PUSTYNNIKOV, Vasiliy Grigor'yevich, kend. tekhn. nauk, detsent; AHSIMOV, Sergey Rmitriyevich, aspirant

Electronic device for controlling quality in thermal treatment of steel components. Tav. vys. ucheb. zav.; elektromekh. 7 no.4x471-478 *64 (MIRA 17:7)

1. Kafedra elektrotekhniki Rostovskogo ma-Donu instituta selisko-khozysystvennogo mashinostroyeniya. 2. Zavedujushchiy kaiedrey elektrotekhniki Rostovskogo na-Donu instituta seliskokhozysystvennogo mashinostroyeniya (for Pustynnikov).

PUSTYNNIKOV, V.G.; ANISIMOV, S.D.

Multiparametric electromagnetic testing of steel products. Zav. lab. 30 no.10:1236-1239 '64. (MIRA 18:4)

1. Rostovskiy institut sel'skokhozyaystvennogo mashinostroyeniya.

ANISIMOV, Sergey Dmitriyevich, aspirant

Formation of a multifrequency signal with consideration of information quantity. Izv. vys. ucheb. zav.; elektromekh. 8 no.4:437-440 '65. (MIRA 18:5)

1. Kafedra elektrotekhniki Rostovskogo instituta sel'skokhozyaystvennogo mashinostroyeniya.

sov/2908

28(0)

PHASE I BOOK EXPLOITATION

Anisimov, Sergey Fedorovich

Chelovek i mashina; filosofskiye problemy kibernetiki (Man and Machine; Philosophical Problems of Cybernetics) Moscow, 1959. 53 p. 24,000 copies printed.

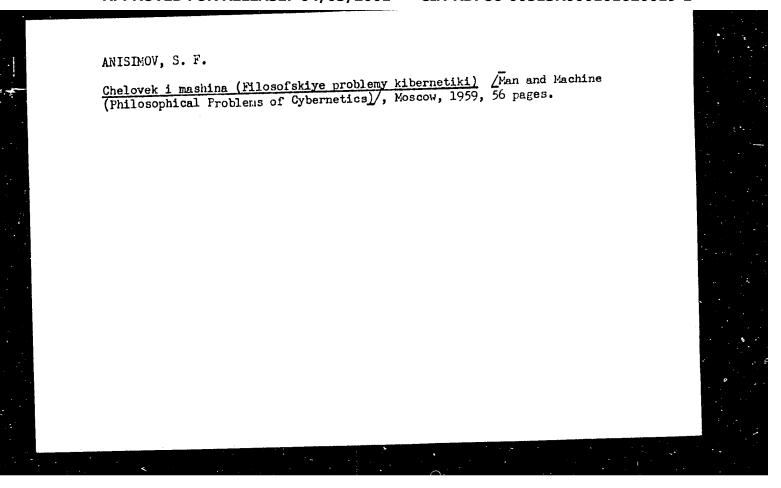
Sponsoring Agency: Obshchestvo po rasprostraneniyu politicheskikh i nauchnykh znaniy RSFSR.

Ed.: V. F. Fal'skiy; Tech. Ed.: I. I. Zhernevskaya.

PURPOSE: This booklet is intended for those interested in methods of control and communication applied to the analysis of the operations of machines.

COVERAGE: The booklet briefly describes the origin and development of cybernetics and its current application in the analysis of the operation of such machines as electronic computers. Some aspects of the theory of information, feed back and self-adjustment of systems, and high-speed electronic computers are

Card 1/2



ANISIMOV, S. and VISLOBOKOV, A.

"Certain Philosophical Problems of Cybernetics," Korumunist, 1960, No. 2, Pages 108 - 118.

11.2000

5/057/60/030/009/019/021 B019/B054

AUTHOR:

Anisimov, S. I.

TITLE:

in a Nonideal Gas γ Heavy Detonation

PERIODICAL:

Zhurnal tekhnicheskoy fiziki, 1960, Vol. 30, No. 9,

pp. 1124-1127

TEXT: The author writes down the equation of state which describes the substance in heavy detonations in a much simplified form:

 $p = gRT[1 + bg + 0.625(bg)^2 + 0.2869(bg)^3 + 0.1928(bg)^4]$ (1). In his

further investigation, the author starts from system (2) which describes the central-symmetric motion of the medium. By substitution (3) this system is transformed into systems of ordinary differential equations whose solution and integrals are thoroughly discussed. The essential physical condition is the assumption that $C_{\mathbf{v}}$ is constant even at high temperatures. Finally, water is considered as an example. As pressure in (1) is assumed to be proportional to temperature, the author had to

Card 1/2

Heavy Detonation in a Nonideal Gas

\$/057/60/030/009/019/021 B019/B054

restrict himself to sufficiently high temperatures. Fig. 1 graphically shows the density-, pressure-, and velocity distributions. The author thanks M. A. Yel'vashevich, Academician of the AS BSSR, and Professor A. S. Kompaneyets for discussing the work. There are 1 figure and 5 references: 4 Soviet and 1 US.

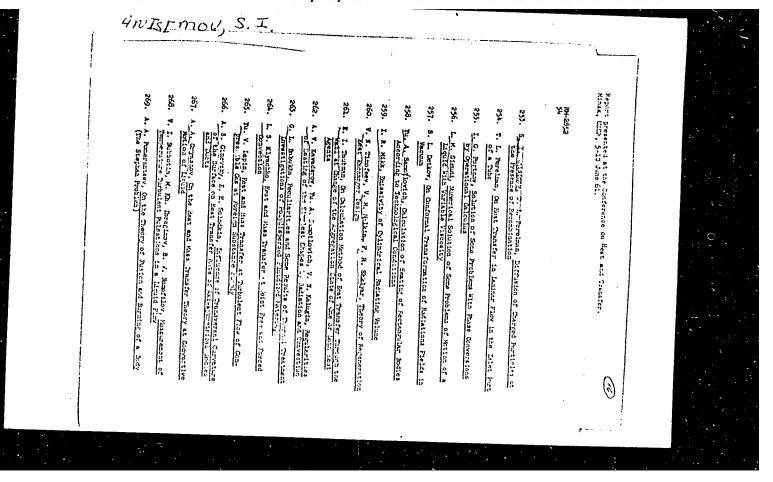
ASSOCIATION: Institut fiziki AN BSSR Minsk (Institute of Physics of the AS BSSR, Minsk)

SUBMITTED:

October 3, 1959

Card 2/2

"APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R000101620019-1



316lili \$/207/61/000/006/021/025 A001/A101

1.1210

AUTHORS: Anisimov, S. I., Kuznetsov, N. M. (Minsk, Moscow)

TITLE:

Self-modeling problem of strong explosion in water

PERTODICAL: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 6, 1961,

167-168

TEXT: The authors consider the self-modeling problem of strong explosion for the case when disturbed motion is spherically symmetric and temperature T₂ (at the shock wave front) exceeds considerably 3,000 K. The equation system of central-symmetrical adiabatic motion in partial derivatives is transformed into a system of ordinary differential equations and its order is lowered by using integrals of energy and adiabaticity following from the self-modeling nature of the motion (investigation of self-modeling solution was conducted by N. N. Kochina and N. S. Mel'nikov) and, after transformations, one differential equation of the first order is obtained. This equation is integrated numerically and the results for velocities, pressures and densities as functions of distances traveled by the shock wave are tabulated and presented graphically. An equation is derived which enables one to calculate the distance r₂ traveled by the shock

Card 1/2

35758 5/124/62/000/003/037/052 D237/D302

11.5300

AUTHORS:

Yel'yashevich, M.A., and Anisimov, S.I.

TITLE:

Relaxation phenomena in high-velocity gas flows

PERIODICAL:

Referativnyy zhurnal, Mekhanika, no. 3, 1962, 103, abstract 3B669 (Dokl. AN BSSR, 1961, no. 8, 5, 324-

326)

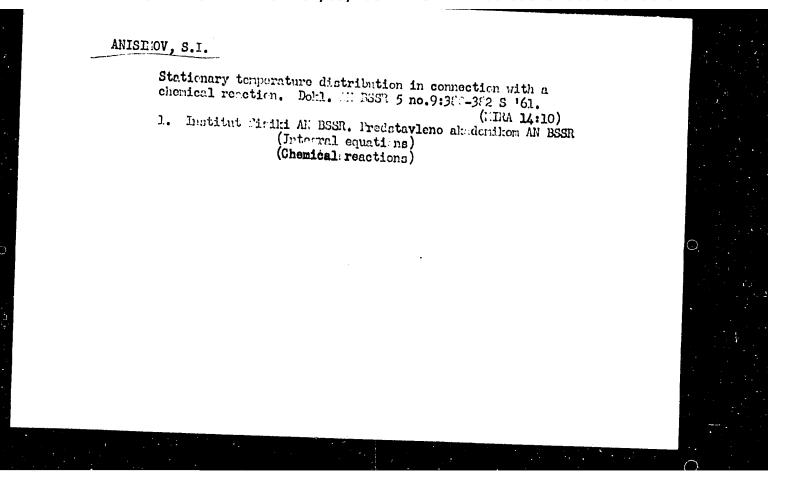
TEXT: A simple, approximate method is considered, of calculating non-uniformities of flow in problems of gaseous dynamics. The menon-uniformities of flow in problems of gaseous dynamics. The motion is based on the fact that in many cases, interesting from the practical point of view, the flow appears to be locally either almost in equilibrium or almost stationary. The reason for this is most in equilibrium or almost stationary for the thermodynamic equitate the time of relaxation t, necessary for the thermodynamic equilibrium to catchlish itself in various weakly excited degrees of librium to establish itself in various weakly excited degrees of freedom, is very seldom temperature dependent. Also, characteristic time of the gas-dynamical process τ_0 which can be defined as $\tau_0 = V(d V/dt)^{-1}$ (W - specific enthalpy), depends on the local temperatures to an even smaller extent. Hence, the temperature inter-Card 1/2

Relaxation phenomena in high- ...

S/124/62/000/003/037/052 D237/D302

val in which τ and τ_0 are comparable, is very narrow. In the zero approximation in solutions of gas-dynamical problems it can be assumed that in the regions where $\tau = \tau_0$ the flow is in equilibrium, while for τ · τ_0 it is stationary. The surface where $\hat{\tau}$ = τ_0 resembles the surface of discontinuity for the derivative da/dx where a - a magnitude characteristic for an unstable process, e.g. degree of dissociation or energy of molecular vibrations. At to to, da/dx = da/dx (\bar{a} - equilibrium magnitude), while for $\tau > \tau_0$, da/dx = 0. All the entropy changes concentrate on the surface of discontinuity, as equilibrium and stationary flows are isentropic. As an example, the dependence of the magnitude ln τ/τ_0 on the x-coordinate is calculated for recombination of oxygen in the flow through a conical nozale. Initial temperature and pressure were 5000°C and 0.1 atm. The graph shows that a hundredfold change of τ/τ_0 occurs at a distance equal to the diameter of a critical cross-section, i.e. a stationary flow occurs very seldom. More exact calculations can beperformed by the method of successive approximations, using the solution obtained by the above method, as a zero approximation. [Abstractor's note: Complete translation].

Card 2/2



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31726 \$/057/61/031/012/013/013 B104/B112

AUTHOR :

Anisimov, S. I.

TITLE:

Establishment of oscillation equilibrium behind a shock

wave

PERIODICAL:

Zhurnal tekhnicheskoy fiziki, v. 31, no. 12, 1961,

1491 - 1493

TEXT: In the range of establishment of oscillation equilibrium, a flow

is described by the system of equations

 $\rho v = \rho_{0} v_{0},$ $p + \rho v^{2} = p_{0} + \rho_{0} v_{0}^{2},$ $l + \frac{v^{3}}{2} = l_{1} + \frac{v_{0}^{2}}{2},$ $l = \frac{7}{2} RT + E_{k_{1}}$ $p = \rho RT,$ $v \frac{dE_{k}}{dx} = \frac{E_{k}(T) - E_{k}}{\sigma(p_{1}T)},$ (1)

Card 1/5

31726 S/057/61/031/012/013/013 B104/B112

Establishment of oscillation...

where E_k is the oscillation energy per unit mass, $E_k(T)$ its equilibrium value at the temperature T, and $T(\rho_1 T)$ the relaxation time. $T(\rho_1 T) = \frac{A}{\rho_1 T^{1/6}} \exp(B/T^{1/3})$ is valid according to L. Landau et al.

(Phys. Zs. d. Sowjetunion, 10, 36, 1936). After introducing the dimensionless specific volume $V = f_0/\rho = v/v_0$ and carrying out a simple

transformation, $\frac{x}{x_0} = \frac{1}{\epsilon} \int_{\frac{\rho_2}{\epsilon}}^{\frac{\tau_0}{\rho}} \frac{\tau(z) \left(6z - \frac{7}{2}a\right) z dz}{E(z) + \frac{7}{2}az - 3z^2 - b},$ (3)

> here $a = 1 + \frac{1}{\tau_0 M^2}; \quad b = \frac{1}{2} \left[1 + \frac{2}{(\tau_0 - 1) M^2} \right]; \quad x_0 = v_2 \tau_2; \quad \epsilon = \frac{\rho_0}{\rho_2};$ $\tau(z) = \frac{\tau \left[\frac{\rho_0}{z} : \frac{v_0^2}{R} z (a - z) \right]}{\tau_0}; \quad E(z) = \frac{1}{v_0^2} E_k \left[\frac{v_0^2}{R} z (a - z) \right].$

 γ_{i}

Card 2/5

Establishment of oscillation...

S/057/61/031/012/013/013 B104/B112

is obtained by integrating the equation of motion. The index "O" refers to the supersonic flow, and the index "2" to the equilibrium flow. Quantities referring to the area immediately behind the wave front are denoted by the index "1". Bearing in mind the above-mentioned function for (, (3) can be integrated only numerically. With reference to a paper by D. A. Frank-Kamenetskiy (Diffuziya i teploperedacha v khimicheskoy kinetike. Izd. AN SSSR, M., 1947), instead of (3),

$$\frac{x}{x_0} = \frac{1}{\epsilon^2} \int_{\frac{h}{h}-\epsilon}^{\frac{h}{h}-\epsilon} \frac{(t+\epsilon)^2 \left(6t - \frac{7}{2}\alpha + 6\epsilon\right) e^{-\frac{h}{2}}}{\left[\left(C + \frac{7}{2}\right)\alpha - (C+6)\epsilon - (C+3)\epsilon\right]} dt,$$

is obtained, where $z=\xi+t$, CR is the specific oscillation heat capacity, and $k=(BR^{1/3}/v_0^{2/3})/\{(a-2\xi)/\xi(a-\xi)^{4/3}\}$. This integral is

Card 3/5

31726 S/057/61/031/012/013/013 B104/B112

Establishment of oscillation ...

given in tables. For the case of strong shock waves,

$$\frac{\pi}{\pi_0} = \frac{354}{29} \left(e^{-k\left(V - \frac{1}{8}\right)} - e^{-\frac{2k}{14}} \right) + \frac{22}{29} \left(EI \left(-\frac{k}{24} \right) - EI \left[-k\left(V - \frac{1}{8}\right) \right] \right).$$
 (A)

is obtained, where Ei(-x) = $\int_0^\infty e^{-t} dt/t$. Terms of the order of $(f_0/f_1 - \xi)^2 \approx 0.0017$ are neglected. The solution

$$p\tau = \frac{\rho_0}{v_0} \frac{E(V) + \frac{7}{2} aV - 3V^2 - b}{\left(6V - \frac{7}{2} a\right)V \frac{dV}{dx}},$$
$$T = \frac{v_0^2}{R} V(a - V).$$

of (1) is given for investigations where the relaxation time of the gas is determined from the experimental density distribution behind a shock

Card 4/5

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Perel'man, T.L., and Anisimov, S.I.

AUTHOR:

Density Distribution of Charged Particles in Meteor Tracks

Doklady Akademii nauk SSSR, 1961, Vol. 136, No. 4, pp. 810-812 TITLE:

For the purpose of studying the reflection of radiowaves from PERIODICAL: meteor tracks it is necessary to know the density distribution of charged particles. By diffusion, recombination, and addition of electrons to neutral atoms and molecules, density changes, the latter effect not changing the density distribution, but the effective recombination coefficient. The relative effect of recombination and diffusion upon the density distribution may be expressed by the dimensionless parameter $\xi=\alpha q/D$, where α is the recombination coefficient , q the number of ionizations per unit length of the meteor track, and D the diffusion coefficient. A differential equation is given, which describes the density of charged particles produced by a meteor moving with uniform speed:

Card 1/3

Density Distribution of Charged Particles S/

88404

S/020/61/136/004/012/026 B019/B056

$$\partial n/\partial t = D_{r}^{1} \frac{\partial}{\partial r} (r \frac{\partial n}{\partial r}) - \omega n^{2} + \frac{q}{2 \sqrt{r}} g(-\frac{r}{r_{0}}) \delta(z - vt)$$
 (2)

$$n(0,t)<\infty$$
 , $n(\infty,t)=0$ (3)

This differential equation may be calculated by means of the perturbation theory in the case of small ε . With ε being greater, the perturbation theory is not applicable, and an approximation has to be found. The authors discuss the two methods of solution and obtain expressions describing the time dependence of the number of charged particles. They thank Academician Ya.B. Zel'dovich for valuable advice, as well as Member of the AS BSSR M.A. Yel'yashevich, G.L. Barenblatt und Yu.P. Rayzer for discussions. There are 3 references: 2Soviet and 1 US.

ASSOCIATION:

Institut fiziki Akademii nauk BSSR

(Institute of Physics, Academy of Sciences BSSR)

PRESENTED:

September 1, 1960, by Ya.B. Zel'dovich, Academician

Card 2/3

Density Distribution of Charged Particles S/020/61/136/004/012/026 B019/B056

SUBMITTED: July 22, 1960

Card 3/3

\$/207/62/000/001/011/018 14 7 6 3 B B145/B138 116360 AUTHORS: Anisimov, S. I., Romanov, G. S. (Minsk) TITLE: Nonequilibrium flow of air in nozzles PERIODICAL: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 1, 1962, 76 - 81 TEXT: The article deals with some problems of the kinetics of adjusting equilibrium between the transletory and inert degrees of freedom of the molecules in air at high temperature. The following slow processes which occur in air at high temperatures are studied: $0 + 0 + M \neq 0 + M$ (1) $N+N+M
ightharpoonup N_0+M$ (2). $N + O + M \stackrel{\longrightarrow}{=} NO + M$ (3) 0+N, ≠N0+N (4) N+0, ≠ NO+0 (5) Os* + M = Os + Y (6) $N_1 + M \Rightarrow N_1 + C$ (7)

Nonequilibrium flow of ...

\$/207/62/000/001/011/018 B145/B138 Since there is up to 150-200% uncertainty in the rate constant values ($k_{\underline{i}}$

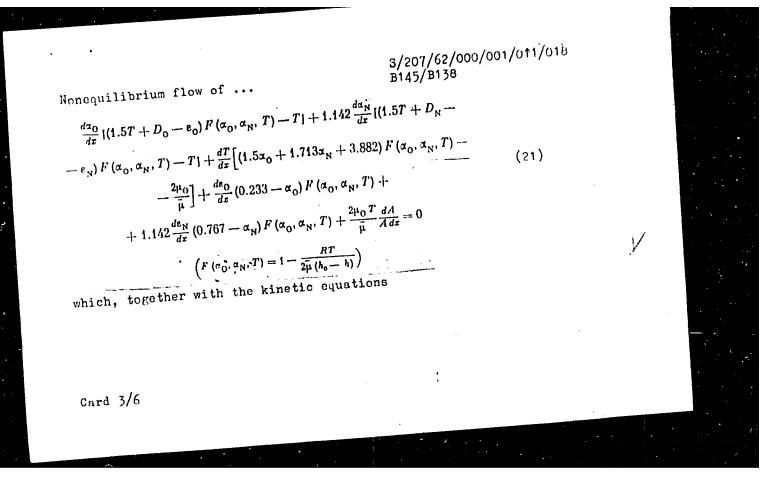
rate constant of the go-reaction, k! of the return reaction), some simplifications are made: ki, any molecule or atom, is equally effective as third body during recombination, the contribution of NO to the total energy and total pressure is neglected and 5 (d [NO]/dt) = 0 is assumed. The effect of the vibrational relaxation on the rate of recombination may be neglected when the condition k $T_{r}/C \ll 1$ (k rate constant of the reaction) $M + 0 \stackrel{*}{2} \rightarrow 0 + 0 + M$, γ density, \tilde{c} mean molecular weight, \tilde{c} relaxation time) is satisfied. If the weight fractions are denoted by α_i (i = 0, N), the dissociation energies by $\mathbf{D}_{\mathbf{i}}$, and the equilibrium energies of vibration by \mathcal{L}_{i} , using the equation system $\langle vA(x) = const, dp/dx + \rho v dv/dx = 0$, $h_0 - h - v^2/2 = 0$ (18) (A(x) nozzle cross section) (for a one-dimensional

flow without diffusion, friction or heat exchange, one obtains the equation

Card 2/6

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Nonequilibrium flow of ...

Nonequilibrium flow of ...
$$\frac{d\alpha_{0}}{dx} = \frac{2p}{v\mu} \left(k_{1} \frac{0.233 - \alpha_{0}}{2} - k_{1}' \frac{\alpha_{0}^{2}p}{\mu_{0}} \right) + \frac{2}{v} \left[k_{5} \frac{p\alpha_{N}(0.233 - \alpha_{0})}{2\mu_{N}} - k_{5}'\alpha_{0}[NO] \right]$$

$$\frac{d\alpha_{N}}{dx} = \frac{2p}{v\mu} \left(k_{2} \frac{0.767 - \alpha_{N}}{2} - k_{3}' \frac{\alpha_{N}^{2}p}{\mu_{N}} \right) + \frac{2}{v} \left[k_{4} \frac{p\alpha_{0}'(0.767 - \alpha_{N})}{2\mu_{0}} - k_{4}'\alpha_{N}[NO] \right] \tag{22}$$

Здесь

$$\frac{d\varepsilon_{0}}{dx} = \frac{1}{v} \frac{\varepsilon_{0}(T) - \varepsilon_{0}}{\tau_{0}(T, \rho)}, \qquad \frac{d\varepsilon_{N}}{dx} = \frac{1}{v} \frac{\varepsilon_{N}(T) - \varepsilon_{N}}{\tau_{N}(T, \rho)}$$

$$NO] = \frac{\rho}{2} \frac{2k_{3}' \alpha_{N} \alpha_{O} \rho / \overline{\mu} + k_{4} \alpha_{O} (0.767 - \alpha_{N}) + k_{5} \alpha_{N} (0.233 - \alpha_{O})}{k_{3} \mu_{O} \mu_{N} / \overline{\mu} + k_{4}' \alpha_{N} \mu_{O} + k_{5}' \alpha_{O} \mu_{N}}$$

forms a closed system, the integration of which requires numerical methods. In the case of a "partial freezing in" (vibration in equilibrium, but without change of gas composition, the following solution is easily obtained:

Card 4/6

Nonequilibrium flow of ...

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(23)

$$\frac{A}{A_{\bullet}} = \left(\frac{T}{T_{\bullet}}\right)^{\frac{0.5\alpha_{O} + 0.671\alpha_{N} + 2.773}{\alpha_{O} + 1.142\alpha_{N} + 1.109}} \times \sqrt{\frac{c^{3}_{\bullet}}{2(h_{0} - h)}} \times$$

$$\times \exp \frac{(0.233 - \alpha_0)(f_0^* - f_0) + 1.142(0.767 - \alpha_N)(f_N^* - f_N)}{\alpha_0 + 1.142\alpha_N + 1.109}$$

$$f_i = \frac{\theta_i}{T} \left(1 - \exp \frac{-\theta_i}{T} \right)^{-1} - \ln \left(\exp \frac{\theta_i}{T} - 1 \right)$$

The asterisks denote quantities which are variable in the critical cross section. The vibration was assumed to be harmonic. In the case of an equilibrium flow it is best to start from the changed Eq. (18):

gvA(x) = const, $h_0 - h - v^2/2 = 0$, $S = S_0$ (S entropy), since integration of (21), (22) leads to unclear solutions. Calculation of the system (21), (22), by means of an electronic computer, for some concrete values of the initial densities and temperatures, showed that the deviation from equilibrium is high for nozzles of about 10 cm, and that the approximation of the "frozen-in flow" is better than that of the equilibrium flow. Ya. B. Card 5/6

S/250/62/006/001/001/002 I028/I218

AUTHOR:

Anisimov, S. I. and Khodyko, Yu. V.

TITLE:

Convective diffusion in the boundary, layer in the case of flow inside an angle

PERIODICAL: Akademiya nauk Belaruskay Doklady. v. 6, no. 1, 1962, 19-21

TEXT: The flow in a dihedral angle formed by plane plates is considered, and the equations of convective diffusion in its boundary layer are solved exactly. The differential equation describing the distribution of the concentration c(x,y)

$$v_x \partial c/\partial x + v_y \partial c/\partial y = D d^2 c/dy^2$$
 (1)

is integrated, and its general solution is given. Two simple particular cases are indicated: a) for $c(x,0) = c_0$ = const, $c(x,y) = c_0$; b) for $c(x,0) = c_0 x^{-n}$, $c(x,y) = c_$

ASSOCIATION: Institut fiziki AN BSSR (Institute of Physics of AS BSSR)

PRESENTED: March 20, 1961

Card 1/1

ANISIMOV, S.I. (Minsk); PEREL'MAN, T.L. (Minsk)

A nonlinear heat transfer problem. PMTF no.5:136-139 S-0
'63. (MIRA 16:11)

ACCESSION NR: AP4004149

\$/0294/63/001/002/0276/0280

AUTHORS: Anisimov, S. I.; Nogotov, Ye. F.

TITLE: Steady-state theory of a thermal explosion

SOURCE: Teplofizika vy*sokikh temperatur, v. 1. no. 2, 1963, 276-

280

TOPIC TAGS: thermal explosion, thermal explosion stationary theory, temperature distribution, iteration method, temperature jump, steady state theory, explosion

ABSTRACT: The conditions under which stationary temperature distribution is possible in a medium containing temperature-dependent heat sources is analyzed mathematically, with a particular aim of determining the critical dimension of the region containing the heat sources (D), beyond which stationary temperature distribution becomes impossible (thermal explosion becomes possible). The problem reduces essentially to an investigation of the existence of a solution of the boundary value problem $\Delta t + qf(u) = 0$ in the domain (D) with

Card 1/12

ACCESSION NR: AP4004149

 $u=u_0$ on the boundary of this domain. It is shown that some results can be obtained with the aid of known existence and uniqueness theorems for the solutions of integral equations. By way of an example a detailed analysis is made of the one-dimensional problem $T^1+q\,\exp(-1/T)=0;\,0\le x\le 1$

 $T(1) = T_0, T'(0) = 0$

(T - temperature in units of activation energy E, $q = Q\ell^2/Ek$ - dimensionless parameter, in which k - thermal conductivity of the medium, Q - intensity of heat release in the chemical reaction, and ℓ - dimension of the vessel) for which uniqueness and existence conditions are obtained. 'In conclusion the authors are grateful to M. A. Yel'yashevich and A. S. Kompaneyets for a discussion of some results of the present work.' Orig. art. has: 10 formulas and 1

ASSOCIATION: Institut fiziki AN BSSR (Physics Institute, AN BSSR)

SUBMITTED: 07Jun63

DATE ACQ: 26Dec63

ENCL: 00

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ANISIMOV, S.I.; ROMANOV, G.S.

Kinetics of the decay of two-atomic molecules in the absence of vibrational equilibrium. Dokl. AN BSSR 7 no.6:376-377 Je '63. (MIRA 16:10)

1. Institut fiziki AN BSSR. Predstavleno akademikom AN BSSR M.A.Yel'yashevichem.

ANISIMOV, S.I.

Effect of vibrational relaxation on the dissociation rate of diatomic molecules. Zhur. fiz. khim. 37 no.12:2754-2757 D '63.

(MIRA 17:1)

1. Institut fiziki AN BSSR.

ANISIMOV, S.I.; KHODYKO, Yu.V.

Flow of a gas with delayed vibrations past the frontal critical point of a blunt-nosed body. Zhur. tekh. fiz. 33 no.ll:1333-1337 N '63. (MIRA 16:12)

1. Institut fiziki AN BSSR, Minsk.

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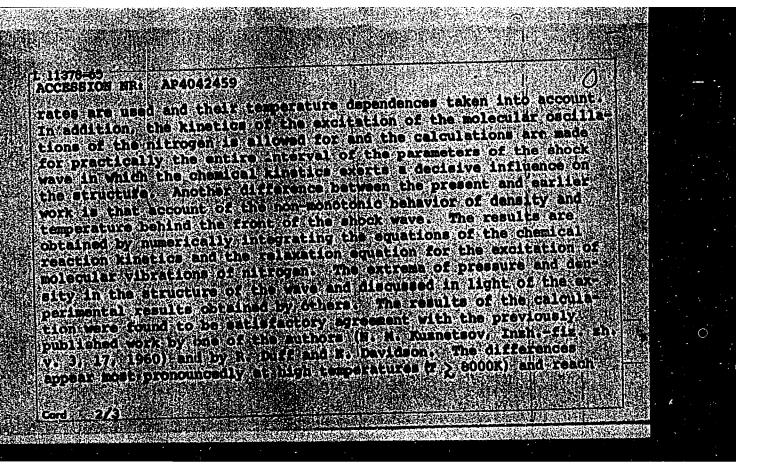
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ACCESSION NR: AP3003176

AUTHORS: Anisimov, S. I.; Romanov, G. S.

TITLE: On kinetics of diatomic molecule dissociation in absence of vibrational equilibrium

SOURCE: AN BSSR. Doklady, v. 7, no. 6, 1963, 376-377

TOPIC TAGS: rotational equilibrium, vibration relaxation, dissociation rate, diatomic molecule, vibration equilibrium, Boltzmann distribution, vibration energy

ABSTRACT: On the assumption of rotational equilibrium, the effect of vibrational relaxation on the dissociation rate has been studied in diatomic molecules. The case of small deviations from vibrational equilibrium was considered, assuming a Boltzmann distribution for the vibrational degrees of freedom, with temperature Ti slightly different from the translational temperature T, or, for Δ = T-T/T

$$\frac{\mu^1}{h} \approx 1 + \frac{E(T) - \vec{E}_m}{KT} \Delta,$$

where $E(T) = \frac{1}{I(T)} \sum_{k=0}^{N-1} E_k - E_k/K_F^2$, and E_m - arithmetic mean of vibrational energy in Cord 1/2

ACCESSION NR: AP3003176

interval (N-m,N). The largest effect caused by vibrational nonequilibrium has been evaluated for the distribution function $\int_{i}^{\infty} \left\{ \begin{array}{c} 0 & i \neq 0 \\ 1 & i = 0 \end{array} \right\}$.

ASSOCIATION: Institut fiziki AN BSSR (Institute of Physics, AN BSSR)

SUBMITTED: 01Nov62

DATE AQ: 21,Jul63

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NO REF SOV: 003

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Card 2/2

ACCESSION NR: AP4028948

AUTHOR: Anisimov, S.I.

8/0057/64/034/004/0620/0623

TITLE: On the non-monotonic variation of temperature and density behind a strong

SOURCE: Zhurnal tekhnicheskoy fiziki, v.34, no.4, 1964, 620-623

TOPIC TAGS: shock wave, shock wave temperature variation, shock wave density varia-

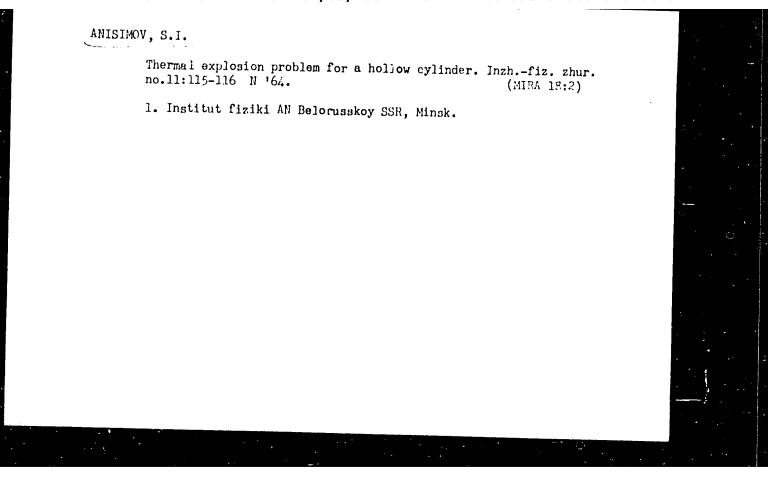
ABSTRACT: The variation of temperature and pressure in the non-equilibrium region behind a shock front is discussed qualitatively. Following Ya.B.Zel'dovich and Yu. P.Rayzer (UFN 63,3,1957), the author calls a degree of freedom "inert" provided its relaxation time is long compared with the mean free flight time of a molecule. It is the presence of inert degrees of freedom (molecular vibrations, dissociation, electron excitation, etc.) that gives rise to extended non-equilibrium regions behind shock fronts. If the relaxation times of all the inert degrees of freedom are distinct and remain so throughout the whole non-equilibrium region (they are functions of the pressure and temperature), the temperature falls monotonically from its Card 1/3

ACCESSION NR: AP4028948

value immediately behind the shock front to its equilibrium value far behind the front. If, however, the difference between the relaxation times of two inert degrees of freedom changes sign at some temperature between the initial and equilibrium values, the temperature may pass through a minimum within the non-equilibrium region, and if those two inert degrees of freedom are the only important ones, it will indeed do so. In this case the density will pass through a maximum if dissociation processes are not involved, and it may pass through a maximum if such processes are involved. The case of dissociation of oxygen and excitation of nitrogen molecular vibrations is adduced as an example of a pair of inert degrees of freedom satisfying the required condition; at sufficiently high temperatures the dissociation is the more rapid process, but since recombination takes place via three-body collisions, it may become the slower process in the cooler regions. An explanation of observed non-monotonic temperature and density variations offered by A.Resler & B.Cary, and J.Logan (references are given only to Russian translations) is criticized, but the discussion is too brief to permit a judgement to be formed concerning the merit (or even the nature) of the rejected explanation. "In conclusion, I express my sincere gratitude to L.E. Gurevich and Yu.P. Rayzer for discussing the

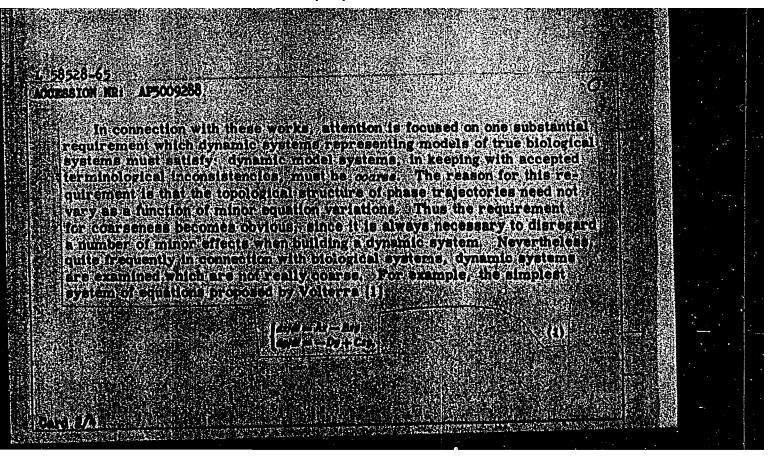
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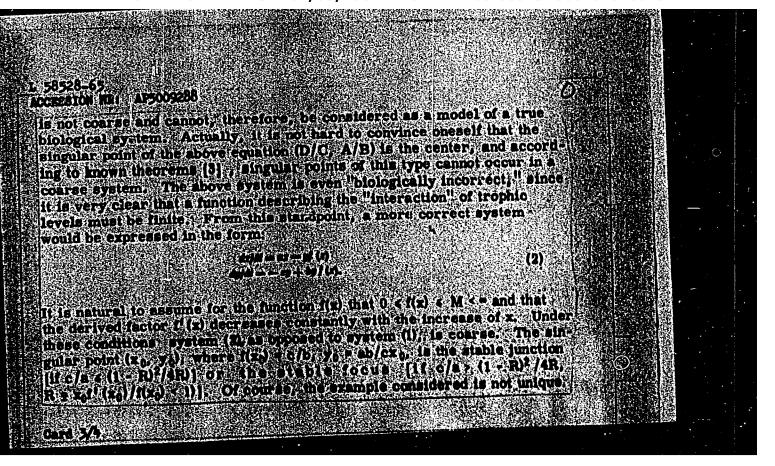
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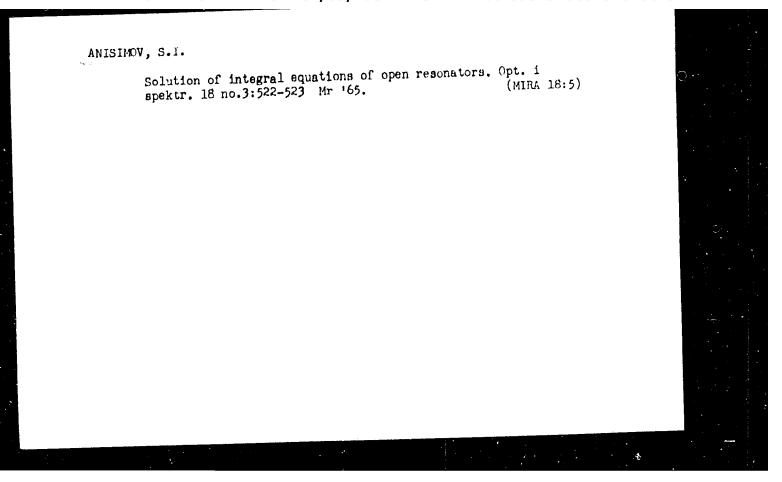
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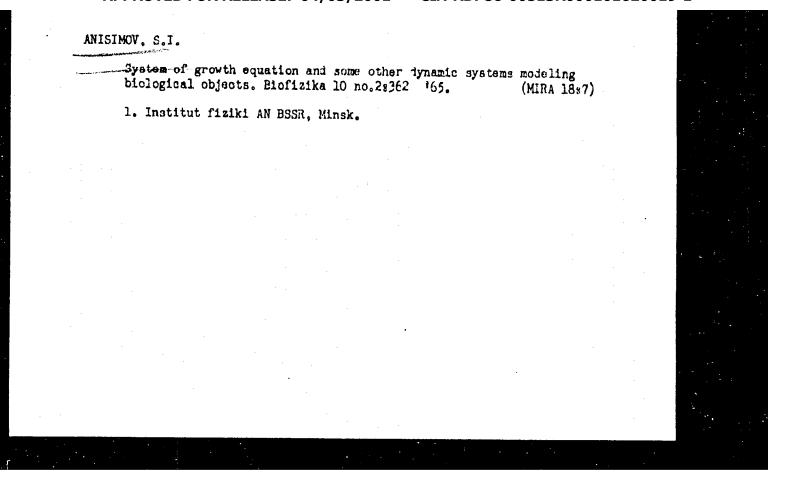
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ACC NR: AP6025256 SOURCE CODE: UR/0057/66/036/007/1273/1284

AUTHOR: Anisimov,S.I.; Bonch-Bruyevich,A.M.; Yel'yashevich,M.A.; Imas,Ya.A.;

Pavlenko,N.A.; Romanov,G.S.

ORG: none

TITLE: The effects of intense light beams on metals

CURCE: Zhurnal tekhnicheskoy fiziki, v. 36, no.7, 1273-1284

TOPIC TAGS: laser effect, metal melting, metal vaporizing, heat of sublimation

ABSTRACT: The authors have investigated theoretically and experimentally the phen-

omena accompanying the disruption of metals by focused laser beams. In the present paper there is considered the case of a laser producing approximately 1 millisec pulses, each consisting of a sequence of approximately 1 microsec spikes. The phenomena accompanying disruption of metals by giant laser pulses will be discussed in a future paper. In the theoretical part of the paper, fluxes of 10¹² to 10¹⁶erg/cm² sec on an approximately 1 mm diameter spot are considered. It is shown that under these conditions the transport of energy in the metal by heat conduction during the duration of a spike is negligible, and the problem of the vaporization of the metal is accordingly treated in one dimension. Formulas are derived, and curves are presented for different metals, relating the energy flux in the laser beam, the temperature of the metal surface, the erosion rate of the metal surface (i.e., the rate of increase

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ACC NR: AP6025256

in the depth of the hole), and the velocity and pressure of the jet of metal vapor. The temperature of the metal surface is not equal to the boiling temperature, as was erroneously assumed by J.F.Ready (J. Appl. Phys., 36, No.2, 462, 1965). The theoretical relations were tested by experiments on some 16 metals and alloys, using neodymium glass lasers producing up to 300 J pulses. The laser beam was focused with a lens onto the parallelepipedonical specimen and the disruptive process was recorded cinematographically at 105 frames per sec. In most of the experiments a glass plate was cemented to one face of the specimen and the laser beam was so directed parallel to the glass-metal boundary that about half of the beam passed freely through the glass and the other half penetrated into the metal, vaporizing it. In those experiments the process was photographed through the glass. The mass of metal removed by the laser pulse was determined by weighing the specimen, and the impulse due to reaction of the metal vapor jet was measured. The experiments were in qualitative agreement with the theory, and quantitative agreement in order of magnitude was found. The authors feel that development of a more accurate theory would not be worthwhile, owing to the large variations between different lasers. Three stages were distinguished in the disruption process: in the first stage the temperature of the metal surface increased at the rate of approximately 10^{10} degree/sec; in the second stage metal was vaporized from the specimen and a hole was formed in it; and in the third stage a pressure of 10^2 to 10^3 atmospheres developed within the hole and a powerful jet of metal vapor issued from it at supersonic velocities. The ratio of the laser pulse energy to the mass of metal

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EMP(m)/EWT(1)/EWT(m) WM/JW/JWD SOURCE CODE: UR/0207/66/000/004/0150/0151 L 09326-67 ACC NR. 126050934 AUTHOR: Anisimov, S. I. (Minsk); Vitkin, E. I. (Minsk) ORG: none TITLE: Some variational problems of the theory of thermal explosions SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 4, 1966, 150-151 TOPIC TAGS: thermal explosion, variational problem, nonlinear differential equation, ABSTRACT: The authors point out that most of the results obtained in stationary theory of thermal explosion pertains to symmetrical regions, in which the temperature distribution depends on a single space coordinate, whereas practical problems deal with two or three independent variables, for which the nonlinear partial differential equations are difficult to solve without a tremendous amount of numerical calculations. It is shown, since the solutions of physical interest are only those corresponding to low temperatures, that the calculations can be simplified by approximating the exponential temperature dependence with a trinomial. The application of this approximation to the variational solution of problems involving a cylinder of finite length, a rectangle, and a parallelepiped show satisfactory agreement with results obtained by others. Orig. art. has: 11 formulas. SUB CODE: 20/ SUBM DATE: 17May65/ ORIG REF: 004/ OTH REF: 001 Card 1/1/

ACC NR. AT7000377

SOURCE CODE: UR/0000/66/000/000/0006/0103

AUTHOR: Anisimov, S. I.; Khodyko, Yu. V.

ORG: Instituto of Physics, AN BSSR, Minsk (Institut fiziki AN BSSR)

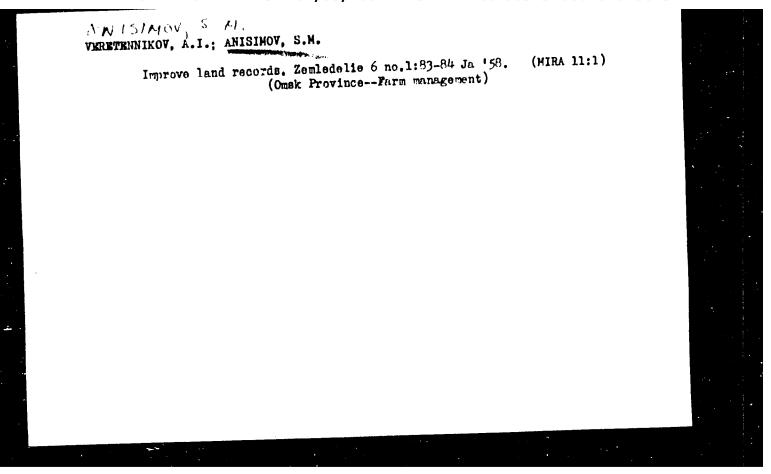
TITLE: . Convective diffusion in the boundary layer with flow in an angle

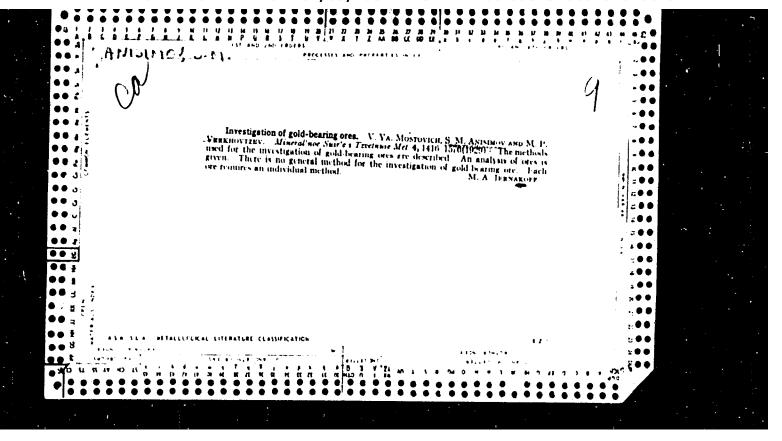
SOURCE: Teplo- i massoperenos, t. 6: Metody rascheta i modelirovaniya protsessov teplo- i massoobmena (Heat and mass transfer, v. 6: Methods of calculating and modeling heat and mass transfer processes). Minsk, Nauka i tekhnika, 1966, 96-103

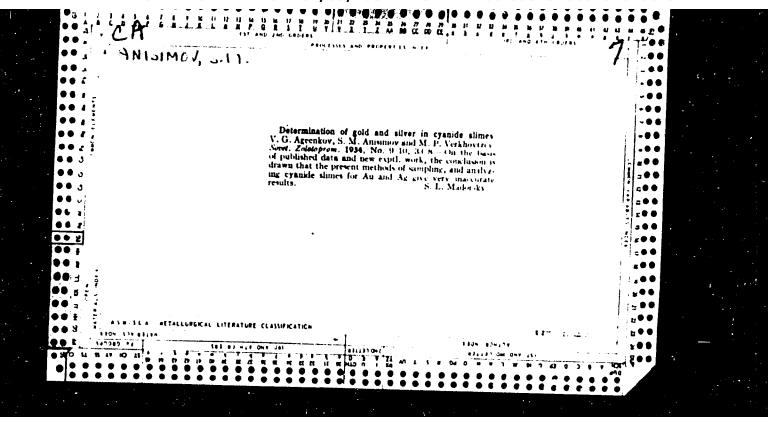
TOPIC TAGS: laminar flow thermal diffusion, mathematic analysis, boundary layer theory

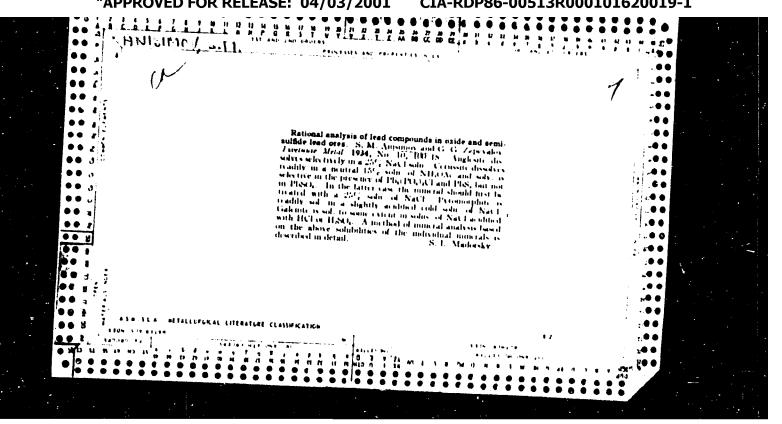
ABSTRACT: The article presents an exact analytical solution for the equation of convective diffusion in the laminar layer with flow between non-parallel flat walls. In the mathematical formulation of the problem it is assumed that the liquid is incompressible and non-dissipating, and the concentration of reacting impurities in the flow is small, so that any change in the parameters of the flow as a function of the composition or the temperature can be neglected. The coordinate system is chosen as the system of equations, which can be integrated, can be writtin in the form:

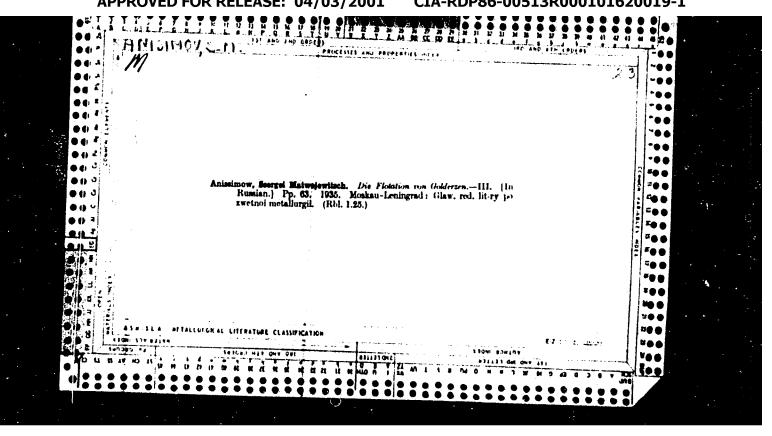
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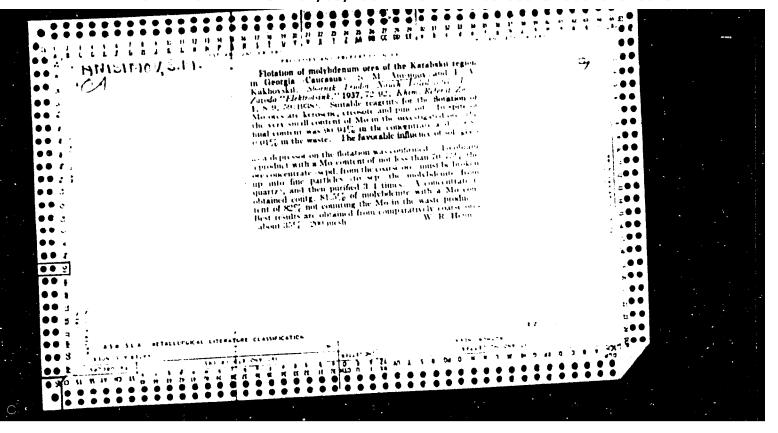


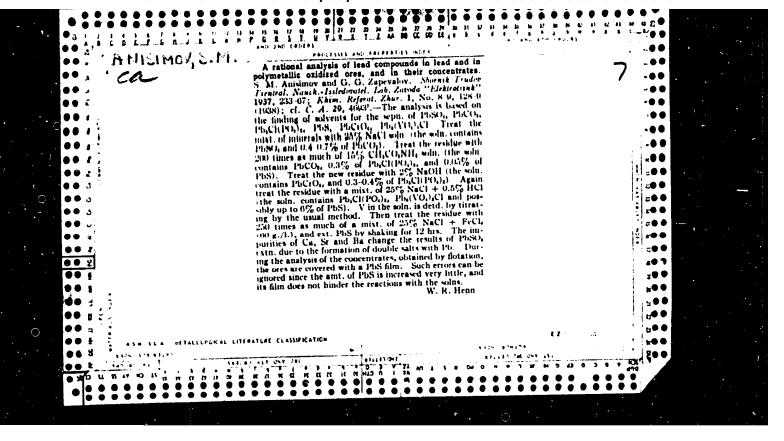










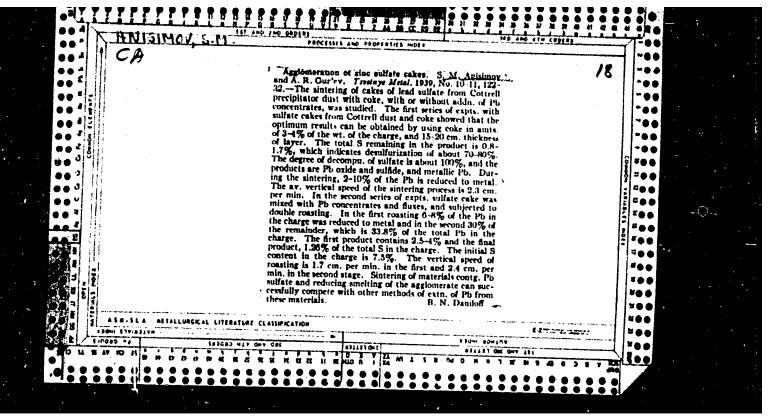


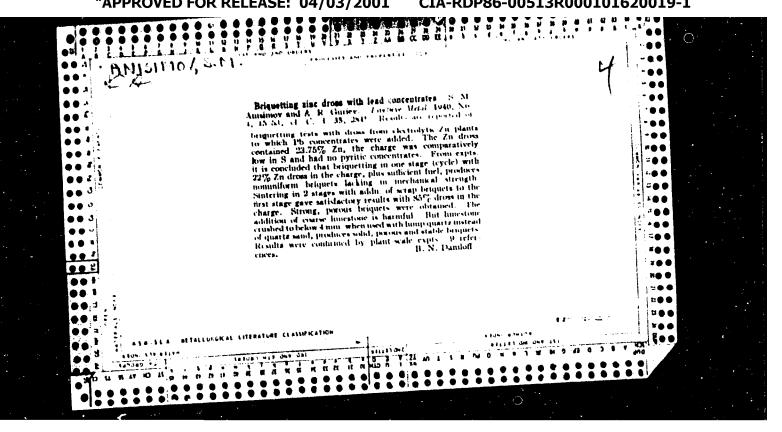
ANISIMOV, S.M., GURIYEV, A. R.

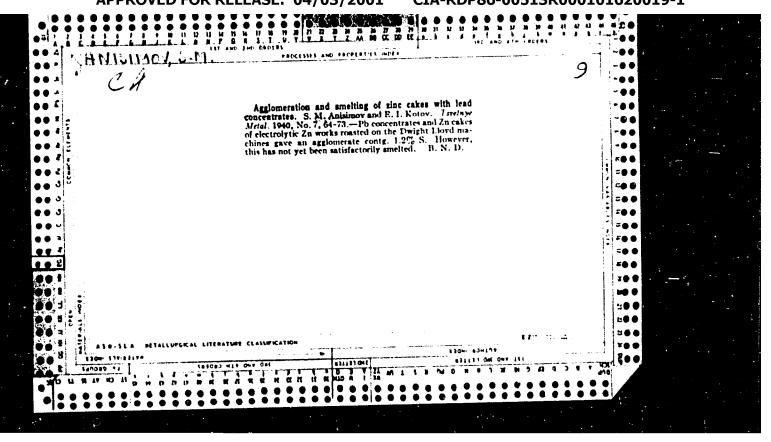
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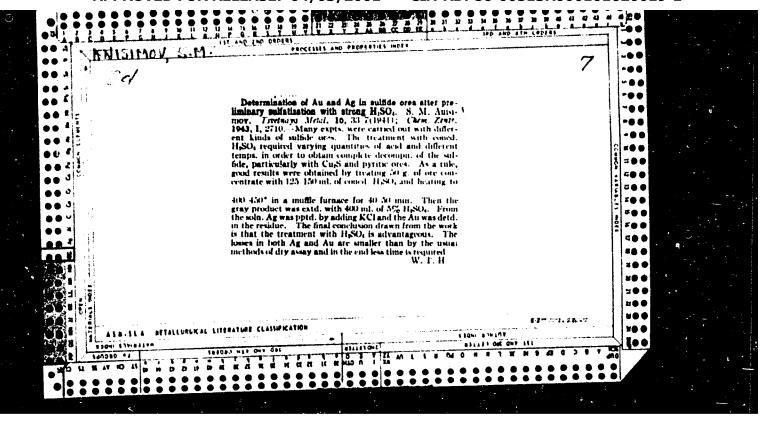
Professor, Cendidate of Technical Sciences
The Sintering of Lead Sulphite Cakes"
Tsvet. Met. 14, No. 10-11, Oct. - Nov. 1939

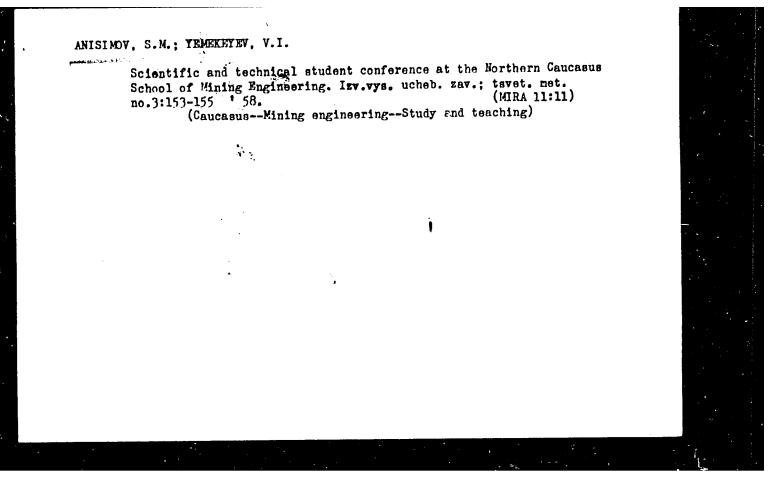
Report U=1506, 4 Oct. 1951











SOV/149-58-6-6/19

AUTHORS: Anisimov, S.M. and Dashkov, N.P. (Deceased)

TITLE: Roasting and Sintering of Zinc and Lead Concentrates in

Oxygen-enriched Air (Obzhig i aglomeratsiya tsinkovogo i svintsovogo kontsentratov v atmosfere vozdukha,

obogashchennogo kislorodom)

PERIODICAL: Izvestiya Vysshikh Uchebnykh Zavedeniy, Tsvetnaya

Metallurgiya, 1958, Nr 6, pp 49 - 63 (USSR)

ABSTRACT: The object of the investigations described in the present

paper was to check the claims made by various workers (Refs 1-5) who have stated that application of oxygeneriched air for roasting zinc concentrates can increase the rate of oxidation, the degree of degulably restion

the rate of oxidation, the degree of desulphurisation and the concentration of SO₂ in the exhaust gases, although

this method of roasting when applied to lead concentrates, which form easily fusible mixtures, might cause diffi-

which form easily fusible mixtures, might cause difficulties in obtaining a completely roasted and desulphurised

product. The experimental work was carried out in a laboratory apparatus for autogenous down-draught blast-roasting, shown in Figure 1, as follows: 1 - oxygen

Cardl/9 cylinder, 2 - pressure regulator, 3 - gas mixer provided

SOV/149-58-6-6/19
Roasting and Sintering of Zinc and Lead Concentrates in Oxygen-enriched Air

with a propeller, 4 - sintering vessel measuring 20 x 20 cm and 50 cm high, with an effective hearth area of 120 cm², 5 - electric igniting device, 6 - two microgauges for measuring the flow of gases, 7 - dust chamber, 8 - suction pump capable of drawing 150 m³ through 1 m² of the hearth area per minute at the maximum vacuum of 390 mm H₂O and 9 - electric motor.

The oxygen content (up to 70%) of the gas mixture could be controlled within + 2% and was periodically checked by chemical analysis of the mixture and by the manometer readings. The quantity of air admitted to the gas mixer was controlled by varying the vacuum under the hearth. The weight of the charge varied between 14 and 30 kg. Before each experiment the charge was moistened and then carefully mixed. A small quantity of roasted agglomerate placed on the grate served to support the charge, on top of which 30 g of coke and 200g of dry sawdustwere placed to facilitate ignition. Gas permeability of the charge

SOV/149-58-6-6/19
Roasting and Sintering of Zinc and Lead Concentrates in Oxygen-

was determined by measuring the rate of flow of the gas mixture on the entry side of the sintering vessel. The temperature of the charge and of the exhaust gases and the vacuum gauge and micro-manometer readings were recorded at least once a minute throughout each experiment. In each experiment three to twelve samples of the exhaust gases were analysed for the CO₂ and oxygen contents. The

charge was made up to dry zinc concentrate - 40 mesh size and partially roasted concentrate - 6 mesh size. The compositions of the concentrate (top line) and the partially roasted concentrate (bottom line) are given in a table on p 51 (in the latter case both the total sulphur content and the proportion of sulphur present in the form of sulphate are given). To obtain maximum gas permeability, in the first series of experiments 8% of H₂O

was added to charge consisting of 85% calcine and 15% concentrate. After each experiment, a sample of the obtained calcine, crushed and screened through a 4 mm sieve was analysed for total sulphur content, sulphur

Card3/9

enriched Air

Roasting and Sintering of Zinc and Lead Concentrates in Oxygenenriched Air

present as SO_{μ} , total zinc and zinc soluble in a 10% solution of H2804. In the first stage of the investigation, the effect of the sulphur content of the charge, consisting of 14.5 to 29% concentrate and 85.5 to 71.0% calcine and forming a layer of 250 mm high, on the rate of roasting was studied. The results of some experiments are given in Table 1 (top for air roasting, bottom for roasting in oxygen-enriched air), and in Figures 2 and 3. The time dependence of the basic parameters of the sintering process in experiments Nr 63 (without added oxygen) and Nr 58 (oxygen-enriched air) is shown in Figures 2 and 3, respectively. The scales of these diagrams (from left to right) are & follows: flowmeter readings in mm H20; vacuum in mm H20; the temperature of the exhaust gases in ^OC; the temperature of the charge in ^OC. In the next series of experiments, in which the sulphur content of the charge remained constant and equal to 5% (corresponding to a content of concentrate of 15%), Card4/9 the effect of the thickness of the layer of the charge and

SOV/149-58-6-6/19
Roasting and Sintering of Zinc and Lead Concentrates in Oxygeneniched Air

of the variation of the oxygen content of the gas mixture were studied. The results of these experiments are given in Table 2 (top part - variable thickness of the charge layer, bottom part - variable oxygen content of the gas mixture). In the next series of experiments, the effect of the oxygen content in the gas mixture and of the rate of flow of the mixture was examined, the other conditions being: the concentrate content of the charge - 13 to 15%; the thickness of the charge layer - 350 mm in experiments with air and 250 mm in experiments with oxygen/air mixture. The data are given in Table 3. The variation of the main parameters of the roasting process during experiments Nrs 31 and 51 is shown in The scales are the same as Figures 4 and 5, respectively. those in Figures 2 and 3 with the exception that the curves shown in Figure 4 do not include a graph of the variation of the temperature of the charge. The charge used in experiments comprising the next stage of the investigation consisted of 10 to 18% concentrate, 40 to 32% partially roasted product and 50% calcine when roasting was done in

Card5/9

Roasting and Sintering of Zinc and Lead Concentrates in Oxygenenriched Air

air, and 10% concentrate, 40% partially roasted product, and 50% calcine when roasting in an air/oxygen mixture. In both cases, 10 to 12% H₂0 was added to the charge and

the thickness of the charge layer in all the experiments was 200 mm. The results of these experiments are given in Table 4.

Finally, roasting and sintering of lead concentrates were studied, using both air, and air/oxygen mixture. Materials used in these experiments included lead concentrate containing 69.1% Pb, iron ore with 64.0% Fe, quartz with 94.7% SiO₂ and limestone containing 50% CaO. Roasting and

sintering were carried out in two stages. The charge used in the first stage consisted of: 100 kg concentrate, 14.7 kg iron ore, 10.6 kg quartz, 13.7 limestone and 0 to 40% sintered agglomerate. The quantity of fluxes used was calculated to give a slag containing 24% SiO₂, 34% FeO,

16% CaO and 14% ZnO. The charge without the sintered Card6/9 agglomerate contained 50% Pb, 11% S in the form of sulphide

Roasting and Sintering of Zinc and Lead Concentrates in Oxygenenriched Air

> and 7% HoO. The charge used for the second roast consisted of the product of the first operation crushed to -6 mm size and contained 4 to 6% moisture, The thickness of the charge layer in the first and in the second stages of the process was 200 and 300 to 325 mm, respectively. results of the experiments are given in Table 5. It is stated in the conclusions that: 1) the results of experiment on single-stage roasting of zinc concentrate with recirculation of the calcine carried out in air and air/oxygen mixture showed that, other conditions being equal, the ate of roasting and, consequently, the output per unit hearth area increased in proportion to the increase of the oxygen content of the air/gas mixture. Application of the air/oxygen mixture increased the degree of desulphurisation of the concentrate and correspondingly decreased the sulphur content of the final product. Calcine was obtained under these conditions which, even when the sulphur-rich fines had not been separated, contained as little as 0.12 to 0.4% S; 2) the higher the quantity of air or the air/oxygen

Card7/9

SOV/149-58-6-6/19 Roasting and Sintering of Zinc and Lead Concentrates in Oxygenenriched Air

> mixture blown through the charge per unit time, the higher was the rate of roasting. 3) when the sulphur content of the charge roasted in air exceeded 5 to 6%, the temperature attained by the charge

during roasting and the rate of moasting increased, a large quantity of ZnO crystals was formed, premature fusion of the charge occurred and calcine with a high S content was obtained. Although the oxidising reaction was even more intensive when an air/oxygen mixture was used, the calcine produced under these conditions had a low S content, did not contain ZnO crystals and had good mechanical strength; application of the air/oxygen mixture resulted in an increase of the SO2 content of the exhaust gases. (Better

utilisation of the oxygen could be obtained if the exhaust gases with low contentration of SO, were re-circulated.); 5) although the cadmium and lead contems of the calcine roasted in air/oxygen mixtures were very low owing to more intensive volatilisation of these impurities, the losses Card 8/9 of zinc under these conditions, due to volatilisation, did

SOV/149-58-6-6/19

Roasting and Sintering of Zinc and Lead Concentrates in Oxygenenviched Air

not exceed 1 to 2% and were not higher than those occurring

during roasting in air.

6) In comparison with two-stage roasting, the one-stage process gives more uniformly roasted and sintered product, increases the output of the hearth reckoned in wight of ZnS treated per unit hearth area per unit time.

7) Application of air/oxygen mixture for roasting Pb-rich concentrates did not increase the rate of burning owing to the fact that these concentrates tend to fuse at comparatively low temperatures.

There are 5 figures, 5 tables and 11 references, 7 of which are Soviet, 3 English and 1 German.

ASSOCIATION: Severokavkazskiy gornometallurgicheskiy intitut.

Kafedra metallurgii tyazhelykh tsvetnykh metallov (North Caucasian Institute of Mining and Metallurgy.

Chair of Heavy Non-ferrous Metals)

SUBMITTED: June 9, 1958

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ROZHKOV, P.I., laureat Stalinskov premii, otv.red.; PSHENITSYN, N.K., retsenzent; ZVYAGINTSEV, O.Ye., prof., doktor khim.nauk, retsenzent; PRILEZHAYEVA, N.A., prof., doktor fiz.nauk, retsenzent; ANISIMOV, S.M., prof., red.; SHULAKOV, P.G., red.; SEMENOVA, N.Ya., red.; GUT'KOV, A.D., red.; DOLGIKH, V.I., red.; KAMAYEVA, O.M., red.izd-va; ISLENT'YEVA, P.G., tekhn.red.

[Methods of analyzing platinum metals] Metody analiza platinovykh metallov, zolota i serebra; sbornik nauchnykh trudov. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1960. 256 p. (MIRA 13:9)

1. Russia (1917- R.S.F.S.R.) Krasnovarskiy ekonomicheskiy administrativnyy rayon. Sovet narodnogo khozyaystva. 2. Chien-korrespondent AN SSSR (for Pshenitsyn).

(Platinum--Analysis) (Gold--Analysis)

(Silver--Analysis)

Drying granulated concentrates and sinter cake by the suction of preheated air. Izv.vys.ucheb.zav.; tsvet.met. 3 no.2:74-79 (60. (MIRA 15:4)

1. Severokavkazskiy gornometallurgicheskiy institut, kafedra metallurgii tyazhelykh metallov. (Ore dressing) (Sintering)

SERIKOV, Z.A.; ANISIMOV, S.M.

Alkali-sulfide method for the treatment of flue dust in lead refineries. Ixv. vys. ucheb. zav.; tsvet. met. 3 no. 6:65-73 (60. (HIRA 14:1))

1.Sb Werokavkazskiy gornometallurgicheskiy institut. Kafedra metallurgi blagorodnykh i redkikh metallov. (Fly ash)

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S/149/61/000/001/006/013 A006/A001

AUTHORS:

Anisimov, S.M., Saval'skiy, S.L., Osipov, A.P.

TITLE:

The Separation of Selenium and Tellurium From Platinum Metals in

the Form of Trivalent Perric Selenite and Tellurite

PERIODICAL:

Izvestiya vysshikh uchebnykh zavedeniy, Tsvetnaya metallurgiya,

1961, No. 1, pp. 101 - 105

A method for the separation of selenium and tellurium from platinum metals used in analytical practice is based on their joint precipitation with ferric hydroxide (Ref. 1). This method was tested and described by M.F. Proshkovich and P.V. Faleyev (Ref. 2). The control of the full separation of selenium and tellurium from platinum metals would be facilitated and simplified, if there were data available on the solubility of trivalent ferric selenites and tellurites in hydrochloric acid solutions at different acidities and temperatures, and on the effect of ammonium chlorides on their solubility. If in hydrochloric acid solutions, containing tetravalent tellurium and trivalent iron, the amount of the latter is not sufficient to form ferric tellurite, tellurium dioxide may be precipitated if the solutions are neutralized. To bring about tellurium separation in

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The Separation of Selenium and Tellurium From Platinum Metals in the Form of Trivalent Ferric Selenite and Tellurite

the form of dioxide, the optimum pH value must be known at which its speeded up precipitation and the effect of ammonium chloride take place. Eventually, to obtain ferric selenite and tellurite precipitates, enriched with selenium and tellurium, the pH values must be selected, at which not only the coprecipitation of platinum metals but also that of some impurities (iron) can be prevented. The aforementioned problems were studied by the authors with the participation of Engineer K.S. Perel'muter. Ferric selenite was prepared by the interaction of ferric sulfate and sodium selenite by a method given in Reference 3, according to which the precipitate has a constant composition with a Re:Se molar ratio corresponding to Fe2(SeO3)3. The composition of the dry precipitate of Fe selenite obtained is expressed by the formulae $Fe_2(SeO_3)_3$. $3H_2O$. Ferric tellurite was prepared by the interaction of 0.1 n. solution of sodium tellurite (pH = 1.1) with 0.3 n. solution of ferric sulfate. The molar Fe:Te ratio exceeded 2 - 3 times the stoichiometric ratio of these elements in the formula Fe₂(TeO₃)3. The composition of the dry precipitate is expressed by the formula Fe2(TeO3) . H2O. The solubility of selenite and tellurite of trivalent iron was studied at 19, 40 and 70°C in hydrochloric acid solutions with pH = 1; 1.5; 2.0 and 2.5 and also in HCl solu-Card 2/4

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The Separation of Selenium and Tellurium Prom Platinum Metals in the Form of Tri-

tions containing 10% $NH_{4}C1$ with pH = 1 and 2.5, at 19°C. It was found that the solubility of ferric tellurites and selenites decreased with a lower acidity of the solutions; it was higher in HCl solutions with 10% ammonium chlorides. At elevated temperatures in HCl solutions with pH = 1, a slight increase of trivalent ferric selenite and tellurite solubility takes place. In saturated solutions with pH 1.5, 2.0 and 2.5, the Te, Se: Fe ratio increases. To investigate the stability of HCl solutions of tetravalent tellurium, two initial solutions were prepared by dissolving TeO2 in HCl. The former had a pH value of 0.85 and contained 0.98 mg/ml Te; the latter contained 2 mg/ml Te and 50 g/l NH4Cl with a pH value equal to 0.5. It was found that the precipitation of tellurium dioxide from HCl solutions of tetravalent tellurium proceeded already at a pH value of 0.5 and attained a maximum rate at pH = 5.3 - 5.4. The precipitation of tellurites and selenites of trivalent iron from HCl solutions containing free HCl, NH4Cl and ammoniates of platinum, palladium rhodium, ruthenium, iridium was investigated at their neutralization with scda. The initial solution was composed of Se - 665; Te - 766; Fe = 708; Pd = 69; Pt = 40; Re = 50; Ru = 30, and Ir = 30 (mg/1). The results

Card 3/4

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The Separation of Selenium and Tellurium From Platinum Metals in the Form of Tri-

obtained show that optimum conditions for the precipitation of tellurites and selenite are pH values of 2.3 - 2.5 and a 90% excess of iron against the stoichiometric amount. Under these conditions tellurium extraction attained 97.5% and selenium extraction 95.4%. The ferric selenite and tellurite precipitates separated out of solutions, at a pH value of 2.28, contained 215 g/t platinum, 460 g/t palladium, and 59 g/t rhodium or 3.7; 4.6 and 5.1% respectively of their content in the initial solution. The precipitate contained very small amounts of ruthenium and iridium. There are 2 tables and 6 Soviet references.

ASSOCIATIONS: Severckavkazskiy gornometallurgicheskiy institut (North Caucasian Institute of Mining and Metallurgy); Kafedra metallurgii tyazhelykh tsvetnykh metallov (Department of Metallurgy of Heavy Non-Ferrous

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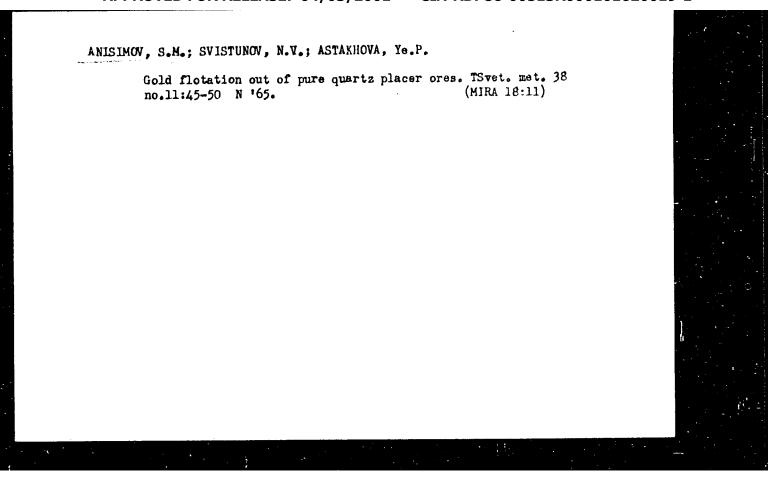
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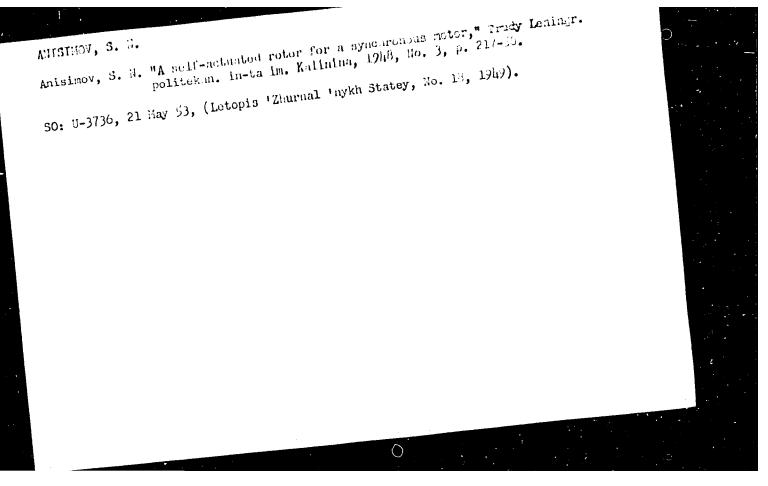
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ANISIMOV. S. V. I EIRINKO, V.I.

Different and separation of impurities during the thermal dissociation of silver nitrate. Izv. vys. ucheb. zav.; tavet. met. 8 no.5:61-65 465. (MIRA 18:10)

1. Severokavkazakiy gornometallurgicheskiy institut, kafedra meta/lurgii blagorodnykh i redkikh metallov.





ANISIMOV, S.S., ingh.; DARAGAN-SUSHCHOV, V.I., inzh.

New pudiometers. Bezop. truda v prom. 2 no.11:25-27 N '58. (MIRA 11:11)

(Mudiometer) (Ultrasonic waves--Industrial applications)

88715

S/127/60/000/006/007/007 B012/B054

9, 6/10 AUTHORS:

Anisimov, S. S., and Daragan-Sushchov, V. I.

TITLE:

New Method of Determining Atmospheric Pollution With Dust

PERIODICAL:

Gornyy zhurnal, 1960, No. 6, p. 74

TEXT: From 1957 - 1959, the Tsentral'naya nauchno-issledovatel'skaya laboratoriya (TsNIL) Gosgortekhnadzora (Central Scientific Research Laboratory (TsNIL) of the Gosgortekhnadzor) developed a dust counter which is based on the capability of the acoustic field of changing its parameters in dependence on the change of physical constants of the air investigated An acoustic field is formed in the production of elastic vibrations by The respective sound or ultrasound vibrator in the direction of the analogous receiver in the gas medium investigated. If the distance between vibrator and receiver is equal to $\lambda/2$ (half wave) or its multiple, a "standing wave" is formed. This state is caused by the physical atmospheric state, the frequency of elastic vibrations, the distance between vibrator and receiver, and corresponds to the maximum energy output on the receiver

Card 1/3

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New Method of Determining Atmospheric Pollution With Dust

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element. On the introduction of components changing the physical atmospheric state (especially dust), the parameters of the standing wave are redistributed, and less energy is put out on the receiver element. The degree of disturbance, and thus the change in emf on the receiver, can be expressed in mg/m3 on the dial of the indicator. Such a device (produced at the TsNIL comprises an electronic vibrator (generating vibrations of 5 - 6 kc/sec), an acoustic working chamber, an acoustic compensation chamber (to eliminate the effect of temperature changes) with transmitters, an electronic differential amplifier, an indicator, and a filter. The airintake system is equipped with a rubber balloon. The electronic part of the device is composed of semiconductors. OP-4 (OR-4) mercury oxide elements are used as feeding source. The device weighs about 1.5 - 2 kg. Its sensitivity can be changed according to the frequency used and the distance chosen. The smallest amount of dust measurable is 10 - 20 mg/m3. After appropriate reconstruction it would be possible to record the dust content continuously. Tests of the device in the dust plants of the Institut gigiyeny truda i profzabolevaniy AMN SSSR (Institute of Labor Hygiene and Professional Diseases of the Academy of Medical Sciences USSR) showed the

88715

New Method of Determining Atmospheric Pollution With Dust

S/127/60/000/006/007/007 B012/B054

high sensitivity of the device. Work is being done at present to simplify the design, increase the dependability, and reduce the weight of the

ASSOCIATION:

Tsentral'naya nauchno-issledovatel'skaya laboratoriya Gosgortekhnadzora RSFSR (Central Scientific Research Laboratory of the Gosgortekhnadzor RSFSR)

Card 3/3

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2209, 1160, 1147

\$/032/60/026/012/011/036 B020/3016

AUTHORS:

Daragan-Sushchov, V. I. and Anisimov, S. S.

TITLE:

An Acoustic Method of Gas Analysis

PERIODICAL:

Zavodskaya laboratoriya, 1960, Vol. 26, No. 12,

TEXT: From the various methods basing upon the measurement of acoustic quantities, the authors chose the measurement of the change in the propagation velocity of acoustic oscillations in air under atmospheric conditions as depending on the change of the density of the gas-air medium effected by various impurities (especially $\mathtt{CH_4}$). The physical basis of

the method is the fact that the propagation rate of sound in a gas mixture is between the respective rates in the pure gases. The velocity of sound in a gas is expressed by the equation

 $V = \sqrt{(p/\varrho) \cdot \gamma}$,

where y is the ratio of the individual specific heats, p the gas pressure, and o the density. With a sound source emitting sound waves in the direc-Card 1/3

the phase snilt is sensitive The device constructed consists of an oscillation transmitter and a receiver of acoustic oscillations made of piezoceramics, which are both located in a 5 cm² chamber. By means of an electron generator, a voltage having a frequency of 165 kcps is applied to the transmitter. The electric signal is transformed into elastic oscillations of the same frequency, which capprovide for release 0.04/03/2004 of CIA-RDP86-0054-8R000101620019-1

Card 2/3

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An Acoustic Method of Gas Analysis

S/032/60/026/012/011/036 B020/B056

tion of the surface of the receiver which is located at a distance d from the sound generator, the relation $t_1=d/V_1$ holds for the time required by the soun to cover this distance, where V_1 is the propagation rate of sound in the gas mixture. If another gas is used, the propagation rate is V_2 , and in that case the relation $t_2=d/V_2$ holds for t_2 , and the

relation $\Delta t = t_1 - t_2 = d(1/V_1 - 1/V_2)$ for the difference in time, where the difference in time is expressed as the phase angle between the transmitted and the received signal by the relation $\theta = 2\pi f \Delta t = 2\pi f d (1/V_1 - 1/V_2)$,

where f denotes the oscillation frequency. The method used for measuring the phase shift is sensitive to small concentrations of the gas impurities. The device constructed consists of an oscillation transmitter and a receiver of acoustic oscillations made of piezoceramics, which are both located in a 5 cm² chamber. By means of an electron generator, a voltage having a frequency of 165 kcps is applied to the transmitter. The electric signal is transformed into elastic oscillations of the same frequency, which cause an electric signal on the surface of the receiver element; this Card 2/3

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An Acoustic Method of Gas Analysis

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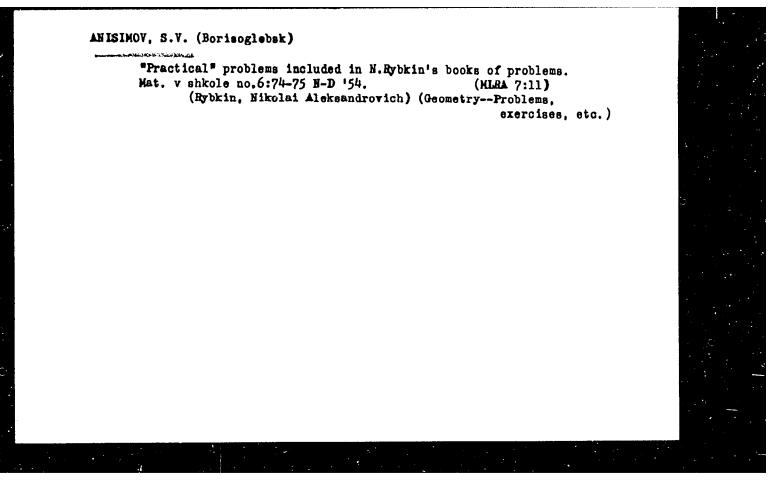
signal is amplified and transmitted to an indicator. At a distance of $\lambda/2$ between transmitter and receiver, a standing wave is formed, whereby the maximum e.m.f. on the surface of the receiver is generated. By changing the composition of the gas mixture, the density of the gas medium and thus also the wave length is changed. This leads to a change in the signal phase, and to a decrease of the energy in the receiver. The scale may be calibrated in percents of the measured gas. The block diagram of the ultrasonic gas analyzer is shown in the figure. The electrical part of the device consists of semiconductor triodes 0.65 (0.65) and is fed by the elements OP-4 (OR-4). Several variants of this device are described. There is 1 figure.

ASSOCIATION:

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Tsentral'naya nauchno-issledovatel'skaya laboratoriya Gosgortekhnadzora RSFSR (Central Scientific Research Laboratory of the State Technical Inspection of Mining of RSFSR)

Card 3/3



GLAZKOV, Aleksandr Nikolayevich, inzh.; PARFENOV, Afanasiy Nikolayevich, kand. tekhn. nauk; Prinimal uchastiye ANISIMOV, Sh.Ya., inzh.; VRONSKIY, L.N., ved. red.; VORONOVA, V.V., tekhn. red.

[Electric equipment for petroleum and gas refineries]Elektro-oborudovanie neftegazopererabatyvaiushchikh zavodov. Moskva, Gostoptekhizdat, 1962. 343 p. (MIRA 16:1)

(Petroleum refineries--Electric equipment)

(Automatic control)

