

A 813

Cement

Hydraulic slag anhydrite cement. P. P. HUDNIKOV.
Novosti Tekhniki, 10 [21 33 35 (1941)]... in
Chem. Zentr., 1942, I [21] 3893 94. As only about 25%
of the blast-furnace slag is put to profitable use in Russian
foundries, a long series of experiments were made to dis-
cover its further application. Good results were obtained
by grinding dried basic Martin, Bessemer, and foundry
slags with 5 to 10% anhydrite (gypsum fired to 500° to
700° or natural anhydrite) as well as 3 to 5% dolomite.
After storage in water for 28 days, a resistance to pressure
of 180 to 335 kgm. per cm² depending on the mixing
proportion (1:3 with standard sand) was obtained. Sug-
gestions for the manufacturing process and uses of these
clinker free blast furnace anhydrite slag cements are given.
M.V.C.

Budnikov, P.P.

BC

Calcium sulphate as a source of sulphur chlorides. I. Chlorination of calcium sulphate in presence of reducing agents. II. Optimum conditions for the chlorination process. P. P. Budnikov and E. I. Kretsch (*J. Appl. Chem. Russ.*, 1941, 14, 747-764, 755-765; cf. A., 1936, 1211).—I. When the mixture CaSO_4 (gypsum) + 4C (lignin C) was chlorinated over the range 225–850°, the CaSO_4 began to decompose at 345° to give S chlorides (I), the yield of S as SO_2 rising rapidly as the temp. increased to 725° (96% yield). The max. yield of S at 740–760° was obtained with the mixture CaSO_4 + 3C. Under these conditions, max. yields were obtained using soot or lignin C or sugar C (95.5–96.7%), and the lowest yield with coke (87.4%); anthracite, bone C, or electrode C gave intermediate yields. At the optimum conditions [740–750°, CaSO_4 + 3C (lignin)], the reaction was very rapid, a 96% yield being obtained in 15 min. The addition of NaCl or Na_2SO_4 (0.1 g.-mol. per g.-mol. CaSO_4) increased the speed of the reaction at 630–640°; addition of Fe_2O_3 or of SiO_2 decreased the yield of S. All experiments were carried out with small samples.

II. Repetition confirmed the above results for larger quantities of the reactants. The optimum temp. for the prep. of (I) by chlorinating the stoichiometric mixture CaSO_4 + 3C (anthracite) + 0.1M- Na_2SO_4 (all previously baked together at 600–800°) was 700–750°. Chlorination of the stoichiometric mixture CaSO_4 + 4C + 0.1M- Na_2SO_4 produced both CS_2 and (I). The heat produced during these reactions is calc.

N. G.

www 3 11

ME

A.C.S.

Refractive

Interaction of kaolin and coal at high temperatures. I.
P. HUBNIKOV AND E. Z. LAMHART. *Compt Rend Acad.
Sci. R.S.S.* 32, 31 (1941); *Brit Chem Phys Abs*
B, 1942, I, Nov, 400. Appreciable quantities of SiC and
 α -Al₂O₃ were formed when a kaolin and a clay were each
heated with 25% of oil-gas coke at 1650° to 2000°.

C-4

Anhydrite cement. P. P. BUDNIKOV. Abstracted in *Visti Akad. Nauk Ukr. R.S.S.R.*, 1942, p. 43.—B. investigated the manufacture of anhydrite cement from gypsum and anhydrite found in the Bashkir Republic of the Soviet Union. The addition of various catalysts in amounts of 1 to 3% during the hydration of the anhydrite was found to have a practical value for "revivification" of the anhydrite and the manufacture of cement. On the basis of extensive laboratory experiments and semicommercial tests, the anhydrite cement is prepared by calcining the gypsum at 600° to 700° (or drying the natural anhydrite) and grinding with suitable additions, such as bisulfate or sodium sulfate (0.6%) and copper sulfate (8%). The cement is being made commercially in Ufa. B.Z.K.

3-3-46

PROCESSES AND PROPERTIES INDEX

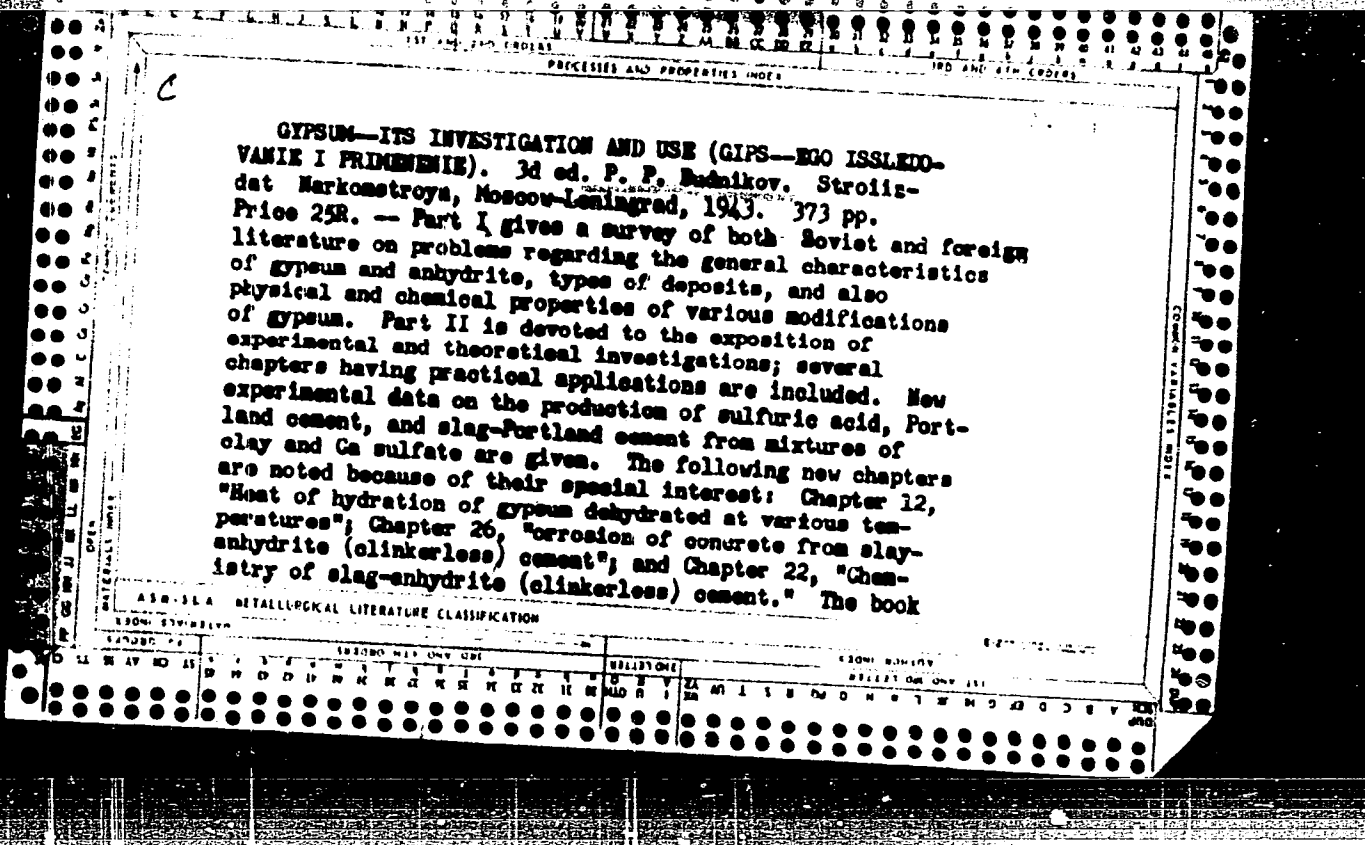
EXTRACTION OF ALUMINA FROM KAOLIN BY MEANS OF SULFUR DIOXIDE. P. P. BYDOROV AND I. I. RIVLIN. *Doklady Akad. Nauk S.S.S.R.*, 37 (3) 121-23 (1942).—Washed clay (Vladimir) containing 63.34 kaolinite, 7.4 feldspar, and 8.26% free quartz served as the raw material. Analysis showed SiO₂ 53.02, CaO 0.67, Al₂O₃ 32.95, MgO 0.45, Fe₂O₃ 1.70% (loss on ignition 11.44%). The clay was calcined at 700° and 800° and mixed with water; SO₂ was passed through the mixture for 2 hr. while it was being stirred in a vessel at 85° and atmospheric pressure. The liquid was periodically decanted and the residue treated with SO₂. By repeated leaching it was possible to extract 94.8% of the alumina in the kaolin of the sample calcined at 700° and 95.4% from the kaolin of the sample calcined at 800°. Insignificant amounts of Fe and small amounts of silica were also extracted.

B.Z.K.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

GROUP #4

GROUP #4	SECTION 410 CHEMISTRY	SECTION 420 METALLURGY	SECTION 430 PHYSICS	SECTION 440 MECHANICS	SECTION 450 ELECTRICITY	SECTION 460 CHEMISTRY	SECTION 470 METALLURGY	SECTION 480 PHYSICS	SECTION 490 MECHANICS	SECTION 500 ELECTRICITY



X

was proofread carelessly. The excellent literature refer-
ences would have far greater value if they were arranged
together in one section at the end of the book instead of
being split up.
B.Z.K.

1ST AND 2ND ORDERS

PROCESSES AND PROPERTIES INDEX

C

Production of ammonium sulfate and Portland cement from a mixture of gypsum (anhydrite) and blast-furnace slag. P. P. BUDNIKOV. *Zhur. Priklad. Khim.*, 16 [1 2] 7-9 (1943).—The mixture of blast-furnace slag and gypsum was wet-ground to pass sieves having 4900 openings/cm.² (10% residue) and 900 openings/cm.² (0.2% residue) and treated with ammonium carbonate at about 40° while being agitated. The yield of ammonium sulfate was 96.4%. The residue was filtered off without difficulty and had a moisture content of about 20%. The residue was fired in an electric furnace at 1400° and yielded a normal Portland cement clinker containing SiO₂ 23.73, Al₂O₃ 3.47, Fe₂O₃ 2.34, CaO 68.26, MgO 1.10, MnO 0.40, and SO₃ 0.38%; the coefficient of saturation was 0.93. The clinker was ground with (1) 2% gypsum, (2) 5% gypsum and 70% slag, and (3) 15% anhydrite and 70% slag. All samples of cements passed the physicommechanical tests.

B.Z.K.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS

1ST AND 2ND COLUMNS PROCESSES AND PROPERTIES INDEX 3RD AND 4TH COLUMNS

c

Separation of sulfur from a mixture of blast-furnace slag and anhydrite in the manufacture of cement. P. P. BUNNIKOV AND I. I. RIVLIN. *Zhur. Priklad. Khim.*, 16(11):11-14 (1943).--Basic blast furnace slag (1.34% S and 1.21% SO₂) was molten at 1400° to 1480°, and 5 to 10% of anhydrite was added. The liberated SO₂ was separated from the molten mass by an air stream. Extraction of S was 86.6% with the addition of 8% anhydrite. The slag was ground with 5 to 10% anhydrite and 5% dolomite calcined at 900°. The slag anhydrite cement (1:3) showed a tensile strength of 30 kg/cm² and a compressive strength of 300 kg/cm² (water storage). The sulfide S in the slag was increased from the original 1.34% to 2.1%, and this improved the hydraulic properties of the basic blast-furnace slag. B.Z.K.

ASME-SLA METALLURGICAL LITERATURE CLASSIFICATION

RECORD NUMBER 6271

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range.

B Z K

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B-3 - 45

Hydraulic cement from acid blast-furnace slags. P. P. GUNIKOV. *J. Applied Chem. (U.S.S.R.)*, 16, 337-41 (1943); *Brit. Abstracts*, 1945, March, B1, 102 -- Acid slags having $\text{CaO}:(\text{SiO}_2 + \text{Al}_2\text{O}_3)$ not less than 0.7 and $\text{SiO}_2:\text{Al}_2\text{O}_3$ not less than 2.2 give, with 10% CaSO_4 and 1 to 3% CaO or 3 to 7% $\text{CaO} + \text{MgO}$ (from dolomite at 1030° to 1150°), hydraulic cements of standard properties. Instead of $\text{CaO} + \text{MgO}$, Portland cement clinker can be used.

1ST AND 2ND ORDERS PROCESSES AND PROPERTIES INDEX 3RD AND 4TH ORDERS

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The problem of production of alite cement. P. I. Budnikoy and M. I. Streikov. *Doklady Akad. Nauk S. S. S. R.* 40, 23-6(1943); *Compt. rend. acad. sci. U. R. S. S. S. R.* 20-1(1943) (in English).—Alite ($2CaO \cdot SiO_2$) is obtained by first calcining a mixt. of CaO or $CaCO_3$ (II) and SiO_2 to form $2CaO \cdot SiO_2$, then adding the requisite amt. of CaO or I and recalcining at $1450-1800^\circ$ for 30-45 min. All materials should be finely ground. On admixing Al_2O_3 (III) in amts. up to 10% (calcd. as $CaO \cdot Al_2O_3$) the caking capacity of the clinker and its hardness increased continuously, while the clinker's activity decreased. In the com. manuf. of alite clinker by double calcining, the amt. of such admixts. should be kept to a min. When calcining is carried out in a slightly reducing atm., factors favoring caking (e. g., admixt. of II or MgO) impart a green color to the clinker. J. W. Perry

A S M - S L A METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND ORDERS 3RD AND 4TH ORDERS

OPEN COMMON ELEMENTS COMMON TABLETS INDEX

1ST AND 2ND LETTER AUTHOR INDEX UNLETTERED 3RD AND 4TH LETTERS P- GROUPS MATERIALS INDEX

R

PREPARATION OF MAGNESIA FROM DOLOMITE AND ITS USE FOR PRODUCING REFRACTORIES. *Doklady Akad. Nauk S.S.S.R.*, 41, 222-24 (1943); *Compt. rend. acad. sci. U.R.S.S.*, 41, 210-12 (1943) (in English).—Approximately 90% of the MgO in dolomite (I) can be recovered in moderately pure form by calcining I at 1200° for 1 hr., cooling, treating with a saturated solution of NH₄Cl (II) at 15 to 18° for 1 hr. and filtering off the undissolved MgO. High calcination temperature of treatment with II is given. However, lowering the concentration of II to 10% had only a slightly adverse effect. Satisfactory refractory products were obtained by slowly heating mixtures consisting of 25, 30, and 40% of serpentine (3MgO·2SiO₂·2H₂O) with, respectively, 75, 70, and 60% of the MgO (produced as described) and then cooling. The possibility of including the above-outlined process for separating MgO as an integral step in the Solvay process is mentioned.

1ST AND 2ND LETTERS UNLETTERED 3RD AND 4TH LETTERS P- GROUPS MATERIALS INDEX

ca

No. 9,

20

On the problem of manufacturing of high-strength gypsum. P. P. Rudnik, *Compt. rend. acad. sci. U. R. S. S. 41, 286-90 (1943) (in English)*.—Steaming gypsum under a range of conditions (e. g., for 7-8 hrs. under 1.3 atm. or for 3 hrs. under 8 atm.) converts it into a felted mass of acicular crystals of semihydrate. The length of the crystals varies from 0.1 to 18 mm. In contrast, the semihydrate produced by calcining at 170° is mostly powder material devoid of well developed crystal structure. After setting the acicular semihydrate retains its felted structure. Compression strengths of 133 kg./cm.² and 280 kg./cm.² after 1 and 7 days, resp., of setting have been observed.

J. W. Perry

ASS-3LA METALLURGICAL LITERATURE CLASSIFICATION

10000 417 047 081

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PROCESS AND PROPERTIES INDEX

20

ca

No. 9

Production of clinkerless cement with utilization of heat from molten blast-furnace slags for calcining of activating admixtures. I. W. Perry. *Compt. rend. acad. sci. U. R. S. S.* 41/379-81 (1943) (in English). --Heat is conserved by using molten slag to calcine gypsum and dolomite to form slag activators. Tabulated data are given on the setting time and the tensile and compression strengths after 4, 7 and 28 days of setting of cements prep'd. by combining 30% of an activator with 65% and 70%, resp., of various slags (Bessemer, open hearth and foundry) and 5% and 0% of gypsum. Retardation of setting rate and loss in strength were observed only after storing the cements for 3 months.

I. W. Perry

A 50-55A METALLURGICAL LITERATURE CLASSIFICATION

A	S	O	B	J	M	E	T	I	C	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T	I	O	N	E	L	I	T	E	R	S	E	T
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LIT. AND THE PATENT PROCESSING AND PROPERTY INDEX 100 AND 4TH EDITION

CA

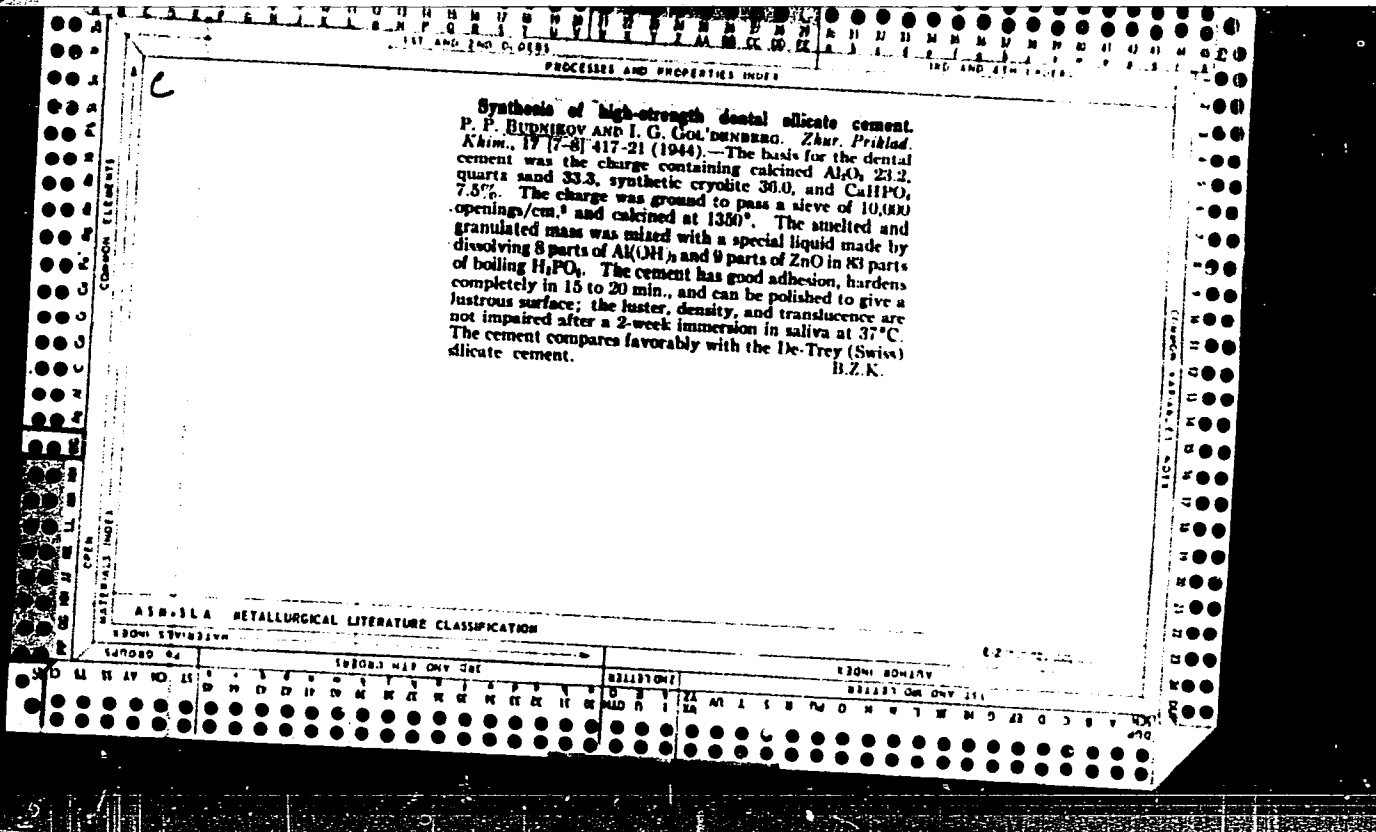
7

Microcolorimetric determination of V in rocks, minerals and ores by means of benzidine. I. P. Allmarin. *J. Applied Chem. (U. S. S. R.)* 17, 83-83(1944)(English summary).—A colorimetric micro or semimicro detn. of V in minerals and ores can be based on oxidation of benzidine in 10 N H₂PO₄, whereby an intense yellow coloration results, which can serve to detect V in diln. of 1:5,000,000. The effect of chromates and manganates is eliminated by the use of Mohr salt and NaNO₂. The sample is treated with H₂PO₄ alone or together with HF. G. M. K.

Determination of P in limestones by titration of excess 8-hydroxyquinoline. P. P. Budnikov and S. S. Zhukovskaya. *J. Applied Chem. (U. S. S. R.)* 17, 165-9(1944)(English summary).—P can be detd. by pptn. with (NH₄)₂MoO₄ together with oxine hydrochloride in dil. HCl soln. The excess oxine is detd. in the filtrate by titration with KBrO₃-KBr soln. G. M. Kosolapoff

ASB-51A METALLURGICAL LITERATURE CLASSIFICATION

FROM SYMBOLS										FROM DOMAINS														
SUBGROUP					SUBGROUP					SUBGROUP					SUBGROUP									
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25



1ST AND 2ND ORDERS PROCESSES AND PROPERTIES INDEX 3RD AND 4TH ORDERS

CA

18

Calced gypsum and dokomite. P. P. Hudnikov. U.S.S.R. 61,280, Jan. 31, 1945. Gypsum and dokomite are added to a ladle contg. molten slag at the time when the ladle is 2/3 full. The calced product is skimmed off the surface of the slag. M. Hosen

COMMON ELEMENTS

MATERIALS INDEX

ASB-3LA METALLURGICAL LITERATURE CLASSIFICATION

FROM STAINLESS

FROM BOWLING

FROM MIP ONLY USE

RELATIONS

1ST AND 2ND ORDERS

3RD AND 4TH ORDERS

Dehydration of gypsum during its treatment with steam in an autoclave. V. K. DEJNEVA, V. I. KUMAROV, V. I. KUROVITSKI, AND I. M. GIBSOV. *Sovetsk. Tshch. Nauch.-Issledovatel'sk. Zhurn. Gipsovoi Prom.*, 1945, pp. 9-12. — A systematic investigation was conducted on the dehydration of gypsum by treating it with steam under pressure in an autoclave to obtain $\text{CaSO}_4 \cdot 0.5\text{H}_2\text{O}$. Gypsum from the Artemovsk deposits in the Donets Basin was used, which analyzed SiO_2 1.51, Al_2O_3 0.21, Fe_2O_3 0.13, CaO 81.92, MgO 0.31, SO_3 46.86, and water of hydration 20.14%. Treatment for 2 hr. at 8 kg./cm.² (gauge pressure) followed by drying at 57° to 70° gave practically 100% of the hemihydrate. Calculation of the heat balance shows that the dehydration can be conducted in one apparatus (autoclave) with the specific heat consumption not greater than that of the most advanced gypsum calcination plants. B.Z.K.

127 AND 128 COPIES PROCESSED AND PROPERTY INDEX 129 AND 130 COPIES

CA

19

Ceramic stoneware from clays of Efreminsk deposit.-
 P. P. Budnikov and S. A. Peterson. *Slehot'saya i Keram.*
Prim. 1945, No. 1-2, 17-18.—Clays from the Efreminsk
 deposit analysis SiO_2 87.0-90.0, Al_2O_3 24.5-28.0, Fe_2O_3
 0.1-3.2, CaO 0.6-1.8, MgO 0.4-3.0, alkali 0.8-1.9, and
 ignition loss 2.6-8.4%. The gray variety is plastic, has a
 refractoriness of 1630-1670° and sintering temp. of 1180°,
 and is suitable for making acid-resisting stoneware.
 Optimum changes can be prepd. from 80% clay and 50%
 grog or 65% clay and 35% grog; grog is obtained by
 calcining clay at about 900°. Optimum grain-size comp.
 of the grog is 1.5-1.0 mm. 30%, and 0.15-0.00 mm. 70%.
 Products fired at 1280° meet requirements for normal
 acid-resisting brick and for Raschig rings.
 B. Z. Kamich

ASB-31A METALLURGICAL LITERATURE CLASSIFICATION

127 AND 128 COPIES 129 AND 130 COPIES

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A. E. S.

Ref. articles

Dolomite and "sivash" solutions as sources of magnesium oxide. *I. P. Litvinov, Zhurnal Priklad. Khim., 1943, No. 2, 10-21*. Details of the treatment of dolomite to obtain magnesium oxide are given. The other sources of magnesium oxide are the numerous salt lakes of northern Crimea, called "sivash". Both of these raw materials are a good source of magnesium oxide. Dolomite should be fired at 1200° and then treated at ordinary temperature with a solution of ammonium chloride. Magnesium oxide obtained in this way can be used for the manufacture of magnesium, magnesite, and forsterite refractories.
11 references. MVC

111 AND 7th COPIES PROCESSES AND PROPERTIES INDEX 100 AND 1th COPIES

CA

19

Dolomite and "slvash" solutions as sources of magnesium oxide. P. P. Budnikov. *Openory* 10, No. 2-3, 16-21(1945).—Details of treatment of dolomite to obtain MgO are given. The other sources of MgO are the numerous salt lakes of Northern Crimea, called "slvash." Dolomite should be fired at 1200° and then treated at ordinary temp. with a soln. of NH₄Cl. MgO thus obtained can be used for the manuf. of magnesium, magnesite, and forsterite refractories. M. V. Condoide

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION 6-277-278-282

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111 AND 7th COPIES	100 AND 1th COPIES

1ST AND 2ND ORDER) 3RD AND 4TH ORDER)

PROCESSES AND PROPERTIES INDEX

c

Physicochemical processes occurring in the stabilization of dolomite with additions of Cr_2O_3 . P. P. BUDNIKOV. *Ognesopoy*, 10 [11-12] 26-30 (1945). A review of the literature indicates the formation of a whole series of compounds of Cr and CaO when Cr_2O_3 is added to dolomite. Mixtures containing various proportions of CaO and Cr_2O_3 were prepared and fired; the free CaO was determined by the phenol method. The coefficient of binding of CaO by Cr_2O_3 in the case of dolomite is between $3CaO \cdot Cr_2O_3$ and $4CaO \cdot Cr_2O_3$. Microscopic studies were seriously hindered because of the coloration of the specimen by the Cr compounds and because of the lack of reliable optical constants for the compounds of Cr and CaO. Conditions of firing had no effect on the amount of free and reacted CaO. To raise the refractoriness of chromic dolomite clinker, it is necessary to add SiO_2 with the chromite. 21 references. H Z K

ASB. S.L.A. METALLURGICAL LITERATURE CLASSIFICATION

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1ST AND 2ND COPIES

PROCESSED AND PROPERTIES INDEX

3RD AND 4TH COPIES

CA

19

Acidproof enamels on iron from available materials. P. P. Budnikoy and I. G. Gol'denberg. *Khimicheskaya Prom.* 1948, No. 12, 14-15. —Of a no. of enamels tested the 2 that proved most satisfactory were: quartz sand 53.2, 57.0; feldspar 11.8, 10.8; calcined soda 21.0, 16.8; potash 3.0, 3.4; CaCO₃ 11.0, 10.0; ZnO 0.0, 2.0%, resp. The chem. compn. was: SiO₂ 69.82, 70.20; Al₂O₃ 2.23, 2.19; Na₂O 6.54, 10.75; K₂O 3.94, 3.73; CaO 17.90, 10.95; ZnO 0.0 and 2.19%, resp. The 2nd enamel (contg. ZnO) is not suitable for app. in which foods are treated. The m.p. of these enamels is 880-600°. They form colorless glasses adhering well to iron. Their resistance to boiling 20% HCl, 20% H₂SO₄, 30% HNO₃, 10% citric acid, and 10% AcOH was satisfactory. Thermal resistance was tested by heating enamelled test pieces to 332° and then plunging them into tap water. The enamels withstood 15 changes (5 is the required no.). The mech. properties of the enamels were good.

M. Hosh

ASM-SLA METALLURGICAL LITERATURE CLASSIFICATION

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PROCESSES AND PROPERTIES INDEX

1ST AND 2ND ORDERS

1ST AND 4TH ORDERS

C

Rate of calcium valfoaluminate in the exothermal hardening of alumina cement. P. P. DIMNIKOV AND I. G. GOL'DENBERG. *Zhur. Priklad. Khim.*, 18 (1-2) 15-19 (1945).—Exothermal curves were obtained of ordinary alumina cement made from blast-furnace alumina slag and of the same cement with additions of anhydrite. Experiments were conducted at 16°C. under conditions of natural liberation of heat and at 65° to 70° and higher analogous to conditions existing in large concrete blocks. The results show that, for cement hardening at high temperatures, the anhydrite binds the $3CaO \cdot Al_2O_3 \cdot 6H_2O$ into useful products. The mechanical properties of the hardened cement were also improved. H. Z. K.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND ORDERS

1ST AND 4TH ORDERS

PACKAGES AND PROPERTIES INDEX

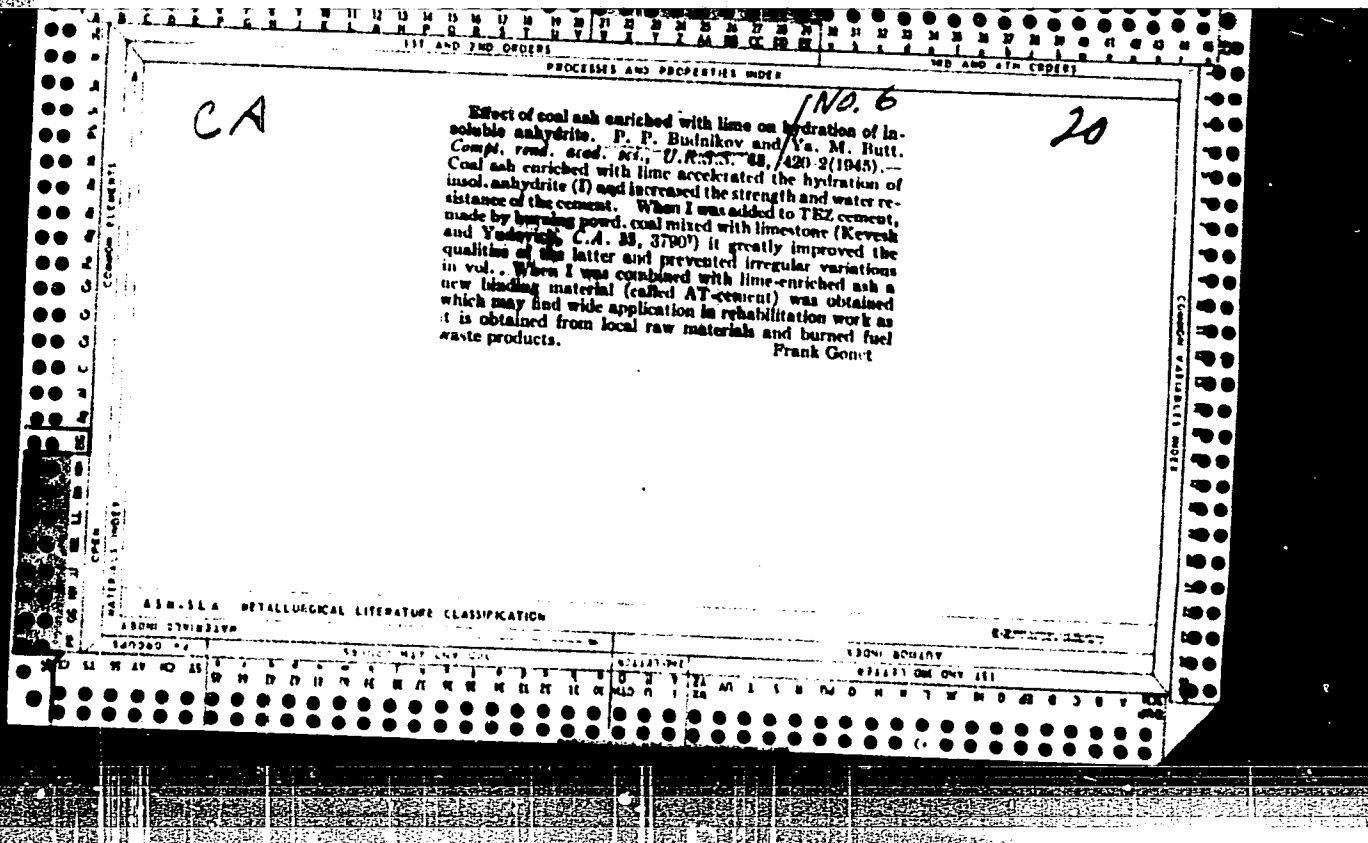
F A

12. CORROSION OF CONCRETE BY MINE AND COAL-WASHING WATERS AND SELECTION OF A MORE RESISTANT CEMENT. *Budnikov, P. P. and Gusev, V. K.* (J. Appl. Chem. (U.S.S.R.)), 1945, 18, 474-82; Chem. Abstr., 1946, 40, 5541).

Examination of resistance of concrete to aggressive waters gave the following gradation of resistance (in descending order): elinkerless cement (90% blast-furnace slag, 5% CaSO_4 , 5% calcined dolomite), slag-portland cement with 5% anhydrite, pozzuelana portland cement, portland cement. Extensive test results are given in table form.

ASR-55.A METALLOGICAL LITERATURE CLASSIFICATION

SECTION	SECTION
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100



Effect of lime-enriched coal ash on the hydration of in-
soluble anhydrite. *Compt. rend. acad. sci. URSS*, 48 (6) 1297 (1963).
The authors suggested the preparation of a two component
cement (AT) from (1) lime-enriched coal ash and (2) in-
soluble anhydrite or some other modification of $CaSO_4$.
Starting materials were (1) 10 to 90 anhydrite and 90 to
10% TEZ cement (32 to 48 lime and 7.5 to 25% alumina),
(2) 83 anhydrite, 10 TEZ ash, and 1% lime, and (3) 81.5
anhydrite, 15 TEZ ash, and 1.5% lime. Hydration of in-
soluble anhydrite was accelerated, and mechanical strength
and water resistance of the cement were increased by the
addition of the lime-enriched coal ash. The properties
of the TEZ cement were greatly improved, and there were
no irregular variations in the volume. High quality bind-
ing material is obtained from insoluble anhydrite and lime-
enriched ash. B.Z.K.

CA

LIST AND THE ORDER

PROCESSES AND PROPERTIES INDEX

190 AND 210 CATEGORIES

19

Mullite refractory from a mixture of kaolin and alumina. P. P. Budnikov. *Compt. rend. acad. sci. U.R.S.S.* 49, 2023 (1948).—A mullitization process takes place when kaolinite is heated in the range of 950-1100° whereby silica is liberated in the form of cristoballite. $3(Al_2O_3 \cdot 2SiO_2 \cdot 2H_2O) = 3(Al_2O_3 \cdot 2SiO_2) + 6H_2O$; $3(Al_2O_3 \cdot 2SiO_2) = 3Al_2O_3 \cdot 2SiO_2 + 4SiO_2$. The yield of mullite and growth of crystals increase with the temp., but the theoretical amt. is never attained, because part of the Al_2O_3 enters into combination with the melts of the clay to form a SiO_2 glass of varying viscosity. The formation of a viscous vitreous phase is unfavorable in a clay refractory on its deformation under load at high temp. The harmful effect of the vitreous phase can be checked somewhat by the introduction of material high in alumina, such as bauxite, diaspore, sillimanite, kyanite, andalusite, or alumina. Best results are obtained when alumina is added, so that at certain temps. the silica liberated from the kaolinite combines to form mullite crystals. $Al_2O_3 \cdot 2SiO_2 + 2Al_2O_3 = 3Al_2O_3 \cdot 2SiO_2$. Initial material may be Prossnansk kaolin and com. alumina. A mixt. of fine-ground kaolin and alumina in the ratio of $Al_2O_3:SiO_2 = 3:2$ was made into briquets which were then burned at 1600, 1650, and 1670° for 2 hrs., given a petrographic investigation and quantitatively examd. for mullite with 20% H_2F . Microscopic examn. showed a homogeneous mass of mullite crystals. The amt. of crystals and the crystal formation were larger in the samples burned at 1670°. Burning temps. and percentages of mullite were: 1600°, 70.2; 1650°, 81.4; 1670°, 83.7. In addn. to

mullite and silica glass, 6-10% corundum was always present. A 2-4% addn. of such substances as cryolite, fluo-rite, $MgCl_2$, P_2O_5 , or B_2O_3 will lower the burning temp. so that the viscosity of the glass is decreased and the crystn. of the mullite accelerated. From a kaolin-alumina mixt. with 2% $MgCl_2$ added, a refractory was prepd. by using grains under 0.5 mm., 30%; from 0.5 to 1 mm., 45%; from 1 to 2 mm., 25%. The binding material was PB clay from Chasov-Yar (12%). The mass (moisture 6.5%) was pressed into cylinders 6 to 6 cm., and burned at 1500°. Results showed that the mullite refractory prepd. from a mixt. of kaolin and silica is superior, as regards deformation under load, to both the ordinary refractory and kaolin refractory.

R. T. Ramsay

ASS-51A METALLURGICAL LITERATURE CLASSIFICATION

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PROCESSES AND PROPERTIES INDEX

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973. MULLITE REFRACTORY FROM A MIXTURE OF KAOLIN AND ALUMINA.—P. P. Budnikov (*Comptes Rendus Acad. Sci. U.R.S.S.*, 84, 202, 1945). An intimate mixture of finely ground kaolin and alumina ($Al_2O_3 : SiO_2 = 3 : 2$) was made into briquettes which were then burned at 1,600°, 1,650°, and 1,670° C. for 2 hr. Their thin sections under the microscope showed a homogeneous mass of mullite crystals, with a certain amount of corundum (6-10%) and silica glass. The amount of the crystalline component was greater, and the crystals were larger, in the samples burnt at 1,670° C. Refractoriness-under-load tests at 2 kg/cm² showed deformation 100°-150° C. higher than for a semi-acid high quality refractory, an ordinary refractory, or a kaolin refractory.

A S B S E A METALLURGICAL LITERATURE CLASSIFICATION

LIST AND INDEX LETTERS

PROCESSES AND PROPERTIES INDEX

14

Technology of Ceramic Shapes (Технология керамических изделий) P. P. BUDNIKOV, A. S. BEREZINOL, V. I. PERKALOV, AND I. S. SMELYANSKIĬ. Published by Gosstizdat, Moscow, 1946. 224 pp., 288 illustrations. Price: 30-25 rubles. Reviewed in *Steklo i Keram.*, 5 [11] 23-24 (1948). Part I covers raw materials. Technological properties and the scientific basis are presented in the light of modern physicochemical views. Part II covers structural ceramics; Part III, stone-ceramic shapes, and Part IV, refractory shapes. Parts V and VI are limited to glazes and ceramic colors. Numerous errors in the book are pointed out. It is approved as a text for chemical-technological institutes and faculties by the Ministry of Higher Education.

H. Z. K.

ASB-514 METALLURGICAL LITERATURE CLASSIFICATION

111 AND 120 ORD(S) 111 AND 120 ORD(S)

PROCESSES AND PROPERTIES MODS

20

CA

Gypsum hemihydrate. P. P. Hudnikov, B. K. Butkevich, and M. O. Vushkevich. U.S.S.R. 63,708, Feb. 28, 1940. The gypsum hemihydrate is obtained by cooking under pressure. To increase its strength, about 1% of alums, $MgSO_4$, or $Al_2(SO_4)_3$ is added to the gypsum.
M. Hosh

ASS. SLA METALLURGICAL LITERATURE CLASSIFICATION

111 AND 120 ORD(S)

111 AND 120 ORD(S)

BUDNIKOV, P. P.

012

ASH-SLA METALLURGICAL LITERATURE CLASSIFICATION										AUTHOR INDEX																																																																																									
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CA

High-strength plaster of Paris. P. P. Budnikov.
 U.S.S.R. 66,235, May 31, 1946. Gypsum is autoclaved
 at 1.2 atm. and the product is ground in a ball mill or a
 rod mill, and at the same time dried with hot flue gases.
 M. Hoesel

1ST AND 2ND ORDERS PROCESSES AND PROPERTIES INDEX 3RD AND 4TH ORDERS

20

Hydraulic cement. P. P. Dudnikov and Yu. M. Butt.
U.S.S.R. 66,238, May 31, 1940. The cement is a mixt.
of anhydrous CaSO₄ ash resulting from the combustion of
powdered coal, and ground limestone of dolomite. M. Hosh

ASB-3LA METALLURGICAL LITERATURE CLASSIFICATION

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

BUDNIKOV, P. P.

Chem

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1ST AND 2ND ORDERS PROCESSES AND PROPERTIES INDEX

CH

High-strength plaster of Paris. *P. P. Budnikov, P. V. Lavshin, and Ya. Yu. Roitberg.* U.S.S.R. 66,330, May 31, 1946. Ground gypsum is treated with approx. 1% of mineral acid and then is heated under pressure. *M. Hoseh*

8

P. P. BUDNIKOV

PROCESSES AND PROPERTIES INDEX

White hydraulic binder for decorative purposes. P. P. Budnikov and L. O. Lungin. U.S.S.R. 66,692, July 31, 1940; abstracted in Chem. Zentr., 1948, I [11/12] 748.—The binder is made of a mixture of granulated blast-furnace slag, lime, and calcined kaolin. These constituents are added without calcining if waste product from the process of producing AlCl₃ from kaolin is used instead of calcined kaolin. M.H.A.

11-3-50

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PROCESSES AND PROPERTIES INDEX

11-3-50

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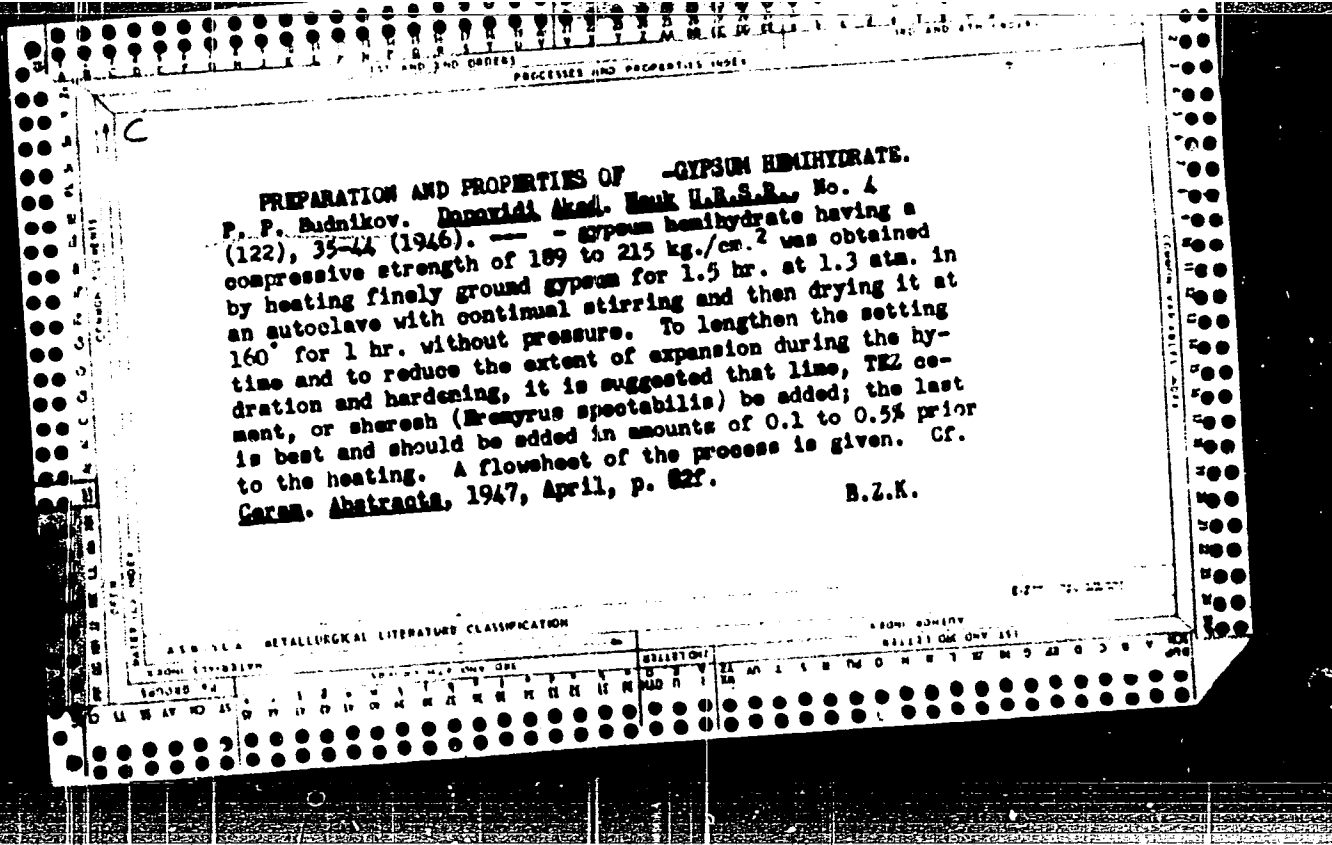
The Refractories Problem in Connection With the Use of Oxygen in the Steel Industry. I. I. Kitigorodakii and P. P. Budnikov. Henry Bratcher (Altadena, Calif.), Translation No. 2081, 1948, 6 pages. Condensed from *Kislorod (Oxygen)*, v. 3, no. 2-3, 1946, p. 29-31.

A general discussion of paper of above title by S. V. Glebov. Includes data on vitrified corundum and zircon cement refractories and refractories of zircon+chromium oxide+calcium oxide for tuyeres in oxygen-blown converters. Gives particulars on a new chrome-dolomite brick for basic O.H. furnaces; its manufacture, properties, and actual performance; test data on cased chrome-dolomite concrete, and on zircon brick, in O.H. furnaces; and details on manufacture of magnesia-spinel refractories and their properties.

METALLURGICAL LITERATURE CLASSIFICATION

A B C D E F G H I J K L M N O P Q R S T U V W X Y Z

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4525. CAUSES OF PREMATURE FAILURE OF REFRACTORY LININGS IN LOCOMOTIVE FIREBOXES. Budnikov, P. F. and Matveev, M. A. (Ogneupory, 1946, No.6, 23-5; Chem. Abstr., 1947, 41, 1074).

The causes are: poor installation, use of low grade materials, use of binders which are not suitable for the brick, too rapid drying after installation and mechanical shocks in service.

ASME-ISA METALLURGICAL LITERATURE CLASSIFICATION

GROUPS: 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

LETTERS: A B C D E F G H I J K L M N O P Q R S T U V W X Y Z

PROCESSES AND PROPERTIES INDEX

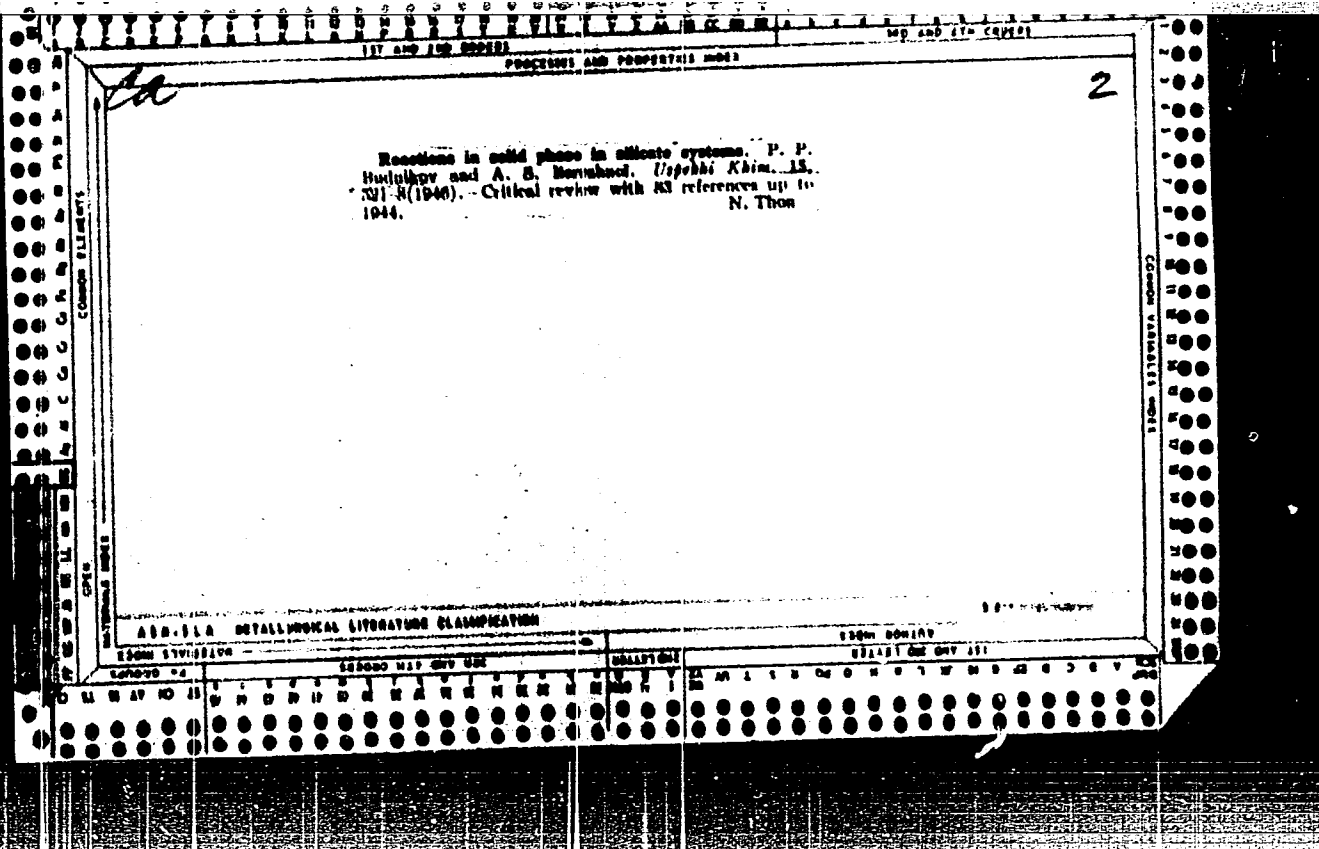
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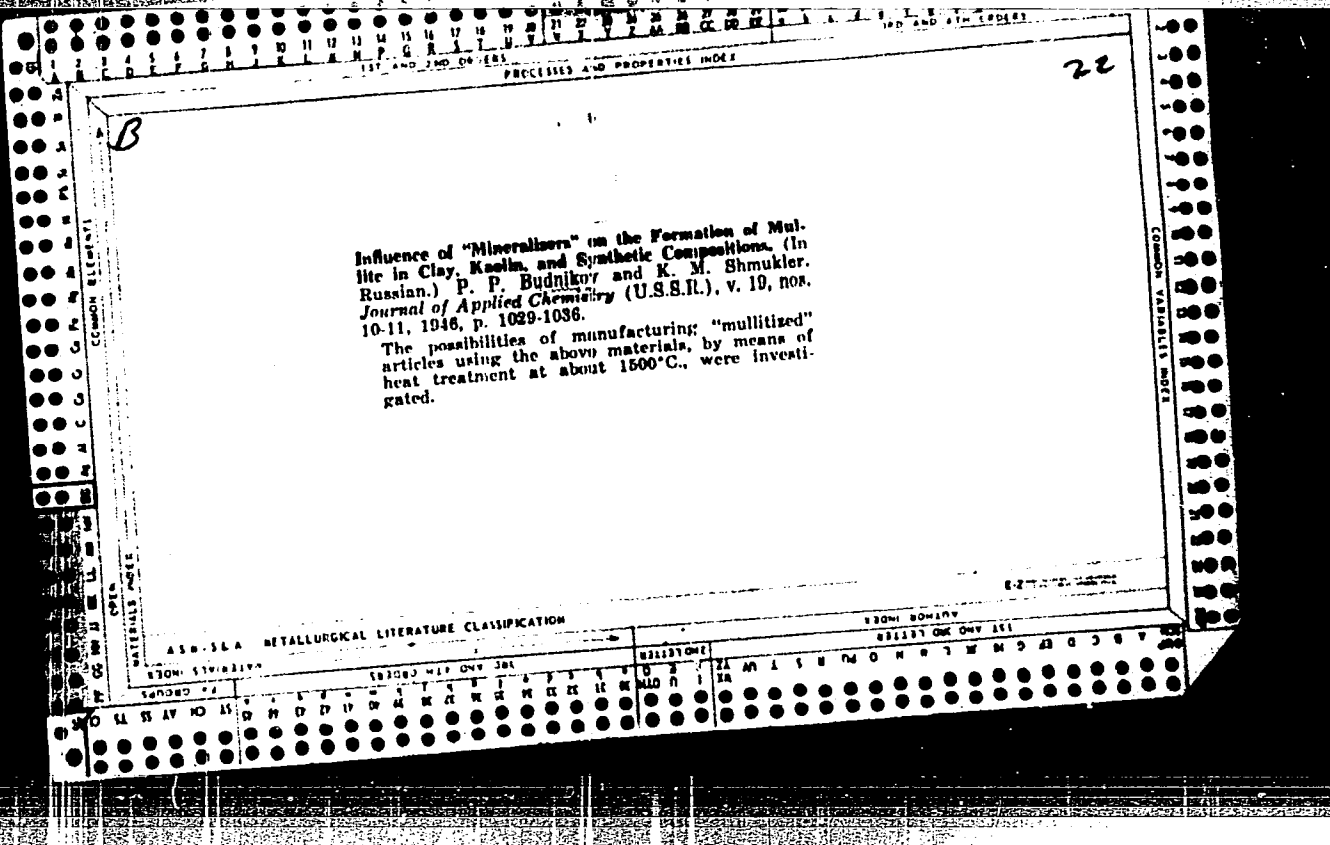
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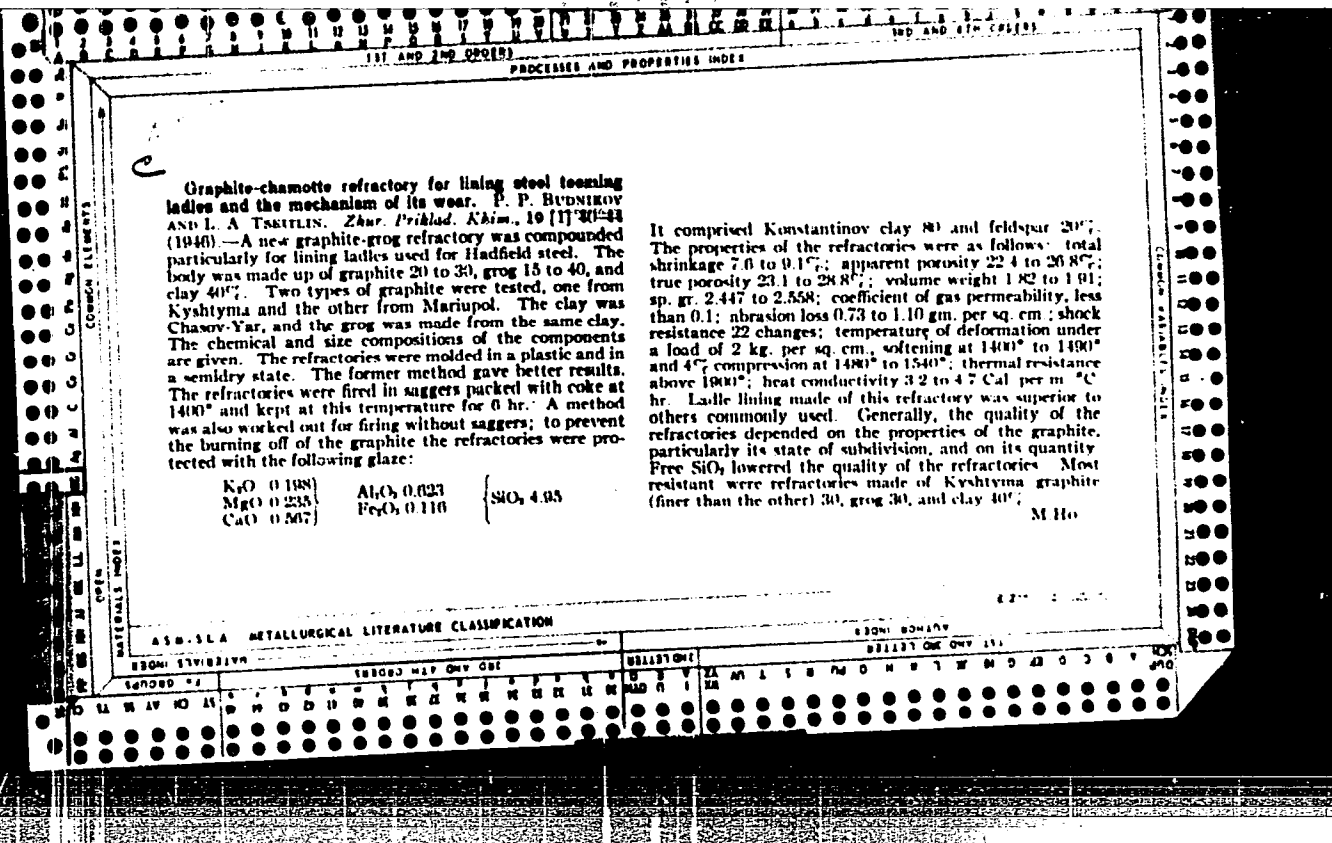
Causes of premature destruction of refractory lining in locomotive fireboxes. P. P. BUDNIKOV AND M. A. MATVEREV. *Ogneprory*, 11 [6] 23-25 (1940). Causes of the premature destruction of the refractory lining in locomotive fireboxes are (1) faulty installation of arches, (2) use of low-grade refractories, (3) use of a binder having a different composition from that of the brick, (4) very rapid drying of the arches after installation, (5) leakage of connectors and tubes, and (6) strong jolts in service. The temperature curve of a fuel oil fired locomotive for a 20-hr. period shows sharp variations. Linings for locomotive fireboxes should have a refractoriness not lower than 1730°C and also high resistance to thermal shock. Compressive strength should be not lower than 120 kg./cm.². Initial softening under a load of 2 kg./cm.² should be not lower than 1350°C. Additional shrinkage at 1400° should not be over 0.7%. B.Z.K.

METALLURGICAL LITERATURE CLASSIFICATION

GROUP	CLASS	INDEX	SEARCH
15	11	11	11
14	10	10	10
13	9	9	9
12	8	8	8
11	7	7	7
10	6	6	6
9	5	5	5
8	4	4	4
7	3	3	3
6	2	2	2
5	1	1	1
4	0	0	0
3			
2			
1			







22

PROCESSES AND PROPERTIES INDEX

Production of Cement with a High Alite Content. P. Budnikov and M. I. Strelkov. *Journal of Applied Chemistry (U.S.S.R.)*, v. 19, no. 4, 1946, p. 341-347. (In Russian.)

Describes new method for the production of alite (tricalcium silicate) cement. The chief characteristic of this method is double calcination performed in a rotary furnace. First calcination is performed at about 900°C., the second, with addition of alumina and chalk, at 1500°C. Cement obtained is green in color and is characterized by very rapid solidification. Its compressive strength reaches 430 kg./cm².

ASAC-55A METALLURGICAL LITERATURE CLASSIFICATION

TECHN. BOMBYN

1111 A B C D E F G H I J K L M N O P Q R S T U V W X Y Z

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

CA

19

Effect of mineralizers on the formation of mullite in clays, kaolins, and synthetic masses. P. P. Budnikov and K. M. Shmukler. *J. Applied Chem. (U.S.S.R.)* 19, 1029-30 (1946) (in Russian).—The amt. of mullite formed at 1000-1600° for 1, 3, and 18 hrs. was detd. by dissolving in 20% HF, by x-rays, and microscopically. With clays mullite formation becomes significant above 1000°. Kirov clay (SiO₂ 44.66, Al₂O₃ 38.77, Fe₂O₃ 1.06, TiO₂ 0.82, CaO 0.83) heated for 3 hrs. at 1100, 1200, 1500°, showed 31, 38, 47% mullite. At const. temp., the amt. of mullite $s = a \log r + b$, where r = time in min., a and b are const., depending on the temp.; the max. s reached was 7-18% below the theoretically possible max. (40-50%). Among the mineralizers investigated (feldspar, H₂BO₃, BaCl₂, CuCl₂, TiO₂, NH₄VO₃, MgCl₂, MnSO₄, Fe(OH)₃), addns. of 4% MnSO₄, 4% CuCl₂, 4% MgCl₂ proved most effective; in the latter case, 6% had less effect. The addn. lowers the temp. of the beginning of mullite formation by 100-200°. In mixts. of SiO₂ + Al₂O₃, held at the specified temp. 3 hrs., the formation of mullite was max. at all temps. in the presence of 2% MnO (4% MnSO₄); thus, in a mixt. of SiO₂, 28.2, Al₂O₃, 71.8, at 1300, 1400, 1500, 1600°, the residual corundum was 30-35, 15, 10, 5%, resp.; the order of decreasing effectiveness of mineralizer addns. was: at 1400°, 4% MnSO₄, 1% MgCl₂, 2% TiO₂, 4% CaF₂; at 1500°, 4% MnSO₄, 2% TiO₂, 4% Cr₂O₃, 4% MgCl₂, 4% Fe(OH)₃, 2% CuCl₂; at 1600°, 4% MnSO₄, 2% TiO₂, 4% MgCl₂, 4% LiCl.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

FROM STOVIBLIV

FROM DOMINY

RETRACTED

19

caused a reduction in the amount of Al_2O_3 relative to that of mullite. It is possible to obtain a mullite refractory suitable for blast-furnace use by the addition of 2% MnO (4% $MnSO_4$) to a charge consisting of clays and kaolins with calcined alumina in proportions that will insure a complete mullite refractory by firing at 1500° to $1600^{\circ}C$. The MnO will not favor carbon deposition within the brick.

B. Z. K.

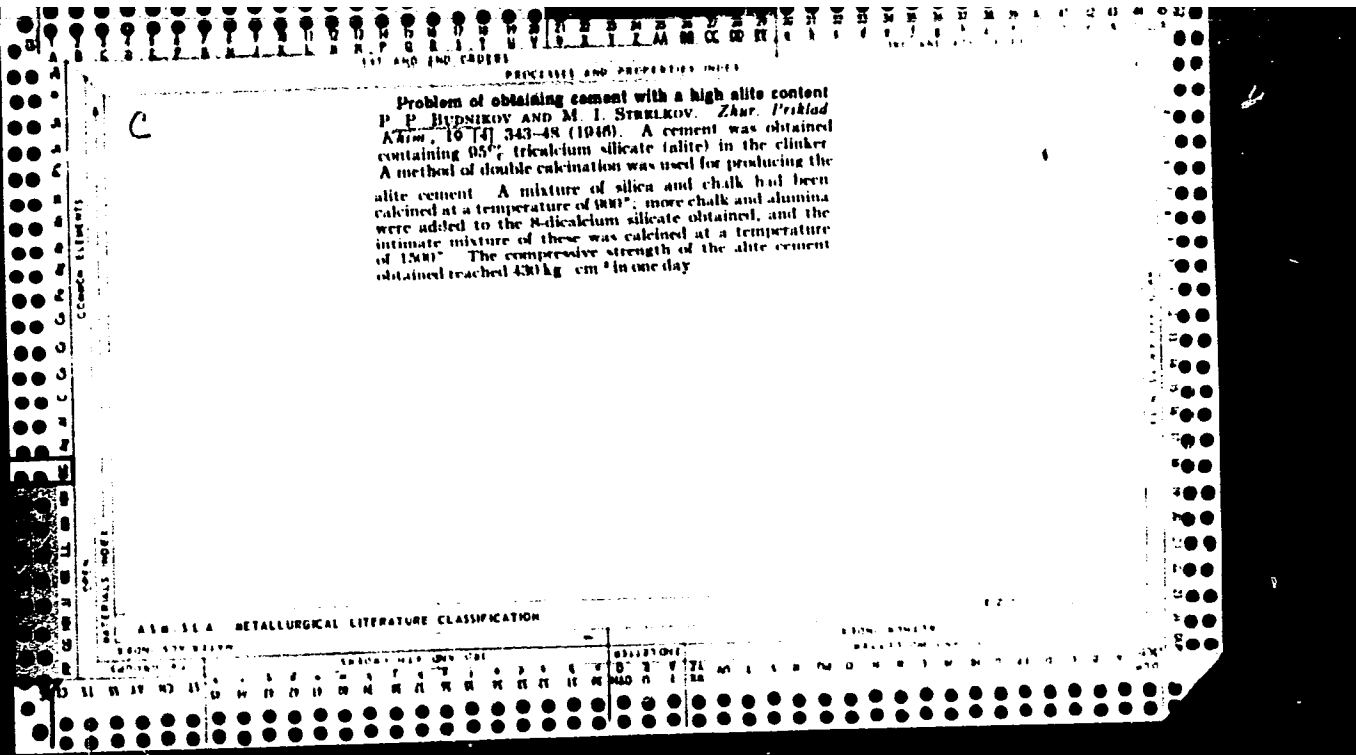
BUDNIKOV, P. P.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG	AH	AI	AJ	AK	AL	AM	AN	AO	AP	AQ	AR	AS	AT	AU	AV	AW	AX	AY	AZ

1. Budnikov, P. P., and Tseitlin, L. A. GRAPHITE-CHROMITE REFRACTORY FOR LINING STEEL TAPPING LADLES AND THE MECHANISM OF ITS WEAR. *Applied Chem. (U.S.S.R.)*, 19 [1] 40-41 (1946) - A new graphite-grog refractory was compounded particularly for lining ladles used for Hadfield steel. The body was made up of graphite 20 to 30, grog 15 to 40, and clay 40%. Two types of graphite were tested, one from Kyshtyma and the other from Mariupol. The clay was Chasov-Yar, and the grog was made from the same clay. The chemical and size compositions of the components are given. The refractories were molded in a plastic and in a semidry state. The former method gave better results. The refractories were fired in saggars packed with coke at 1400° and kept at this temperature for 6 hr. A method was also worked out for firing without saggars; to prevent the burning off of the graphite the refractories were protected with the following glaze:

K ₂ O 0.198	}	Al ₂ O ₃ 0.623	}	SiO ₂ 4.05
MgO 0.236				
CaO 0.597				

It comprised Konstantinov clay 80 and feldspar 20%. The properties of the refractories were as follows: total shrinkage 7.6 to 9.1%; apparent porosity 22.4 to 26.8%; true porosity 23.1 to 28.8%; volume weight 1.82 to 1.91; specific gravity 2.417 to 2.558; coefficient of gas permeability, less than 0.1; abrasion loss 0.73 to 1.10 gm./sq. cm.; shock resistance 22 changes; temperature of deformation under a load of 2 kg./sq. cm., softening at 1400° to 1490° and 4% compression at 1480° to 1510°; thermal resistance above 1900°; heat conductivity 3.2 to 4.7 Cal./m. °C. hr. Ladle lining made of this refractory was superior to others commonly used. Generally, the quality of the refractories depended on the properties of the graphite, particularly its state of subdivision, and on its quantity. Free SiO₂ lowered the quality of the refractories. Most resistant were refractories made of Kyshtyma graphite (finer than the other) 30, grog 30, and clay 40%.



100 AND 4TH CODES

1ST AND 2ND CODES

PROCESSES AND PROPERTIES INDEX

21

Preparation of cement with high alite (tricalcium silicate) content. P. P. Hudnikov and M. I. Strelkov. *J. Applied Chem. (U.S.S.R.)* 19, 343-8(1946).--By means of double calcining the authors prepd. cements with up to 85% content of tricalcium silicate in the clinker. The ingredients used were sand (99.8% SiO₂), chalk, and pure CaCO₃, which were finely ground and mixed in the ratio required for formation of tricalcium silicate, then calcined at 900°; the resulting calcium ortho-silicate was recalcined at 1450-1500°. The cement thus formed hardens more rapidly than the standard alumina cement giving a higher flexure strength, while reaching a compression strength of 430 kg./sq. cm. in 24 hrs. The presence of tricalcium aluminate in this cement failed to improve its hydraulic properties further. The alite cement as produced has green color if calcining is done in reducing atm. The cement can be produced in rotating kilns. G. M. Kosolapoff

COMMON ELEMENTS

COMMON VARIABLES INDEX

ASPH-51A METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND CODES

3RD AND 4TH CODES

1ST AND 2ND ORDERS 3RD AND 4TH ORDERS

PROCESSES AND PROPERTIES INDEX

Chromo-dolomite high refractory concrete and brick.
 P. P. NUNSIKOV. *Compt. Rend. Acad. Sci. U.S.S.R.*, 31
 [8] 615-17 (1960). --The object of this investigation was to
 determine the ratio in which Cr_2O_3 and CaO combine in
 dolomite. Mixtures of 1 Cr_2O_3 with 2, 3, 4, 6, and 8 CaO
 were studied. The proportions in which the two were
 combined were between $3CaO \cdot Cr_2O_3$ and $4CaO \cdot Cr_2O_3$.
 In a mix calculated as $3CaO \cdot Cr_2O_3$ to which was added
 SiO_2 , Al_2O_3 , or Fe_2O_3 , all of the CaO was combined. A
 mix calculated as $4CaO \cdot Cr_2O_3$ contained 1.00 to 4.00%
 free lime. On this basis a mix was made comprising dolo-
 mite 74, chromite 20, and quartzite 6%. The mix was
 briquetted and fired at 1600° to 1680°. The pulverized
 clinker had good hydraulic properties; setting began after
 50 min. and was completed after 3 hr. 10 min. The com-
 pression strength of specimens made of this cement was 110,
 130, and 205 kg. per sq. cm. after 4, 7, and 28 days, respec-
 tively. Brick were made of this cement without adding any
 bonding agents. The brick withstood temperatures above
 1000°. Under a load of 2 kg. per sq. cm. deformation began
 at 1450° and failure occurred at 1500°. Tested for
 open-hearth and electric-furnace linings, chromo-dolomite
 refractories fully equaled magnesite and chrome-magnesite
 refractories.

M 110

ASB-31A METALLURGICAL LITERATURE CLASSIFICATION

FROM 177-02100 123003 MET ONLY 001 001121001 123003 001 001 101

MATERIALS INDEX OPEN COMBINATION INDEX

P. P. BUDNIKOV

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41											
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	BB	CC	DD	EE	FF	GG	HH	II	JJ	KK	LL	MM	NN	OO	PP	QQ	RR	SS	TT	UU	VV	WW	XX	YY	ZZ

1ST AND 2ND ORDERS

PROCESSES AND PROPERTIES INDEX

3RD AND 4TH ORDERS

A
B
C
D
E
F
G
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CC
DD
EE
FF
GG
HH
II
JJ
KK
LL
MM
NN
OO
PP
QQ
RR
SS
TT
UU
VV
WW
XX
YY
ZZ

CH

Setting time and strength of α -hemihydrated gypsum as affected by addition of Sheresh (*Eremyrua spectabilis*).
P. P. Budnikov. *Compt. rend. acad. sci. U.R.S.S.* 52, 325-8(1948); cf. Bachinsky, *Compt. rend. acad. sci. U.R.S.S.* 30, 280-3(1941).—The addn. of 0.5-1.0% dried and crushed sheresh roots to gypsum increased the setting time several fold as well as the ultimate compression strength by 20% or more. Ernst M. Cohn

Brit. ab.

*32. 10 Emulsiy and Konditsy
1946*

Setting time and strength of α -hemihydrated gypsum as affected by addition of glucose (*Eremyus spicatus*). P. L. BUDAKOV. (C. R. Acad. Sci. U.R.S.S., 1946, 61, 325-326).—The effect of the addition of 0.1–1.0% of a glue prepared from the roots of *Eremyus spicatus* and containing 27–33% of Ca arabiato on the rate of setting and ultimate compression of technical α -hemihydrated gypsum have been studied. The time of setting is increased. Up to 0.3% of glue increases the ultimate compression strength, but a fall occurs at higher concn. O. D. SALTAMEN.

Ex. 16

Bl. I. Buzilov & P. A. Mikhlin
1948

Corrosion of aluminum silicate cement by mineralized waters.
P. A. Hudnikov and V. R. Gusev (*Compt. rend. Acad. Sci. U.R.S.S.*,
1948, 18, 31-34).—A cement is prepared from blast-furnace slag
of wet granulation (18 pts.), anhydrite (1 pt.), and calcined dolomite
(1 pt.). It withstands 10% of NaCl and Na₂SO₄ better than does
Portland cement (compression strength after 3 years reduced by
15.1 and 21%, respectively, as compared with immersion in H₂O;
comparative vals. for Portland cement, 48.5 and 100%), but is
not superior in regard to 10% aq. MgCl₂ and 10% aq. MgSO₄
(comparative vals. 38.0 and 100%, as against 42.8 and 100%).
S. A. M.

FA 21 M16

USSR/Chemistry
Cement
Lime

Sep 1946

"The Chemical Formula of the Limiting Content of Lime (CaO) in the Portland Cement Domain of a CaO-SiO₂-Al₂O₃-Fe₂O₃-MgO System," P. P. Budnikov, Corresponding Member of the Academy of Sciences of the USSR, M. I. Strelkov, 2 pp

"Comptes Rendus (Doklady)" Vol III, No 8

Since the composition of commercial portland cement is very complicated, studies are first made of cements containing only one, then two, three and so on, of the main oxides making up ordinary cement. The chemical equation relating CaO and the other oxides 21M16

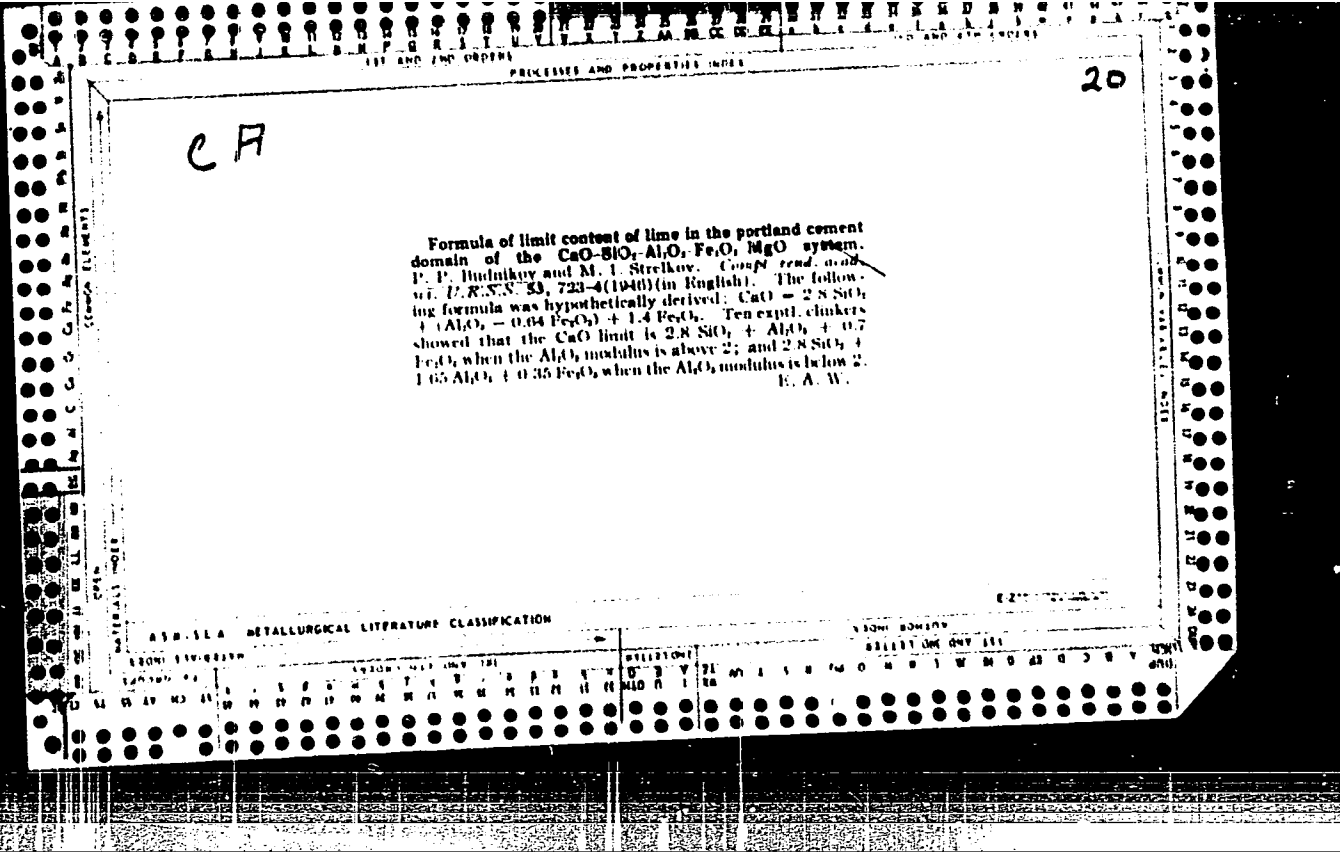
USSR/Chemistry (Contd)

Sep 1946

Cement
Lime

are studied to obtain the "limit" or "asymptotic" value of CaO as the number of other oxides are increased in the formulas.

21M16



1ST AND 2ND DEGREE

PROCESSES AND PROPERTIES INDEX

CA

Anhydrite cement P. P. Budnikov and Yu. M. Butt.
U.S.S.R. 69,294, Sept. 30, 1947. To increase the strength
and hydraulic properties of anhydrite cement, natural or
artificial anhydrite is mixed with 5-20% of TETs cement
(power station cement) or its mixt. with granulated blast-
furnace slag. M. Hosh

6

2

Expanding cement. P. P. Hudzikov. U.S.S.R. 69-600, Nov. 30, 1947. An expanding cement is made of a hydraulic binder and an expanding addn. The latter is made of a mixt. of clay or kaolin fired at 700-800°, lime, and portland cement. The last one can be omitted. The dry ingredients are mixed with water and after hardening and drying, the mass is ground and mixed with an equal vol. of gypsum hemihydrate. M. Hesch

CA

M

F

712. ASH CEMENTS. Budnikoy, P.P. and Butt, Y. M. (Tsement, 1947, vol. 15, (7), 9-11; abstr. in Chem. Abstr., 1949, vol. 43, 1938). Ash from power station boilers in combination with other substances was tested for its suitability as a bonding material. For these tests the ash was mixed with anhydrite or with anhydrite and lime. In addition was also tested a mixture of cement and anhydrite. The mixtures of anhydrite and ash were weaker than anhydrite alone. The addition of up to 10% of lime and keeping the ash content at not over 10% improved the resistance of the mixture.

C.A.

COMMON ELEMENTS
OPEN
MATERIALS INDEX
METALLURGICAL LITERATURE CLASSIFICATION
LIST AND INDEX

LIST AND INDEX
METALLURGICAL LITERATURE CLASSIFICATION
OPEN
MATERIALS INDEX

LIST AND INDEX
METALLURGICAL LITERATURE CLASSIFICATION
OPEN
MATERIALS INDEX

22

B

508. Heat of Solution of Magnesium Oxide (Sintered Magnesite) Fired at High Temperatures. (In Russian.)
 P. P. Budnikov. *Journal of Applied Chemistry* (U.S.S.R.), v. 20, no. 4, 1947, p. 319-326.

Shows that the amount of heat evolved on dissolving sintered magnesite in HCl depends upon the temperature of firing and is also increased by the presence of CaO in the magnesite. Describes use of diphenylmethane calorimeter to determine the approximate temperature of firing, from the heat evolved on solution in HCl.

AS 6-51 A METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND GROUPS PROCESSES AND PROPERTIES INDEX

3RD AND 4TH GROUPS

5TH AND 6TH GROUPS

7TH AND 8TH GROUPS

9TH AND 10TH GROUPS

11TH AND 12TH GROUPS

13TH AND 14TH GROUPS

15TH AND 16TH GROUPS

17TH AND 18TH GROUPS

19TH AND 20TH GROUPS

21ST AND 22ND GROUPS

23RD AND 24TH GROUPS

25TH AND 26TH GROUPS

27TH AND 28TH GROUPS

29TH AND 30TH GROUPS

31ST AND 32ND GROUPS

33RD AND 34TH GROUPS

35TH AND 36TH GROUPS

37TH AND 38TH GROUPS

39TH AND 40TH GROUPS

41ST AND 42ND GROUPS

43RD AND 44TH GROUPS

45TH AND 46TH GROUPS

47TH AND 48TH GROUPS

49TH AND 50TH GROUPS

51ST AND 52ND GROUPS

53RD AND 54TH GROUPS

55TH AND 56TH GROUPS

57TH AND 58TH GROUPS

59TH AND 60TH GROUPS

61ST AND 62ND GROUPS

63RD AND 64TH GROUPS

65TH AND 66TH GROUPS

67TH AND 68TH GROUPS

69TH AND 70TH GROUPS

71ST AND 72ND GROUPS

73RD AND 74TH GROUPS

75TH AND 76TH GROUPS

77TH AND 78TH GROUPS

79TH AND 80TH GROUPS

81ST AND 82ND GROUPS

83RD AND 84TH GROUPS

85TH AND 86TH GROUPS

87TH AND 88TH GROUPS

89TH AND 90TH GROUPS

91ST AND 92ND GROUPS

93RD AND 94TH GROUPS

95TH AND 96TH GROUPS

97TH AND 98TH GROUPS

99TH AND 100TH GROUPS

Technology (1947)
(1/1/47)

1309. THIRTY YEARS OF SOVIET SCIENCE IN THE FIELD OF SILICATES.
P.P. Eudnikov (J. Appl. Chem., U.S.S.R. 20, 1097, 1947). A full
summary of work carried out by Russian scientists in the field of silicate
technology is given, authors' names are quoted but no references are
given to the sources of their original papers.

1ST AND 2ND COLLETS PROCESSES AND PROPERTIES INDEX 22

COMMON ELEMENTS

OPEN MATERIALS INDEX

RESISTANCE OF Sulfated Alumina Cement to Chemical Attack. (In Russian.) P. P. Budnikov and I. G. Gol'denberg. *Zhurnal Prikladnoi Khimii* (Journal of Applied Chemistry), v. 20, Nov. 1947, p. 1155-1158.

Gives results of a study of the comparative resistances of ordinary alumina cement and, that to which CaSO_4 was added, on exposure to soft and to salt water. Data are tabulated and discussed. 13 ref.

ASIA-SLA METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND COLLETS

COMMON VARIANTS INDEX

1ST AND 2ND COLLETS

COMMON VARIANTS INDEX

Cement from calcium sulfate, ashes, and lime. P. P. Budnikov and Yu. M. Butt. *Soviet. Prom.* 25, No. 8, 31-3(1947)(in Russian).—Cements were compounded from lime, coal-dust ashes (50, 49.50, Al₂O₃ 37.42, Fe₂O₃ 6.60, CaO 3.03, MgO 0.82, SO₃ 1.14, ignition loss 1.42) and 3 modifications of CaSO₄ (made from natural gypsum, CaO 33.00, SO₃ 46.01, Al₂O₃ + Fe₂O₃ 0.52, H₂O 19.18, CO₂ 0.47, insol. 1.02): (I) CaSO₄· $\frac{1}{2}$ H₂O, made by heating at 160-70°, (II) anhydrite, obtained by ignition at 700°, 3 hrs., (III) ignited at 900°, 3 hrs. The batches were made up with 20, 30, 40% ashes, 5, 5, 10% lime and 75, 65, 50% CaSO₄ (I, II, or III). With increasing content of I, the water requirement decreases (60, 55, 48%, resp.); it increases slightly with increasing amt. of II (56, 38, 40% H₂O) or of III (35, 40, 42). Setting is slowed down with decreasing amts. of I or II and is accelerated with decrease of III. With 40% ashes, after 28 days' standing, the best samples had the compressive strengths: with I 115 kg./sq. cm., with II 210 kg./sq. cm., and with III 120 kg./sq. cm. Addn. of ashes and lime accelerates the setting of CaSO₄ and increases its waterproofness. Cements with I are best allowed to set in air or are dried to const. wt., whereas cements with III harden best in a moist atm. Best waterproofness is obtained with III.

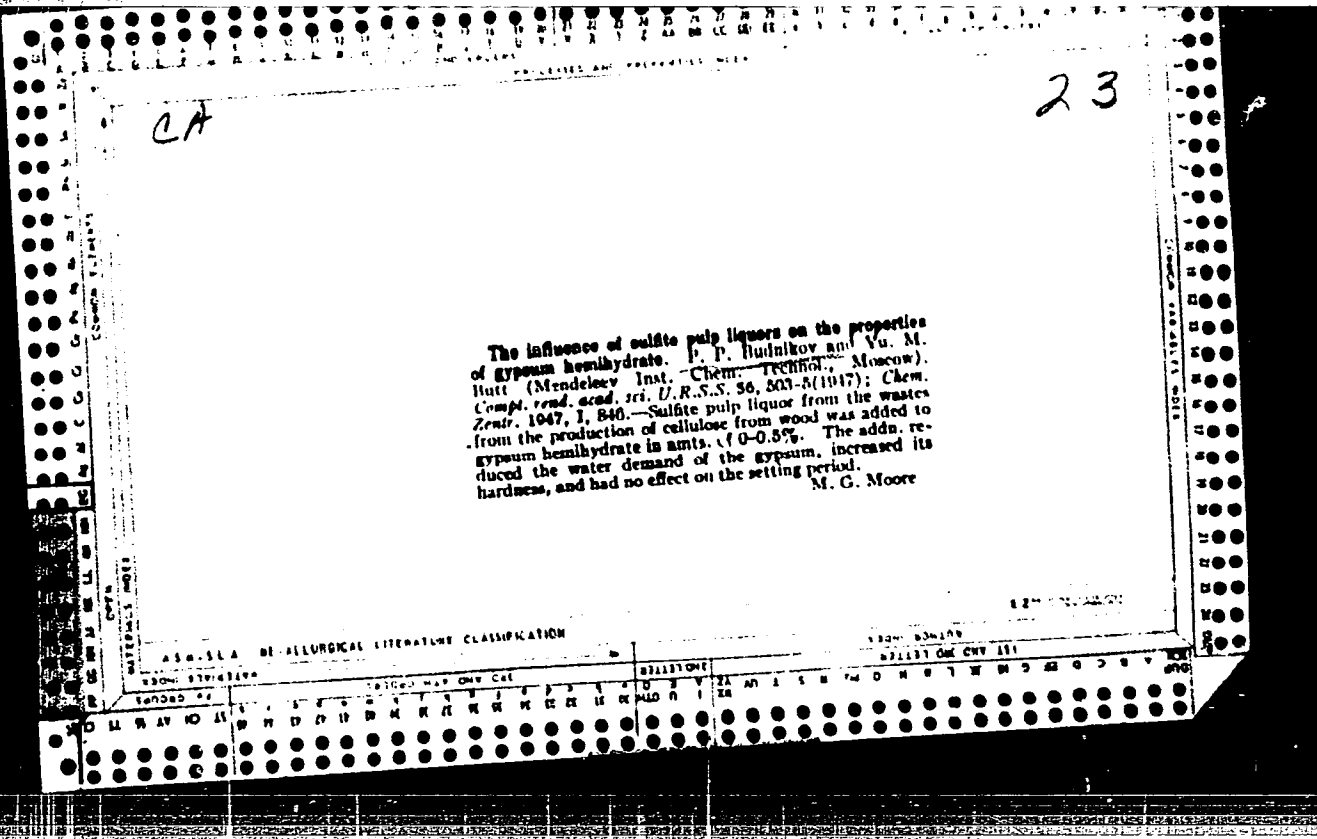
N. Thon

PROCESSES AND PROPERTIES INDEX

Influence of sulfite cellulosic lye on the properties of gypsum hemihydrate. P. P. BYDNIKOV AND YU. M. BUTT. *Doklady Akad. Nauk S.S.S.R.*, 96, 303-305 (1947); abstracted in *Chem. Zentr.*, 1948, I [17/18] 1048.—By adding 0.8% sulfite lye, the natural density of $\text{CaSO}_4 \cdot \frac{1}{2}\text{H}_2\text{O}$ is reduced from 60 to 47% without much change in the setting time. Tensile and bending strengths are increased by the addition, a maximum occurring at 0.5 to 1%. M 11a

ASM-35A METALLURGICAL LITERATURE CLASSIFICATION

GROUPS: A, B, C, D, E, F, G, H, I, J, K, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z, AA, AB, AC, AD, AE, AF, AG, AH, AI, AJ, AK, AL, AM, AN, AO, AP, AQ, AR, AS, AT, AU, AV, AW, AX, AY, AZ, BA, BB, BC, BD, BE, BF, BG, BH, BI, BJ, BK, BL, BM, BN, BO, BP, BQ, BR, BS, BT, BU, BV, BW, BX, BY, BZ, CA, CB, CC, CD, CE, CF, CG, CH, CI, CJ, CK, CL, CM, CN, CO, CP, CQ, CR, CS, CT, CU, CV, CW, CX, CY, CZ, DA, DB, DC, DD, DE, DF, DG, DH, DI, DJ, DK, DL, DM, DN, DO, DP, DQ, DR, DS, DT, DU, DV, DW, DX, DY, DZ, EA, EB, EC, ED, EE, EF, EG, EH, EI, EJ, EK, EL, EM, EN, EO, EP, EQ, ER, ES, ET, EU, EV, EW, EX, EY, EZ, FA, FB, FC, FD, FE, FF, FG, FH, FI, FJ, FK, FL, FM, FN, FO, FP, FQ, FR, FS, FT, FU, FV, FW, FX, FY, FZ, GA, GB, GC, GD, GE, GF, GG, GH, GI, GJ, GK, GL, GM, GN, GO, GP, GQ, GR, GS, GT, GU, GV, GW, GX, GY, GZ, HA, HB, HC, HD, HE, HF, HG, HH, HI, HJ, HK, HL, HM, HN, HO, HP, HQ, HR, HS, HT, HU, HV, HW, HX, HY, HZ, IA, IB, IC, ID, IE, IF, IG, IH, II, IJ, IK, IL, IM, IN, IO, IP, IQ, IR, IS, IT, IU, IV, IW, IX, IY, IZ, JA, JB, JC, JD, JE, JF, JG, JH, JI, JJ, JK, JL, JM, JN, JO, JP, JQ, JR, JS, JT, JU, JV, JW, JX, JY, JZ, KA, KB, KC, KD, KE, KF, KG, KH, KI, KJ, KK, KL, KM, KN, KO, KP, KQ, KR, KS, KT, KU, KV, KW, KX, KY, KZ, LA, LB, LC, LD, LE, LF, LG, LH, LI, LJ, LK, LL, LM, LN, LO, LP, LQ, LR, LS, LT, LU, LV, LW, LX, LY, LZ, MA, MB, MC, MD, ME, MF, MG, MH, MI, MJ, MK, ML, MM, MN, MO, MP, MQ, MR, MS, MT, MU, MV, MW, MX, MY, MZ, NA, NB, NC, ND, NE, NF, NG, NH, NI, NJ, NK, NL, NM, NN, NO, NP, NQ, NR, NS, NT, NU, NV, NW, NX, NY, NZ, OA, OB, OC, OD, OE, OF, OG, OH, OI, OJ, OK, OL, OM, ON, OO, OP, OQ, OR, OS, OT, OU, OV, OW, OX, OY, OZ, PA, PB, PC, PD, PE, PF, PG, PH, PI, PJ, PK, PL, PM, PN, PO, PP, PQ, PR, PS, PT, PU, PV, PW, PX, PY, PZ, QA, QB, QC, QD, QE, QF, QG, QH, QI, QJ, QK, QL, QM, QN, QO, QP, QQ, QR, QS, QT, QU, QV, QW, QX, QY, QZ, RA, RB, RC, RD, RE, RF, RG, RH, RI, RJ, RK, RL, RM, RN, RO, RP, RQ, RR, RS, RT, RU, RV, RW, RX, RY, RZ, SA, SB, SC, SD, SE, SF, SG, SH, SI, SJ, SK, SL, SM, SN, SO, SP, SQ, SR, SS, ST, SU, SV, SW, SX, SY, SZ, TA, TB, TC, TD, TE, TF, TG, TH, TI, TJ, TK, TL, TM, TN, TO, TP, TQ, TR, TS, TT, TU, TV, TW, TX, TY, TZ, UA, UB, UC, UD, UE, UF, UG, UH, UI, UJ, UK, UL, UM, UN, UO, UP, UQ, UR, US, UT, UY, UZ, VA, VB, VC, VD, VE, VF, VG, VH, VI, VJ, VK, VL, VM, VN, VO, VP, VQ, VR, VS, VT, VU, VV, VW, VX, VY, VZ, WA, WB, WC, WD, WE, WF, WG, WH, WI, WJ, WK, WL, WM, WN, WO, WP, WQ, WR, WS, WT, WU, WV, WW, WX, WY, WZ, XA, XB, XC, XD, XE, XF, XG, XH, XI, XJ, XK, XL, XM, XN, XO, XP, XQ, XR, XS, XT, XU, XV, XW, XX, XY, XZ, YA, YB, YC, YD, YE, YF, YG, YH, YI, YJ, YK, YL, YM, YN, YO, YP, YQ, YR, YS, YT, YU, YV, YW, YX, YY, YZ, ZA, ZB, ZC, ZD, ZE, ZF, ZG, ZH, ZI, ZJ, ZK, ZL, ZM, ZN, ZO, ZP, ZQ, ZR, ZS, ZT, ZU, ZV, ZW, ZX, ZY, ZZ



BUDNIKOV, P. F.

PA 9T50

USSR/Building Materials
Gypsum

May 1947

"The Influence of Sulphite Cellulose Lye Upon the Properties of Semi-hydrous Gypsum," P. P. Budnikov, W. Yu. M. Butt, Member Correspondents of the Academy of Sciences, 2 pp

"Doklady Akademii Nauk SSSR" Vol LVI, No 5

Tables showing the consistency of plaster of Paris for varying amounts of the sulphite, which reduces the necessary amount of water and increases strength.

9T50

BUDNIKOV, P.P.

Budnikov, P.P. "Stone ceramic articles," in symposium: Syr'yevyye resursy tonkokeram. prom-sti SSSR i puti ikh ispol'zovaniya, Moscow-Leningrad, 1948, p. 72-78

SO: U-2888, Letopis Zhurnal'nykh Statey, No. 1, 1949

BUDNIKOV, P. P.

USSR/Engineering
Cement

Mar 1948

"Sulphated Hydraulic Slag Cements," P. P. Budnikov, Corr. Mbr., Acad. Sci., USSR, 9 pp.
Izv. Akad. Nauk SSSR, Otdel Tekh. Nauk, No. 3

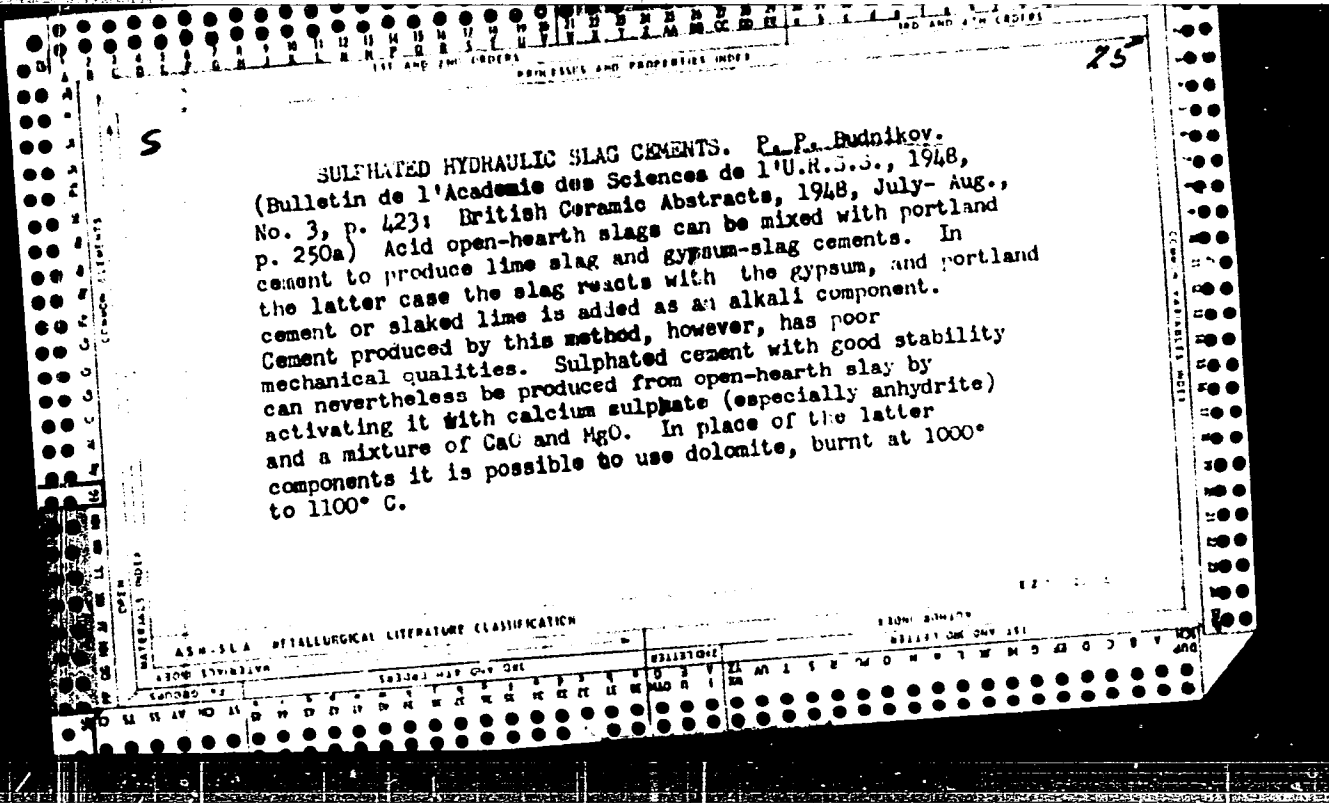
Details various experiments carried out on sulphated hydraulic slag cement to test its durability. Includes tables showing results of experiments.

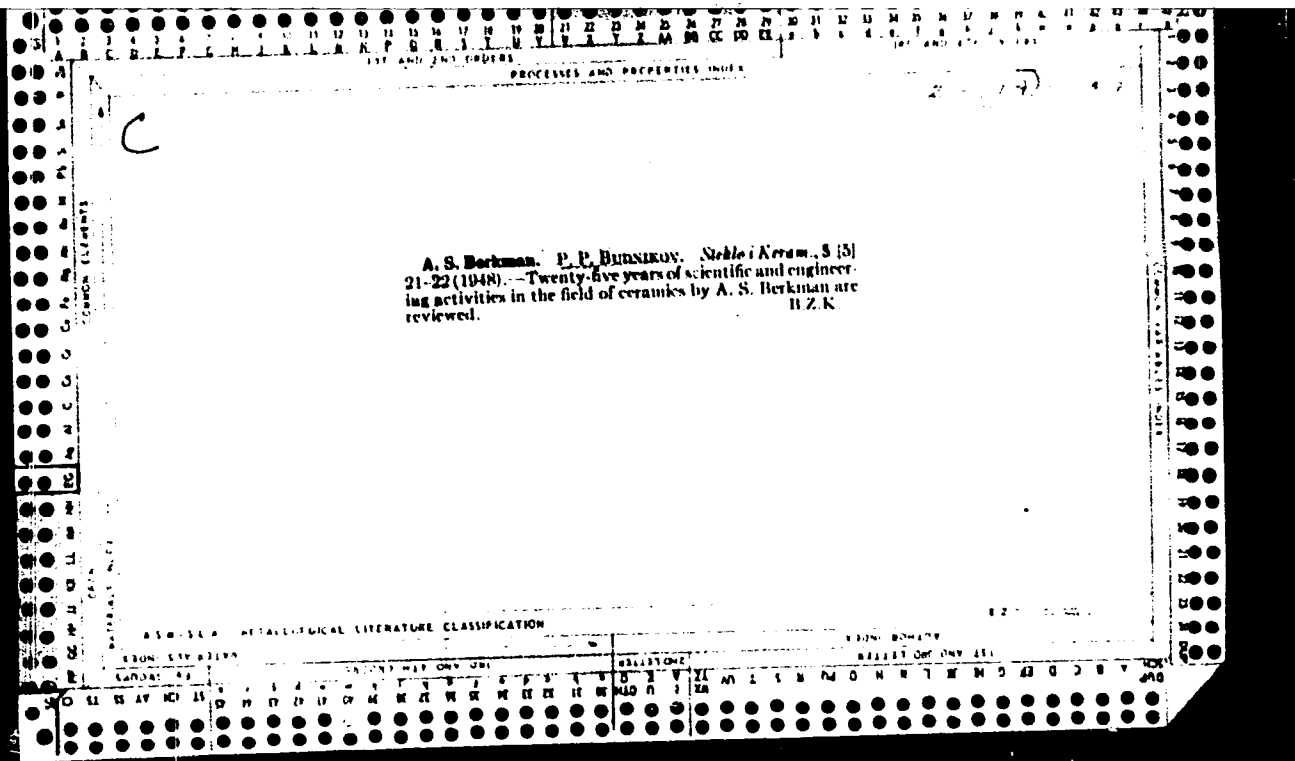
39T18

CA

Sulfated hydraulic slag cements. P. F. Dudnikov, *Izv. Akad. Nauk S.S.S.R., (Sov. Tech. Note 1968), 423-32.* Granulated blast-furnace slags possess latent hydraulic properties, higher with greater contents of Al₂O₃ as compared with SiO₂; the harmful effect of too much CaO should be offset by correspondingly more Al₂O₃. Presence of MnO at even as low as 1% lowers the hydraulic properties. The setting of slag cements can be efficiently activated by CaSO₄ with cements contg. 20% Al₂O₃; CaSO₄ disappears from the liquid phase in 1-2 days, with 10% Al₂O₃ in 3-6 days. As long as CaSO₄ is present in the liquid, practically no Al₂O₃ goes over into it. The compounds formed in the interaction between slags and Ca-compounds formed in the interaction between slags and Ca-compounds in Ca(OH)₂ water, are: basic slag [CaO] + MgO/SiO₂ in Ca(OH)₂ water, are: basic slag [CaO] + MgO/SiO₂ + Al₂O₃ = 1.04, SiO₂ 1.27, 3CaO, Al₂O₃, 3CaSO₄, H₂O + 2CaO, Al₂O₃, 3CaSO₄, H₂O + 1.22 acid slag [0.80, 1.72] 3CaO, Al₂O₃, 3CaSO₄, H₂O + 1.22 CaO, SiO₂, H₂O. Setting is at its best in the presence of 0.4-0.5 g./l. CaO in the liquid (not over 1 g./l.) which is attained by adding up to 3% CaO to the slag-CaSO₄ mixt.; this amt. of CaO in the liquid ensures best mech. properties, e.g., the curves of compressive strength of 7-day samples in water have a max. (280 kg./sq. cm.) at about 0.35 g./l. CaO, 28 days under water, max. (380 kg./sq. cm.) at 0.5 g./l. Examples of prolonged tests: basic slag (SiO₂ 35.51, Al₂O₃ 8.01, Fe₂O₃ 0.90, CaO 45.98, MgO 1.07, MnO 2.12, SO₃ 0.56, S 2.31%), 90% + CaSO₄ (anhydrite) 5% + calcined dolomite 5% compressive strength after 6 months and 3 years in fresh water, 284 and 324 kg./sq. cm.; in air, 381 and 408; in 10% NaCl, 267 and 270; in 10% Na₂SO₄, 272 and 230; after 1 year in 10% Na₂SO₄, MgSO₄, NaCl, and MgCl₂, the sulfated slag cement was stronger than portland cement. The heat

evolved in the setting of the sulfated slag cement is 20-20 cal/g. as against 30-50 cal/g. for portland cement. With basic slags, it is not necessary to add CaO, as enough of it is formed by hydrolysis of the CaS present in the slag. In addition, MgO in the form of dolomite fired at 1000-1100° is beneficial, as illustrated by the following 12-yr. tests: slag (SiO₂ 37.73, Al₂O₃ 0.07, Fe₂O₃ 0.51, CaO 47.30, Mg 1.21, Mn 1.80, CaS 2.30) 92% + CaSO₄ (anhydrite) 8%, after 12 yrs. under water, tensile strength 33.4, compressive strength 300 kg./sq. cm.; slag 90 + CaSO₄ 5 + MgCO₃ (fired) 5%, 41.4 and 340. In 1-year combined water and air tests, slag 92 + CaSO₄ 8%, 40.1 and 308; slag 93 + 01 + CaSO₄ 7 + chalk 2%, 52.8 and 338; slag 90 + CaSO₄ 5 + CaSO₄ 7 + clinker 10%, 43.5 and 314; slag 90 + CaSO₄ 5 + MgCO₃ (fired) 8%, 41.5 and 308. Acid slags are less suitable for hydraulic cements than basic slags. However, satisfactory cements can be made from acid slags with addition of CaSO₄ and either CaO or MgO or dolomite fired at not lower than 1000-1100°, example, slag (SiO₂ 30.16, CaO 44.40, Al₂O₃ 20.25, Fe₂O₃ 1.20, MgO 1.00, MnO 3.65, SO₃ 0.33, sulfide S 0.23) 80% + CaSO₄ (fired at 1000°) 15% + dolomite (fired at above 1000°) 8%, ground to 0.5-0.8% residue on a 900 mesh/sq. cm. sieve, after 3 months, tensile strength 33.3, compressive 408 kg./sq. cm. N. Thon





1ST AND 2ND ORDERS PROCESSES AND PROPERTIES INDEX

22

B

The Spinel. Formation of Spinel and Similar Compounds at High Temperatures. (In Russian.) P. P. Byd-nikov and A. S. Berezhnoi. *Uspekhi Khimii* (Progress in Chemistry), v. 17, Sept.-Oct. 1948, p. 585-605. A comprehensive review, including synthesis and properties. 108 ref.

COMMON ELEMENTS

MATERIALS INDEX

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

FROM SOURCE

LIST ONE ONLY

FROM SOURCE

LIST ONE ONLY

FROM SOURCE

LIST ONE ONLY

BUDNIKOV, P. P.

PA 64T1

USSR/Chemistry - Cement
Chemistry - Calcium Sulfate

Jan 1948

"Effect of TeTs-Cement on the Binding Properties of
Various Modifications of Calcium Sulfate," P. P.
Budnikov, Yu. M. Butt, 7 pp

"Zhur Prik Khim" Vol XXI, No 1

Subject cement speeds up hydration of calcium sulfate
and increases its hardness and water resistance.
Hardening of semihydrated and anhydrous cements goes
on best in air media, and takes approximately 7 days.
Humid climates cause setting to take place in about
28 days. Cements containing gypsum set faster than
ordinary cements. Submitted 28 Mar 1947.

64T1

BUDNIKOV, P. P.

Budnikov, P. P. and Zhukovskaia, S. S., The method of determination of silicon by volume in cast iron and steel. p. 959

The checking of the volume method of determining silicon in bakelite vessels on standard sample gave satisfactory results. It was interesting to apply this method to the quick-cutting instruments and other kinds of steel containing tungsten, the presence of which complicates the determination of silicon by the weight method.

April 13, 1948

SO: Journal of Applied Chemistry (USSR) 21, No. 9 (1948)

BUDNIKOV, P. P.

PA 11/49T33

USSR/Chemistry - Silicates -
Chemistry - Ceramic Industry

Aug 48

"Session on the Progress of Science in the Field of
Silicates," P. P. Budnikov, 3 pp

"Zhur Priklad Khimi" Vol XXI, No 8

Session was held in Oct 47. Organized by All-Union
Sci, Eng and Tech Soc of Silicate Industry and All-
Union Chem Soc imeni D. I. Mendeleev. Reports
speeches made. Submitted 20 Nov 47.

11/49T33

BUDNIKOV, P. P.

PA 11, 4973

USSR/Academy of Sciences
Chemistry

Aug 48

"Twenty Years in the Institute of Physical Chemistry
Imeni L. V. Pissarzhevskiy, Academy of Sciences,
Ukrainian SSR," P. P. Budnikov, 2½ pp

"Zhur Priklad Khimii" Vol XXI, No 8

Institute originated from Chair of Electronic Chem
organized by Pissarzhevskiy in 1922 at the Yekater-
inoslav (now Dnepropetrovsk) Mining Inst. Describes
work of Institute during past 20 years.

11/4973

BUDNIKOV, P.P.; YURKOV, M.I.

Cathodoluminescence of synthetic silicates and aluminates. Dep. AN URSR
no. 4:3-11 '48. (MLRA 9:9)

1. Diysniy chlen AN URSR (for Budnikov). 2. Ordona Lenina khimiko-tekhnologichnyy institut imeni D.I. Mendeleeva.
(Cathode ray tubes) (Silicates) (Aluminates)

BUDNIKOV, P. P.

PA 43/43T28

USSR/Geology
Clay
Gypsum

Feb 1948

"Gasha [TN: Mixture of Clay and Gypsum] and Its
Thermal Dissociation," P. P. Budnikov, Corr Mem,
Acad Sci USSR, O. P. Mchedlav-Petrosyan, 3 pp

"Dok Akad Nauk SSSR, Nova Ser" Vol LIX, No 4

Describes deposits of gasha at Tbilisi, Signakh,
Akhaltzikh (Georgian SSR), Erevan, Takhmagan,
Leminakan (Armenian SSR), Kirovobad, Lenkoran, Taus
(Azerbaijani SSR) and others. Tabulates percentage
dissociation under different conditions.

43T28

F. P. BUDNIKOV

Thermal dissociation of "garzha." F. I. Budnikov and

G. P. Mchedlov-Petrosyan. *Doklady Akad. Nauk S.S.S.R.*
59, 719-21(1948). -- In the production of SO_2 and cement from
"garzha" (a mixt. of lime, sand, gypsum, and related prod-
ucts), special attention must be paid to garzha contg. little
gypsum. If the gypsum content is high (over 30% $CaSO_4$),
a high temp. is required for thermal dissoen., but the re-
moval of SO_2 is complete in 30-60 min. at 1100° .
H. K. Livingston

6

BUDNIKOV, P. P.

Gypsum clay and its thermal dissociation. ✓ P. P. Budnikov and
✓ O. P. Mchedlov-Petrosyan. Doklady Akad. Nauk S.S.S.R., 59 [4] 719-21
(1948).---Thermal dissociation tests were conducted with gypsum clay contain-
ing 20 to 90% gypsum obtained from the largest deposits in the Georgian
S.S.R. When the gypsum content is less than 30%, it is possible to obtain
almost complete liberation of SO_3 by heating at $1100^{\circ}C$. for 0.5 to 1 hr.;
complete expulsion of SO_3 occurs from the melt. Gypsum clay having a low
gypsum content should be utilized for making binders or SO_3 .

B.Z.K.

PA 77189

BUDNIKOV, P. P.

USSR/Minerals

May 1948

Gypsum
Cement

"Research on the Gypsum of the Stalinogorsk Deposit,"
P. P. Budnikov, Corr Mem, Acad Sci USSR, 2 pp

"Dok Ak Nauk SSSR" Vol LX, No 4

(Gives tables of chemical analysis of specimens from
above deposit and properties of various cements pre-
pared from them. Submitted 9 Mar 1948.

77189

PROCESSES AND PROPERTIES INDEX

Gypsum of the Stalingorah deposit. P. P. HUDNIKOV. Doklady Akad. Nauk S.S.S.R., 60 [4] (35-36) (1948). Average analysis of the gypsum shows CaO 32.35, SO₃ 42.61, SiO₂ and Al₂O₃ 0.62, Fe₂O₃ 0.30, MgO 0.79, and H₂O 19.10%. CaSO₄·2H₂O constitutes as high as 93.07% of the material; organic matter is 0.34%; and CO₂ 3.23%. Structural hemihydrate and molding gypsums were made in the laboratory by calcining at 170°C. In making an hydraulic cement, the gypsum was calcined at 700° to 750° and ground together with 3% of Nikitovo dolomite calcined at 850°. After 28 days, compressive strength was 196 kg./cm.² and rupture strength 24 kg./cm.². To prepare estrich gypsum, the natural gypsum was calcined at 1050° and ground so that 67% and 21.90% remained on sieves of 900 and 4000 openings/cm.², respectively. The calcine contained 0.43% free lime, and the water-gypsum ratio was 24%; setting began after 1 hr. 25 min and ended after 2 hr. 19 min. After 28 days compressive and rupture strengths were 128 and 12.5 kg./cm.², respectively, and after water storage these values were 190 and 20 kg./cm.². Finishing white cement was made by calcining at 550° and 740°, grinding to leave a residue of 1 to 2% on a sieve of 1600 openings/cm.², and mixing with 2, 4, and 6% of a 35% solution of alum. Results are tabulated. H.Z.K.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

A U T H O R S

T I T L E

S U B J E C T

C O N T R O L

C O M M O N

V A R I A B L E S

I N D E X

BUDNIKOV, P. P.

Sulfoaluminate as a positive factor in preparing expanding cement. P. P. BUDNIKOV AND Z. S. KOVREVA. *Doklady Akad. Nauk S.S.S.R.*, 61 [4] 881-84 (1948). Swelling of sulfoaluminate is observed only in those cases when there is a concentration of CaO in the liquid phase. When the CaO content is less than 0.1 gm./liter, a small amount of the Ca aluminates goes into solution, the resulting sulfoaluminate formed is small, and the strength of the cement is not impaired. When the CaO content is over 1.08 gm./liter, the Ca aluminates do not dissolve and the cement acquires the characteristic of swelling due to the formation of Ca sulfoaluminate from the reaction of solid Ca aluminates with the dissolved CaO and gypsum. The swelling process was utilized as a positive factor in preparing expanding cement. The hardened products of the reaction of a mixture of activated kaolin (calcined at 800°C.), Portland cement, and lime (or lime alone) with definite amounts of water were immersed in water for 10 days, then dried at 120°C., and ground with a definite amount of gypsum. The addition of this expanding product in amounts of 5 to 15% to cement will cause the cement to expand in a moist medium. The compressive strength of the cement is slightly below that of ordinary Portland cement only during the first period of hardening. The phenomenon of expansion may be explained by the following reaction: $3(2CaO \cdot Al_2O_3 \cdot 7H_2O) + 6CaSO_4 \cdot 2H_2O + nq =$

$(3CaO \cdot Al_2O_3 \cdot 3CaSO_4 \cdot nq) + Al_2O_3 \cdot nq$. The difficultly soluble crystals of Ca sulfoaluminate thus formed gradually expand the cement in the colloidal medium of hydrated Ca silicates and aluminates. The formation of inner destructive stresses in the hardened cement does not take place because the formation of the sulfoaluminate occurs not through the reaction of the latter with gypsum but mostly through reaction of the latter with $2CaO \cdot 3H_2O \cdot 7H_2O$. Optimum compositions of expanding products are (1) kaolin (calcined at 800°C) 26%, lime 43%, Portland cement 31%; and (2) kaolin (800°C) 35% and lime 65%. The optimum addition of the expanding product is 5 to 10%. This will produce a 0.17 to 0.10% expansion of the hardened Portland cement; a greater percentage reduces the strength. Cement containing the expansion product and 1% $CaCl_2$ became impermeable to water after 13 days under a hydrostatic pressure of water of 3 atm. The addition of basic granulated blast-furnace slag to the expanding cement reduced the linear expansion considerably.

R.Z.K.

GROUPS
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Stalinogorsk deposit. P. P. BUDNIKOV. *Doklady*

P. P. BUDNIKOV

PROCESSES AND PROPERTIES INDEX

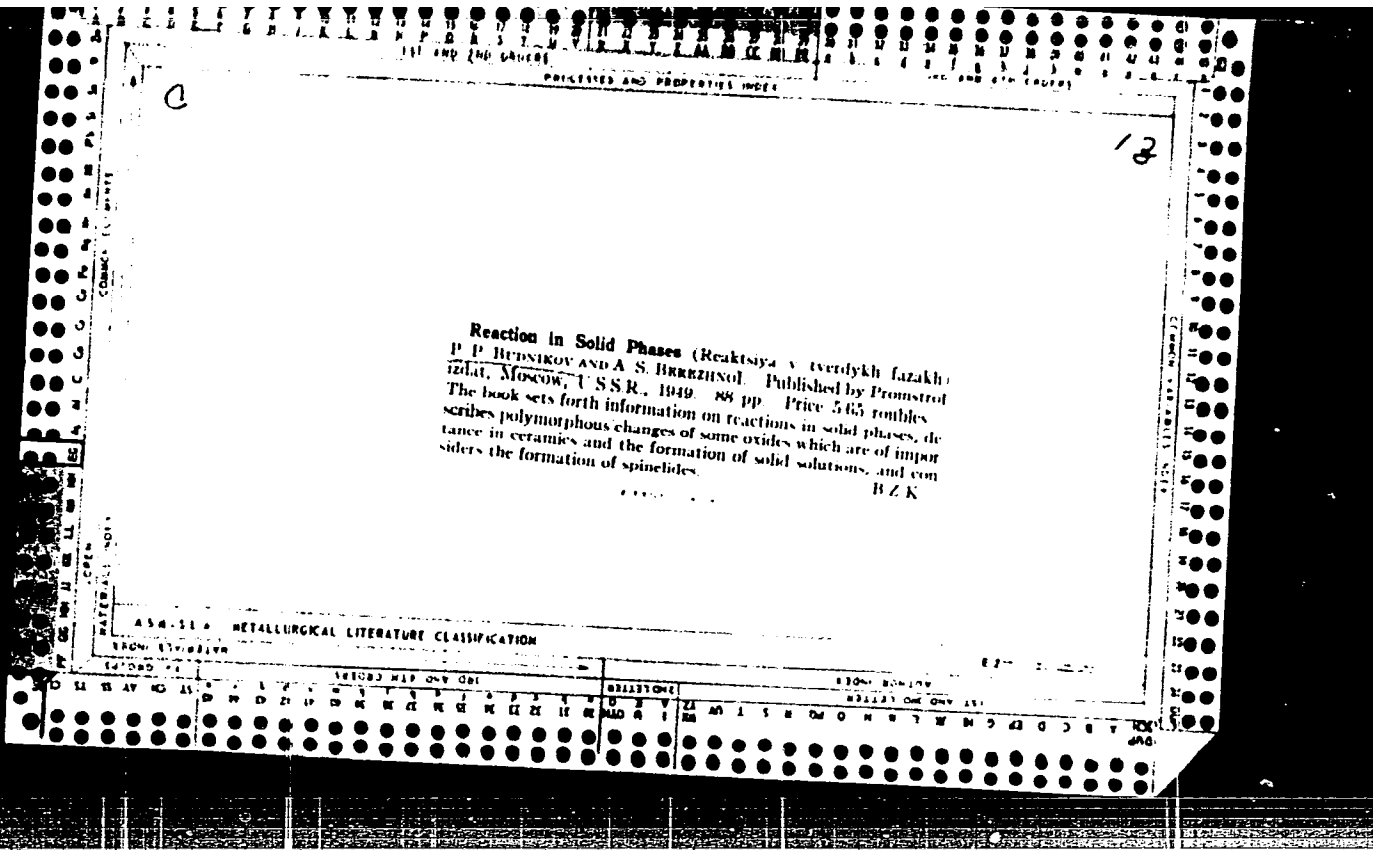
C. 17

Sulfoaluminate as an essential factor in the production of expanding cements. P. P. Budnikov and Z. S. Kosyrev. *Prokhody Akad. Nauk U.S.S.R.* 61, 681-4 (1948).

The generally known expansion effect in hardening cements and concretes accompanying the formation of $3CaO \cdot Al_2O_3 \cdot 3CaSO_4 \cdot 31H_2O$, by the reaction of excess gypsum, or by $CaSO_4$ dissolved in industrial waters, etc., with the basic Ca aluminates, e.g. with $4CaO \cdot Al_2O_3 \cdot 13H_2O$, can be made helpful if the shrinkage of the hydrated silicate gels in the setting cement is compensated by that expansion effect. The method of Lossier (*C.A.* 39, 793^a) for the production of a shrinkage-free mortar or concrete is based on this idea. B and K. recommend the production of an expanding mix by calcining kaolin at 800° , adding hydrated lime with or without an addn. of portland cement, and grinding in water the somewhat hardened mix after drying at 120° , then adding gypsum in definite ratios (e.g. 26 or 35% calcined kaolin; 43 or 65% hydrated lime; 31 or 0% portland cement; 70-75% water; gypsum added to the dried mass in the ratio 1:1). If 5-10% of this strongly expanding mass is added to portland cement, a mix is produced with practically no changes in mech. strength, but with a very low vol. change. For the production of a mortar which is also impermeable to water the addn. of 1% $CaCl_2$ to the portland cement is advisable. Also, the addn. of granulated blast-furnace slag considerably reduces the vol. changes.

W. Eitel

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GINZBURG, D.B., dktor tekhn. nauk; DELIKISHKIN, S.N., kand. tekhn. nauk;
KHODOROV, Ye.I., kand. tekhn. nauk; CHIZHSKIY, A.F., inzh.;
BUDNIKOVA, P.P., red.; SMIRNOVA, I., red.; PANOVA, L., tekhn. red.

[Furnaces and drying apparatus for the silicate industry] Pechi i su-
shila silikatnoi promyshlennosti. Pod red. P.P.Budnikova. Moskva,
Gos. izd-vo lit-ry po stroit. materialam, 1949. 483 p.
(MIRA 15:1)

1. Deystvitel'nyy chlen AN USSR (for Budnikova).
(Kilns)

BUBNIKOV, P. F. I. BLYUDNAYA, L. N.

29082

K. Voprosu o Stoyakoperaniye. (V svyaz s Stat'ey V. V. Gancharova
"O Stoyakoperaniye Kak Otnosheniye" V Zhurn. "Obyedyneniye". 1949,
No 4) Obyedyneniye, 1949, No 9, S. 393-97, -- Bibliogr: 9 Naev.

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