniusz Brzezicki as art collector and connectment. Februal. neurochir. psychiat. Fol. 15 no.4:543-550 di-hg tet.

1. 7 Muzeum UJ w Krakowie (Dyrektor: prof. dr. K. Estreicher).

Bildil, A. L. 34027. Opyt provedeniya ransejo okota karakul shiidi astob v sevidezeki. astrakilanskoy oblasti. Karakulevodstvo t zverovodstvo, 1949, No. 5.

30: Knishuaya, Letopis', Vol. 7, 1955

c. 15,21

ESTRIN, B.M., BAST, A.I.

Bright annealing of wire in continuous shaft furnaces. Metalloved. i term. obr. met. no.4:40-42 Ap 164. (MIRA 17:6)

1. Tientroenergometallurgprom, zavod im. lepse.

GOL'SHTEYN, M.I.; ESTRIM. B.M.; IVANCHENKO, N.P.; AYZENBERG, S.A.

A compound method for the prevention of influenza and of acute catarrhs of the upper respiratory tract in metal workers at the G.I.Retrovskii Plant. Vop.virus. 1 no.2:10-13 Mr-Ap 156. (MIRA 10:1)

1. Kafedra epidemiologii Dnepropetrovskogo meditsinskogo instituta
Dnepropetrovskaya gorodskaya sanitarno-epidemiologicheskaya i medikop
sanitarnaya chast' zavoda imeni G.I.Petrovskogo, Dnepropetrovsk.

(INFLUENZA, prevention and control,
in indust. (Rus))

(COMMON COLD, prevention and control,
in indust. (Rus))

SOV/133-59-9-30/31

Estrin, B.M. and Bertol'man, Ye.N., engineers AUTHORS:

Preparation and Utilization of Protective Atmosphere TITLE:

from Technical Nitrogen

PERIODICAL: Stal', 1959, Nr 9, pp 854-861 (USSR)

A description of the plant producing protective ABSTRACT:

atmosphere for muffle furnaces, laboratory work on catalytic decomposition of ammonia and purification of nitrogen from oxygen are given. The atmosphere is produced from technical nitrogen containing about 3% of oxygen (from the oxygen plant) and ammonia. The diagram

of the plant - Fig 1. Liquid ammonia is filtered, evaporated and passed into dissociation reactor (Fig 4),

mixed with nitrogen and passed into a reactor for catalytic removal of oxygen, then cooled for the removal of moisture (2 stage cooling). Final drying is done by

passing through a column of alumogel (which is

regenerated by blowing hot air). In laboratory experiments (apparatus - Fig 2) a suitable catalyst was developed (TsEChM-1). The comparison of the activity of

the catalyst with that of Rashig iron rings is shown in Card 1/3

SOV/133-59-9-30/31

Preparation and Utilization of Protective Atmosphere from Technical Nitrogen

Fig 3. The catalyst is made up of two layers - the first layer contains for each 100 cm3 of the carrier, 7.5 g of Ni and 4.0 g of MgO and the second layer, 3.0 g of Fe, 4.5 g of Ni and 4.0 g of MgO. At present the retort for the dissociation of ammonia is being redesigned according to the scheme shown in Fig 5. As a catalyst for the removal of oxygen, copper-nickel catalyst on α-alumina beads TsEChM-2 at 350°C was found to be most suitable. Catalytically active components (copper and nickel) as well as the promoter (Al203) are introduced in the form of nitrates (for each 100 g of the carrier 3g of Ni, 4.5 g of Cu and 1.5 g of Al_2O_3). The design of the oxygen purification reactor is shown in Fig 9. Typical compositions of the protective atmosphere during annealing of strip from steel UlOA and alloy steel Kh05 are shown in Fig 10 and 11 respectively. There are 11 figures and 4 references, 3 of which

Card 2/3

sov/133-59-9-30/31

Preparation and Utilization of Protective Atmosphere from Technical Nitrogen

Soviet and 1 English.

ASSOCIATIONS: Tsentroenergochermet and
Leningradskiy staleprokatnyy zavod (Leningrad Steel
Rolling Works)

Card 3/3

GORGIYEV, T.B.; KRASNOVA, V.G.; YARTSEVA, I.M.; KHODOS, A.D.; ESTRIN, B.M.; RUKAVITSA, T.Z.; KAPLINA, A.N.

Characteristics of the postepidemic period of influenza A2. Zhur. mikrobiol. epid. i immun. 31 no. 10:65-71 0 160. (MIRA 13:12)

le Iz Dnepropetrovskogo instituta epidemiologii, mikrobiologii i gigiyeny imeni Gamalei i Dnepropetrovskoy gorodskoy sanitarnoepidemiologicheskoy stantsii. (INFLUENZA)

ESTRIN, B.M.

New equipment for the preparation of protective atmospheres from ammonia. Stal* 22 no.6:573-576 Je *62. (MIRA 16:7)

1. TSentroenergochermet.
(Protective atmospheres)

ESTRIN, Boris Moiseyevich; LANOVSKAYA, M.R., red.izd-va; KARASEV, A.I., tekhn. red.

[Preparation and use of controlled atmospheres]Proizvodstvo i primenenie kontroliruemykh atmosfer. Moskva, Metallurgizdat, 1963. 342 p. (Protective atmospheres)

 $\frac{1}{2} \left(\frac{1}{2} + \frac{1}{2} \right) = \frac{1}{2} \left(\frac{1}{2} + \frac{1}{2} \right)$

ESTRIN, B.M.; SOKOLINSKIY, F.D. Purification of technical gases having a high oxygen content.

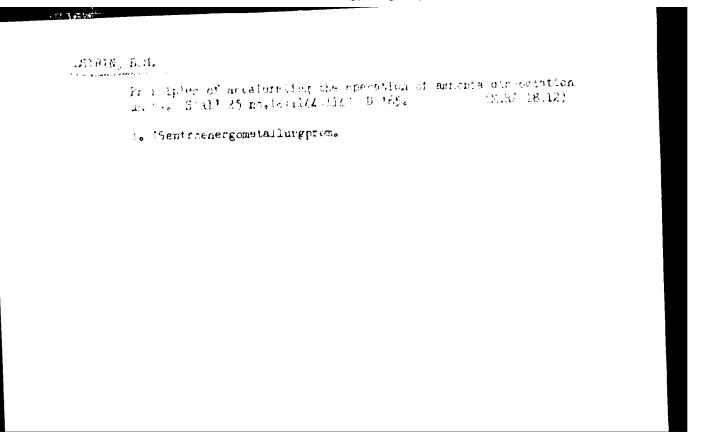
Khim. prom. no.8:588-591 Ag '63. (MIRA 16:12)

ESTRIN, B.M.; PETRUN, A.P.; PEKER, Yaul.

Starting, adjusting, and studying the operation of a protective gas station. Stall 24 no.5:472-475 My 164. (MISA 17:12)

1. TSentroenergometallurgprom 1 Novolipetskiy metallurgicheskiy zavod.

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00041222



KAPTOR, P.B.; ESTRIN, B.S. kyrotelle sette little little little A water thermostat with automatic temperature control. Ism.tekh. no.5:50-52 S=0 155. (Thermostat)

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SOV/115-59-10-9/29

Measuring the Temperatures in the 300-500°C Range

and n the number of degrees from 1 - 10, remains linear in the given range with an error of 10^{-40} C. In the diagram (Fig 1) R1 and R2 are the constant bridge arms and Rt is the arm of the measuring bridge (the platinum thermometer of resistance). The variable bridge arm is composed of coupled resistance coils R3 and R4 forming a decade of "ten degrees", and of resistance coil R5 forming the decade of "single degrees". The values of R3, R4, and R5 resistances are so chosen that the R3 and R4 values remain constant in each "ten degree" decade and the variation of the R5 resistance, which by-passes the R3 resistance, corresponds to the variation of resistance of the thermometer when the temperature increases from k to $k\,+\,10\,^{\rm o}\text{C}_{\rm \cdot}$ The diagram of the bridge for measuring temperature in the group 1 - 100C is shown in Fig 2. If the movable contact of R₅ resistance is in the position n (0 < n <10) the element of the diagram with R3 and R5 resistances forming a triangle with R3, and Rn and R5 - Rn sides, can

Card 2/3

SOV/115-59-10-9/29

Measuring the Temperatures in the 300 - 500°C Range

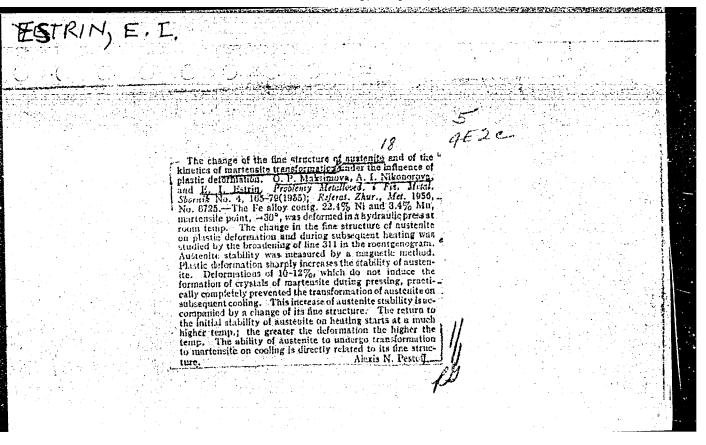
be transformed into a star with the Ra, Rb and Rc rays, where

$$R_{a} = \frac{R_{n} (R_{5} - R_{n})}{R_{5} + R_{3}} \qquad R_{b} = \frac{(R_{5} - R_{n}) R_{3}}{R_{5} + R_{3}} \qquad R_{c} = \frac{R_{n} R_{3}}{R_{5} + R_{3}}$$

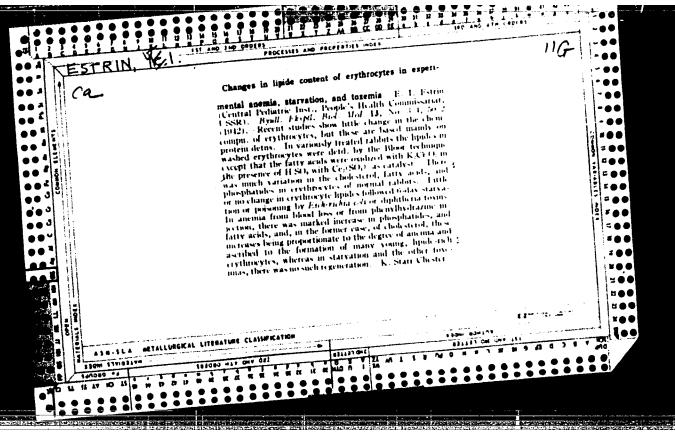
The values of R4 and R3 resistance for all temperatures in a multiple of 10 in the 300 - 500°C range can be obtained from the formula derived from the above formulae; the R5 value is accepted at 30 ohms. There are 2 diagrams and 3 Soviet references.

Card 3/3

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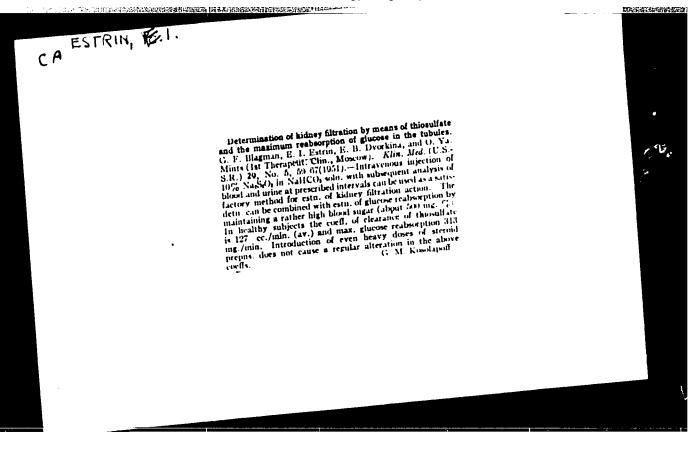


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CIA-RDP86-00513R00041222



ESTRIN, El.

FRADKINA, V.Ye. (Moscow); ESTRIN, E.I. (Moscow).

Protein content of blood in gastric and duodenal ulcers. Klin.med. 31 no.10: (MLRA 6:11)

1. Is 1-y terapevticheskoy kafedry (direktor - deystvitel'nyy chlen Akademii meditsinskikh nauk SSSR professor M.S. Vovsi) TSentral'nogo instituta usovershenstvovaniya vrachey. (Ulcers) (Bleod)

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SETTI/E352 Estrin, E.I. (Moscow) Maksimova, O.P., Seredenko,

AUTHORS:

The Additional Stabilization Effect in Annealing Internally

Work-hardened Austenite

Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1960, Nr 3, pp 57 - 65 (USSR) PERIODICAL:

ABSTRACT:

TITLE:

Indications have been obtained by O.P. Maksimova et al (Ref 7) that annealing at temperatures near and somewhat below the reverse α and γ transformation should produce substantial changes in the state and stability of internally work-hardened austenite. The present work is devoted to this problem. Three type N23GZ alloys of the Fe-Ni-Mn system, A, B and C, were used containing

respectively 0.06, 0.03, 0.06% C, 23.4, 22.9 and 23.7% Ni, 3.30, 3.06 and 2.82% Mn. Phase work-hardening was produced

by forward and reverse transformation of a definite percentage ("degree of phase work-hardening") of the austenite, effected by controlled cooling and warming. The overall martensite transformation effect is plotted against this degree in Figure 1 for alloys B (Curve 1) and C. Figure 2 shows for alloy A the overall effect as a

Card1/4

80979 S/180/60/000/03/010/030 E111/E352

The Additional Stabilization Effect in Annealing Internally Work-hardened Austenite

function of annealing temperature for 0, 30 and 65% degrees of phase work-hardening. Martensite transformation curves are given for alloy B for various annealing temperatures in Figure 3, while Figures 4 and 5 show the change in work-hardened austenite stability in relation to annealing temperature respectively for alloy B at 400 - 575 °C and alloy C at room temperature - 800 °C. Curves illustrating the change in stability with respect to duration (hours) of annealing at various temperatures are given in Figure 6 for alloys B and C (left- and righthand graphs, respectively). To elucidate the nature of changes in the crystal structure of internally workhardened austenite during annealing, the authors studied alloy C in detail. Its hardness, electrical resistance. temperature-dependence of internal friction and fine structure of the internally work-hardened austenite annealed under various conditions were investigated. resistance and internal-friction results are to be reported

Card2/4

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The Additional Stabilization Effect in Annealing Internally Work-hardened Austenite

shortly. The hardness remains constant while the temperature rises to 500-550 C and beyond that begins to fall, reaching the value for austenite which has not been work-hardened (Figure 7). The results of X-ray interference study of alloy C are given in Table 2. The results of the present work confirm the complexity of stability changes of internally work-hardened austenite during gradually increasing annealing. The state produced immediately after the completion of reverse martensite transition does not, contrary to previous ideas, correspond to the highest austenite stability; annealing under definite conditions can increase it further. At least two elementary processes with opposite effect on stability occur during the annealing; they give the observed de-stabilisation and stabilisation. The additional stabilisation at ${}^{l}_{1}$ 00 - 550 ${}^{\circ}$ C is attributed to polygonisation processes occurring in austenite disturbed by phase work-hardening. From the present and previous (Ref 8) work it appears that four pronounced stages exist in the

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80979 \$/180/60/000/03/010/030

The Additional Stabilization Effect in Annealing Internally Work-hardened Austenite

γ-phase stability change during annealing of previously phase work-hardened austenite in type N23GZ alloys: two at temperatures below the recrystallisation temperature. the third near this temperature and the fourth extending from it to 1 150 - 1 200 °C. The authors recommend research to find whether the relations apply to other types of alloy as well as their more detailed study. There are 7 figures, 2 tables and 10 Soviet references.

SUBMITTED: July 30, 1959

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Card 4/4

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S/126/60/009/03/018/033 E111/E452

18.7500

Maksimova, O.P. and Estrin, E.I.

AUTHORS:

The Autocatalytic Effect in the Martensite Transformation

PERIODICAL: Fizika metallov i metallovedeniye, 1960, Vol 9, Nr 3,

pp 426-436 (USSR)

ABSTRACT:

Card 1/4

The authors survey some literature on effects involved in the martensite transformation (Ref 1 to 11), excluding distortions taking place in the lattice of newly formed martensite alpha phase. The object of the present investigation was the examination of the role of elastic deformations arising in the austenite crystal lattice during the martensitic transformation; these could have a definite autocatalytic influence on the further development of the process from its earliest stages. They supplement the considerable experimental evidence on type N23GZ alloys supporting this possibility (Ref 12,13, 14,17; Fig 1,2,3,4 respectively), with their own previously obtained results for several iron-nickelmanganese alloys obtained when investigating the influence of preliminary plastic deformation and other factors on the kinetics of the martensite transformation.

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The Autocatalytic Effect in the Martensite Transformation

This phenomenon, so far incompletely explained, is a relaxation effect (Ref 7,8) involving both elimination of activating faults and formation of inhibiting faults. The authors attribute the autocatalytic effect to the special features of the process giving rise to elastic deformation of the austenite crystal lattice near the martensite crystals formed. These elastic distortions are due to the cooperative mechanism of the transformation and the close association of atomic movements; the relatively high yield-point strength of austenite at low temperatures corresponding to martensite transformation; the small extent of relaxation processes at relatively low temperatures. A contributing factor can be the volume change in phase transition due to different directional growth rates of the martensite crystal. conclusion, the authors maintain that the cooling effect is a more direct characteristic of austenite stability than is the overall cooling + heating; the strictest characteristics are the temperature of the start of Card 3/4 isothermal transformation and its initial speed. There

69695 S/126/60/009/03/018/033 E111/E452

The Autocatalytic Effect in the Martensite Transformation

are 6 figures and 18 references, 15 of which are Soviet and 3 English.

ASSOCIATION: Institut metallovedeniya i fiziki metallov TsNIIChM (Institute of Metallurgy and Physics of Metals TsNIIChM)

SUBMITTED: November 9, 1959

Card 4/4

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18.7500

Maksimova, O. P., Estrin, E. I.

TITLE:

The Effect of the Phase Hardening of Austenite $\$

PERIODICAL:

Doklady Akademii nauk SSSR, 1960, Vol. 132, No. 6,

pp. 1303 - 1306

TEXT: The authors describe investigations they carried out of the influence exerted by phase hardening on the kinetics of martensite transformation. The results were obtained by means of thermomagnetic, X-ray, and metallographic studies. Phase hardening was carried out by sharp quenching to various temperatures followed by heating, so that the transformation $\alpha \longrightarrow \gamma$ was secured. It turned out that direct and inverse martensite transformation cause stabilization of austenite. The influence exerted by phase hardening upon the transformation in the case of continuous cooling manifested itself in temperature rise at the beginning of transformation. The influence exerted by the transformations $\gamma \longrightarrow \gamma$ on isothermal martensite transformation manifested itself in an increase of the martensite point. The metallographic studies disclosed

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The Effect of the Phase Hardening of Austenite S/020/60/13

S/020/60/132/06/21/068 B014/B007

the formation of a structural disturbance. Moreover, it was found that phase hardening changes the stability of various austenite zones, and that the martensite crystals formed in the cooling of austenite are considerably smaller than those formed in the cooling of annealed austenite. The diagrams of Fig. 2 graphically show the structural changes, and details of such changes are discussed. Diagram B in Fig. 2 shows the broadening of the line (311) of austenite, and diagram V shows the microhardness. The complex interrelations show that the annealing process takes place not only within a range of temperature in which quick recrystallization occurs, but also at considerably lower temperatures. Finally, the results obtained by investigations of the annealing process of strainhardened austenite are given. It was found that during annealing in the temperature range of from 450 to 550°C the stabilization process is increased. A broadening of the X-ray interference lines is observed already at 350°C. Thus, it may be said that the change in the crystal structure of austenite in direct and inverse martensite transformation leads not only to a stabilization of austenite, but is also the cause of the changes occurring as a result of subsequent annealing, as is shown by the increasing stability of austenite against martensite transformation. There

Card 2/3

"APPROVED FOR RELEASE: Thursday, July 27, 2000

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The Effect of the Phase Hardening of Austenite

5/020/60/132/06/21/068 B014/B007

are 3 figures and 10 Soviet references.

ASSOCIATION: Institut metallovedeniya i fiziki metallov Tsentral'nogo nauchno-issledovatel'skogo instituta chernoy metallurgii (Institute of Metallography and Metal Physics of the Central Scientific Research Institute of Ferrous Metallurgy)

PRESENTED: March 7, 1960, by G. V. Kurdyumov, Academician

SUBMITTED: March 2, 1960



Card 3/3

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S/020/60/134/004/019/023 B004/B064

AUTHORS:

Maksimova, O. P., Soboleva, N. P., Estrin, E. I.

TITLE:

The Autocatalytic Character of the Martensite Transformation

PERIODICAL3

Doklady Akademii nauk SSSR, 1960, Vol. 134, No. 4, pp. 871-874

TEXT: In the introduction, the authors give a survey of publications on martensite transformation (Refs. 1-24). They investigated the autocatalytic effect of this process by analyzing the experimental material so far available and by new experiments. On the basis of data found in the course of the last ten years for martensite transformation in strong cooling and subsequent heating, the ratio between the heating effect M heat and the effect M cool of the previous cooling was determined for Fe-Ni-Mn and Fe-Cr-Ni alloys (Fig. 1). The alloys [124] (N24G3) with 0.065% C, 23.7% Ni, 2.82% Mn and H23[4 (N23G4) with 0.05% C, 23.0% Ni, 4.00% Mn are mentioned. The curves obtained show a distinct maximum near the ordinate (M heat M cool). Therefore, the martensite crystals formed already

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The Autocatalytic Character of the Martensite Transformation

S/020/60/134/004/019/023 B004/B064

at low temperature exerted a strong stimulating effect on the subsequent transformation. With a given M cool, M heat is a constant for each alloy that does not depend on the preliminary treatment. Experimentally, the course of isothermal transformation was investigated in an Fe-Ni-Mn alloy at -90°C as a function of the martensite (M_1960) formed at -196°C (Figs. 2,3). Also in this case the autocatalytic character of transformation was confirmed. The rate of transformation increases rapidly up to M_1960 = 5%; a lesser increase was observed at M_1960 = 10%. Furthermore, isothermal transformation was investigated under conditions under which the transformation rate is low. As may be seen from Fig. 4, the transformation rate undergoes an acceleration that even after three hours has not yet reached its maximum. There are 4 figures and 24 references: 14 Soviet, 5 US, 1 British, 1 Chinese, 1 French, and 1 Japanese.

ASSOCIATION: Institut metallovedeniya i fiziki metallov Tsentral nogo nauchno-issledovatel skogo instituta chernoy metallurgii im.

I. P. Bardina (Institute of Metal Studies and Physics of Metals of the Central Scientific Research Institute of Ferrous

Metallurgy imeni I. P. Bardin)

20213

5/126/61/011/002/012/025 E193/E483

187500

AUTHORS:

Card 1/4

E.I. Zuyeva, O.M. Maksimova, O.P. and

Piguzov

On the Problem of Internal Friction Effects TITLE:

Associated With the Direct and Reverse Martensitic

Transformation

Fizika metallov i metallovedeniye, 1961, Vol.11, No.2, PERIODICAL:

pp.252.260

The object of the present investigation was to study the phenomena of "phase work-hardening". I.e. the structural changes brought about in the Y-phase of the 73.5 Fe 23.7 Ni-2.8 Mm alloy during the martensitic transformation. variation of the kinetics of the martensitic transformation during cooling was studied as well as the character of the temperature dependence of internal friction of specimens subjected to one of the following heat treatments: {1} young transformation, carried (2) γ→α→γ transformation out to various degrees of completion: carried out to attain various degrees of stability of austenite; (3) Y=3 x → Transformation, followed by annealing under conditions

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On the Problem of Internal

ensuring the maximum supplementary stabilization of the γ -phase (1 h at 525°C). The kinetics of the martensitic transformation were studied by the magnetostriction measurements, the torsional vibration method having been used to determine the temperature dependence of internal friction. In both cases, wire specimens (0.7 mm in diameter) preliminarily varuum annealed at 1100°C were used, extra precautions having been taken to avoid any plastic deformation of the specimens during handling. Specimens, containing various proportions (11, 24, 28 and 48%) of martensite, were prepared by rapid quenching in liquid nitrogen, followed by heating to room temperature at various heating rates. The a = Y transformation was carried out by immersing the specimens for 10 sec in a salt bath at 540°C and water quenching. The results of the study of the kinetics of the $\gamma \rightarrow \alpha$ transformation in wire specimens confirmed the results obtained earlier on standard specimens (Ref.2 and 4); with increasing degree of "phase work-hardening" the stability of austenite increased after both yard and yarayy transformation. The stability of martensite was further increased by annealing at 525°C. Card 2/4

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On the Problem of Internal

results of the study of the temperature dependence of internal friction can be summarized as follows (1) no anomalies were observed on the internal friction curves for the fully annealed (ii) curves for specimens that had undergone partial γωλα transformation had the following specific features: a peak (A) at 170°C, the magnitude of which increased with increasing proportion of martensite in the specimens, a peak (B) at 290°C, a ledge (C) at 580°C. a ledge (D) at 730°C. a sharp peak (E) at (iii) after the Y-32-37 transformation, the specific features (A) and (C) disappeared completely and the ledge (D) almost 810°C; completely, peak (B) becoming more pronounced and shifted to a lower temperature (approx 250°C) (1v) after a supplementary annealing, the height of peak (B) decreased. Since the specific features (A), (D) and (E) have no direct bearing on the problem under investigation, peaks (B) and (C) are discussed in detail. It is shown that the internal friction peak at 250°C is associated with the re-extentation of pairs of carbon atoms which takes place as a result of stresses set up in the alloy, it being postulated that the relexation processes leading to the appearance of peak (B) cannot take place in the absence of Card 3/4

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On the Problem of Internal ... S/126/61/011/002/012/025 E193/E483

lattice distortions. Regarding the peak (C), the fact that it was observed only in specimens containing martensite and that it occurred in the temperature range of the reverse martensitic transformation indicated that this peak is due to the increase in the internal friction, caused by the army transformation.

K.M.Rozin, B.N.Finkel'shteyn, P.Ke and Ch.Tszen are mentioned for their contributions in this field. There are 4 figures, I table and 20 references: 13 Soviet and 7 non-Soviet.

ASSOCIATION: Institut metallovedeniya i fiziki metallov TSNIICHM (Institute of Science of Metals and Physics of Metals, TSNIICHM)

SUBMITTED: March 12, 1960

Card 4/4

24.2200 (1137,1144,1147) 187500

30045 \$/032/61/027/011/016/016 B104/B138

AUTHOR:

Estrin, E. I.

TITLE:

Device for studying the kinetics of phase transformations in

metals

PERIODICAL: Zavodskaya laboratoriya, v. 27, no. 11, 1961, 1423 - 1425

TEXT: The instrument described here is a non-equilibrium a-c bridge which measures the amount of the ferromagnetic phase in a specimen. The instrument consists of an a-d measuring bridge and a thermostat which permits the determination of the changes of the magnetic properties of specimens at low temperatures. Fig. 1 shows a diagram of the measuring bridge. Fig. 3 shows a diagram of the entire device. The isopentane, with which the Dewar vessel (1) is filled, is cooled by means of liquid nitrogen flowing through the cooling spirals 2). The amount of martensite in the specimen is determined by the change in inductance Lx in the measuring bridge. As is shown by the calibration curve the indication of the instrument up to 35% martensite is almost proportional to the amount of martensite. There are 4 figures.

30045 \$/032/61/027/011/016/016 B104/B138

Device for studying the...

ASSOCIATION: Tsentral'nyy nauchno-issledovatel'skiy institut chernoy metallurgii im. I. P. Bardina (Central Scientific Research Institute of Ferrous Metallurgy imeni I. P. Bardin)

Fig. 1. Diagram of the a-c measuring bridge. Legend: (1) \exists $\Pi \cap 09$ (EPP-09) measuring bridge; (2) 28 \bowtie (28 \bowtie M) measuring amplifier (3) \bowtie M82 (\bowtie 82) millivoltmeter; (4) \exists $\Pi \cap 09$ (ZG-12M) a-c generator. Fig. 3. Diagram of the device. Legend: (1) Dewar vessel; (2) cooling coil, (3) Dewar vessel (nitrogen), (4) Dewar vessel (5) valve (6) \exists $\Pi \cap 09$ (EPV-01) potentiometer; (7) heater; (8) thermocouple (9) copper shielding (10) mixer; (11) thermocouple (12) millivoltmeter. A) liquid nitrogen; B) measuring bridge

Card 2/1 2

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00041222

S/020/62/142/002/016/029 B104/B138

AUTHORS:

Maksimova, O. P., and Estrin, E. I.

TITLE:

Variation in the kinetics of martensite transformation under the influence of previously formed martensite

PERIODICAL:

Akademiya nauk SSSR. Doklady, v. 142, no. 2, 1962, 330-333

TEXT: The influence of an existing partial martensitic structure on the rate of martensite transformation was studied on four different H 23P4 (N23G4) alloys (Table 1). In specimens cooled down to -196°C a specified amount of martensite was produced by isothermal transformation at this temperature. The specimens were then quickly transfered to a tank, and a special device was used to record the martensite development at the tank temperature. The martensite point T_M of the four alloys after annealing is between -70 and -90°C, and after partial martensitic transformation at -196°C, it (T_M) lies between +15 and +55°C. The initial rate of isothermal transformation grows with transformation temperature (Fig. 1), and the range increases (more than 100°). A very sharp increase in T_M occurs if Card 1/4°

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Variation in the kinetics ...

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only 1% martensite formed at -196° C is present. Further increase of up to 10% in pre-formed martensite causes only slight further increases in TM. It is known that martensitic transformations can be produced above $\mathbf{T}_{\underline{\mathbf{M}}}$ by plastic deformations. A point $\mathbf{M}_{\underline{\mathbf{d}}}$ exists above which deformation ceases to cause this transformation. M_d is a little below $T_{\underline{M}}^{\prime}$. Comparison of $\mathbf{M}_{\mathbf{d}}$ and $\mathbf{T}_{\mathbf{M}}^{\prime}$ leads to the conclusion that distortions of the austenite lattice caused by the martensite transformation (i.e. due to internal effects) reduce the amount of energy of elastic distortions dissipated in the nucleation of the new phase to a greater extent than do the defects due to plastic deformations (i.e. external effects). G. A. Levin participated in the experimental work. There are 1 figure, 5 tables, and 8 references: 5 Soviet and 3 non-Soviet. The three references to English-language publications read as follows: L. Kaufman, M. Cohen, J. Metals, 8, no. 10 (II), 1393 (1956); A. W. McReynolds, J. Appl. Phys., 20, no. 10, 896 (1949); J. B. Hess, C. S. Barret, Trans. AIMME, 194, 645 (1952).

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Institut metallovedeniya i fiziki metallov Tsentral'nogo nauchno-issledovatel'skogo instituta chernoy metallurgii im. I. P. Bardina (Institute of Metallography and Physics of Metals of the Central Scientific Research Institute of

Ferrous Metallurgy imeni I. P. Bardin)

PRESENTED:

ASSOCIATION:

August 4, 1961, by G. V. Kurdyumov, Academician

SUBMITTED:

August 4, 1961

Table 1. Composition of alloys.

Fig. 1. Initial rate of martensitic transformation, and isothermal martensitic transformation with 4.3% previous partial transformation as functions of temperature.

Legend: (a) rate of transformation in 10/min (b) quantity of isothermal martensitic (1) after annealing (2) after partial transformation at -196°C (3) maximum rate of transformation after annealing.

Card 3/4

ESTRIN, E.I.

Nature of certain peculiarities of martensite transformations. Fiz.met.i metalloved. 15 no.4:638-640 Ap '63. (MIRA 16:6)

1. Institut metallovedeniya i fiziki metallov TSentral'nogo nauchno-issledovatel'skogo instituta chernoy metallurgii.

(Phase rule and equilibrium)

ESTRIN, E.I.

Effect of martensite already formed on the kinetics of further martensitic transformation. Dokl.AN SSSR 148 no.4:818-820 F *63. (MIRA 16:4)

1. Institut metallovedeniya i fiziki metallov TSentral'nogo nauchno-issledovatel'skogo instituta chernoy metallurgii im. I.P.Bardina.

(Martensite) (Metallurgy)

ESTRIN, E.I.

Gertain regularities of martensite transformation. Probl. metalloved. i fiz. met. no.8:187-204 '64. (MIRA 18:7)

L 4185-66 EWP(e)/EWT(m)/EWA(d)/T/EWP(t)/EWP(z)/EWP(b)/EWA(c)

MJW/JD/JW

ACCESSION NR: AP5016534

UR/0126/65/019/006/0929/0932 539.292: 548.53

AUTHOR: Estrin, E. I.

TITLE: Effect of a magnetic field on the martensite transformation

SOURCE: Fizika metallov i metallovedeniye, v. 19, no. 6, 1965, 929-932

TOPIC TAGS: martensitic transformation, pulsed magnetic field, constant magnetic field, nickel steel, manganese steel

ABSTRACT: The effect of a magnetic field of 18.6 kOe (produced in an ordinary electromagnet) on the martensite transformation in 50N19 nickel steel, fin which this transformation has a pronounced "athermio" character was investigated dilatometrically. No changes were found in the overall picture of the transformation when the field was applied; the influence of the field is manifested in a displacement of the martensite point and of the entire martensite curve toward a temperature about 6°C higher. The effect of the same magnetic field on the martensite transformation in an Fe-Ni-Mn alloy of type N2ZGZ was also studied. In this case also the effects of the magnetic field can be explained in terms of the thermody-

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SOURCE CODE: UR/0370/66/000/003/0150/0155

AUTHOR: Estrin, E. I. (Moscow)

ORG: none

33 B

TITLE: Kinetics of the isomorphous transformation in iron-rhodium alloys

SOURCE: AN SSSR. Izvestiya. Metally, no. 3, 1966, 150-155

TOPIC TAGS: phase transition, iron alloy, rhodium alloy, martensitic transformation

ABSTRACT: One of the typical first-order metamagnetic transformations, the low-temperature isomorphous transformation in the ordered alloy Fe-Rh, was investigated kinetically in an effort to clarify the general relationships governing the so-called cooperative transformations. The study was made on three Fe-Rh alloys containing 46, 50, and 56 at.% Rh, and some of the experiments were carried out on an Fe-Rh alloy of equiatomic composition. All the specimens were first vacuum-annealed at 1150°C for 3 hr, then furnace-cooled. The metamagnetic transformation studied was found to have the same basic characteristics as the martensitic transformations: it is rapid, does not supercool (is athermic in character), does not develop under isothermal conditions in the presence of the original phase, extends over a certain temperature range, and occurs in the forward and reverse direction with the thermal hysteresis. It is therefore assumed that the characteristics of the transformation

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UDC: 669.15*235

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"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00041222

, ACC NR. AP7005764

SOURCE CODE: UR/0126/67/023/601/01/3/6183

AUTHOR: Korneyev, G. N.; Estrin, E. I.

ORG: Institute of Metal Physics (Institut metallofiziki); TsNIIChERMET im. I. P. Bardin

TITLE: Effect of hot plastic deformation on the kinetics of isothermal transformation of

austenite

SOURCE: Fizika metallov i metallovedeniye, v. 23, no. 1, 1967, 182-183

TOPIC TAGS: metal deformation, austenite transformation, phase composition, pearlite / 41KhN55 steel, Kh8N2 alloy

ABSTRACT: The absence of nonmartensitic products of austenite transformation in the final structure of steel is a prerequisite for an effective thermomechanical treatment (TMT), including high-temperature thermomechanical treatment (HTTMT). In this connection, the effect of plastic deformation of austenite on the kinetics of austenite transformation in the pearlitic and bainitic regions is highly important to practical TMT and HTTMT. In view of the scarcity and contradictory nature of the available literature on this question, the authors investigated the effect of hot plastic deformation of austenite on the kinetics of pearlitic transform-

Card 1/2

UDC: 669.15:539.37

. ACC NR. AP7005764

ation in 4x4x45 mm specimens of 41KhN5S steel (0.41% C, 1.15% Si, 0.55% Mn, 1.62% Cr, 5.02% Ni, 0.002% S and 0.004% P) and Kh8N2 alloy (8.5% Cr, 2.5% Ni) austenized at 900°C for 5 min and deformed 25-27%(in height) by single-pass rolling at 900°C in a laboratory rolling mill, after which they were immediately inserted in the microfurnace of the measuring device, and subjected to isothermal heating at 450-670°C. Findings: hot plastic deformation of the γ -phase leads to a marked acceleration of both pearlitic transformation in the steel and polymorphic $\gamma \rightarrow \alpha$ transformation in the alloy. The incubation period and transformation time markedly shrink following the deformation, while the temperature range of the transformation expands. This may in principle be associated both with the acceleration of the diffusion of alloy elements and carbon and with the acceleration of the period of lattice rearrangement. The latter factor plays a decisive role as demonstrated by the discovery of acceleration of polymorphic transformation in the alloy. These findings indicate that during practical employment of HTTMT an allowance must be made for the possible decrease in stability of austenite following hot plastic deformation. Orig. art. has: 3 figures.

SUB CODE: 13, 20, 11/ SUBM DATE: 31Mar66/ ORIG REF: 004

Card 2/2

LIPKOVICH, Z.; ESTRIN, G.; MIROSHNICHENKO, D.; TRUBITSYN, N.; STRELKOV, I., master; LARIONTSEV, A.; ROMANOVICH, K.

Experience of innovators and efficiency promoters. Stroitel' 8 no.10:25-26 0'62. (MIRA 15:11)

1. Predsedatel' komiteta professional'nogo soyuza rabochikh stroitel'stva i promyshlennosti stroitel'nykh materialov stroitel'nogo uchastka No.108 tresta Mosstroy No.18 (for Lipkovich).

(Building—Technological innovations)

ESTRIE G.B. (Voronezh)

Technic in setting backward dislocations of the elbow. Ortop., traym.
i protez. 17 no.1:39-40 Ja-F '56.
(DISLOCATIONS
elbow, setting technic)
(ELBOW, dislocation
setting technic)

ISTRIN, G.B.

Significance of Manassein's journal "Vrach" (1880-1901) in the development of surgery in Russia; its 75th anniversary. Vest.khir. 77 no.3:128-132 Mr '56. (MLRA 9:7)

1. Iz lazareta voyskovoi chasti 23435 (nach. - G.V.Estrin). (PERIODICAIS, hist.
"Vrach" in Russia)

MILASHKIN, A.G., kand.med.nauk; ESTRIN, G.B.

Fifthe scientific session of the Research Institute for Experimental Surgical Apparatus and Instruments. Vest.khir. 89 no.9: 147-149 S '62. (MIRA 15:12) (SURGICAL INSTRUMENTS AND APPARATUS—CONGRESSES)

ESTRYH L. M. (Kiray, 71, ul. Konstantinovskaya, d.33/8, kv. 6); MEL'NIK, A.N.

Carcinosarcoma of the breast. Nov. khir. arkh. 5:115-117 S-0 '58. (MIRA 12:1)

 Kafedra patologicheskoy anatomii (zav. - zasl. deyateli nauki prof. M. K. Dali) Kiyevskogo instituta usovershenstvovaniya vrachey. (BREAST--CANCER)

ESTRIN, I.M., kand.med.nauk (Kiyev)

Problem of mycosis of the thyroid gland. Probl. endok. i gorm 4 no.4:111-113 J1-Ag '58 (MIRA 11:10)

1. Iz kafedry patologicheskoy anatomii (zav. - zaslushennyy deyatel' nauki prof. M.K. Dal') Kiyevskogo instituta usovershenstvo-vaniya vrachey.

(THYROID GLAND, dis.
fungus dis. (Rus))
(FUNGUS DISEASES,
thyroid gland (Rus))

ESTRIN, I.M., kand.med.nauk; MAKUKHA, A.L.

Xanthomatous tumor of the accessory nasal sinuses. Zhur. ush., nos. i gorl, bol. 20 no.6:77-79 N-D '60. (MIRA 15:2)

1. Iz kafedry patologicheskoy anatomii (zav. - zasluzhennyy deyatel† nauki prof. M.K.Dal;) i otorinolaringologicheskoy kafedry (zav. - zasluzhennyy deyatel¹ nauki prof. A.I.Kolomiychenko) Kiyevskogo instituta usovershenstvovaniya vrachey.

(NOSE, ACCESSORY SINUSES OF_TUMORS)

YESTRIN, I.M. [Estrin, I.M.]; SHAL'MAN, R.D.

Congenital cyst of the lungs. Ped., akush. i gin. 22 no.5:31 '60. (MIRA 15:6)

1. Kafedra petologicheskoy anatomii (zaveduyushchiy - zasluzhennyy deyatel' nauki prof. M.K. Dal') Kiyevskogo instituta usovershenstvovaniya vrachey (direktor - dotsent V.D. Bratus').

(CYSTS)

(LUNGS-TUMORS)

ESTRIN, I. M.

Primary cancer of the pleura. Vrach. delo no.6:18-23 Je '62. (MIRA 15:7)

1. Kafedra patologicheskoy anatomii (zav. - zasluzhennyy deyatel' nauki prof. M. K. Dal') Kiyevskogo instituta usovershenstvovaniya vrachey.

(PLEURA-CANCER)

ESTRIN, I. M.; BURKOVSKAYA, A. P.

Primary malignant tumors of the pericardium. Grud. khir. 4 no.3: 89-91 My-Je *62. (MIRA 15:7)

1. Iz kafedry patologicheskoy anatomii (zav. - prof. M. K. Dal') Kiyevskogo instituta usovershenstvovaniya vrachey.

(PERICARDIUM-CANCER)

MOREYNIS, Yu.A.; ESTRIN, I.M.

Some data on the toxicity of sevin. Vrach.delo no.1:100-104
Ja 163. (MIRA 16:2)

l. Kafedra gigiyeny (zav. - dotsent N.A. Baran) i kafedra patologicheskoy anatomii (zav. - zasluzhennyy deyatel' nauki, prof. M.K. Dal') Kiyevskogo instituta usovershenstvovaniye vrachey. (SEVIN—TOXICOLOGY)

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00041222

SUDENKO, V.M.; ESTRIN, I.M.

Rupture of the pulmonary artery. Vrach. delo no.12:119-121 D 163. (MIRA 17:2)

1. Kafedra patologicheskoy anatomii (zaveduyushchiy - zasluzhennyy deyatel' nauki, prof. M.K. Dal') Kiyevskogo instituta usovershenstvovaniya vrachey i patologoanatomi-cheskoye otdeleniye Cherkasskoy ohlastnoy bol'nitsy.

'APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00041222

L 54653-65

ACCESSION NR: AT5014960

UR/000D/65/000/000/0059/0061

AUTHOR: Sivachenko, T. P.; Estrin, I. M.

TITLE: Morphological changes in some organs of white rats due to neutron irradiation

SOURCE: All UkrSSR. Institut fiziologii. Biologicheskoye deystviye neytronnogo izlucheniya (Biological effect of neutron radiation). Kiev, Naukova dumka, 1965,59-61

TOPIC TAGS: neutron irradiation, biological effect, fast neutron, radiation injury, RBE, rat

ABSTRACT: Morphological changes in selected organs of white rats were studied after various doses of neutron irradiation. Thirty-two male white rats, weighing 110-140 g, were irradiated with fast neutrons in a specially equipped nuclear reactor (lethel dose- 300 rad; sublethal doses- 175 and 200 rad). Symptoms of radiation sickness in rats subjected to a sublethal radiation dose (200 rad) included noticeable sluggishness, diarrhea, and in half the animals, rhinitis, conjunctivitis, and loss of weight. Adynamia, loss of appetite, and then diarrhea and weight loss preceded the death (on the 9th day) of snimals exposed to a lethal radiation dose. Macroscopic examination showed irregular blood supply in internal organs and some focal hemorrhages in subcutaneous tissue and the lungs. Miscroscopic examination revealed

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changes in brain tissue (edema, hemorrhages of small blood vessels, vacuolation of ganglionic cells, and cirrhosis). Three days after irradiation, reticular cells and megakaryocytes appeared in the bone marrow, and there was a decrease in the differentiation of red and white cells. By the tenth day, pathological changes included severe destruction of the bone marrow, focal hemorrhages, and small focal accumulations of plasma. Disintegration of lymphocytes occurred in the lymph nodes and the spleen. Plethora, recent hemorrhages, and focal proliferation of cells in interveolar septa were observed in the lungs. In the gastrointestinal tract, edema of the submucosa occurred with subsequent enrichment of the mucous membrane with plasma. Irregular blood supply, dystrophy, and then focal proliferation of Kupffer cells were noted in the liver. Hyperemia, swelling or shrinkage of some chromophil cells, and turbidity of their protoplasm were observed in the hypophysis of the pituitary gland. Hyperemia, vacuolation of the epithelium, and a decrease in the follicular dimensions were among the changes observed in the thyroid gland. In the adrenal glands, hemorrhages and disintegration of nuclei in cells of the reticular zone were noted. Plethora and focal dystrophic changes were observed in the testes. Experimental data indicate that, in general, changes in several organs of rats subjected to neutron irradiation correspond to changes during other types of irradiation. Unusual changes with neutron irradiation are proliferation of cells in the interalveolar septa of the lungs and proliferation of Kupffer cells in the liver. In both cases metabolic disturbances may be responsible for the changes.

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Advanced Training of Th	institut usovershenstvovaniya ysicians); Institut fiziologi Physiology, AN UkrSSR) ENCL: 00	a vrachey (Kiev Insti i im. A. A. Bogomol' SUB CODE: IS	tute for tsa
NO REF SOV: 006	OTHER: 000	ATD PRESS: 4026	
Card 3/3			

ESTRIN, K.M.

Solving problems in geometry with application of trigonometry in the 8th grade. Uch.zap.Ped.inst.Gerts. 218:279-299 '61.

(Geometry--Study and teaching)

"APPROVED FOR RELEASE: Thursday, July 27, 2000

CIA-RDP86-00513R00041222

14(%)

sov/66-59-4-14/28

AUTHOR:

Estrin, L., Engineer

TITLE:

Repairing of an Ammonia Two-Stage Vertical Compressor

PERIODICAL:

Kholodil'naya tekhnika, 1959, Nr 4, pp 52-55 (USSR)

ABSTRACT:

The article describes a grinding and honing machine which is used for repairing ammonia two-stage vertical compressors of the type PBSD-4-18 at the Kaluga Cold Storage Plant. The machine consists of an 1.7 kw electric motor, which by means of a pulley drive and a worm reducer (1:10) actuates a spindle, at the end of which the honing head is mounted, the moving parts of the machine are balanced by counterweight. There are two sizes of honing heads, one having a diameter of 230 mm and the other of 178 mm; the former has a cutting speed of 72 m/min and the latter of 56 m/min at a revolving speed of the spindle of 100 rpm. Liquid kerosene, with or without an addition of 10-20% machine oil, is used as a coolant. In the process of honing the liquid flows into the crank case, from which it is pumped back into the cylinder. The machine is guaranteed for accurate honing up to 0.03 - 0.05 mm of conicity or

Card 1/2

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Repairing of an Ammonia Two-Stage Vertical Compressor

SOV/66-59-4-14/28

ovalness, which is permissible. An increase of the diameter of the cylinder after its honing amounts to 0.1 - 0.2 mm only. The repair work with this machine is cheaper than with any other machine or method. There are: 2 tables, 2 diagrams and 1 photo.

Card 2/2

Doc Med Sci

ESTRIN, L. M.

Dissertation: "Thermal Burns and their Treatment." 14/2/50

Central Inst for Advancement of Physicians

so Vecheryaya Moskva Sum 71

ESTRIN, M., kandidat tekhuicheskikh nauk, laureat Stalinskoy premii; MISHREVICH, G.

> Excavator with a soil slinger. Znan.sila 35 no.7:24-25 J1 160. (MIRA 13:7) (Excavating machinery)

Plastics used in the machinery of grain-processing enterprises. Muk.-elev. prom. 26 no. 11:20-22 N '60. (MIRA 13:11)

1. Starshiy inzhener Glavsnaba Gosudarstvennogo komiteta Soveta Ministrov SSSR po khlebosnabzheniyu (for Mestechkin). 2. Spetselevatormel'stroy (for Estrin. Ageyev). (Grain--Handling machinery) (Plastics)

(Grain--Milling machinery)