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AMERICAN METEOROLOGICAL SOCIETY
3 Joy Street
Boston, Mass.

Translation of

**OBSERVATIONAL DATA OF THE SCIENTIFIC-RESEARCH DRIFTING
STATION OF 1950-1951, Vols. I-III.**

EDITOR, M. M. SOMOV

[Materialy nabludenii nauchno-issledovatel'skoi drei-
fuiushchei stantsii 1950/51 goda, red. M. M. Somov,
Leningrad, Izd. 'Morskoi Transport,' 1954-1955]

VOLUME III

SECTION 9

This translation has been made by the American
Meteorological Society under contract AF 19(604)-
1936, through the support and sponsorship of the

GEOPHYSICS RESEARCH DIRECTORATE
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PREFACE

The source material for these translations was submitted to the U. S. Delegation attending the CSAGI Arctic Conference in Stockholm, May 22-25, 1956 and loaned for the purpose of these translations by the National Academy of Sciences, U. S. National Committee for the International Geophysical Year.

It is felt that the translated articles have a timely appropriateness in view of the IGY plans for the occupation of Arctic Ocean Drift Stations. They are offered in rough draft in order to insure their speedy distribution to all concerned with the Arctic operations. It will be noted that consecutive pagination was not attempted in yielding to the most expeditious means of translating and reproducing the material. Each translated article has its own number sequence. The tables and appendices for the most part retain the page numbers of the original text.

Articles 1, 2, and 3 of Volume I translated by Mr. E. R. Hope have been made available to the American Meteorological Society through the kind cooperation of the Department of Defence, Ottawa, Canada, in the interest of promoting Arctic research.

The assistance of the National Academy of Sciences, USNC-IGY, in the preparation of the translated text for reproduction is also gratefully acknowledged.

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AEROLOGICAL OBSERVATIONS

by

V. G. Kanaki and
V. E. Blagodarov

Source:

Materialy nabludeniĭ nauchno-issledovatel'skoi drefufushchei stantsii 1950/51 goda, ed. M. M. Somov, Leningrad, Izd. 'Morskoi Transport', 1954. pp. 218-228 and Appendix, pp. 229-495.

ORGANIZATION OF THE WORK

Aerological observations on the ice of the Central Arctic were first undertaken on a large scale at the Scientific-Research Drifting Station of 1950/51. The experience of the High-Latitude Aerial Expeditions of 1946 and 1949 was used widely in planning these observations.

The work program of the aerologists at the drifting station included the following:

- 1) Daily release of two radiosondes;
- 2) Pilot-balloon observations of the radiosondes from one point;
- 3) Releases of radiosondes in series, four sondes per day (by special order of the Arctic Institute).

The work was to have been carried out by two aerologists. Later, on the spot, one more observer was added to the group. Thus, the aerological group consisted of three members, P. F. Zaichikov, V. G. Kanaki and V. E. Blagodarov. This made it possible to expand the program somewhat, particularly to organize systematic base-line observations of the radiosondes and even to give help to other groups.

Much attention was devoted to the organization of the physical labor program. Daily watches were maintained from the first. The man on duty had the following tasks: preparation and release of two radiosondes, processing of the data and conduct of the meteorological observations during the other /Observation/ intervals. The assistant to the man on duty produced the hydrogen, filled the radiosonde balloons and made the theodolite observations from the first base point. The third aerologist made the theodolite observations from the second base point, did the housekeeping for the group, kept a general camp watch, helped other groups and saw to the replenishment of household supplies and equipment for the group.

The aerological equipment of the drifting station was prepared at the Arctic Institute and in its Experimental Workshops. Considerable assistance was given by the Central Aerological Observatory (CAO)* where all instruments were tested in a very short time, and from which improved radiosonde balloons No. 150 were procured.

*Tsentral'naiia aerologicheskaiia observatoriia (TsAO).

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The Aerostat Workshops of the CAO prepared 5-m³ gas containers for the hydrogen; they were made of four-ply percale; wind shelters were also prepared there. The Experimental Workshops of the Arctic Institute prepared gas generators of the ordinary Kanaki-Ledokovich type and portable "KL" radiosonde laboratories.

The aerological group of the drifting station had the following equipment:

1) comb radiosondes	420 sets
2) balloons, No. 150	200 items
3) balloons, No. 100	250 "
4) aerologic theodolites	2 "
5) gas generators	2 sets
6) gas containers	3 items
7) wind shelters	1 item
8) "Kapsch-2" tents	1 "
9) duralumin radio masts	2 items
10) field telephones	2 "
11) electric inflaters for the radiosondes	1 item
12) "KUB-4" radio receivers	1 "
13) "BAS-80" batteries	40 items
14) "BNS-100" batteries	16 "
15) radiosonde field laboratories	2
16) locksmith's tools	1 set
17) spare radio tubes	4 sets
18) "5NKN-45" storage batteries	3 items
19) ferrosilicon	1.6 tons
20) caustic soda	3.0 tons
21) ammonium chloride	5 kg

On 15 April 1950 the aerologists finished their preparatory work and began observations. The "Kapsch-2" tent was set up as living and work quarters for the three-man crew, the aerological and meteorological equipment was kept there. The KUB-4 receiver was set up on the bench below the skylight. The /radiosonde/ signals were received and the radiosonde data processed there. The aerological and meteorological area could be seen easily from the skylight, as could the place where the radiosondes were released, which made it possible to detect the moment of release. The bench with the portable KL aerological laboratory, used to prepare the radiosondes for release, was placed next to the work table. Besides, there was a bench for meteorological apparatus and three folding cots in the tent. No more than two men could work in the tent at one time, since there was so little free space.

An area 75 m north of the tent was outfitted, hydrogen was produced there and used to fill the radiosonde balloons. A wind shelter 3.5 m in circumference was set up for this purpose; it consisted of a piece of material 3 x 12 m with nine duralumin rods spaced equally. Fish netting was pulled over this shelter as a roof to prevent the

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accidental escape of a balloon. Two hydrogen-filled gas containers were placed inside the shelter. The balloons were filled there. During the period of operations, the shelter had to be moved three times, because the waste products of the gas production dirtied the snow and caused deep pools to form.

Twenty meters to the south of the spot where the balloons were filled a stake with the electric inflater attached was frozen into the ice to hold the balloon before its release.

Two 7-m duralumin masts with 20-m antennas were erected near the tent; they were used to receive time and radiosonde signals. The reception of radiosonde signals by the KUB-4 receiver was always good and, as a rule, they were received as long as the radio transmitter functioned. The radio receiver was fed by "BAS-80" and "BNS-100" batteries.

Hydrogen production is the most laborious task of the aerologists. Therefore, special attention was paid this matter in providing the equipment, and some innovations were made in the method of obtaining the hydrogen. First of all, the aerological group was provided with containers for storing the gas. These containers made it possible to store gas enough for 4-5 radiosonde ascents, thanks to which a whole day could be spent in carrying out this time-consuming operation. Fig. 1 shows the filling of a gas container from the gas generator.

The hydrogen was transferred from the gas containers into the radiosonde balloons by a diaphragm pump (from a rubber liferaft) specially adapted for this work. A nozzle with a flange was attached to the suction end of the pump. A hose, connected with the gas container, was attached to this nozzle. The second (forcing) hose was hooked up to the balloon. It took 10 to 15 minutes to fill a balloon.

In the gas generator used at the drifting station, the intensity of the reaction was regulated by changing the dose of ferrosilicon, gradually feeding it in (as needed) from a special tank connected to the tank of the gas-generator by a durite hose 45 mm in diameter. Sea water was used for gas generation, and in the summer, water from fresh pools. In both cases, 5-6 liters of hot water were poured in to start the reaction. The salinity of the water did not seem to affect the process. The weather conditions, however, exerted a great influence on the process and the intensity of the reaction. For example, with low temperatures and winds with drifting snow, the tank of the gas generator had to be protected from the wind by a special shield (Fig. 2) or covered with insulating material, otherwise the reaction would not begin immediately and it would be very weak. When the process was too intense, however, the gas generator was cooled by covering it with snow.

Chemicals of home manufacture were used to produce the hydrogen; their quality was good enough, although they had been at the Cape Schmidt polar station for about two years. The ferrosilicon, however,

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was somewhat damp and had frozen together in a solid lump. Much time and labor had to be expended in drying it and breaking it up. The caustic soda (in standard 300 kg lots) was also in solid form. As a consequence, the aerologist whose duty it was to produce the hydrogen spent at least half his day breaking up the chemicals.

Despite the effort required by this process, during the whole drift we always had enough hydrogen and we had it in time.

The aerological observations were carried out from 15 April through 19 October 1950. From the beginning of operations to 1 September they were made twice a day (at 0400 and 1600 hours Moscow time), from 1 September on they were made only once a day (0400 hours), due to a shortage of chemicals. In all, 313 radiosondes were released, for which 222 observations were made by theodolite (25 of these were base-line observations). After the data were processed and examined carefully, the following were selected for publication:

radiosonde observations - 291
theodolite observations - 212

The mean height of ascent of the radiosondes was 18.6 km. The maximum height reached was 32.8 km, on 23 May. Two hundred eighty radiosondes reached the stratosphere,

height of more than 10 km - 275 radiosondes
15 - 263
20 - 148
30 - 2

Table 1 gives data of the distribution of the radiosonde ascents: the length of time signals were received, height reached and the month of release.

Table 1

Length of time signals were received and height of ascent of the radiosondes

	Apr.	May	June	July	Aug.	Sept.	Oct.	Whole period
Mean length of signal reception (min.)	61	71	74	82	70	73	47	71
Mean height of ascent (km)	15.2	19.4	20.0	22.4	18.2	17.7	13.5	18.6
Maximum height of ascent (km)	26.4	32.8	27.7	28.9	25.0	23.5	18.8	32.8
Minimum height of ascent (km)	6.9	5.0	8.7	10.8	6.0	6.4	7.4	5.0
Number of observations	28	58	53	59	51	27	15	291

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All observations were carried out in conformity with the assigned instructions and directions. Below we give an account of the various changes in method. The data on the processed material are given in the Appendix.

THE RADIOSONDE WORK

A control check on the radiosondes was made before the expedition set out, in January of 1950 at the CAO. The results of checking the temperature recorders were entered in the specification sheet* for each instrument and, in case they did not check out with the factory specifications, the latter were corrected. The pressure recorder was checked at positive and negative temperatures. New specification sheets for the pressure recorder were made on the basis of the data from this check at the CAO.

Before being prepared for release the instruments were examined carefully and those whose condition seemed doubtful were not used. The instruments were made ready 3-4 hours before release.

The portable "KL" laboratory was used to check the electrical systems of the instruments. The radio transmitter and the feeding source were mounted as suggested by V. G. Kanaki. This differs from the ordinary method in that the radio transmitter is not placed inside the radiosonde, but is packed together with its batteries and attached to the casing of the balloon before its release. The transmitter tubes keep the batteries warm, preventing them from freezing.

The radio transmitter was tuned by the thermocouple of the field laboratory or by "mikro" radio tubes. It was fed by 3-5 anode and 1 filament battery, which were drenched with a saturated solution of ammonium chloride with 25% alcohol added. The drenching lasted for 1-2 hours before release, and the batteries together with the radio transmitter were taken out to the release area 10 minutes before release time.

The instruments were "exposed" only before the release and at the release area. Attempts to "expose" the instruments in the tent failed because of the differences in the air temperature and the different inertia of the instruments (the temperature recorder of the radiosonde and the psychrometer). In taking down the initial position of the recording pens in the specially equipped box with a ventilator the readings of the radiosonde and the mercury thermometer did not coincide; this was due to the causes mentioned above and to the inadequacy of the ventilator.

*In Russian the word here is "certificate," perhaps this is preferable to "specification sheet." (Tr. note)

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The instruments were "exposed" on the area before release on a stake frozen into the ice to which the ventilator and two hooks for the radiosonde and psychrometer were attached at a height of 2 m above sea level.

In individual cases the radiosondes were "exposed" along with the psychrometer shelter as a control and calibration of the readings made during the basic "exposure" on the electric inflater as against the readings of the instruments in the psychrometer shelter. In ordinary work, the humidity instruments were taken out onto the release area an hour to an hour-and-a-half before release. The readings of the initial position of the recording pens at the release site were entered in the appropriate columns of the radiosonde sheet. The results of the "exposure" made in the tent or at the psychrometer shelter were entered in the blank titled "Exposure and place".

Humidity at a temperature higher than -5°C * was determined by the aspiration psychrometer, at a temperature below -5°C by the hygrometer. Pressure was measured by a mercury inspector's barometer** which was kept in the tent. Wind was measured by the Tret'iakov wind gauge*** set up on the meteorological area. The data on atmospheric phenomena and cloudiness at the moment of release were entered in the pilot-balloon log (with subsequent transfer onto the radiosonde sheet).

*All temperatures are in $^{\circ}\text{C}$ (Tr. note).

**Inspector's barometer. A barometer carried by an inspector of a meteorological network to a station to check the accuracy of the barometers at that station. An inspector's barometer is an instrument intermediate between a normal working barometer for a given meteorological region and a stationary barometer. Before the inspector makes his trip the instrument correction of the inspector's barometer is made by comparing it with a normal working barometer. A second comparison with the normal working barometer is made after the inspector returns. The inspector's barometer must be portable, durable and accurate. These requirements are satisfied by the Wild-Turretini barometer used at stations in the USSR (Tr. note). Source: *Meteorologicheskii slovar'*, Khromov and Mamontova, p. 153.

***Tret'iakov wind gauge. A portable instrument for determining the velocity and direction of the wind under field conditions. The wind velocity is measured by the deflection of a freely suspended metal plate having a spoon-shaped form. The direction of the wind is determined by a special vane included in the construction of the instrument. The scale for this wind gauge was obtained experimentally from determinations in an aerodynamic tube (Tr. note). Source: *Meteorologicheskii slovar'*, Khromov and Mamontova, p. 283.

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The radiosonde balloons were hung about, over the gas burner or the kerogaz,* before filling and were rotated constantly for half an hour. The heating provided additional vulcanization. The preparation made the balloons elastic and insured a great height of ascent.

After the radio receiver had been tuned in on the transmitter wave band, the radiosondes were released on a signal from the aerologist on duty at the tent window. On days when the wind was light, the balloons were towed with the wind for take-off. During high winds, by way of experiment, the F. F. Zaichikov method was sometimes used. The equipment necessary for this was prepared on the spot by station mechanic M. S. Komarov. The radiosonde was hung so that it could slide easily along the cable. The cable was stretched out with the wind at a height of 1.5 m, one end of it was firmly fixed to a stake frozen into the ice, the other end to a duralumin mast through an automatic release mechanism. The balloon, under the influence of the wind, would pull the instrument along the cable; in the process the ring would strike the automatic release and the cable would be detached from the mast, which, because of the rubber guy lines, would be cast in the direction opposite that in which the instrument was moving, and the radiosonde, breaking free of the cable, would continue in flight.

The signals were received (Fig. 3) by one of the aerologists through a speaker or, in case reception were poor, by earphones. Besides the temperature, pressure and humidity signals, signals were received of the speed of rotation of the propeller. For this purpose, the time of the beginning and end of all control humidity signals were entered on a separate form. These observations were conducted to study atmospheric turbulence.

The data on the ascent of the radiosonde up to 5 km were worked up very soon after the signals were received, since the information had to be included in the *Weather* telegram. The remaining information was processed at the Arctic Institute after the expedition had returned.

The pressure data were processed according to the specifications of the CAO. The correction for layer thickness was determined by slide rule from the formula:

$$\Delta h = \frac{Ht}{273} \text{ av.}$$

where H is the layer thickness and t_{av} is the average temperature of the layer.

*Kerogaz. A kerosene heating device on the order of a noiseless primus stove (Tr. note).

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Temperature observations were processed according to the factory specification sheets, with account taken of the corrections made at the time of the instrument check at the CAO. The dew-point temperature was determined by nomogram.

THEODOLITE OBSERVATIONS OF THE RADIOSONDES

The pibal theodolite on the first base point, fixed on a tripod, was located at the release area for radiosondes. Before an observation was made, the theodolite's position with respect to the level was checked, as well as its orientation. The theodolite was lined up with a surveyor's stake, which first was a peg frozen into the ice on the meridional line to the north of the instrument. Beginning 19 May, the theodolite of the second base point located in the same direction, served as the surveyor's mark. Since the floe gradually turned, a correction factor had to be introduced to account for the change in the azimuth of the stake, which increased from 0° (15 April) to 34° (20 October).

The azimuth was determined by the North Star and by the sun. In the first case the telescope of the theodolite, oriented with zero on the surveyor's stake, was fixed on the North Star and readings were made by the horizontal circle of the theodolite. The difference between the readings with the theodolite directed on the stake (360°) and on the North Star was taken as the azimuth of the stake. In the second instance, the azimuth was determined by the familiar formula:

$$\sin A = \frac{\cos \varphi \cdot \sin t_{\text{local}}}{\sin Z_{\text{combined}}}$$

Since the zero of the theodolite was always directed on the stake, the difference 360°-A gave the azimuth of the stake according to the sun.

The pilot-balloon observations were processed in the usual manner, whereby the heights were determined by the mean vertical velocity of the radiosonde.

By the time the base was laid out (19 May), the floe had already turned 5°. In order to preserve the initial position of the theodolite at the first point of the base, the place for the second theodolite of the base was selected exactly in the direction of the stake (peg), whose azimuth at that time was 5°. The dimensions of the floe did not permit us to lay out a base line of more than 600 m.

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The length of the base was measured twice with a steel tape:

First measurement	- 600.08 m
Second	- 600.90 m
Average length of base line	- 600.50 m

A pibal theodolite on a tripod was set at the second base point as well as the first. Both points were connected by field telephones. To synchronize the readings from the tent by a line connected to the telephone line, signals of 2-3 sec duration were sent every minute. This was attained by use of a contact on the timing gear of an alarm clock and the sound mechanism. This device was prepared at the drifting station.

The base observations were taken only on days without fog and low cloud cover.

As the floe turned, the azimuth of the base changed correspondingly. The processing was done with a Molchanov circle* according to the instructions of the Hydrometeorological Service. The base line observations were processed using a 25-cm slide rule.

The small length of the base line did not permit us to process the prolonged observations to the end, since angles B and B' often were smaller than 4°.

The expedition's observational data were completely processed, checked and prepared for publication at the Arctic Institute by N. V. Basieva, L. I. Vorontsova, L. P. Kuritsyna, N. V. Shiposh under the general direction and with the aid of I. M. Dolgin, Candidate in Geographical Sciences, and Junior Scientific Colleague T. V. Nikolaeva.

In conclusion let us note a number of organizational and methodological inadequacies which could not but have had an effect on the work progress and the quality of the individual observations. These inadequacies include, first of all, the lack of general standard

*Molchanov circle. An instrument for constructing the horizontal projection of the path of a pilot balloon, to a certain scale, by angles plotted during theodolite observations of the balloon. The direction and speed of the wind aloft is then determined from the projection. The Molchanov circle consists of a wooden board with a diagram glued to it, of a movable celluloid disk that turns about the center and of a movable celluloid ruler. Designed by P. A. Molchanov (Tr. note). Source: *Metecrologicheskii slovar'*, Khrcmov and Mamontova, p. 190.

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aerological field equipment. Therefore, in preparing for the expedition ordinary station instruments were selected and to a certain degree adapted to the specifications of work on an ice floe. A number of instruments and objects of secondary equipment were invented or re-designed. As a consequence, the aerological equipment of the drifting station was quite diverse, which doubtless complicated the work in a number of cases. Some pieces of equipment, as was found when the work was processed, were not thought out well enough. In particular, the wind shelter proved unsatisfactory, since in autumn much snow entered it during the ground blows, and covered the hydrogen gas containers. In the future, instead of shelters a large Danish-type tent with a wide entrance should be used.

The initial positions of the recording pens of the instruments, "exposure" in the tent, were not recorded, although instructions had been given to do this, because the temperature measurement and the taking of the position of the recording pens lost all physical sense in view of the large temperature gradients. In individual cases and when the instruments were exposed to air on sunny still days even the use of the electric inflater with a flow of air 5-6 m/sec did not guarantee reliable enough initial data. This is to be explained by the large contrasts between the temperatures of the air and the inflater that had been warmed in the sun.

In the future it will be necessary to work out a device for exposing the apparatus both in the tent and in the open air. Thermostats and the necessary shading together with good ventilating apparatus may serve this purpose.

The shortness of the base line and the crude nature of its equipment may be considered a real disadvantage for pilot-balloon observations. For example, in assembling the equipment, the contact watches for the transmission of time signals were forgotten. The apparatus to replace the watches was made at the station from an ordinary alarm clock and was not very reliable, and often the convergence of the base altitudes was poor.

The work was complicated a great deal by the fact that the caustic soda, moulded in solid 300-kg masses, was contained in iron barrels. Under the work conditions at the drifting station it is quite necessary to have caustic soda either in pulverized form sealed in 2-3 kg tin cans, or, still better, in flake form.

Finally, neither the method of observations nor the suitability of this or that piece of equipment needs special comment.

A preliminary examination and analysis of the data makes it possible to draw certain conclusions as to the stratification of the atmosphere in the central part of the Arctic Basin. Below we give a space-time graph of isopleths, constructed on the basis of the data of the morning radiosonde ascents (Fig. 4). One hundred sixty seven.

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ascents for the period from 15 April through 19 October were used in constructing this graph; all radiosondes reached the tropopause and in most cases sounded the stratosphere up to 20-25 km.

The isopleth graph clearly shows the existence of an inversion layer in the lower troposphere. As a rule this layer lies between the heights 0.5 and 2.5-3.0 km. At the same time, a seasonal character of the inversions was discovered. Thus, the deepest inversion was observed in the middle of July. This was connected with the transport northward of warm Pacific-Ocean air, arriving from the American continent. The inversion occurred as a result of the cooling of the lower layer of air because of the expenditure of heat on the intensive thawing of the snow and ice cover. In the inversion layer the growth of temperature with height reached 10°C at the 3.5 km level. The maximum air temperature (10-11°C) in that layer was noted at 1.0-1.5 km. The ice-adjacent layer of air, in moving northward, became 8-9° cooler than the higher layers.

At the same time, at a height of 3.5 km, the zero isotherm held steady, during the remaining time it appeared only episodically (in the second ten days of June and then during all of August). In October, with the arrival of polar night and the increase in radiation, the winter inversions were observed, which can also be seen clearly on the isopleth graph.

Fig. 5 shows a graph of temperature distribution with height for 15 October. The deep inversion in the layer from the ice surface to a height of 1 km can be explained by the great loss of heat from the low-lying layer due to night radiation. In the 0-0.5 km layer, the negative temperature gradient amounted to 2.56°C per 100 m, while the absolute rise in temperature reached 12.8°C.

The trend of the isopleths above the inversion layer, for the whole period investigated, almost exactly followed the variations of the tropopause; the vertical temperature gradient of the layer from 4 km to the tropopause sharply departed from its mean value, which was 0.56°C. This indicates the connection between the thermal regime of the upper troposphere and the height of the tropopause.

The height of the tropopause fluctuates on an average around the 9.8 km level, dropping sometimes to 7.0 km (30 June-1 July) and rising to 12.0 km (5-15 July, during the invasion of warm masses of Pacific Ocean air).

In the spring period, when cyclonic activity is strongly developed, frequent fluctuations in the height of the tropopause are to be observed. For example, between 23 June and 2 July the height of the tropopause dropped sharply from 11 km to 7 km, while in the succeeding days it again rose to 12 km. This amplitude of variation of the height of the tropopause, the greatest for the whole period, was caused by an abrupt change in the air currents in the troposphere.

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From the data given it is evident that the mean height of the tropopause in the central part of the Arctic Basin has approximately the same values as in the temperate latitudes. Proceeding from this we may conclude that warm air masses, embracing the whole troposphere, penetrate into the central Arctic. The transport of warm air into the high latitudes leads to frontogenesis in these regions. In his time B. L. Dzerdzeevskii noted this and it was confirmed by observations of the aerial expeditions of 1948, 1949 and 1950.

During the whole period of operations of the drifting station, the temperature of the tropopause varied within the limits -39.4° and -64.2° C. The lowest temperature values were observed in April and October, while the highest values occurred in the warm season of the year. From this we can conclude that the temperature of the tropopause has a seasonal character. The layer of the stratosphere above the tropopause has great temperature fluctuations.

The following detailed study and analysis of the data from radiosonde ascents combined with the study of the synoptic characteristics of the atmospheric processes makes it possible to broaden our knowledge of the dynamics and transformation of air masses of the Arctic Basin.

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Figure Captions

- Figure 1: Filling a gas container with hydrogen.
- Figure 2: A radiosonde balloon in the wind shelter.
- Figure 3: Preparing a radiosonde for release and reception of signals in the tent.
- Figure 4: Graph of isopleths, according to morning radiosonde ascents.
- x-axis (bottom, reading left to right): April, May, June, July, August, September, October
- Figure 5: Distribution of temperature in the troposphere according to the morning radiosonde ascent of 15 October 1950.

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APPENDIX

Explanation of the tables

Radiosonde observations were conducted at 0400 and 1600 hours Moscow time.

For the majority of the radiosondes, the observations were conducted by theodolite (base or from one point), and by this the direction and velocity of the wind aloft were determined.

The release time of the radiosondes, mean local solar time, is given in four ciphers in the tables, of which the first two indicate the hour, the last two, the minute.

The heights of the clouds was determined by the moment "it becomes hazy" by the theodolite observation; they are expressed in geopotential decameters above sea level.

The results of the aerological radiosonde ascents are given in table form, where the meteorological data are given, computed by height stages for the main isobaric surfaces and for the individual levels and expressed in geopotential kilometers above sea level.

The upper and lower boundaries of the inversions and isotherms, the boundaries of the segments with decreased gradient, and also the height of the lower boundary of the tropopause are referred to particular levels.

The table contains the following data: Date, release time of the radiosonde, coordinates, cloudiness, height of the clouds; pressure, temperature, vertical temperature gradient, relative and specific humidity, wind velocity and direction (data obtained from the base observations are given in heavy type), and vertical velocity of the radiosondes are given by heights.

The values of the gradients and the vertical velocities are given in the line corresponding to the height of the upper boundary of the layer for which the computations were made. Heights given in parentheses mean that such data are not accurate for the beginning or the end of the particular point. The temperature and humidity data given in parentheses were taken from interpolated curve segments. Discontinuities in the wind data (direction or velocity) are marked with an asterisk.

The organization of the aerological observations (radiosonde ascents, pilot balloon observations) and their processing were carried out in compliance with the "Instructions to the hydrometeorological stations and posts" (Nastavlenie gidrometeorologicheskim stantsiam i postam), Pub. Gidrometeoizdat, 4th ed., Parts I, II, and III, 1944, 1945, 1947.

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CONVENTIONAL SYMBOLS

H height in geopotential kilometers	✱	wet snow
B atmospheric pressure in mb	*	rain (° light)
t temperature in degrees	△	granular snow (° light)
vertical temperature gradient	∇	snow shower
U relative humidity of the air	☉	drizzle (° light)
q specific humidity in grams per kg of air	☉	fog with charges
d wind direction in degrees	☉	sea fog
V wind direction in m per sec	☉	ground-level fog
W vertical velocity of the radiosonde in m per min	☉	unbroken fog
	☉	fog with gaps (sky visible)
✱	✱	glaze
	☉	low drifting snow
	☉	surface snowstorm



Рис. 15. Наблюдение за работой в поле.

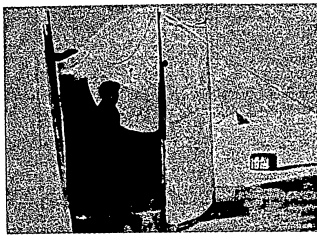


Рис. 23 Шар радиозонда в островной защите.

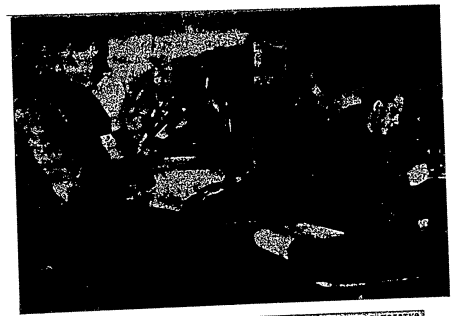


Рис. 24 Подготовка радиозонда к выпуску в гидротехнической лаборатории.

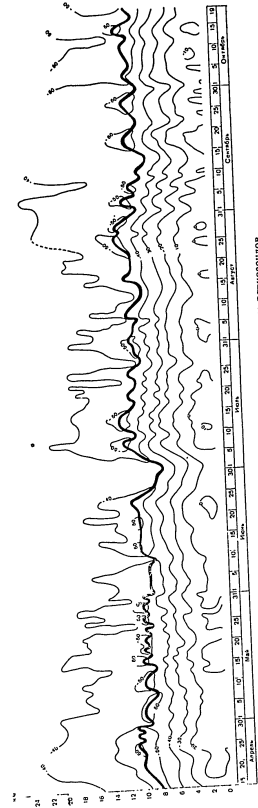


Рис. 4. График изредет по утрешним почтеням радиосигналов.

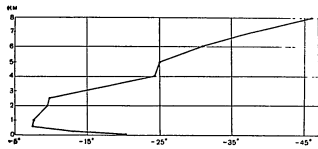


Рис. 5. Распределение температуры в тропосфере по утреннему подъему радиозонда 15 октября 1950 г.

APPENDIX

See translated text for column headings and additional notes.

УСЛОВНЫЕ ОБОЗНАЧЕНИЯ

H — высота в геопотенциальных километрах;	☼ — мокрый снег;
B — давление воздуха в миллибарах;	● — дождь (●° — слабый);
t — температура в градусах;	△ — снежные зерна (△° — слабые);
γ — вертикальный температурный градиент;	☂ — ливневой снег;
U — относительная влажность воздуха;	☉ — морось (☉° — слабая);
q — удельная влажность в граммах на килограмм воздуха;	☁ — туман зарядами;
d — направление ветра в градусах;	☁ — морской туман;
V — скорость ветра в метрах в секунду;	☁ — поземный туман;
W — вертикальная скорость радиозонда в метрах в минуту;	☁ — сплошной туман;
✱ — снег (✱° — слабый);	☁ — туман с просветами;
	☁ — гололед;
	☁ — поземок
	☁ — метель верхняя.

РАДИОСОУДЪ ОБСЕРВАТОРИИ
РАДИОНОВЫЕ НАБЛЮДЕНИЯ

Приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.4 1339 $\varphi = 76^{\circ}26'$ $\lambda = 192^{\circ}52'$																	
10/0 Cl, Cs																	
0.0	0.19	-22.7	0.50	0.68	5				3.0	679	-25.2	0.38			088	4	321
0.06	0.10	-23.0		0.60	7				3.89	600	-30.4				098	5	
0.13	0.00	-23.0	0.00	0.75	7				4.0	591	-30.8	0.56			100	5	
0.2	0.91	-23.0	0.00	1.01	9				5.0	513	-36.4	0.56			125	5	
0.43	0.61	-23.0	0.00	1.04	10				5.17	500	-37.4						361
0.5	0.92	-22.6		1.04	10				6.0	443	-41.5	0.51					
0.93	0.90	-20.4		1.05	9				6.7	400	-45.8						
1.0	0.91	-20.2		1.05	9				7.0	381	-47.7	0.62					
1.06	0.83	-20.0	-0.48	1.04	8				7.7	344	-51.3	0.51					
1.35	0.85	-20.2	0.11	1.03	7				8.0	328	-51.3	0.00					
1.5	0.83	-20.5	0.11	1.00	7				8.57	300	-51.3	0.00					
1.78	0.80	-20.9	0.12	0.89	7				9.0	281	-51.3	0.00					
2.0	0.78	-21.1	0.12	0.88	5				10.0	241	-48.6	-0.27					340
2.2	0.75	-21.5	0.20	0.87	4				11.0	208	-46.0	-0.26					
2.5	0.72	-23.3	0.60	0.87	3				11.25	200	-45.6						
2.78	0.70	-24.2		0.81	3				12.0	178	-43.7	-0.23					
									13.0	153	-42.9	-0.08					
									14.0	132	-41.9	0.10					
									15.0	115	-40.4	-0.15					
									16.0	100	-39.7	-0.07					

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Приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
16.4 1352 $\varphi = 76^{\circ}24'$ $\lambda = 192^{\circ}20'$																	
0/0 Cl																	
17.0	85	-38.8	-0.09						2.5	726	-22.5	0.14			071	7	
18.0	75	-37.8	-0.10						2.77	700	-23.3				072	7	
19.0	64	-37.0	-0.08						3.0	678	-24.1	0.32			071	7	356
20.0	55	-36.4	-0.06						3.9	600	-28.9				077	9	
20.62	50	-35.4							4.0	591	-29.3	0.52			078	7	
21.0	47	-34.9	-0.15						5.0	513	-34.0	0.47			079	7	
21.72	40	-34.9	0.00						5.18	500	-34.7				080	7	
									6.0	444	-39.4	0.54			080	7	389
									6.68	400	-43.5				085	8	
									7.0	382	-45.2	0.58			091	7	
									8.0	330	-51.3	0.61			074	2*	
									8.4	310	-52.3	0.25			345	3	
									9.4	300	-52.3	0.00			311	4	
									9.62	283	-52.3						
									9.46	263	-52.3						
17.4 0156 $\varphi = 76^{\circ}22'$ $\lambda = 192^{\circ}21'$																	
2/0 Cl																	
0.0	0.22	-24.0		0.45	4				0.0	056	-33.0				94	315	5
0.16	0.00	-24.2	0.10	0.54	6				0.16	000	-28.0					334	5
0.2	0.94	-24.2	-0.40	0.59	7				0.2	586	-27.2	-2.90				335	5
0.5	0.93	-23.0		0.64	4				0.5	555	-22.0	-1.73					
0.92	0.90	-21.0	-0.34	0.66	4												
1.0	0.91	-21.3	0.10	0.65	4												
1.1	0.78	-21.0	0.20	0.60	4												
1.35	0.80	-21.0	0.13	0.64	5												
1.5	0.83	-21.2	0.13	0.67	6												
1.8	0.80	-21.5	0.11	0.66	6												
2.0	0.78	-21.8	0.11	0.66	6												

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Продолж. приложения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
0.95	900	-19.6							0.2	997	-22.8				822	10	
1.0	895	-19.5	-0.30						0.25	990	-22.8	0.00			313	10	
1.4	850	-18.9							0.5	958	-19.4	-1.35			302	9	
1.5	838	-18.7	-0.16						0.86	914	-17.0	-0.67			318	7	
1.84	800	-18.4	-0.09						0.97	900	-17.0	0.00			320	6	
2.0	783	-18.8	0.25						1.0	897	-17.0	0.00			339	5	
2.5	731	-19.8	0.20				290		1.4	850	-17.0	0.00			345	5	
3.0	683	-21.8	0.40						1.5	839	-17.0	0.00			359	5	
3.94	600	-25.6							2.0	785	-17.0	0.00			350	5	
4.0	595	-27.0	0.52						2.15	770	-17.0	0.00			601	5	
5.0	516	-33.7	0.67						2.5	734	-18.0	0.29			607	5	
5.21	500	-35.1							2.85	700	-20.0				015	6	329
6.0	447	-41.0	0.73				300		3.0	686	-20.7	0.54			016	6	
6.75	400	-46.9							4.0	600	-25.5	0.48			034	6	
7.0	385	-48.4	0.74						5.0	522	-31.1	0.56			046	3	
8.0	330	-56.0	0.75				318		5.29	500	-33.1				035	3	278
									6.0	451	-38.5	0.74			059	3	
									6.82	400	-43.0				092	5	
									7.0	390	-44.4	0.59			091	5	
									8.0	335	-50.2	0.58			113	6	
									8.4	316	-53.5	0.82			110	4	224
									8.73	300	-59.5				187	2	

17.4 1359 $\varphi=76^{\circ}21'$, $\lambda=192^{\circ}23'$

2/0 Cl

0.0	025	-22.8					315	5
0.17	000	-23.8					328	11
							85	

Продолж. приложение

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
9.0	288	-53.5	0.00				250	1	9.87	700	-20.0						
9.65	260	-53.5	0.00				300	2	10.0	687	-20.8	0.46					369
10.0	248	-52.0	-0.43				298	2	9.98	690	-25.8	0.51					
11.0	212	-48.8	-0.32				0	0	9.0	500	-31.3	0.54					
11.35	200	-47.5					0	0	9.25	489	-38.5	0.75					
12.0	181	-46.4	-0.24				0	0	6.77	409	-40.0	0.60					350
12.23	174	-46.2	-0.09				224		7.0	387	-44.8	0.60					
									8.0	323	-50.0	0.72					
									8.68	300	-55.0	0.72					
									8.83	294	-56.3	0.90					
									9.0	283	-56.3	0.90					
									10.0	244	-56.8	0.90					
									10.13	238	-56.8	0.90					
									11.0	207	-55.2	-0.18					
									11.29	200	-54.0	-0.40					439
									12.0	178	-51.2	-0.10					
									13.0	154	-49.7	-0.10					
									14.0	132	-48.7	-0.10					333
									15.0	113	-47.7	-0.10					
									15.77	100	-47.0	-0.10					
									16.0	96	-46.7	-0.10					
									17.0	84	-46.2	-0.15					319

18.4 0143 $\varphi=75^{\circ}20'$, $\lambda=192^{\circ}25'$

10/10 Sc (108)

0.0	095	-20.1					338	4
0.17	000	-19.8					349	4
0.5	638	-18.5	-0.40				355	4
0.6	616	-17.3	-1.20				350	5
0.98	600	-17.3	0.00				347	7
1.43	650	-17.3	0.00					
1.87	600	-17.3						
2.0	767	-17.3	0.00					
2.1	776	-17.3	0.00					
2.5	736	-18.3	0.30					

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
17.32	81	-44.2	-0.31						3.98	600	-26.4	0.55			311	5	
18.0	73	-44.2	0.00						5.0	520	-53.0	0.65			302	4	
19.0	62	-44.2	0.00					254	5.26	500	-34.3				297	4	
20.0	53	-44.2	0.00						6.0	450	-39.8	0.68			300	3	307
									6.78	400	-45.2				306	3	
									7.0	387	-47.0	0.72			306	4	
									8.0	333	-52.1	0.51			306	7	
									8.68	300	-55.6				313	7	287
									(8.74)	298	-56.0	0.53			313	7	
									9.0	285	-	-			312	8	
									10.0	245	-	-			310	8	
									11.0	210	-51.5	-			311	7	248
									11.29	200	-51.0				305	6	
									12.0	180	-49.3	-0.22			290	3	
									13.0	155	-47.3	-0.20			259	3	210
									14.0	133	-45.8	-0.15			262	4	
									15.0	114	-44.4	-0.14			191	3	
									15.85	100	-42.9				199	5	
									16.0	97	-42.6	-0.18			202	5	
									17.0	85	-41.5	-0.11			183	4	256
									18.0	75	-40.9	-0.06			177	4	
									19.0	65	-40.5	-0.04			174	4	
									20.0	55	-40.5	0.00			165	4	302

18.4 1343 φ = 76°19' λ = 192°27'

0/0 CI

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
20.7	50	-40.5	0.00						3.83	600	-25.6				272	5	
21.0	48	-39.5	-0.33						4.0	595	-26.2	0.55			272	5	
22.0	40	-38.8	-0.07					304	5.0	519	-33.3	0.71			271	5	
22.8	35	-38.5	0.00						5.24	500	-35.0						283
									6.0	449	-39.7	0.64					
									6.78	400	-45.4						270
									7.0	386	-47.2	0.75					
									8.0	332	-53.0	0.58					
									8.64	300	-56.2						
									8.72	297	-56.4	0.47					
									9.0	285	-56.4	0.00					
									9.52	262	-56.4	0.00					226
									10.0	242	-55.7	-0.15					
									11.0	209	-53.3	-0.24					
									11.27	200	-52.8						
									12.0	178	-51.5	-0.18					
									13.0	153	-49.4	-0.21					
									14.0	131	-48.2	-0.12					238
									15.0	113	-46.4	-0.18					
									15.77	100	-45.0						
									16.0	96	-44.6	-0.18					
									17.0	83	-43.7	-0.09					252
									18.0	72	-43.0	-0.07					

19.4 0149 φ = 76°19' λ = 192°29'

2/0 CI

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
20.4 0139 $\varphi=76^{\circ}17'$ $\lambda=192^{\circ}32'$																	
7,0 Cl, Cs																	
0.0	030	-29.3							8.0	340	-48.0	0.53					244
0.1	000	-20.3							3.8	300	-52.5	0.50					
0.2	963	-17.1							9.0	290	-53.0	0.00					
0.3	943	-16.2							9.9	233	-53.0	0.00					175
0.65	943	-16.2							10.0	230	-52.8	-0.20					164
1.0	800	-15.9							11.0	214	-50.5	-0.23					
1.45	830	-15.2							11.44	200	-49.4						
1.5	845	-15.2							12.0	184	-48.2	-0.23					161
1.84	807	-16.2							13.0	158	-45.9	-0.23					
1.9	800	-16.4							13.82	140	-45.6	-0.04					
2.0	789	-16.3							21.4 0165 $\varphi=76^{\circ}17'$ $\lambda=192^{\circ}35'$								
2.5	738	-16.4							0,0								
2.88	700	-16.6							0.0	030	-30.8						2
3.0	689	-20.0							0.21	000							
4.01	600	-25.1							0.5	969							
5.0	523	-23.9							0.97	900							
5.31	500	-31.4							1.0	897							
6.0	454	-35.7							1.4	850							
6.87	400	-40.7							1.5	839							
7.0	383	-41.7							1.85	800	-17.8						
									2.0	784	-18.6						

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
19.4 1359 $\varphi=76^{\circ}18'$ $\lambda=192^{\circ}31'$																	
0,0 Cl																	
0.0	029	-22.4							4.0	877	-37.3	0.58					200
0.1	014	-22.6							5.0	819	-30.1	0.48					
0.2	000	-22.3							5.27	800	-30.1						
0.5	951	-19.4							6.0	650	-37.1	0.50					194
0.55	955	-19.2							6.83	600	-42.1	0.63					
0.99	900	-19.2							7.0	590	-46.4	0.46					
1.43	850	-19.2							8.0	538	-46.0						198
1.5	841	-19.2							8.73	500	-52.1	0.51					
1.87	500	-19.2							9.0	287	-55.1	0.50					
2.0	786	-19.2							9.17	280	-54.1	0.50					
2.3	755	-19.2							9.89	251	-54.1	0.50					
2.5	735	-19.7							10.0	246	-53.7	-0.36					
2.85	700	-20.8							11.0	212	-50.5	-0.32					
3.0	686	-21.5							11.33	200	-49.7	-0.23					
3.97	600	-27.2							12.0	182	-48.2	-0.28					
									13.0	157	-45.4	-0.28					
									14.0	134	-43.4	-0.20					
									15.0	116	-41.8	-0.14					
									16.0	100	-40.4	-0.14					
									17.0	86	-39.1	-0.13					
									18.0	74	-38.4	-0.07					
									19.0	62	-37.5	-0.09					
									19.65	55	-37.4	-0.02					

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.5	733	-20.1	0.30						2.0	787	-18.9	0.30					
2.85	700	-21.7	0.48					320	2.3	735	-20.2	0.26					
3.0	685	-22.5	0.46						2.86	700	-21.1	0.22					329
3.98	600	-27.0	0.54						3.0	687	-21.3	0.22					
5.0	519	-32.5	0.54						4.0	600	-25.1	0.38					
5.27	500	-34.2	0.57						5.0	522	-30.5	0.54					
6.0	449	-39.2	0.57						5.3	500	-32.2	0.62					
6.79	400	-44.2	0.57					314	6.0	462	-36.7	0.62					
7.0	388	-44.9	0.57						6.86	400	-43.2	0.87					350
7.2	376	-45.6	0.35						6.9	398	-44.5	0.87					

22.4 0155 $\phi = 76^{\circ}17'$ $\lambda = 192^{\circ}36'$
8/0 Ci, Cs

H	B	t	Y	U	q	d	V	W
0.0	1	031	-28.7	87			315	3
0.22	000	-24.0	-2.14				353	5
0.46	967	-17.1	-2.88				358	5
0.5	922	-17.1	0.00				343	6
1.0	900	-17.1	0.00				334	5
1.3	865	-17.1	0.00				330	5
1.44	850	-17.3	0.15				330	5
1.5	843	-17.4	0.15				330	5
1.88	800	-18.5						

22.4 1652 $\phi = 76^{\circ}17'$ $\lambda = 192^{\circ}36'$
8/0 Ci, Cs

H	B	t	Y	U	q	d	V	W
0.0	1	034	-20.4	94	0.6	338	2	
0.2	065	-18.7	-0.85	94	0.7	001	5	
0.24	000	-18.7	0.00	94	0.8	002	5	
0.5	985	-18.7	0.00	96	0.8	003	6	
1.0	903	-18.7	0.00	96	0.8	003	6	
1.03	900	-18.7	0.00	96	0.8	022	4	
1.17	883	-18.7	0.00	96	0.9	013	4	
1.45	850	-19.1	0.15	97	0.8	001	5	
1.5	845	-19.2	0.15	97	0.8	358	5	

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.9	800	-19.6	0.14	97	0.8	343	4		16.0	97	-45.5	-0.18					265
2.0	789	-19.9	0.16	97	0.8	338	4		17.0	82	-45.5	0.00					
2.5	757	-20.7	0.16	95	0.8	310	5										
2.88	700	-21.5	0.20	95	0.8	297	6	316									
3.0	689	-21.7	0.20	95	0.8	297	6										
4.01	600	-26.8	0.50	93	0.5	306	9										
5.0	523	-32.4	0.57	91	275	7											
5.31	500	-34.5	0.64	90	273	10											
6.0	453	-38.8	0.64	88	300	16	371										
6.85	400	-43.5	0.51	88	305	21											
7.0	391	-43.9	0.43	87	314	35											
8.0	337	-48.2	0.43	86													
8.75	300	-53.2	0.73	85													
9.0	288	-55.5	0.34	85													
9.32	274	-56.6	0.34	85													
10.0	246	-56.6	0.00	84			344										
11.0	211	-52.8	-0.38	82													
11.33	200	-51.8	-0.17														
12.0	180	-51.1	-0.17														
13.0	155	-50.2	-0.09				268										
14.0	133	-49.2	-0.10														
15.0	115	-47.3	-0.19														
15.85	100	-45.6															

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.0	530	-25.8	0.41			308	4		0.9	923	-16.8	-0.65			081	4	
5.4	500	-27.2				325	4		1.0	911	-16.8	0.00			088	4	
6.0	461	-28.9	0.31			332	6		1.09	900	-16.8	0.00			096	2	
7.0	400	-33.5	0.46			334	10	440	1.5	854	-16.8	0.00			103	2	
8.0	347	-40.0	0.65			332	10		1.53	850	-16.8	0.00			109	2	
8.98	300	-46.4	0.65			329	22		1.8	819	-16.8	0.00			146	2	
10.0	256	-54.5	0.79			324	26		1.97	800	-17.7	0.50			168	2	
10.42	240	-57.3	0.67			325	25		2.0	797	-17.8	0.50			171	2	
11.0	219	-57.3	0.00			326	23		2.5	746	-19.2	0.28			216	2	
11.1	215	-57.3	0.00			325	22		2.97	700	-20.4				242	2	
11.57	200	-56.3				324	19		3.0	697	-20.5	0.26			244	3	330
12.0	188	-54.4	-0.32			323	16		3.56	647	-22.5	0.36			276	4	
13.0	160	-50.0	-0.34			317	12		4.0	609	-23.3	0.18			306	5	
14.0	137	-51.0	-0.10			312	12		4.1	600	-23.4	0.10			314	5	
15.0	117	-50.4	-0.06					596	4.8	543	-24.1				345	6	
									5.0	530	-25.8	0.85			347	7	
									5.41	500					349	7	
									6.0	460		0.84			347	9	310
									6.97	400	-41.8				330	8	
									7.0	397	-42.0	0.78			330	9	
0.0	042	-19.8		86		135	1		8.0	343	-48.2	0.62			335	11	
0.2	012	-21.1	0.65			106	3		8.83	300	-55.0				339	16	250
0.23	000	-20.8				089	4		9.0	292	-56.2	0.80			340	16	
0.5	973	-19.4	-0.57			086	5										

23.4 1404 $\varphi = 76^{\circ}17'$ $\lambda = 192^{\circ}34'$

1070 Ci, Cs

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
9.86	256	-60.0	0.46			324	21		1.0	911	-14.6				190	5	
10.0	250	-60.0	0.00			324	22		1.05	905	-14.5	-0.38			191	5	
10.73	223	-60.0	0.00			320	15	247	1.09	900	-14.5				192	5	
11.0	214	-58.4	-0.39			322	13		1.5	854	-14.5	0.00			202	2	
11.44	200	-55.0				328	11		1.53	850	-14.5	0.00			204	2	
12.0	183	-53.5	-0.49			314	8		1.86	814	-14.5	0.00			242	2	
13.0	156	-50.7	-0.28			314	5		1.99	800	-15.0	0.38			265	2	
14.0	134	-50.0	-0.07			313	6	223	2.5	747	-16.5	0.29			270	2	293
15.0	116	-49.4	-0.06			310	6		3.0	700	-17.7	0.24					
15.35	100	-47.9				299	5		4.0	612	-19.1	0.14					
16.0	99	-47.8	-0.16			299	4		4.15	600	-19.6						
17.0	85	-46.8	-0.10			297	6		5.16	534	-25.2	0.61					
18.0	74	-45.9	-0.09			288	5	290	6.47	500	-28.0	0.68					322
19.0	64	-45.3	-0.06			298	4		7.0	463	-32.0	0.64					
20.0	55	-44.5	-0.07					316	7.9	404	-38.4	0.64					
									7.96	400	-39.0						
									8.0	348	-46.3	0.79					
									8.36	300	-52.4						
									9.0	298	-52.6	0.73					
									10.0	254	-59.6	0.50					
									10.6	230	-61.7	0.52					
									10.88	221	-61.7	0.06					
									11.0	217	-61.1	-0.30					

24.4 0149 $\varphi = 76^{\circ}17'$ $\lambda = 192^{\circ}34'$

870 Ci, Cs

0.0	043	-24.8		99		135	1	
0.2	014	-20.2	-2.30			180	4	
0.3	000	-18.2				188	4	
0.5	973	-16.5	-1.23					

Пробл.к. приложения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
11.5	200	-57.9							2.5	746	-17.0	0.25			964	2	231
12.0	185	-54.3	-0.68						3.0	700	-17.7	0.14			971	2	
13.0	158	-52.6	-0.17						4.0	613	-19.4	0.17			980	5	
14.0	135	-51.9	-0.07				238		4.15	600	-20.1				989	6	
15.0	116	-50.9	-0.10						5.0	534	-24.0	0.46			998	7	248
16.0	100	-48.7	-0.22						5.47	500	-26.5				998	8	
16.2	97	-48.4	-0.15				233		6.0	465	-29.5	0.55			998		
									7.0	404	-37.0	0.75					236
24.4 1356 $\varphi=76^{\circ}17'$ $\lambda=192^{\circ}32'$																	
10 ¹⁰ Cs (580)																	
0.0	043	-18.5		84					8.0	348	-37.3	0.68					241
0.1	029	-18.7	0.20				135		9.02	300	-39.6	0.97					
0.2	015	-18.3	-0.40				137		10.08	252	-40.2	0.59					218
0.31	000	-17.5					162		11.0	221	-40.2	0.00					
0.5	975	-16.7	-0.33				156		11.61	200	-55.1						
0.8	937	-15.5	-0.40				169		12.0	188	-53.2	-0.70					216
1.0	913	-15.5	0.00				1		13.0	161	-50.1	-0.31					
1.11	900	-15.5	0.00				1		13.32	153	-48.9	0.00					
1.5	855	-15.5	0.00				1		14.0	139	-48.9	-0.37					212
1.54	850	-15.5	0.00				142		15.0	118	-48.9	0.00					
1.9	810	-15.5	0.00				1		15.88	103	-48.9	0.00					
1.99	800	-15.8					1										

Пробл.к. приложения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
0.0	044	-25.0							7.0	406	-33.3	0.62					
0.2	016	-18.0	-3.50						7.11	400	-34.0	0.69					
0.3	000	-16.0							8.0	352	-40.2	0.71					
0.5	975	-14.3	-1.23						9.0	304	-47.3	0.71					
0.84	932	-12.9	-0.41						9.09	300	-48.1	0.56					480
1.0	913	-12.9	0.00						10.0	261	-52.9	0.61					
1.11	900	-12.9	0.00						10.8	230	-57.8	0.61					
1.5	855	-12.9	0.00														
1.55	850	-12.9	0.00														
1.9	812	-12.9	0.00														
2.0	800	-13.1	0.20														
2.5	750	-14.3	0.24														
3.0	703	-14.9	0.12														
3.03	700	-15.0	0.15				383										
4.0	615	-16.4	0.15				301										
4.19	600	-17.0	0.49														
5.0	537	-21.3	0.38														
5.51	500	-23.5															
6.0	468	-27.1															

Продолж. приложения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
3.01	700	-16.7	0.10					350	0.7	553	-13.3	-0.50					
4.0	615	-18.1	0.14						1.0	916	-13.3	0.00					
4.17	600	-19.0							1.13	900	-13.3	0.00					
5.0	537	-24.0	0.59						1.5	859	-13.3	0.00					
5.51	500	-29.7							1.57	850	-13.3	0.00					
6.0	467	-30.0	0.60					342	1.95	809	-13.3	0.00					
7.0	405	-37.0	0.70						2.0	803	-13.4	0.20					
7.08	400	-37.4							2.03	800	-13.4						
8.0	350	-45.0	0.80						2.5	753	-14.6	0.24					
9.0	300	-50.8	0.58						3.0	705	-15.7	0.22					
10.0	258	-57.0	0.62						3.05	700	-15.8						
10.5	240	-60.3	0.66						4.0	616	-18.0	0.23					
11.0	222	-60.3	0.66						4.19	606	-18.5						
11.3	211	-60.3	0.66						5.0	538	-22.8	0.46					
11.47	205	-58.9	-0.32					400	5.53	500	-26.5	0.68					
									7.0	407	-36.6	0.70					
									7.13	400	-37.3						
									8.0	352	-43.1	0.65					
0.0	047	-22.7				0.00	3		9.0	303	-49.0	0.59					
0.2	019	-18.1	-2.30						9.06	300	-49.4						
0.33	000	-15.8							10.0	260	-54.7	0.57					
0.5	578	-14.3	-1.27						11.0	222	-59.6	0.49					

26.4 0129 φ = 76°19' λ = 192°18'

3,0 Cs

Продолж. приложения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
11.13	218	-60.2	0.46						1.61	850	-12.2	0.00					165
11.57	200	-60.2	0.00						1.7	839	-12.2	0.20					
12.0	190	-60.2	0.00					214	2.0	806	-12.8						
13.0	163	-54.2	-0.24						2.06	800	-12.9	0.24					
14.0	139	-51.8	-0.24						2.5	755	-14.0	0.36					168
15.0	119	-50.0	-0.60					211	3.0	707	-15.8	0.39					
16.0	102	-50.1	-0.68						3.07	700	-17.4	0.39					
16.12	100	-50.0							4.0	619	-19.7						
17.0	88	-49.3	-0.08					220	4.22	600	-20.3	0.46					
18.0	78	-47.8	-0.15						5.55	500	-27.3	0.66					
									6.0	469	-30.9	0.64					
									7.0	406	-37.3	0.64					
									7.1	400	-38.2	0.72					
									8.0	351	-44.5	0.65					
									9.0	301	-51.0	0.56					
									9.04	300	-51.4						
									10.0	258	-56.5	0.56					
									10.62	235	-59.3	0.44					
									11.0	221	-58.3	0.00					
									11.16	216	-58.3	0.00					
									11.64	200	-55.7						
									12.0	169	-54.0	-0.63					

26.4 1356 φ = 76°21' λ = 192°14'

0,0

0,0

0,1

0,2

0,35

0,5

1,0

1,15

1,2

1,5

0,1

0,20

0,37

0,36

0,25

0,00

91

112

5

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
13.0	161	-50.5	-0.35					169	4.0	617	-20.2	0.53					
14.0	139	-49.0	-0.15						4.2	600	-20.6						
15.0	119	-48.1	-0.09						5.0	537	-24.3	0.41					
16.0	102	-47.6	-0.05						5.51	500	-27.0						
16.12	100	-47.5						180	6.0	467	-30.2	0.59					
16.46	95	-47.4	-0.04						7.0	406	-37.0	0.68					
									7.09	400	-37.6						420
									8.0	352	-43.8	0.68					
									9.0	303	-50.8	0.70					
									9.05	300	-51.3						425
									10.0	258	-57.0	0.62					
									10.6	232	-59.6	0.43					

27.4 0154 φ = 76°22' λ = 192°11'

H	B	f	T	U	q	d	V	W
0.0	047	-22.5		97		135	5	
0.2	019	-18.6	-1.95			149	12	
0.33	000	-16.2				152	12	
0.5	978	-14.4	-1.40			152	12	
1.0	916	-12.4	-0.40			157	8	
1.13	900	-12.1				158	7	
1.5	858	-11.5	-0.18			154	8	
1.57	850	-11.5				153	7	
2.0	803	-12.2	0.14					
2.03	800	-12.3						
2.5	752	-13.3	0.22					
3.0	704	-14.9	0.32					383
3.03	700	-15.1						

27.4 1434 φ = 76°23' λ = 192°07'

H	B	f	T	U	q	d	V	W
0.0	047	-15.7				94	133	5
0.2	020	-15.7	0.00				164	8
0.34	000	-14.5					168	8
0.5	979	-13.2	-0.83				167	7
1.0	918	-11.5	-0.34				173	6
1.15	900	-11.2					170	5
1.3	880	-11.0	-0.10				156	4

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
1.59	850	-11.2				153	4		14.0	138	-49.6	-0.20			004	3	230
2.0	806	-12.2	0.24			135	4		15.0	120	-48.2	-0.14			031	3	
2.06	800	-12.4				131	4		16.0	103	-46.8	-0.14			020	3	
2.5	755	-13.4	0.24			123	5		16.2	100	-46.3				024	3	232
3.0	708	-14.2	0.16			109	6	322	17.0	89	-45.3	-0.15					
3.07	700	-14.4				106	6										
4.0	619	-19.0	0.48			072	3										
4.23	600	-20.4				062	2										
5.0	539	-24.0	0.50			344	2	240	0.0	047	-25.2				135	4	
5.54	500	-27.5				360	3		0.2	019	-17.0	-3.10			169	7	
6.0	469	-30.0	0.60			017	3		0.33	000	-15.4				166	5	
7.0	407	-36.9	0.69			012	4	225	0.45	985	-13.8	-1.28			101	5	
7.1	400	-38.0				018	4		0.5	978	-13.8				162	5	
8.0	353	-43.1	0.62			050	5		1.0	916	-13.8	0.00			142	3	
9.0	303	-50.4	0.73			022	6		1.14	900	-13.8				143	5	
9.05	300	-50.7				021	6		1.5	859	-13.8	0.00			121	4	
10.0	258	-56.4	0.60			020	7		1.57	850	-13.8						
10.8	237	-59.9	0.44			024	6	220	1.9	813	-13.8					181	
11.0	230	-59.9	0.00			026	5		2.0	803	-14.0	0.20					
11.4	207	-59.9	0.00			030	4		2.03	800	-14.1						
11.59	200	-57.0				032	3		2.5	751	-14.9	0.18					
12.0	189	-54.4	-0.92			031	4	230									
13.0	162	-51.6	-0.28			015	2										

28.4 0149 φ = 76°25' λ = 192°07'

H	B	f	T	U	q	d	V	W
0.0	047	-25.2				100	135	4
0.2	019	-17.0	-3.10				169	7
0.33	000	-15.4					166	5
0.45	985	-13.8	-1.28				101	5
0.5	978	-13.8					162	5
1.0	916	-13.8	0.00				142	3
1.14	900	-13.8					143	5
1.5	859	-13.8	0.00				121	4
1.57	850	-13.8						
1.9	813	-13.8						
2.0	803	-14.0	0.20					
2.03	800	-14.1						
2.5	751	-14.9	0.18					

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
3.0	704	-16.0	0.22					155	0.0	048	-16.5	1.00	89	112	3		
3.04	700	-16.2	0.44					155	0.06	041	-17.1	0.00		102	3		
4.0	616	-20.4	0.54					157	0.2	021	-17.1	0.00		128	5		
4.19	600	-21.6	0.54					157	0.35	000	-17.1	0.00		119	5		
5.0	538	-25.8	0.59					170	0.5	979	-17.1	0.00		110	4		
5.53	500	-28.7	0.59					170	1.0	917	-17.1	0.00		103	5		
6.0	468	-31.7	0.59					170	1.14	500	-17.1	0.00		100	5		
7.0	407	-37.6	0.59					170	1.5	858	-17.1	0.00		089	5		
7.11	400	-38.5	0.59					167	1.57	850	-17.1	0.00		087	5		
8.0	351	-43.5	0.59					167	2.0	800	-17.1	0.00		072	7		
9.0	303	-49.4	0.47					167	2.2	780	-17.8	0.33		068	8		
9.05	300	-49.5	0.34					167	2.5	749	-19.4	0.32		062	9		
10.0	259	-54.1	0.34					167	3.0	700	-24.6	0.42		054	13		294
11.0	222	-57.5	0.00					168	4.0	613	-29.6	0.63		053	14		
11.25	214	-57.5	0.00					167	4.16	600	-24.4	0.54					
11.64	200	-55.2	-0.68					167	5.0	584	-29.9	0.63					
12.0	189	-52.4	-0.25					167	5.47	500	-32.4	0.54					
13.0	185	-49.9	-0.02					167	6.0	463	-35.3	0.54					
14.0	189	-49.7	0.00					167	7.0	402	-42.5	0.73					
14.2	135	-49.7	0.00					167	7.0	402	-42.5	0.73					

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
7.04	400	-42.8	0.68					258	0.5	974	-15.5	-0.97		081	6		
8.0	345	-49.4	0.68					258	0.8	936	-13.8	-0.57		075	7		
8.9	300	-54.5	0.58					231	1.0	912	-13.8	0.00		074	8		
9.0	295	-55.2	0.55					231	1.1	900	-13.8	0.00		072	9		
9.6	269	-58.5	0.55					231	1.5	854	-18.8	0.00		069	10		
10.0	251	-58.5	0.00					231	1.94	800	-19.8	0.00		065	11		
10.7	226	-58.5	0.00					231	2.4	758	-13.5	0.00		065	11		
11.0	216	-56.5	-0.67					231	2.5	748	-14.4	0.00		064	12		284
11.46	200	-54.3	-0.47					226	3.0	700	-16.2	0.56		061	17		
12.0	185	-51.8	-0.13					230	4.0	614	-20.0	0.58		061	18		
13.0	159	-50.5	-0.12					230	4.17	600	-20.8	0.48		057	22		265
14.0	138	-49.3	-0.11					230	5.0	538	-24.8	0.51		061	17		
15.0	117	-48.2	-0.14					191	5.5	500	-27.5	0.57		061	18		
16.0	101	-46.8	-0.16					191	6.0	468	-29.9	0.51		061	18		
16.04	100	-46.7	-0.16					191	7.0	405	-35.6	0.57		062	25		
17.0	87	-45.2	-0.12					184	7.08	400	-36.2	0.64		062	25		
18.0	76	-44.0	-0.12					184	8.0	349	-42.0	0.67		061	18		
18.5	69	-44.0	0.00					184	9.0	300	-48.7	0.64		061	18		
								184	10.0	258	-54.4	0.57		061	18		
								184	10.41	242	-56.8	0.59		061	18		
								184	11.0	221	-56.8	0.00		061	18		
								184	11.14	216	-56.8	0.00		062	25		

29.4 0105 φ=76°26' λ=192°03'

5.0 Cs

0.0	010	-55.9						112	1
0.2	015	-55.4						104	5
0.31	000	-17.0						093	6

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
11.6	200	-54.7							5.0	529	-37.0	0.40					
12.0	188	-83.1	-0.43					300	3.41	500	-30.5	0.20					
12.3	179	-32.6	-0.17						0.0	459	-32.0	0.20					
									7.0	400	-37.9	0.29					
									8.0	345	-43.2	0.33					
									8.53	300	-48.4						
									9.0	297	-48.7	0.55					
									10.0	254	-52.7	0.40					
									10.55	235	-54.6	0.38					
									10.88	232	-54.6	0.00					
									11.0	218	-54.0	-0.50					
									11.59	200	-51.3						
									12.0	187	-49.2	-0.48					
									13.0	160	-46.8	-0.24					
									14.0	138	-45.7	-0.11					
									15.0	119	-44.9	-0.08					
									16.15	100	-43.4	-0.15					
									17.0	88	-42.4	-0.10					
									18.0	77	-41.7	-0.07					
									19.0	65	-40.9	-0.08					
									20.0	57	-39.8	-0.11					
									21.0	50	-39.1	-0.07					

29.4 1351 $\varphi = 76^{\circ}26'$ $\lambda = 191^{\circ}55'$
 0,0 Cs
 0.0 037 -17.0 0.00
 0.2 039 -17.0 0.00
 0.25 039 -16.9 0.00
 0.3 039 -16.4 -0.20
 0.9 919 -15.3 -0.23
 1.0 907 -15.5 0.00
 1.05 900 -15.5 0.00
 1.5 850 -15.5 0.00
 1.95 800 -15.5 0.00
 2.0 795 -15.5 0.00
 2.16 777 -15.5 0.00
 2.5 743 -16.5 0.29
 2.95 700 -18.0 0.38
 3.0 695 -18.4 0.38
 4.0 607 -23.0 0.46
 4.15 600 -23.6

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
22.0	42	-38.6	-0.05						4.0	604	-24.5	0.42	100	0.7			
23.0	36	-38.2	-0.04						4.04	600	-24.7	0.32	100	0.7			
24.0	31	-37.6	-0.06						5.0	525	-29.7	0.32	100	0.5			
25.0	27	-37.0	-0.06						5.35	500	-32.2	0.65	99				
26.0	23	-36.5	-0.05						6.0	455	-36.2	0.65	97				
26.4	21	-36.2	-0.08						6.89	400	-42.2	0.67	97				
									7.0	393	-42.9	0.70					
									8.0	339	-49.9	0.70					
									8.79	300	-52.8	0.38					
									9.0	290	-53.7	0.00					
									9.83	255	-53.7	0.00					
									10.0	249	-52.9	-0.47					
									11.0	213	-49.7	-0.32					
									11.37	200	-48.8						
									12.0	181	-47.6	-0.21					
									12.32	173	-46.9	-0.22					
									13.0	154	-46.9	0.00					
									14.0	133	-46.9	0.00					

30.4 0235 $\varphi = 76^{\circ}25'$ $\lambda = 191^{\circ}44'$
 5/5
 0.0 030 -20.9
 0.21 000 -17.4 -1.57
 0.5 963 -14.9 -0.86
 0.64 947 -13.9 -0.72
 1.02 900 -13.9 0.00
 1.45 850 -13.9 0.00
 1.5 844 -13.9 0.00
 1.71 821 -13.9 0.00
 1.91 800 -14.4
 2.0 790 -14.7
 2.5 739 -16.5
 2.9 700 -19.5
 3.0 693 -20.3

30.4 1355 $\varphi = 76^{\circ}25'$ $\lambda = 191^{\circ}26'$

10/0 Cs

H	B	f	T	U	q	d	V	W	H	B	f	T	U	q	d	V	W
0.0	027	-13.1							0.0	027	-13.1		100	0.45	12		
0.2	000	-11.3							0.2	000	-11.3		100	0.67	12		

Продолж. приложения

1.5 0149 $\phi = 76^{\circ}24'$ $\lambda = 191^{\circ}04'$
1000 Cs

H	B	f	Y	U	q	d	V	W	H	B	f	Y	U	q	d	V	W
0.5	962	-8.8	-0.83			072	12		0.0	026	-17.1		94	0.8	045	9	
0.64	945	-7.6	-0.86			071	16		0.19	000	-15.2		94	0.9			
1.02	910	-7.6	0.00			067	15		0.3	985	-12.8		93	1.2			
1.47	850	-7.6	0.00			073	14		0.5	960	-12.8		93	1.2			
1.5	847	-7.6	0.00			074	14		0.59	900	-12.8		92	1.3			
1.6	835	-7.6	0.00			077	12		1.43	850	-12.8		91	1.4			
1.93	800	-9.2	0.50			087	8	232	1.5	841	-12.8		89	1.4			
2.0	792	-9.2	0.56			087	8		1.87	800	-12.8		89	1.4			
2.5		-14.8	0.00			079	11		2.0	786	-12.8		89	1.4			
2.94	694	-15.2	0.56			080	9		2.04	786	-12.8		89	1.4			
3.0	607	-21.8	0.66				9	247	2.3	737	-15.1		89	1.2			
4.09	600	-22.3							2.89	700	-16.7		89	1.2			
5.0	531	-25.7	0.39						3.0	689	-17.4		89	1.1			
5.43	500	-27.7						174	4.0	603	-23.6		89	0.7			322
6.0	462	-31.2	0.55						4.03	600	-23.7		89	0.7			
7.0	400	-36.3	0.51					175	4.77	542	-28.2		89	0.4			
8.0	345	-43.4	0.71						5.0	525	-28.8		89	0.4			
8.75	309	-49.0	0.75						5.35	500	-29.6		89	0.4			
8.94	300	-49.0							6.0	455	-32.4		89	0.4			290
9.0	297	-49.0	0.00														
9.95	237	-49.0	0.00					175									
10.0	255	-48.7	-0.60														

Продолж. приложения

2.5 0152 $\phi = 76^{\circ}23'$ $\lambda = 190^{\circ}55'$
1000 As

H	B	f	Y	U	q	d	V	W	H	B	f	Y	U	q	d	V	W
6.80	400	-38.2							1.03	960	-13.2				069	10	
7.0	303	-38.8	0.64					238	1.14	888	-13.2	0.00			067	10	
8.0	340	-46.0	0.72						1.3	845	-14.0	0.22			068	10	
8.82	300	-52.4							1.92	800	-14.3	0.20			068	9	
9.0	292	-54.5	0.80						2.0	791	-15.0	0.34			060	8	
9.06	290	-54.5	0.00					195	2.5	741	-16.7				065	11	246
9.39	266	-53.1	-0.34						2.92	700	-19.0	0.56			065	10	
10.0	250	-58.1	-0.41						3.0	692	-19.5	0.46			065	10	
11.0	214	-60.0							4.0	604	-24.3	0.45			069	9	
11.45	200	-66.0							4.05	600	-24.5				070	9	
12.0	184	-67.0	-0.21					195	5.0	526	-28.8				070	9	
12.08	182	-66.7	0.00						5.35	500	-31.1	0.53			102	7	318
13.0	138	-66.7	0.00						7.0	400	-39.2	0.59			103	7	
14.0	136	-66.7	0.00						8.0	341	-46.3	0.63			115	8	
									8.84	300	-53.0				123	12	
									9.0	294	-54.2	0.79			130	11	255
0.0	030	-17.8				015	5		10.0	248	-51.2	0.00			145	4	213
0.2	003	-16.2	-0.80			065	10		11.0	214	-68.9	-0.53			150	4	
0.23	000	-16.1				072	10		11.43	200	-47.8				158	4	
0.5	963	-13.2	-1.00			070	10		12.0	183	-47.2	-0.17					
1.0	964	-13.2	0.00														

Продолж. приложения

H	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
13.0	158	-46.6	-0.06				177	5		5.38	500	-33.0	0.42					4	282
14.0	158	-46.6	0.00				148	7	210	6.0	458	-35.1						884	
14.5	128	-46.6	0.00							6.91	400	-42.0	0.73					886	5
2.5 1338 $\varphi = 76^{\circ}23'$ $\lambda = 190^{\circ}50'$																			
10/0 Cl, Cs																			
0.0	033	-13.2	0.67				89			8.87	300	-50.4	0.51						365
0.06	024	-13.6	0.00				022	5		9.3	281	-52.5	0.37						
0.2	004	-13.6	0.00				018	7		11.0	217	-48.4	-0.41						235
0.23	000	-13.6	0.00				059	8		11.54	200	-47.6							
0.5	965	-13.6	0.00				056	6		12.0	186	-47.2	-0.12						250
1.0	805	-13.6	0.00				049	6		13.0	160	-45.9	-0.13						
1.04	800	-13.6	0.00				048	6		14.0	138	-45.3	-0.06						
1.49	800	-14.7	0.24				050	6		15.0	119	-44.6	-0.07						230
1.94	800	-15.9	0.59				059	6		16.0	102	-44.0	-0.06						
2.5	743	-16.1	0.27				059	6		16.1	100	-44.0							
2.95	700	-18.5	0.48				089	6		17.0	88	-43.5	-0.05						218
3.0	695	-19.6	0.35				063	7	304	18.0	76	-43.0	-0.05						
4.0	607	-25.3	0.55				078	7		19.0	64	-42.8	-0.02						232
4.08	600	-25.6	0.46				078	7		19.43	59	-42.8	0.00						
5.0	528	-29.9	0.46				094	5											

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Продолж. приложения

H	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
3.5 0139 $\varphi = 76^{\circ}22'$ $\lambda = 190^{\circ}49'$																			
8/0 Cl																			
0.0	033	-20.6	-17.1	-1.75			100			5.35	500	-31.4	0.47						345
0.2	000	-16.8					068	8		6.0	455	-34.4							
0.4	977	-13.7	-1.70				067	8		6.9	400	-39.8	0.60						
0.5	965	-13.7	0.00				066	8		7.0	384	-40.4	0.60						
1.0	800	-13.7	0.00				067	7		8.0	360	-46.3	0.59						290
1.04	800	-13.7	0.00							8.42	319	-50.2	0.83						
1.4	838	-13.9	0.00							9.0	285	-50.2	0.00						
1.47	830	-14.0	0.30							10.0	231	-50.2	0.00						
1.5	847	-14.0	0.30							10.4	226	-48.7	-0.25						
1.53	800	-15.0	0.25							11.5	200	-47.2							270
2.0	732	-17.5	0.25							12.0	184	-45.3	-0.24						
2.5	740	-17.5	-0.44							13.0	158	-45.3	-0.10						
2.91	700	-19.0	0.34							14.0	135	-44.9	-0.04						310
3.0	692	-19.2	0.45							15.0	117	-44.5	-0.05						
4.0	604	-23.7	0.45							16.0	101	-43.9	-0.05						
4.05	600	-24.0	0.60							16.08	100	-43.3	-0.05						
5.0	525	-29.7	0.60							17.0	88	-43.4	-0.05						
337																			
										18.0	76	-43.4	0.00						
										19.0	66	-43.4	0.00						
										19.5	60	-43.4	0.00						310

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Продолж. приложения

H	D	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
4.5 01.49 $\varphi = 76^{\circ}22'$ $\lambda = 190^{\circ}45'$																	
8/0 Ci, Cc																	
0.0	0.03	-20.6	-	-	1.0	0.6	0.6	3	7.0	395	-12.2	0.70	71	305	3	256	
0.2	0.05	-	-	-	-	-	0.68	10	8.0	311	-48.8	0.66	69	232	3		
0.5	0.06	-	-	-	-	-	0.68	10	8.83	300	-54.0	0.68	68	203	4		
1.0	0.03	-	-	-	-	-	0.68	9	9.0	292	-54.9	0.61	68	207	4		
1.45	0.00	-	-	-	-	-	0.68	10	9.25	281	-56.4	0.60	68	192	4		
1.5	0.15	-	-	-	-	-	0.68	9	9.76	260	-56.4	0.60	67	151	3	250	
1.92	0.00	-15.0	-	-	9.9	1.2	0.68	9	11.0	214	-9.7	-0.52	65	141	3		
2.0	0.791	-15.2	-	-	9.9	1.2	0.68	11	11.45	200	-8.6	-0.18	64	147	3		
2.5	7.41	-17.0	0.36	-	7.5	1.0	0.68	11	12.0	183	-7.9	-0.08	61	146	3		
2.92	7.00	-18.8	0.42	-	7.3	0.7	0.68	8	13.0	158	-7.1	-0.08	61	142	2	236	
3.0	6.62	-19.1	0.43	-	7.3	0.5	1.04	6	14.0	135	-6.1	-0.07	59	161	2		
4.0	6.06	-21.9	0.53	-	7.3	0.5	1.06	6	15.0	117	-4.9	-0.13	57	164	1	234	
4.06	6.00	-23.2	0.32	-	7.3	0.65	1.06	5	16.0	101	-4.6	-0.03	54				
5.0	5.26	-30.1	-	-	7.3	0.65	1.06	5	17.0	87	-4.6	0.00	53				
5.37	5.00	-32.0	-	-	7.3	0.65	1.06	5									
6.0	4.57	-35.2	0.51	-	7.3	0.58	1.06	5									
6.33	4.00	-41.3	-	-	7.2	0.29	3										
4.5 1337 $\varphi = 76^{\circ}23'$ $\lambda = 190^{\circ}45'$																	
8/0 Ci																	
0.0	0.03	-14.8	-	-	9.9	1.0	0.65	5	0.0	030	-14.8	-	99	1.0	0.65	5	
0.22	0.09	-14.4	-	-	9.9	1.1	-	-	0.22	009	-14.4	-0.18	99	1.1	-	-	
0.5	0.95	-13.7	-	-	9.8	1.2	0.97	8									

Продолж. приложения

H	D	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
4.5 01.83 $\varphi = 76^{\circ}28'$ $\lambda = 190^{\circ}43'$																	
10/0 Ci																	
0.6	952	-13.5	-0.20	86	1.2	0.68	10		11.0	219	-48.7	-0.48	80	104	4		
1.0	903	-13.5	0.00	86	1.3	0.68	8		11.55	200	-47.3	-0.26	80	143	5	266	
1.03	900	-13.5	0.00	86	1.3	0.68	9		12.0	187	-46.1	-0.16	76	151	5		
1.3	869	-13.5	0.00	87	1.4	0.68	9		13.0	161	-44.3	-0.11	76	166	3		
1.46	850	-13.8	0.20	87	1.4	0.68	8		14.0	139	-43.2	-0.11	76	171	3	271	
1.5	846	-13.9	0.20	87	1.4	1.04	8		15.0	120	-42.7	-0.06	76	175	3		
1.93	800	-15.0	0.24	86	1.2	1.05	8		16.0	104	-42.0	-0.07	76	172	2		
2.0	791	-15.1	0.24	86	1.2	1.05	8		16.25	100	-41.8	-0.11					
2.5	740*	-17.0	0.38	82	1.1	1.08	8		17.0	89	-40.9	-0.11					
2.92	700	-17.8	0.20	80	1.0	1.10	9	330	18.0	78	-40.2	-0.07					273
3.0	692	-18.0	0.20	80	1.0	1.18	9										
4.0	604	-23.6	0.56	85	0.7	1.18	9										
4.05	600	-23.9	0.57	85	0.6	1.05	6										
5.0	536	-29.3	0.57	86	0.4												
5.35	500	-30.8	0.54	84	0.4												
6.94	400	-36.9	0.45	83	0.4												
7.0	396	-39.2	0.45	83	0.4												
8.0	342	-44.2	0.50	83	0.4												
8.53	300	-49.8	0.61	82	0.4												
9.0	297	-50.3	0.61	82	0.4												
9.68	268	-54.3	0.59	81	0.4												
10.0	255	-53.5	-0.25	81	0.4												
4.5 01.83 $\varphi = 76^{\circ}28'$ $\lambda = 190^{\circ}43'$																	
10/0 Ci																	
0.0	0.05	-23.5	-	-	10.0				0.0	026	-23.5	-	100	0.45	2		
0.19	0.00	-19.0	-	-	10.0				0.19	000	-19.0	-2.37	100	0.81	4		
0.5	0.95	-	-	-	10.0				0.5	055	-	-	100	0.81	7		
0.98	900	-	-	-	10.0				0.98	900	-	-	100	0.86	8		
(1.14)	881	-13.1	-	-	315				(1.14)	881	-13.1	-	100	0.86	9		
1.41	850	-13.7	0.25	-					1.41	850	-13.7	0.25	100	0.94	9		
1.5	840	-14.0	0.25	-					1.5	840	-14.0	0.25	100	1.01	10		
1.85	800	-14.7	0.22	-					1.85	800	-14.7	0.22	100	1.02	10		
2.0	785	-15.1	-	-					2.0	785	-15.1	-	100	1.02	10		

Прилож. приложение

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H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
2.5	745	-16.5	0.28			110	11	255	0.5	938	-15.1				062	3	
2.86	700	-17.8				111	9		0.86	914	-14.1				076	4	
3.0	687	-18.6	0.42			113	8		0.99	900	-14.4	0.28			075	4	
3.98	600	-23.2	0.47			116	9		1.43	850	-15.9				081	5	
5.0	522	-28.5	0.52			113	6	174	1.5	842	-16.0	0.31			084	6	
5.31	500	-30.0				117	6		1.89	800	-16.7				084	6	
6.0	451	-34.1	0.56			149	4	168	2.0	788	-16.9	0.18			085	6	
6.57	400	-39.4				125	3		2.5	737	-18.6	0.34			082	5	
7.0	333	-40.4	0.63			122	5	174	2.89	700	-20.4				083	5	310
8.0	339	-47.7	0.73			112	6		3.0	690	-21.2	0.52			084	5	
8.8	300	-53.1				111	6		4.01	600	-25.9	0.46			144	2	
8.88	206	-53.8	0.69			112	6		5.0	523	-31.1	0.52			170	3	
9.0	200	-53.8	0.00			114	5		5.29	500	-32.4				197	3	240
9.6	265	-53.8	0.00			117	5	167	6.0	451	-37.3	0.62			198	3	
10.0	248	-52.0	-0.45			112	6		6.85	400	-42.8				226	3	198
10.34	236	-50.3	-0.50			149	6	160	7.0	391	-43.9	0.66			226	3	
									8.0	337	-49.8	0.59			180	2	
									8.17	329	-50.3	0.29			184	2	
									8.77	300	-50.3				187	3	
									9.0	290	-50.3	0.00			189	3	
0.0	026	-15.6				045	2		9.21	280	-50.3	0.00			191	2	191
0.17	000			100		066	3		10.0	247	-46.3	-0.48			188	4	
0.2	937					072	3		11.0	215	-45.3	-0.30			192	4	

5.5 1338 $\varphi = 76^{\circ}22'$ $\lambda = 190^{\circ}36'$
O, O Ci, Ac

Прилож. приложение

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H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
11.47	900	-42.7	-0.08			103	4	188	1.4	850	-13.7	0.00			90	1.3	085
12.0	185	-42.7	-0.07			203	4		1.5	839	-13.7				69	1.2	088
13.0	180	-42.0	-0.07			210	3	177	1.85	800	-13.7	0.00			87	1.3	111
14.0	138	-41.2	-0.08			194	3		1.9	795	-13.7	0.00			87	1.3	103
15.0	119	-40.5	-0.06			187	4	186	2.0	784	-14.2	0.50			88	1.3	123
16.0	103	-40.0	-0.06			206	4		2.5	733	-17.3	0.62			93	0.9	132
16.17	100	-39.7	-0.07			195	3		2.85	700	-18.5				81	0.9	178
17.0	88	-39.3	-0.05			184	3	205	3.0	685	-18.9	0.32			81	0.8	179
18.0	78	-38.3	-0.05			188	3		3.98	600	-24.3	0.60			81	0.6	151
19.0	67	-38.1	-0.07			217	3		5.0	520	-29.4	0.45			81	0.4	195
20.0	58	-38.0	-0.01			207	3		5.29	500	-31.6	0.68			81		
20.4	54	-38.0	0.00			235			6.0	451	-36.2	0.68			81		
									6.79	400	-42.9						
									7.0	389	-44.2	0.30					
									8.0	335	-51.3	0.71					
									8.25	322	-52.9	0.64					
									8.69	300	-52.9						
									9.0	286	-52.9	0.00					
									9.16	273	-52.9	0.00					
									10.0	245	-50.0	-0.34					
									11.0	212	-45.8	-0.42					
									11.36	200	-45.2						
									12.0	181	-44.8	-0.10					

6.5 0146 $\varphi = 76^{\circ}22'$ $\lambda = 190^{\circ}42'$
7,0 Ac, Ci

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W	
12.44	170	-44.5	-0.07						1.41	850	-11.7		(79)	1.3	168	6		
13.0	156	-44.5	0.00					231	1.5	840	-11.8	0.20	(80)	1.3	168	6		
14.0	134	-44.5	0.00						1.86	800	-12.9		(92)	1.3	175	5		
14.5	124	-44.5	0.00					225	2.0	787	-13.7	0.38	(82)	1.2	179	5		
15.0	115	-44.1	-0.08						2.5	737	-15.7	0.40	(85)	1.2	174	6		
15.9	100	-43.7							2.89	700	-17.9		(86)	0.9	169	5	360	
16.0	98	-43.6	-0.05						3.0	690	-18.5	0.56	(87)	1.0	169	3		
17.0	86	-43.1	-0.05					225	4.03	600	-23.4	0.49	(92)	0.7	183	6		
17.3	82	-42.8	-0.10						5.0	525	-27.5	0.41	(94)	0.6				
18.0	75	-42.8	0.00						5.36	500	-30.2		(92)	0.7				
19.0	63	-42.8	0.00					225	6.0	456	-34.0	0.65	(89)					
19.65	58	-42.8	0.00						6.89	400	-39.2		(85)				379	
									7.0	394	-40.8	0.68	(84)					
									8.0	339	-49.0	0.82	(78)					
									8.45	315	-51.0	0.44						
									8.78	300	-51.0	0.00						
0.0	021	-11.5		100	1.4	090	2		9.0	291	-51.0	0.00						
0.17	090	-11.5	0.00	92	1.3	101	3		9.35	276	-51.0	0.00						
0.2	995	-11.5	0.00	83	1.2	137	5		10.0	249	-46.4	-0.40					344	
0.5	957	-11.5	0.00	(77)	1.2	161	5		11.0	214	-44.7	-0.37						
0.97	900	-11.5	0.00	(77)	1.2	161	5		11.44	200	-43.9							
1.0	897	-11.5	0.00	(79)	1.3	168	5		12.0	184	-42.8	-0.19						
1.35	856	-11.5	0.00															

6.5 1358 φ = 76°21' λ = 190°46'

9/0 C1, Cc, Ac (348)

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W	
12.41	173	-42.3	-0.12						2.5	732	-20.2						268	
13.0	159	-42.3	0.00					302	2.83	700	-21.2	0.30						
13.14	156	-42.3	0.00						3.0	684	-21.7							
14.0	138	-41.8	-0.06						3.95	600	-25.8	0.43						
15.0	117	-41.1	-0.07						4.0	596	-26.0	0.50					282	
16.0	101	-40.5	-0.06						5.26	500	-32.8	0.70						
16.07	100	-40.5	0.00					320	6.0	450	-38.0							
17.0	88	-40.5	0.00						6.81	400	-45.6	0.89						
17.65	80	-40.5	0.00						7.45	359	-46.9	0.89						
									7.65	353	-51.1	0.93						
									8.06	331	-52.5							
									8.35	300	-52.7	0.26						
									8.62	297	-52.7							
									9.0	289	-51.9	-0.44						
									10.0	250	-46.7	-0.32						
									11.0	216	-43.6	-0.31						
									11.49	200	-42.9							
									12.0	188	-42.3	-0.13						
									13.0	161	-42.3	0.00						
									14.0	159	-41.1	-0.12						
									14.27	133	-40.9	-0.07						
0.0	019	-10.8																
0.15	090	-11.4		85														
0.2	993	-11.5	0.35															
0.5	953	-12.0	0.17															
0.94	900	-12.6																
1.0	893	-12.7	0.14															
1.39	850	-14.6																
1.5	837	-15.2	0.30															
1.84	800	-17.4																
3.0	783	-18.2	0.60															

7.5 1343 φ = 76°21' λ = 190°46'

0,0

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.0	119	-40.9	0.00			198	8		1.0	891	-12.0	0.00			153	6	
16.0	104	-40.9	0.00			204	7	259	1.37	850	-14.0	0.00			157	6	
16.22	100	-40.9	0.00			202	6		1.5	835	-14.6	0.52			157	6	
17.0	90	-40.9	0.00			200	6		1.83	800	-16.4	0.48			159	5	
17.12	87	-40.9	0.00			202	6		2.0	781	-17.0	0.36			173	3	
18.0	77	-37.5	-0.39			207	6		2.5	720	-18.8	0.36			190	3	
19.0	67	-37.5	0.00			211	6		2.82	700	-20.3	0.44			201	3	
22.0	57	-37.5	0.00					261	3.0	683	-21.0	0.44			215	5	353
22.0	50	-37.5	0.00					263	3.95	600	-24.6	0.38			215	5	
22.0	42	-37.5	0.00						4.0	595	-24.8	0.38			214	5	
23.0	37	-37.5	0.00						5.0	519	-31.0	0.62			214	5	
23.8	33	-37.5	0.00					263	5.27	500	-33.0	0.87			228	4	
									6.0	450	-39.7	0.87			228	4	
									6.79	400	-46.3	0.81			217	4	343
									7.0	387	-47.8	0.81			237	6	
									7.8	343	-53.5	0.71			233	7	
									8.0	332	-53.5	0.00			220	8	
									8.66	300	-53.5	0.00			221	8	
									8.8	294	-53.5	0.00			232	8	
									9.0	283	-52.9	-0.20			217	9	312
									10.0	244	-48.8	-0.41			211	8	
									11.0	210	-46.1	-0.27			211	8	
									11.31	200	-45.9				212	7	

8.5 0120 $\varphi = 76^{\circ}21'$ $\lambda = 190^{\circ}48'$

100 Cs

H	B	t	Y	U	q	d	V	W
0.0	018	-18.4				135	2	
0.14	000	-14.7				188	3	
0.2	991	-13.3				187	4	
0.25	985	-12.0	-2.55			184	4	
0.5	951	-12.0	0.00			163	5	
0.83	900	-12.0				152	6	

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
12.0	180	-45.3	-0.08			194	8	275	0.95	900	-13.2	0.33			212	4	
13.0	155	-44.6	-0.07						1.0	885	-13.4	0.33			215	4	
14.0	133	-44.2	-0.04					296	1.30	850	-14.9	0.42			242	4	
15.0	115	-43.8	-0.04						1.5	838	-15.5	0.42			258	5	
16.0	100	-43.4	-0.04						1.85	800	-16.4	0.26			257	5	
17.0	85	-43.0	-0.04						2.0	783	-16.8	0.26			240	3	
18.0	74	-42.2	-0.08						2.5	722	-18.7	0.38			225	3	298
18.5	69	-41.9	-0.06					324	2.83	700	-20.3	0.46			222	3	
19.0	64	-41.9	0.00						3.0	684	-21.0	0.46			212	4	
20.0	55	-41.9	0.00						3.96	600	-24.3	0.35			211	4	
20.6	50	-41.9	0.00						4.0	597	-24.5	0.35			203	8	280
21.0	47	-41.9	0.00						5.0	520	-30.0	0.55			213	8	
21.25	45	-41.9	0.00						5.29	500	-31.8	0.70			219	10	
									6.0	451	-37.0	0.81			215	12	245
									6.81	400	-42.3	0.83			218	14	
									7.0	389	-43.3	0.83			220	14	
									8.0	335	-49.5	0.62			220	14	
									8.17	328	-50.5	0.59			224	16	
									8.74	300	-50.5	0.00			223	15	
									8.81	296	-50.5	0.00			224	16	
									9.0	283	-49.5	-0.53			221	15	229
									10.0	248	-46.1	-0.34			221	15	
									11.0	214	-43.5	-0.26			220	12	

8.5 1338 $\varphi = 76^{\circ}21'$ $\lambda = 190^{\circ}47'$

0/0

H	B	t	Y	U	q	d	V	W
0.0	011	-10.8				94	1	292
0.1	008	-12.4	1.60					217
0.15	000	-12.4						215
0.2	993	-12.4	0.00					214
0.5	955	-12.4	0.00					200
0.7	930	-12.4	0.00					212

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
11.44	200	-43.2				219	12		9.83	700	-19.4		88	0.9	214	2	
12.0	184	-42.9	-0.06			217	12		3.0	684	-20.0	0.34	88	0.9	210	3	
13.0	159	-42.4	-0.05			213	12	217	3.57	650	-24.0		83	0.6	210	7	327
14.0	138	-41.9	-0.05			214	10		4.0	589	-24.1	0.41	83	0.6	210	7	
15.0	118	-40.6	-0.13			205	9		5.0	521	-25.1	0.50	72	0.4	209	14	
15.8	104	-39.7	-0.11					272	5.3	500	-31.5		71		210	14	
									6.0	455	-33.2	0.61	70		217	18	338
									6.89	400	-40.7	0.83	70		225	26	
									7.0	394	-41.0	0.83	70		225	26	
									8.0	340	-46.2	0.32	69		227	38	
									8.81	300	-51.8		69		227	38	294
									9.0	291	-51.8	0.56	68		227	38	
									9.65	265	-51.8	0.40	68		223	28	
									10.0	251	-50.5	-0.37	67		219	22	
									11.0	215	-46.4	-0.41	66				
									11.46	200	-45.5		66				
									12.0	185	-44.5	-0.19	65				345
									13.0	160	-43.1	-0.14	64				235
									14.0	138	-42.3	-0.09	63				273
									15.0	117	-41.6	-0.07					
									16.0	101	-41.4	-0.02					

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9.5 0128 $\varphi=76^{\circ}21'$ $\lambda=190^{\circ}47'$

9.0 Ci

H	B	t	Y	U	q	d	V	W
0.0	019	-21.1				100	0.6	022
0.14	009	-17.2				99	0.9	075
0.2	092	-16.2	-2.45			99	1.0	124
0.41	065	-12.8	-1.62			99	1.2	0
0.5	053	-12.8				97	1.2	0
0.94	000	-12.8				97	1.4	1
1.0	893	-12.8	0.00			97	1.4	289
1.3	858	-12.8	0.00			96	1.4	302
1.37	850	-13.2				95	1.3	305
1.5	885	-13.7	0.45			95	1.3	311
1.82	900	-15.2				94	1.2	310
2.0	781	-16.0	0.46			93	1.1	314
2.5	732	-16.3	0.46			91	0.9	270

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.0	017	-12.6				068	4		7.0	391	-38.3		0.57				373
0.13	000	-13.8				079	5		8.0	339	-44.0		0.57				
0.2	591	-14.4				085	6		8.82	300	-50.7						
0.5	953					092	7		9.0	292	-52.4	0.84					
0.94	900					090	8		9.44	272	-56.6	0.95					328
1.0	893					080	8		10.0	249	-56.6	0.00					
1.37	850					080	7		10.16	242	-56.6	0.00					
1.5	835					089	7		11.0	213	-51.9	-0.56					
1.82	800	-14.9				11.43	300	-49.5	11.43	300	-49.5						263
2.0	780	-15.1				12.0	183	-47.2	12.0	183	-47.2	-0.47					
2.5	729	-16.0	0.18			13.0	157	-45.9	13.0	157	-45.9	-0.13					298
2.81	700	-17.3				14.0	135	-44.4	14.0	135	-44.4	-0.05					
3.0	683	-18.3	0.46			15.0	115	-44.1	15.0	115	-44.1	-0.13					
3.96	600	-22.2				16.0	99	-41.8	16.0	99	-41.8	-0.23					
4.0	596	-22.4	0.11														
5.0	520	-27.0	0.46														
5.98	500	-28.6															
6.0	451	-32.6	0.56														
6.85	400	-37.6															

10.5 0158 $\varphi=76^{\circ}23'$ $\lambda=190^{\circ}58'$

10/10 St (95)

H	B	t	Y	U	q	d	V	W
0.0	012	-13.8				100	1.1	090
0.1	000	-14.2				100	1.1	094
0.2	587	-14.8				100	1.1	103
0.39	963	-14.8				100	1.1	

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Продолж. приложения

H	B	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
0.5	949		-12.4	-2.18	100	1.4					11.0	217	-48.0	-0.31	79				211	
0.89	900		-10.3	-0.54	100	1.7					11.82	200	-45.5	-0.46	78					
1.0	888		-10.4	0.09	100	1.8					12.0	186	-43.4	-0.10	77					
1.34	850		-11.4		85	1.4					13.0	161	-42.4	-0.10	76				221	
1.5	831		-11.9	0.30	84	1.3					14.0	139	-42.0	-0.04						
1.70	800		-12.7		81	1.3					15.0	120	-41.6	-0.04						
2.0	779		-13.4	0.30	80	1.2					16.0	103	-41.3	-0.03						
2.5	759		-15.7	0.46	76	1.1					16.21	100	-41.2						254	
2.8	700		-17.3	0.32	76	0.9					17.0	89	-41.0	-0.03						
3.0	681		-17.3	0.32	77	0.8					18.0	78	-40.9	-0.01						
3.35	600		-19.9	0.37	79	0.9					19.0	67	-40.9	0.00					285	
4.0	558		-20.0	0.36	85	0.7					20.0	58	-40.9	0.00						
5.0	520		-23.6	0.58	85	0.5					21.0	50	-40.9	0.00						
5.29	500		-25.3	0.59	85	0.5					22.0	44	-40.9							
6.0	455		-29.5	0.59	85	0.3					22.04	43	-40.9	0.00					306	
6.89	400		-34.0	0.51	85															
7.0	394		-34.6	0.51	85						10.5	1343	$\phi = 76^{\circ}25'$	$\lambda = 195^{\circ}37'$						
8.0	341		-40.5	0.59	84						10/10 St									
8.85	300		-46.1	0.65	82						0.0	605	-10.6	97	1.5	180			2	
9.0	293		-47.0	0.58	81						0.05	600	-12.2	97	1.4					
9.57	269		-50.3	0.58	81						0.2	575	-14.6	98	1.1	150			3	
10.0	252		-50.3	0.00	81						0.29	567	-15.2	1.59	98	1.1	146			3
10.35	243		-50.3	0.00	80															

Продолж. приложения

H	B	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.5	940		-15.2	0.00	98	1.1					10.3	237	-52.8	0.00	85				
0.6	928		-15.2	0.00	98	1.1					11.0	214	-47.8	-0.71	84				
0.84	900		-13.3		99	1.2					11.42	200	-46.1	-0.40	83				
1.0	881		-12.8	-0.60	99	1.4					12.0	183	-43.8	-0.40	82				315
1.20	850		-12.0		100	1.6					13.0	158	-42.6	-0.12	82				
1.5	806		-11.8	-0.20	100	1.6					14.0	136	-42.1	-0.05	82				
1.70	774		-13.0	0.24	100	1.6					15.0	117	-41.6	-0.05	82				341
2.0	774		-14.9	0.38	100	1.4					16.0	100	-41.2	-0.04	82				
2.5	720		-15.9	0.58	100	1.4					17.0	87	-40.6	-0.05	82				
2.75	700		-16.8	0.38	100	1.4					18.0	74	-39.9	-0.07	82				
3.0	677		-20.5	0.58	100	1.3					19.0	64	-39.7	-0.02					
3.51	600		-20.8	0.40	100	1.0					20.0	56	-39.7						
4.0	583		-24.5	0.37	95	0.8					20.8	50	-39.7	0.06					377
5.0	518		-26.0	0.55	93	0.7					21.0	48	-39.7						
5.25	500		-26.0	0.55	91	0.5					21.28	46	-39.7	0.00					
6.0	451		-32.0	0.58	90														
6.85	400		-35.8	0.58	90														
7.0	391		-36.4	0.76	88						11.5	0138	$\phi = 76^{\circ}25'$	$\lambda = 195^{\circ}39'$					
8.0	337		-46.4	0.76	88						10/10 St								
8.78	300		-49.6	0.76	87						0.0	010	-18.4	100	0.7	270			3
9.0	290		-50.9	0.76	87						0.07	000	-18.2	100	0.8				
9.46	271		-52.8	0.39	86						0.2	983	-17.5	-0.45	100	0.8			
10.0	249		-52.5	0.00	85						0.5	944	-15.6	-0.63	100	1.1			

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.87	900	-12.9		52	1.4				11.0	213	-49.4	-0.19	68				
1.0	885	-12.4	-0.64	57	1.4				11.4	200	-49.2	-0.06	68				280
1.31	850	-12.4		55	1.5				12.0	183	-48.8	-0.05	68				
1.5	829	-12.4	0.00	53	1.5				13.0	159	-48.3	-0.22	68				
1.77	800	-12.4		50	1.4				14.0	136	-46.1	-0.22	68				292
2.0	777	-12.4		47	1.5				15.0	118	-43.5	-0.35					
2.06	771	-12.4	0.00	85	1.5				16.0	102	-42.8	-0.07					
2.5	737	-14.6	0.50	80	1.2				16.1	100	-42.8	-0.05					
2.79	700	-15.9		80	1.1			332	17.0	88	-42.3	-0.07					284
3.0	681	-16.4	0.35	79	1.0				17.0	88	-42.3	-0.05					
3.05	690	-20.0		78	0.9				17.44	82	-42.0	-0.07					
4.0	595	-20.2	0.38	78	0.9												
5.0	519	-24.9	0.47	76	0.6												
5.27	500	-26.6		75	0.5												
6.0	450	-29.1	0.72	75													
6.81	400	-27.1		74				311	0.0	013	-13.9		100	1.1	338	2	
7.0	390	-28.0	0.65	73					0.2	985	-17.1		97	0.9			
8.0	335	-46.0	0.30	72					0.24	980	-17.2	1.38	96	0.9			
8.74*	300	-52.1		70					0.5	918	-14.6	-1.00	93	1.0			
9.0	288	-53.5	0.69	70					0.86	905	-12.9	-0.47	88	1.2			
9.17	281	-54.5	0.39	70				310	0.9	900	-12.9		87	1.2			
9.6	264	-54.5	0.00	69					1.0	889	-12.9	0.00	84	1.2			
10.0	248	-51.3	-0.80	69					1.35	850	-12.9		77	1.2			

11.5 1342 φ = 76°25' λ = 190°42'

10/10 ≡ (6)

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
1.5	832	-12.9	0.00	75	1.1				14.0	137	-42.3	-0.05					
1.6	821	-12.9	0.00	74	1.1				15.0	119	-41.3	-0.08					279
1.8	800	-13.3		74	1.1				16.0	102	-40.0	-0.15					
2.0	779	-13.7	0.20	75	1.1				16.1	100	-39.9	-0.15					
2.5	729	-15.3	0.32	80	1.1				16.64	92	-39.0	-0.15					
2.8	700	-16.5		87	1.1				17.0	86	-39.0	0.00					275
3.0	681	-17.5	0.44	84	1.1			303	18.0	72	-39.0	0.00					
3.95	600	-20.9		84	0.8												
4.0	597	-21.0	0.35	83	0.8												
5.0	521	-25.1	0.41	72	0.6												
5.27	500	-26.5		71	0.5												
6.0	451	-29.2	0.72	69					0.0	011	-14.6		100				8
6.85	400	-27.5		67					0.07	000	-15.3	1.00					352
7.0	389	-28.9	0.65	67					0.2	983	-14.8	-0.38					9
8.0	330	-45.3	0.64	67					0.43	954	-12.4	-1.04					359
8.8	300	-51.6						273	0.5	945	-12.4	0.00					11
9.0	291	-52.5	0.73						0.74	916	-12.4	0.00					13
9.32	283	-52.6							0.88	900	-11.0	0.00					16
9.9	251	-52.1	-0.60						1.0	887	-11.0	0.00					11
11.0	216	-46.8						272	1.33	850	-11.0	0.00					10
11.48	200	-44.8							1.5	832	-11.0	0.00					10
12.0	184	-43.3	-0.23						1.7	810	-11.0	0.00					9
13.0	159	-42.9	-0.80					265	1.79	800	-11.1						

12.5 0133 φ = 76°22' λ = 190°31'

10/10 As (190)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.0	779	-11.7	0.23						16.16	100	-41.7	0.00					
2.5	729	-13.1	0.28						17.0	88	-41.7	0.00					326
2.81	700	-14.0							18.0	78	-41.7	0.00					
3.0	683	-14.6	0.30					335	19.0	66	-41.7	0.00					
3.97	600	-19.0							19.6	59	-41.7	0.00					326
4.0	597	-19.3	0.47														
5.0	523	-24.3	0.50														
5.33	500	-26.0															
6.0	454	-30.0	0.57														
6.88	400	-36.1						417	0.0	009	-13.2			98	1.2	300	14
7.0	394	-37.0	0.70						0.06	000	-13.6			97	1.2		
8.0	341	-43.3	0.63						0.14	990	-13.8	0.43		97	1.2		
8.86	300	-46.9	0.67						0.2	982	-13.8	0.00		97	1.2		
9.0	292	-48.0	0.73						0.5	945	-13.8	0.00		97	1.2		
9.3	280	-52.2	0.00						0.88	900	-10.4			97	1.7		
10.0	252	-52.2	0.00						1.0	886	-9.6	-0.84		97	1.8		
11.0	216	-47.6	-0.46					367	1.32	850				97			
11.48	200	-44.6							1.5	831				97			
12.0	185	-43.0	-0.46						1.78	800				97			
13.0	161	-42.0	-0.10						2.0	778				97			
14.0	139	-41.7	-0.03					303	2.5	729				97			
15.0	119	-41.7	0.00						2.81	700				96			
16.0	103	-41.7	0.00						3.0	682				96			

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.98	600	-16.8		96	1.3			363	20.0	58	-41.2	-0.02					325
5.0	524	-23.6	0.67	81	0.7				21.0	50	-41.2	0.00					
5.33	500	-25.0		78	0.6												
6.0	456	-27.7	0.41	74	0.5												
6.93	400	-33.5		71													
7.0	396	-31.0	0.63	71					0.0	012	-10.1						
8.0	343	-42.3	0.83	70					0.09	000							
8.88	300	-46.0		69					0.2	986							
9.0	294	-50.4	0.31	69					0.5	947							
9.25	270	-54.2	0.69	69					0.9	900							
10.0	253	-64.2		68					1.0	889							
10.04	251	-54.2	0.00	68					1.16	871	-6.8						
11.0	218	-47.1	-0.74	67					1.35	850	-6.8						
11.54	200	-44.6		66					1.5	835	-6.5	0.00					
12.0	187	-43.8	-0.33	66					1.83	800	-6.8						
13.0	161	-43.1	-0.07	65					2.0	782	-6.8	0.00					
14.0	140	-42.7	-0.01	64					2.5	733	-8.8	0.40					
15.0	120	-42.7	0.00	62					2.87	700	-11.2						
16.0	104	-42.4	-0.03	60					3.0	687	-12.0	0.64					
16.2	100	-42.4		60					4.0	603	-17.8	0.58					
17.0	89	-42.1	-0.03	59					4.04	600	-13.0						
18.0	78	-41.8	-0.03	57					5.0	526	-22.8	0.50					
19.0	67	-41.4	-0.04	57													

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.35	500	-24.5							1.5	833	-6.7	0.00			172	13	
6.0	457	-28.2	0.54					236	1.81	800	-7.7				163	13	
6.94	400	-33.1							2.0	781	-8.7	0.40			156	13	
7.0	357	-33.5	0.53						2.5	731	-11.7	0.60			141	12	
8.0	345	-40.4	0.69						2.83	700	-14.0	0.70			137	11	292
8.9	300	-49.0	0.97					272	3.0	685	-15.2	0.64					
9.0	286	-50.1	0.90						4.0	600	-21.6	0.72					
9.86	200	-61.6	1.07						5.0	524	-28.8	0.72					
10.0	254	-65.6	1.07						6.0	455	-34.0	0.52					302
11.0	219	-63.7	-0.49					240	7.0	392	-37.4	0.31					
11.59	200	-62.5							8.0	339	-44.7	0.73					
12.0	189	-62.0	-0.17						8.38	300	-46.0	0.37					874

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14.5 0123 $\varphi = 76^{\circ}18'$ $\lambda = 190^{\circ}16'$

7/8 Ac (273), Sc

H	B	t	Y	U	q	d	V	W
0.0	011	-6.8						158
0.09	000	-6.7	-0.11					151
0.2	985	-6.7	0.00					180
0.5	947	-6.7	0.00					140
0.89	900	-6.7	0.00					175
1.0	888	-6.7	0.00					174
1.35	850	-6.7	0.00					173

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.0	120	-41.8	0.00					210	2.5	739	-15.5	0.42			76	1.2	
16.0	104	-41.7	-0.01						2.91	700	-16.8				73	0.9	
16.22	100	-41.6							3.0	691	-17.1	0.72			71	0.9	363
17.0	90	-41.0	-0.07					208	4.0	605	-23.1	0.60			61	0.5	
18.0	77	-40.4	-0.05						4.05	600	-23.5	0.59			59	0.5	
									5.0	527	-28.4	0.53			42	0.2	
									5.38	500	-29.7	0.41			51		354
									6.0	459	-32.5	0.41			53		
									6.95	400	-39.5	0.77			51		
									7.0	386	-40.2	0.77			51		
									8.0	340	-49.1	0.59			48		
									8.14	300	-49.6	0.36			47		
									9.0	292	-46.4	-0.37			44		
									10.0	232	-44.2	-0.22			37		335
									11.0	217	-41.7	-0.25			32		
									11.55	200	-41.5	0.32			32		
									12.0	187	-41.3	-0.04			32		
									13.0	163	-40.8	-0.05			32		294
									14.0	141	-40.3	-0.05			32		
									15.0	123	-40.1	-0.02			32		
									16.0	103	-40.1	0.00			32		
									16.3	100	-40.1	0.00			32		
									17.0	89	-39.6	-0.07			29		311

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14.5 1332 $\varphi = 76^{\circ}19'$ $\lambda = 190^{\circ}16'$

10/10 Sc (172)

H	B	t	Y	U	q	d	V	W
0.0	018	-3.5						10
0.09	008	-4.2	0.78					87
0.15	000	-4.2						87
0.2	993	-4.2						86
0.29	982	-4.2	0.00					84
0.44	955	-2.8	-0.93					84
0.5	955	-2.8						83
0.68	934	-2.8	0.00					80
0.89	900	-3.7						77
0.97	897	-3.8	0.31					77
1.0	880	-7.3						77
1.4	850	-7.9	0.82					77
1.5	842	-11.0						77
1.58	800	-11.0						77
2.0	789	-11.4	0.70					77

Продолж. приложения

H	B	t	t	U	q	d	V	W	H	B	t	U	q	d	V	W
5.36	500	-24.5							1.5	833	-6.7	0.00		172	13	
6.0	457	-28.2	0.51					238	1.81	800	-7.7			163	13	
6.94	400	-33.1							2.0	781	-8.7	0.40		156	13	
7.0	397	-33.5	0.35						2.5	731	-11.7	0.60		150	12	
8.0	343	-40.4	0.69					272	2.83	700	-14.0			141	12	292
8.9	300	-49.0							3.0	685	-15.2	0.70		137	11	
9.0	296	-50.1	0.97						4.0	600	-21.6	0.64				
9.85	260	-59.1	0.00						5.0	524	-28.8	0.72				
10.0	254	-45.6	-1.07						6.0	455	-34.0	0.52				302
11.0	219	-43.7	-0.49					240	7.0	392	-37.4	0.34				
11.59	200	-42.3							8.0	339	-41.7	0.73				
12.0	189	-42.0	-0.17						8.35	322	-46.0	0.37				
									8.84	300	-46.0	0.00				874
									9.0	282	-46.0	0.00				
									9.1	288	-46.0	0.00				
									10.0	251	-43.7	-0.26				228
									11.0	217	-42.6	-0.11				
									11.58	200	-42.2	0.08				213
									12.0	187	-41.6	0.00				
									13.0	162	-41.6	0.00				
									14.0	140	-41.3	0.00				

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14.5 0123 $\varphi = 76^{\circ}18'$ $\lambda = 190^{\circ}16'$

7/9 Ac (273), Sc

H	B	t	t	U	q	d	V	W
0.0	011	-6.8						
0.09	000	-6.7	-0.11					158
0.2	985	-6.7	0.00					151
0.5	947	-6.7	0.00					180
0.89	900	-6.7						140
1.0	888	-6.7						175
1.35	850	-6.7						174
								173
								14

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Продолж. приложения

H	B	t	t	U	q	d	V	W	H	B	t	U	q	d	V	W
15.0	120	-41.8	0.00					210	2.5	729	-13.5	0.42		76	1.2	
16.0	104	-41.7	-0.01						2.91	700	-16.6	0.72		73	0.9	
16.22	100	-41.6							3.0	691	-17.1	0.60		71	0.9	363
17.0	90	-41.0	-0.07					208	4.0	605	-23.1	0.60		61	0.5	
18.0	77	-40.4	-0.05						4.05	600	-23.5	0.58		59	0.5	
									5.0	527	-26.4	0.55		42	0.2	
									5.38	500	-25.7	0.41		42	0.2	
									6.0	459	-35.5	0.41		50		364
									6.95	400	-39.5	0.77		51		
									7.0	396	-40.2	0.77		51		
									8.0	340	-49.1	0.89		48		
									8.14	300	-49.6	0.36		47		
									9.0	292	-46.4	-0.37		44		
									10.0	252	-44.2	-0.22		37		355
									11.0	217	-41.7	-0.25		32		
									11.55	200	-41.5	-0.04		32		
									12.0	187	-41.3	-0.05		32		
									13.0	163	-40.8	-0.05		32		294
									14.0	141	-40.3	-0.02		32		
									15.0	123	-40.1	-0.02		32		
									16.0	103	-40.1	0.00		32		
									16.3	100	-40.1	0.00		32		
									17.0	89	-39.6	-0.07		32		

14.5 1332 $\varphi = 76^{\circ}19'$ $\lambda = 190^{\circ}16'$

10/10 Sc (172)

H	B	t	t	U	q	d	V	W
0.0	018	-3.5						
0.09	008	-4.2	0.78					87
0.15	000	-4.2	0.00					87
0.2	989	-4.2	0.00					84
0.29	982	-4.2	0.00					84
0.44	953	-2.8	-0.93					82
0.5	955	-2.8	0.00					82
0.68	934	-2.8	0.00					80
0.97	900	-3.7	0.31					77
1.0	897	-3.8	0.00					77
1.43	850	-7.3	0.82					77
1.5	842	-7.9						77
1.89	800	-11.0						77
2.0	789	-11.4	0.70					77

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
18.0	77	-38.5	-0.11						0.0	024	-5.2	1.16	93	2.3	338		
19.0	57	-38.5	0.00					315	0.19	000	-7.4	0.70	90	1.9			
									0.5	961	-7.4	0.00	84	1.8			
									0.82	922	-7.4	-1.45	81	2.0			
									0.93	910	-5.8	0.00	76	2.0			
									1.01	900	-5.8	0.00	72	1.8			
									1.25	875	-7.2	0.64	71	1.7			
									1.5	845	-7.4	0.32	55	1.3			
									2.0	792	-9.0	0.28	49	1.0			
									2.5	742	-10.4	0.50	49	0.9			
									2.94	700	-12.6	0.50	49	0.9			
									3.0	695	-12.9	0.51	48	0.6			
									4.0	610	-18.0	0.44	47	0.5			
									4.12	600	-22.4	0.54	47	0.4			
									5.0	533	-24.8						
									5.46	500	-27.8						
									6.0	464							

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
7.0	403	-33.4	0.56	45					0.0	026	-6.8	1.16	97	2.0	338		
7.04	400	-33.5	0.61	45				279	0.2	000	-6.8	-0.10	96	2.1			
8.0	348	-39.5	0.77	45					0.5	302	-47.2	0.77	45				
9.0	302	-47.2	0.77	45					0.6	950	-3.7	-0.90	94	2.8			
9.03	300	-47.6	0.75	44					1.0	900	-3.7	0.00	86	2.9			
10.0	259	-54.8	0.75	44					1.03	900	-3.7	0.00	67	2.3			
10.15	283	-55.2	0.83	44					1.48	850	-3.7	0.00	51	1.5			
10.5	240	-56.2	0.00	43					1.95	800	-5.3	0.35	51	1.3			
11.0	222	-52.4	-0.76	43					2.0	785	-5.5	0.46	51	1.3			
11.64	200	-49.1	-0.44	43				303	2.5	746	-7.9	0.46	51	1.4			
12.0	189	-48.0	-0.44	43					3.0	700	-10.2	0.50	66	1.1			
13.0	163	-45.2	-0.28	43					4.0	614	-15.2	0.50	66	1.1			
14.0	141	-44.1	-0.11	43				314	4.17	600	-15.9	0.61	65	0.6			
15.0	122	-43.5	-0.06	43					5.0	537	-21.3	0.61	65	0.6			
16.0	105	-43.0	-0.03	43					5.52	500	-24.8	0.61	64	0.4			
16.3	100	-42.8	-0.05	43				365	7.0	405	-27.4	0.53	63				
17.0	90	-42.4	-0.05	43					7.1	400	-33.3	0.55	62				
18.0	78	-41.7	-0.07						8.0	352	-39.2						
19.0	67	-41.1	-0.05														
20.0	57	-40.5	-0.05														
20.86	50	-39.9	-0.07														
21.0	49	-39.8	-0.07														
22.0	42	-39.2	-0.06					369									

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18*

Предлож. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
9.0	304	-45.1	0.59	61				220	0.17	000	-6.9	0.30					076	8
9.09	300	-45.7		61					0.2	596	-7.0	0.30					080	9
10.0	281	-52.4	0.73	61					0.5	939	-7.7	0.23						
10.7	235	-56.5	0.59	60				231	0.7	935	-8.1	0.20						
11.0	224	-56.5		60					1.0	900	-3.9	-1.40						
11.04	223	-56.5	0.00	60					1.44	850	-3.9	0.00						
11.75	200	-52.0		60					1.5	844	-3.9	0.00						
12.0	192	-50.6	-0.61	59					1.91	800	-5.9	0.00						
13.0	164	-46.8	-0.38	59				252	2.0	791	-6.3	0.48						
14.0	142	-45.9	-0.09	57					2.5	711	-8.8	0.50						
15.0	121	-45.5	-0.04	56					2.95	700	-11.0	0.50						
16.0	105	-45.1	-0.04	55				262	3.0	695	-11.5	0.54						
16.29	100	-45.0		55					4.0	610	-16.5	0.50						
17.0	90	-44.7	-0.04	54					4.13	600	-16.9	0.43						
18.0	78	-44.2	-0.05	53				297	5.0	534	-20.8	0.43						
19.0	67	-43.5	-0.04	52					5.48	500	-24.0	0.72						
20.0	58	-43.4	-0.04	51					6.0	465	-28.0	0.72						
21.0	50	-43.1	-0.03	51					7.0	405	-31.9	0.39						
22.0	42	-43.1	0.00					329	7.07	400	-32.4	0.84						
									8.0	349	-40.3	0.84						
									9.0	303	-47.5	0.72						
									9.07	300	-48.5	0.72						
									10.0	259	-55.0	0.75						

16.5 1332 $\varphi = 76^{\circ}26'$ $\lambda = 189^{\circ}58'$
10/10 Sc (93)

0.0 | 023 | -6.4 | 100 | 068 | 5 |

Предлож. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
10.65	236	-55.0	0.00						0.15	000	-7.2	0.15	98	2.1			
11.0	225	-52.4	-0.74						0.2	692	-7.3	0.15	98	2.1			
11.8	200	-48.2						300	0.5	655	-8.5	0.40	95	1.9			
12.0	194	-47.7	-0.47						0.7	631	-8.7	0.10	94	1.9			
13.0	167	-45.3	-0.24						0.97	590	-5.7	0.10	93	2.5			
13.45	156	-44.1	-0.27						1.0	695	-5.5	-1.07	93	2.5			
14.0	144	-44.1	0.00						1.3	683	-4.4	-0.37	88	2.6			
15.0	125	-44.1	0.00						1.42	650	-4.3	0.10	81	2.1			
16.0	108	-43.4	-0.07						1.5	641	-4.6	0.10	81	2.1			
16.56	100	-43.1						383	1.89	600	-5.3	0.24	88	2.0			
17.0	94	-42.8	-0.06						2.0	789	-5.8	0.24	88	2.0			
18.0	82	-41.3	-0.15						2.5	740	-8.0	0.44	90	1.6			
19.0	72	-40.2	-0.11					360	2.93	700	-10.0	0.44	90	1.6			
20.0	63	-39.4	-0.08						3.0	693	-10.2	0.44	90	1.6			
21.0	56	-38.7	-0.07						4.0	609	-16.5	0.63	93	0.8			
21.9	50	-38.1							4.1	600	-17.0	0.38	92	0.7			
22.0	49	-38.0	-0.07						5.0	533	-22.3	0.38	90	0.5			
22.13	48	-37.9	-0.08					361	5.45	500	-24.6	0.38	90	0.4			
									6.0	463	-28.1	0.58	98	0.3			
									7.0	402	-33.8	0.57	98	0.3			
									7.03	400	-34.0	0.57	98	0.3			
									8.0	347	-40.3	0.63	98	0.3			
									8.6	317	-45.2	0.82	98	0.3			

17.5 0121 $\varphi = 76^{\circ}28'$ $\lambda = 189^{\circ}47'$
10/10 Ξ 9

0.0 | 020 | -7.0 | 100 | 2.1 | 0.90 | 6 |

Продолж. приложения

H	B	i	T	U	q	d	V	W	H	B	i	T	U	q	d	V	W
17.5 1411 $\varphi=76^{\circ}28'$ $\lambda=189^{\circ}45'$																	
10/10 St (87)																	
0.0	020	-2.2		90	2.9	180	9		7.0	397	-42.7	0.95	57				339
0.15	000	-2.7		90	2.8	132	10		8.0	342	-48.2	0.55	57				
0.2	983	-3.0	0.40	90	2.7	132	10		8.84	304	-48.2	0.00					
0.5	935	-3.6	0.87	87	2.3				8.93	300	-47.8						267
0.97	900	-5.6	0.00	87	2.3				9.0	295	-47.7	-0.31					
1.0	896	-5.6	0.00	86	2.4				11.0	219	-43.3	-0.09					
1.41	850	-5.6	0.00	85	2.4				11.59	200	-42.8						
1.5	841	-5.6	0.00	84	2.3				12.0	187	-42.5	-0.08					249
1.87	808	-7.0	0.50	84	2.1				13.0	162	-42.3	0.00					242
2.0	798	-8.1	0.50	84	2.1				15.0	121	-42.3	0.00					
2.5	738	-9.9	0.36	78	1.7				16.3	100	-41.4	-0.04					
2.91	700	-12.3	0.58	74	1.4				17.0	90	-40.8	-0.11					278
3.0	692	-12.3	0.58	71	1.3				18.0	78	-40.8	0.00					
4.0	607	-19.0	0.62	62	0.7			351	19.0	67	-40.2	-0.06					
4.08	600	-19.7	0.71	62	0.7				20.0	56	-39.3	-0.06					273
5.0	530	-25.1	0.71	57	0.4				18.5 0119 $\varphi=76^{\circ}30'$ $\lambda=189^{\circ}42'$								
5.43	500	-28.9	0.71	57	0.3				10/10 Sc (191)								
6.0	461	-33.2	0.71	57	0.3				0.0	021	-6.5		100		135	4	
6.97	400	-42.4		57					0.16	000			100		133	6	

Продолж. приложения

H	B	i	T	U	q	d	V	W	H	B	i	T	U	q	d	V	W
18.5 1929 $\varphi=76^{\circ}32'$ $\lambda=189^{\circ}36'$																	
10,10 St (18)																	
0.2	955			99		122	6		12.0	188	-43.6	-0.14					254
0.5	938			94		153	7		13.0	162	-43.1	-0.05					
1.0	900			94		123	7		14.0	139	-42.3	-0.03					
1.44	850			93		137	7		15.0	120	-42.3	-0.05					273
1.5	844			93		138	8		16.0	104	-42.0	-0.03					
1.91	800			92		145	9		16.25	100	-42.0	0.00					
2.0	790			91		146	8		17.0	91	-42.0	0.00					284
2.5	740			89					18.0	78	-41.9	-0.04					
2.93	700			89				239	19.0	68	-41.3	-0.03					
3.0	693			89					20.0	53	-40.9	-0.04					
4.0	607			86					21.0	50	-40.9	-0.03					
5.0	530	-24.1		86					22.0	43	-40.1	-0.05					
5.43	500	-27.2		82	0.5				23.0	38	-39.4	-0.07					
6.0	461	-31.6	0.75	78					24.0	33	-39.1	-0.03					348
6.98	400	-39.3	0.79	73					24.33	31	-39.1	0.00					
8.0	344	-45.7	0.63	73					18.5 1929 $\varphi=76^{\circ}32'$ $\lambda=189^{\circ}36'$								
8.91	300	-51.5							10,10 St (18)								
9.0	296	-51.7	0.60						0.0	021	-7.9		100	1.9	135	4	
9.1	291	-52.2	0.50						0.16	000	-9.5		100	1.7			
10.0	254	-49.1	-0.34						0.2	955	-10.1		100	1.6			
11.0	218	-45.0	-0.41						0.42	938	-10.1		95	1.6			
11.57	200	-44.1															

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.5	950	-7.8		81	1.7				11.0	220	-48.2	-0.51					
0.6	946	-5.8	-2.39	77	1.8				11.61	200	-45.7						
1.0	900	-5.8	0.00	50	1.3				12.0	189	-41.5	-0.37					
1.43	850	-5.8	0.00	50	1.4				13.0	163	-43.0	-0.15					282
1.5	843	-5.8	0.00	50	1.4				13.17	159	-42.9	-0.06					
1.6	831	-5.8	0.00	50	1.4				14.0	140	-42.9	0.00					
1.9	800	-6.4		50	1.4				15.0	121	-42.9	0.00					
2.0	789	-6.7	0.22	50	1.4				16.28	100	-42.6						
2.5	741	-9.3	0.52	50	1.2				17.0	90	-42.0	-0.09					
2.93	700	-11.6	0.93	50	1.0			353	18.0	77	-40.9	-0.11					317
3.0	693	-11.9	0.92	50	1.0				19.0	67	-39.1	-0.18					
4.0	609	-18.3	0.64	50	0.6				20.0	58	-37.4	-0.17					
4.1	600	-18.9	0.64	50	0.6				21.0	50	-36.5	-0.09					388
5.0	532	-23.2	0.49	50	0.4			344									
5.44	500	-25.9	0.49	50	0.3												
6.0	462	-29.4	0.77	50	0.3												
7.0	400	-37.1	0.77	50													
8.0	346	-43.8	0.67	50													
8.96	300	-50.5	0.68						0.6	019	-10.9		100	1.5	135	1	
9.0	298	-50.6	0.68					338	0.16	000	-11.1	0.10	89	1.5	142	3	
9.28	286	-52.4	0.64						0.2	985	-11.1	0.10	98	1.3	149	5	
10.0	256	-52.4	0.00						0.5	958	-5.5	-1.87	90	2.2	148	7	
10.18	249	-52.4	0.00						0.6	916	-4.0	-0.60	85	2.0			
									0.83	919	-4.9	0.00	76	2.0			

19.5 0117 $\varphi=76^{\circ}32'$ $\lambda=189^{\circ}35'$
10 10 $\frac{1}{3}$

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.99	900	-5.3	0.25	65	1.8				13.0	163	-43.1	-0.08					
1.46	850	-6.5	0.29	58	1.5				14.0	141	-42.3	-0.08					288
1.5	842	-6.8	0.29	55	1.4				15.0	121	-41.7	-0.06					
1.9	800	-8.2	0.48	49	1.2				16.0	105	-41.3	-0.04					
2.0	798	-8.7	0.38	48	1.2				16.32	100	-41.2						
2.5	738	-11.1	0.48	45	0.9				17.0	91	-40.9	-0.04					
2.91	700	-13.4	0.54	43	0.7			327	18.0	77	-40.8	-0.01					266
3.0	691	-13.8	0.54	42	0.7				19.0	67	-40.8	0.00					
4.0	606	-18.1	0.43														
4.07	600	-18.4	0.60														
5.0	530	-24.1															
5.4	500	-26.5	0.64														
6.0	459	-30.5	0.68					346	0.0	017	-7.8	1.00	85	1.5	135	3	
6.98	400	-37.2	0.76						0.2	891	-9.1	0.00	84	1.5	142	4	
8.0	346	-44.9	0.76						0.5	852	-9.1	0.00	80	1.5	138	5	
8.96	300	-48.0							0.94	800	-9.1	0.00	77	1.5	142	3	
9.0	298	-48.0	0.36					339	1.0	893	-9.1	0.00	76	1.5	144	3	
9.03	297	-48.6	0.00						1.29	893	-9.1	0.00	74	1.5	150	5	
10.0	257	-48.6	0.00						1.37	850	-9.5	0.30	74	1.5	152	5	
10.22	248	-48.6	-0.40						1.5	839	-9.8	0.30	73	1.4	153	5	
11.0	221	-46.5	-0.40						1.86	800	-10.9	0.30	71	1.4	141	6	
11.66	200	-44.5	-0.16					278	2.0	765	-11.3	0.30	70	1.3	146	6	
12.0	190	-43.0	-0.16														

19.5 1330 $\varphi=76^{\circ}33'$ $\lambda=189^{\circ}33'$
2,0 C1

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
2.5	735	-13.3	0.40	67	1.1	145	6		17.0	67	-30.3	-0.14			143	4	246
2.87	700	-15.3	0.38	67	0.9	153	6		18.0	72	-38.7	-0.06			120	3	
3.0	689	-16.2	0.35	67	0.9	152	6	349	19.0	53	-33.3	-0.04			100	3	248
4.0	603	-23.0	0.68	67	0.5	147	6		20.0	56	-38.3	0.00			116	4	
4.03	600	-23.4	0.68	67	0.5	148	6		20.5 0124 φ = 76°34' λ = 189°34'								
5.0	524	-30.5	0.75			158	6		10/10 III								
5.34	500	-32.9				163	6	329	0.0	017	-9.2		96	1.6	225	2	
6.0	455	-36.6	0.61			173	6		0.13	000	-10.1	0.69	95	1.5			
6.87	400	-42.4	0.65			230	5		0.12	690	-10.1	0.00	93	1.5			
7.0	302	-43.1	0.65			193	6		0.34	671	-10.1	0.00	91	1.5			
8.0	338	-48.7	0.56			177	8		0.34	653	-8.2	-1.19	88	1.8			
8.3	323	-50.0	0.43			172	10	310	0.3	616	-7.1	-0.37	84	1.8			
8.78	300	-50.0	0.43			173	10	310	0.3	600	-7.2	-0.37	82	2.0			
9.0	290	-50.0	0.43			171	9		0.54	590	-7.5	0.20	81	1.9			
9.65	262	-50.0	0.43			174	9		1.0	593	-8.3	0.22	64	1.4			
10.0	250	-48.8	-0.34			180	7		1.4	550	-8.6	0.22	64	1.4			
11.0	215	-47.0	-0.18			187	7		1.5	539	-10.4	0.48	53	1.0			
11.45	200	-46.5	-0.09			180	6	276	1.96	500	-10.4	0.48	53	1.0			
12.0	184	-46.1	-0.14			175	6		2.0	783	-10.4	0.28	49	0.9			
13.0	159	-44.7	-0.11			173	3		2.3	753	-10.4	0.28	48	0.8			
14.0	137	-43.5	-0.11			154	2	250	2.38	700	-10.5	0.34	48	0.8			
15.0	118	-42.7	-0.09			150	2		3.0	689	-14.1	0.34	48	0.8			303
16.0	100	-40.7	-0.20			150	2										

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
4.0	604	-20.8	0.67	45	0.4				14.0	139	-43.0	-0.05	37				276
4.04	600	-21.0	0.4	45	0.4				15.0	121	-42.6	-0.04	37				
5.0	525	-27.0	0.62	42	0.3				16.0	104	-42.4	-0.02	37				
5.36	500	-29.1		41	0.2				16.23	100	-42.4	0.00	37				
6.0	455	-32.7	0.57	40				292	17.0	89	-42.4	0.00	37				
6.93	400	-38.8		37					18.0	77	-41.4	-0.10					294
7.0	396	-38.4	0.67	37					19.0	67	-40.7	-0.07					
8.0	342	-46.1	0.67	37				273	20.0	57	-40.7	0.00					
8.65	310	-49.3	0.49	37					20.87	50	-40.7	0.00					
8.86	300	-49.3	0.49	37					21.0	49	-40.7	0.00					
9.0	294	-49.3	0.49	37					22.0	43	-40.7	0.00					
9.26	278	-49.3	0.49	37					23.0	35	-40.7	0.00					
10.0	253	-47.9	-0.22	37				296	23.26	34	-40.7	0.00					
11.0	216	-45.5	-0.24	37					20.5 1327 φ = 76°34' λ = 189°34'								
11.54	200	-44.4	-0.24	37					10/10 Sc								
12.0	188	-44.0	-0.15	37					0.0	019	-7.6		100	2.0	315	4	
13.0	161	-43.5	-0.05	37					0.14	000	-8.8		99	1.8	288	5	

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.	903	-0.2	0.80	98	1.8	294	4		6.92	400	-38.0		65		227	15	
	555	-11.6	0.80	95	1.4	288	3		7.0	396	-38.4	0.58	65		238	16	
0.7	930	-10.2	-0.70	91	1.7	299	4		8.0	341	-41.6	0.62	65		250	18	
0.95	900	-10.2		93	1.7	293	4		8.89	300	-49.2		65				344
1.0	895	-10.2	0.00	92	1.7	291	4		9.0	294	-49.4	0.48	65				
1.1	894	-10.2	0.00	91	1.7	288	4		9.34	280	-50.4	0.29					
1.4	890	-10.7		89	1.6	288	5		10.0	292	-50.4	0.00					
1.5	839	-10.9	0.17	89	1.6	286	5		11.0	216	-45.5	-0.49					
1.85	800	-11.4		85	1.6	281	7		11.51	200	-44.2						298
2.0	784	-11.8	0.18	85	1.4	256	7		12.0	186	-43.3	-0.22					
2.5	735	-13.3	0.20	80	1.3	246	7		13.0	160	-42.0	-0.13					
2.86	700	-14.9		75	1.1	244	7		14.0	139	-41.2	-0.08					
3.0	687	-15.7	0.38	73	1.1	244	7	311	15.0	119	-41.2	0.00					300
4.02	600	-21.6	0.53	65	0.6	224	9		16.0	104	-40.7	-0.05					
5.0	525	-27.8	0.63	65	0.4	221	10		16.27	100	-40.5						
5.35	500	-28.9		65	0.3	216	9		17.0	90	-40.2	-0.05					
6.0	645	-32.6	0.48	65		229	11	321	18.0	79	-39.6	-0.05					

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
18.0	69	-38.8	-0.08					380	1.5	841	-8.6		76	1.7			
20.0	59	-38.1	-0.07						1.97	800	-9.2	0.00	71	1.6			
21.0	50	-37.2	-0.09						2.0	787	-9.4	0.16	69	1.3			
22.0	44	-36.3	-0.09					387	2.3	737	-10.7	0.26	64	1.3			
23.0	37	-35.2	-0.11						2.89	700	-12.9	0.58	61	1.0			313
24.0	33	-35.2	0.00						3.0	690	-13.6	0.47	59	0.8			
25.0	30	-35.2	0.00						4.0	605	-16.3	0.39	58	0.8			
26.0	27	-35.2	0.00					373	4.05	600	-16.3	0.52	59	0.5			
26.6	26	-35.2	0.00						5.38	500	-25.3	0.38	59	0.5			352
									6.0	453	-25.3	0.51	51	0.4			
									7.0	400	-35.4	0.61	51				
									8.0	346	-40.8	0.54	51				
									8.99	300	-46.0	0.53	51				352
									9.84	253	-49.1	0.36	51				
0.0	020	-11.8		93	1.2	248	1		10.0	237	-49.1	0.00	51				
0.14	000	-11.8	0.00	100	1.4				10.24	248	-49.1	0.00	51				
0.2	903	-11.8	0.00	100	1.4				11.0	222	-48.7	-0.71					
0.45	961	-11.8	0.00	100	1.6				11.67	200	-41.7						
0.5	955	-11.0	-1.50	100	1.9				12.0	190	-41.2	-0.25					270
0.75	925	-8.6	-0.95	97	1.9				13.0	164	-40.4	-0.08					
0.97	900	-8.6	0.00	92	1.9				14.0	142	-39.8	-0.06					
1.0	896	-8.6		81	1.8				15.0	123	-39.2	-0.06					
1.41	850	-8.6															270

21.5 0128 $\varphi=76^{\circ}35'$ $\lambda=189^{\circ}34'$

10/10 III

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
16.0	107	-39.0	-0.02						2.5	736	-13.6	0.42	51	0.8			
16.47	100	-38.8							2.88	700	-15.1		50	0.7			330
17.0	92	-38.6	-0.04					288	3.0	689	-15.6	0.40	49	0.7			
18.0	79	-38.4	-0.02						4.02	600	-20.7	0.50	45	0.4			
19.0	68	-38.0	-0.04					267	5.0	525	-24.8	0.62	45	0.3			
20.0	60	-37.8	-0.02						5.36	500	-28.4	0.70	45	0.3			311
									6.0	457	-33.8		45				
									6.91	399	-39.6	0.84	45				
									7.0	385	-40.2	0.64	45				
									8.0	341	-47.1	0.69	45				
									8.81	300	-50.5		45				
									9.0	282	-53.9	0.65					295
									9.08	288	-54.2		0.60				
									9.52	270	-54.2	0.38					257
									10.0	251	-57.4	-0.38					
									11.0	215	-65.5	-0.58					
									11.48	200	-65.3						
									12.0	185	-64.2	-0.24					261
									13.0	159	-63.2	-0.10					
									14.0	137	-63.0	-0.02					
									15.0	119	-64.9	-0.11					
									16.0	103	-60.8	-0.11					
									16.13	100	-40.6						

21.5 1358 φ = 76°38' λ = 189°34'
10,10 Ns (14)

H	B	t	γ	U	q	d	V	W
0.0	019	-8.8		88	1.5	180	4	
0.15	000	-10.7		86	1.3			
0.2	992	-11.2	1.20	86	1.2			
0.3	979	-12.1	0.90	84	1.2			
0.5	953	-12.1	0.00	82	1.1			
0.58	943	-12.1	0.00	81	1.2			
0.8	917	-10.5	-0.73	79	1.3			
0.94	900	-10.5	0.00	75	1.3			
1.0	893	-10.5	0.00	71	1.3			
1.39	850	-10.5	0.00	65	1.2			
1.5	838	-10.6	0.09	64	1.2			
1.85	800	-11.2	0.00	60	1.1			
2.0	785	-11.5	0.18	58	1.0			

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
17.0	88	-10.0	-0.08					255	2.5	735	-12.5	0.42	59	1.1			
18.0	77	-39.8							2.88	700	-14.2		57	0.9			342
19.0	67	-38.4	-0.14					246	3.0	689	-14.7	0.44	56	0.8			
20.0	57	-37.5	-0.09						4.02	600	-19.3	0.45	52	0.6			
21.0	50	-36.5	-0.10						5.0	525	-24.8	0.56	52	0.4			
22.0	41	-35.7	-0.08						5.36	500	-28.9	0.56	52	0.3			
23.0	37	-35.0	-0.07					239	6.0	457	-29.9	0.51	52	0.3			322
									6.9	400	-34.9		51				
									7.0	394	-35.7	0.58	51				
									8.0	341	-42.9	0.72	50				
									8.89	300	-47.5		48				
									9.0	294	-48.2	0.53	48				299
									9.45	276	-50.9	0.60	48				
									9.75	263	-50.9	0.00	48				
									10.0	253	-50.0	-0.36	47				
									11.0	217	-65.1	-0.49	46				
									11.55	200	-62.9		46				
									12.0	187	-61.8	-0.33	46				261
									13.0	162	-61.0	-0.08	45				
									14.0	140	-60.8	-0.02	45				
									15.0	123	-60.6	-0.02	45				314
									16.0	108	-60.5	-0.01	45				
									16.65	100	-40.4						

22.5 0123 φ = 76°39' λ = 189°34'
10,10 Ns (21)

H	B	t	γ	U	q	d	V	W
-0.1016	-10.0			95	1.5	135	2	
0.13	000	-6.3		92	1.9			
0.2	992	-6.0	-2.00	91	2.1			
0.5	955	-7.1	0.37	87	1.9			
0.71	929	-9.0	0.90	84	1.6			
0.95	900	-9.0	0.00	81	1.6			
1.0	895	-9.0	0.00	80	1.6			
1.39	850	-9.0	0.00	74	1.6			
1.5	837	-9.0	0.00	72	1.5			
1.55	839	-9.0	0.00	71	1.5			
1.85	800	-10.0	0.00	67	1.3			
2.0	785	-10.4	0.33	65	1.3			

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
17.0	95	-60.3	-0.02						5.0	521	-28.0	0.60					
18.0	81	-60.0	-0.03					337	5.29	500	-29.3						
19.0	68	-59.8	-0.02						6.0	453	-34.0	0.60					372
22.5 1328 $\phi=76^{\circ}40'$ $\lambda=189^{\circ}34'$																	
10/10 St (19)																	
0.0	015	-8.9		90			180	5	8.35	322	-49.4	0.51					
0.11	000	-10.5							9.0	291	-49.4	0.00					391
0.2	988	-11.4	1.25						10.0	251	-45.6	-0.38					
0.5	969	-13.8	0.80						11.0	216	-43.2	-0.22					
0.87	904	-10.5	-0.89						11.51	200	-49.5						
0.91	900	-10.2							12.0	186	-42.2	-0.12					
1.0	889	-10.3	0.00						13.0	161	-41.8	-0.04					
1.36	850	-10.5	0.00						14.0	139	-41.4	-0.04					
1.5	834	-11.1	0.43						15.0	120	-41.0	-0.04					
1.83	800	-12.3							16.0	103	-40.7	-0.03					
2.0	782	-13.0	0.38						16.21	100	-40.6						
2.5	731	-14.8	0.36						17.0	89	-40.0	-0.07					
2.83	700	-15.9						327	18.0	77	-38.7	-0.13					
3.0	684	-16.6	0.36						19.0	65	-38.7	0.00					
3.97	600	-21.9							20.0	52	-39.7	-0.01					
4.0	588	-22.0	0.54						20.0	57	-38.7	0.00					388

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Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.0	013	-7.2		86			180	8	6.91	400	-37.1	0.74					
0.09	000	-7.7							7.0	394	-36.2	0.75					287
0.2	985	-8.2	0.50						8.0	340	-46.7	0.67					
0.5	947	-10.1	0.63						8.54	314	-49.3						
0.6	934	-10.8	0.70						8.83	300	-50.2	0.30					
0.86	904	-10.8	0.00						9.0	293	-50.7	0.30					
0.89	900	-10.4							9.1	289	-51.0	0.00					
1.0	888	-9.2	-1.14						9.3	280	-51.0	0.00					
1.34	850	-9.2							10.0	250	-47.3	-0.53					240
1.5	833	-9.2	0.00						11.0	216	-43.9	-0.34					
1.6	823	-9.2	0.00						11.51	200	-43.2						
1.83	800	-10.3							12.0	186	-42.4	-0.15					
2.0	781	-10.8	0.40						13.0	161	-41.8	-0.06					240
2.5	732	-12.0	0.24						14.0	139	-41.4	-0.04					
2.84	700	-13.0						319	15.0	121	-41.1	-0.03					
3.0	685	-13.4	0.28						16.0	104	-40.8	-0.03					
4.0	600	-18.7	0.53						16.25	100	-40.7						
5.0	524	-23.9	0.32						17.0	89	-40.5	-0.03					
5.25	508	-25.2						281	18.0	79	-40.2	-0.03					
0.0	458	-30.8	0.69						19.0	68	-40.0	-0.02					
									20.0	59	-39.8	-0.02					
									21.0	52	-39.7	-0.01					
									21.3	50	-39.6						

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Пробное приращение

H	B	t	γ	U	q	d	V	W	H	U	t	γ	U	q	d	V	W
22.0	44	-39.5	-0.02						0.93	180	-7.2		64	1.1			
23.0	38	-39.3	-0.02						1.0	388	-7.2		64	0.9			
24.0	34	-39.2	-0.01					450	1.34	650	-7.2		69	1.0			
25.0	30	-39.0	-0.02						1.3	853	-7.2		69	1.4			
26.0	28	-38.9	-0.01						1.7	811	-7.2		50	1.3			
27.0	25	-38.7	-0.02						1.8	800	-7.8		50	1.2			
28.0	22	-38.1	-0.05						2.0	780	-9.0		40	1.2			
29.0	20	-37.4	-0.07						2.3	731	-10.7		40	1.0			
30.0	17	-37.0	-0.04						2.83	700	-11.9		48	0.9			
31.0	14	-37.0	0.00						3.0	684	-12.3		47	0.9			
32.0	11	-37.0	0.00						4.0	600	-16.9		45	0.6			
32.75	10	-37.0	0.00						5.0	525	-22.8		45	0.4			
									5.35	500	-24.5		45	0.4			
									6.0	438	-29.1		45	0.3			
									6.97	400	-34.8		45				
									7.0	397	-35.0		45				
									8.0	343	-41.8		45				
									8.91	300	-46.2		45				
									9.0	295	-46.6		45				
									9.34	279	-48.8		45				
									9.85	259	-48.8		45				
									10.0	254	-48.1		45				
									11.0	220	-41.9		45				

23.5 1353 φ = 76°44' λ = 189°41'
10/10 St (10)

H	B	t	γ	U	q	d	V	W
0.0	009	-5.6		87	2.1	180		
0.07	000	-5.6		87	2.1	11		
0.2	993	-6.5	0.45	87	2.0			
0.46	972	-8.6	0.81	87	1.7			
0.5	947	-8.6		87	1.7			
0.7	923	-8.6	0.00	87	1.7			
0.8	911	-7.2	-1.40	87	2.0			

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Пробное приращение

H	B	t	γ	U	q	d	V	W	H	U	t	γ	U	q	d	V	W
11.63	200	-40.7							2.5	729	-14.1		69	1.1			
12.0	190	-40.4	-0.15						2.8	700	-15.3		64	0.8			
13.0	163	-39.7	-0.07						3.0	681	-16.4		60	0.8			
14.0	141	-39.1	-0.06				248		3.94	600	-21.9		55	0.5			342
15.0	121	-39.1	0.00						4.0	595	-22.1		55	0.5			
16.0	103	-39.1	0.00						5.0	520	-27.5		55	0.3			
16.15	100	-39.1							5.27	500	-29.6		55	0.3			
16.85	88	-39.1	0.00						6.0	452	-33.6		55				
									6.84	400	-41.0		55				
									7.0	391	-41.9		55				
									8.0	337	-47.9		55				
									8.12	331	-48.3		55				
									8.5	313	-48.3		55				
									8.75	300	-48.0		55				
									9.0	290	-47.3		55				
									10.0	219	-49.2		55				
									11.0	216	-41.3		55				
									11.5	200	-41.0		55				
									12.0	185	-41.3		55				
									12.0	160	-42.4		55				
									13.0	138	-42.4		55				
									15.0	119	-42.4		55				
									16.0	102	-41.4		55				
									16.0	89	-41.8		55				

24.5 0158 φ = 76°46' λ = 189°45'
10/10 St (19)

H	B	t	γ	U	q	d	V	W
0.0	008	-5.2		80	2.2	225		
0.07	000	-6.6		83	2.0	240		
0.2	981	-7.5	1.15	95	2.0	240		
0.5	945	-10.2	0.50	100	1.7			
0.87	900	-10.2	0.00	100	1.8			
1.0	885	-10.2	0.00	100	1.8			
1.33	850	-10.2	0.00	83	1.6			
1.5	831	-10.2	0.00	83	1.7			
1.67	813	-10.2	0.00	83	1.7			
1.79	800	-10.9		83	1.6			
2.0	778	-11.8	0.49	83	1.4			

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
16.14	100	-62.4	0.00					240	5.33	500	-27.2		38	0.2			276
16.6	93	-62.4	0.00						4.55	455	-31.8	0.62	38				
									6.01	400	-38.4	0.72	38				
									7.91	394	-39.0	0.72	38				
									7.76	354	-38.8	0.63	37				293
									8.0	340	-43.8	0.00	37				
0.0	012	-5.4		68	1.6	225	3		8.85	293	-43.8	0.00	36				
0.09	000	-6.1		74	1.7	207	4		9.0	285	-43.8	0.00	35				
0.2	985	-7.6	1.10	80	1.7	217	4		9.18	285	-43.8	0.00	35				
0.3	949	-9.6	0.67	78	1.4	246	4		10.0	253	-41.3	-0.30	35				
0.92	900	-12.6		76	1.1				11.0	219	-39.4	-0.19	34				
1.0	891	-12.7		76	1.1				11.32	209	-38.8	-0.19	34				
1.2	869	-9.5	-1.00	74	1.5				11.62	200	-38.8	0.00	34				
1.38	850	-9.5		73	1.5				12.0	189	-38.8	0.00	34				
1.5	835	-9.5	0.00	71	1.4				13.0	163	-38.8	0.00	33				
1.66	819	-9.5	0.00	70	1.5				14.0	141	-38.8	0.00	32				
1.84	800	-10.0		69	1.4				14.15	138	-38.8	0.00	32				
2.0	783	-10.4	0.26	62	1.2				15.0	121	-38.0	-0.09	32				
2.5	733	-12.4	0.40	48	0.9				16.0	105	-37.2	-0.08	32				
2.85	700	-13.9		45	0.7				16.35	100	-36.8						
3.0	687	-14.5	0.42	44	0.7	277			17.0	92	-36.6	-0.06					
4.0	600	-18.8		43	0.5				18.0	80	-35.8	-0.08					
5.0	524	-23.6	0.68	38	0.3				19.0	68	-35.6	-0.02					

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
20.0	59	-35.4	-0.02						1.82	800	-11.6		71	1.3			
21.0	52	-35.0	-0.04						2.0	781	-12.2	0.32	67	1.1			
21.22	50	-34.8							2.5	732	(-14.3)	0.43	66	1.0			
22.0	45	-34.3	-0.07			409			3.84	700	(-15.9)	0.46	66	0.9			310
23.0	38	-33.3	-0.10						3.99	685	(-16.6)	0.43	66	0.7			
24.0	33	-32.1	-0.12						4.0	660	-20.9	0.56	66	0.5			
25.0	30	-31.7	-0.04						5.31	522	-23.7	0.59	66	0.4			
26.0	26	-31.2	-0.05					403	6.0	453	-25.5	0.59	66				313
27.0	22	-30.8	-0.04						6.86	400	-36.5	0.69	66				
									7.0	383	-39.4	0.69	66				
									8.0	358	-46.5	0.71	66				
									8.22	327	-46.2	0.77	66				
									9.0	300	-48.2	0.80	66				
									9.0	291	-48.2	0.80	66				

25.5 1333 $\phi=76^{\circ}54'$, $\lambda=190^{\circ}00'$

10 10 St (50), Sc

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.0	013	-8.6		99	1.8	158	1		0.0	012	-5.0		88	1.2	180	4	
0.1	000	-		99	-				0.09	000	-6.9		87	1.8	160	5	
0.2	985	-		99	-				0.2	985	-8.5	1.75	87	1.7	155	6	
0.5	949	-		100	-				0.5	949	-10.6		85	1.4	144	7	
0.92	900	-9.7		97	1.8												
0.96	894	-9.2		96	1.9												
1.0	890	-9.2		94	1.9												
1.24	863	-9.2	0.00	80	1.8												
1.56	850	-10.0		80	1.5												
1.5	835	-10.6	0.54	78	1.5												

Продолж. приложение

H	B	f	γ	U	q	d	V	W	H	B	f	γ	U	q	d	V	W
0.57	940	-10.9	0.65	85	1.4				10.0	253	-51.0	-0.20					
0.8	913	-10.9	0.00	84	1.3				11.0	216	-48.4	-0.26					303
0.91	900	-9.5	-1.27	84	1.6				11.51	200	-46.2	-0.33					
1.0	890	-9.5		83	1.6				12.0	186	-45.1	-0.11					
1.37	870	-9.5		71	1.4				13.0	161	-44.0	-0.11					286
1.5	835	-9.5	0.00	66	1.4				14.0	139	-43.6	-0.04					
1.72	811	-9.5	0.00	66	1.4				15.0	119	-43.0	-0.06					
1.83	800	-9.7		64	1.3				16.0	102	-41.4	-0.16					
2.0	781	-10.2	0.25	52	1.1				16.25	100	-41.4	0.00					246
2.5	732	-12.5	0.46	50	0.9				17.0	89	-41.4	0.00					
2.85	700	-13.9		50	0.8			284									
3.0	685	-14.4	0.38	50	0.8												
4.0	600	-17.6	0.32	50	0.7												
5.0	526	-23.0	0.54	50	0.4												
5.37	500	-23.6		50	0.4			287	0.0	010	-6.2		95	2.2	180	6	
6.0	457	-30.2	0.72	50					0.07	030	-6.4		95	2.1			
6.94	400	-36.3	0.61	50					0.2	033	-6.9	0.35	95	2.1			
7.0	396	-36.3	0.61	50				288	0.3	045	-8.7	0.60	93	1.9			
8.0	341	-42.8	0.85	50					0.75	015	-8.6	0.30	94	1.8			
8.87	300	-49.2		50					0.89	000	-8.3		94	2.0			
9.0	294	-49.8	0.70	50					1.0	087	-7.3	-0.92	94	2.2			
9.3	291	-51.6	0.60						1.1	076	-6.6	-0.70	94	2.4			
9.7	265	-51.6	0.00						1.34	030	-6.6		87	2.3			

26.5 0132 φ = 76°56' λ = 190°00'
10/10 St (26)

Продолж. приложение

H	B	f	γ	U	q	d	V	W	H	B	f	γ	U	q	d	V	W
1.5	833	-6.6	0.00	85	2.3				16.0	104	-43.1	-0.07					300
1.82	800	-6.6	0.00	75	2.1				16.26	100	-43.0						
2.0	781	-6.6	0.00	71	2.0				17.0	90	-42.5	-0.06					
2.1	771	-6.6	0.00	68	2.0				18.0	77	-42.0	-0.05					328
2.5	732	-8.0	0.35	67	1.8				19.0	65	-41.5	-0.05					
2.85	700	-8.7	0.18	66	1.8				20.0	58	-41.0	-0.05					
3.0	686	-8.9	0.18	65	1.7			347	21.0	50	-40.6	-0.04					
4.0	604	-11.6	0.27	63	1.5				22.0	43	-40.2	-0.04					376
4.05	600	-11.7		63	1.5				23.0	38	-39.8	-0.04					
5.0	526	-17.1	0.55	61	1.0				24.0	32	-39.4	-0.04					374
5.41	500	-19.5		60	0.8			342	25.0	29	-39.0	-0.04					
6.0	461	-23.4	0.70	57	0.6												
7.02	400	-31.4	0.92	56													
8.0	348	-39.4	0.82	54													
9.0	300	-45.3	0.59	54				328	0.0	011	-6.0		84	2.2	225	4	
10.0	259	-51.3	0.50	53					0.07	000	-6.7		85	2.1			
10.6	236	-53.7	0.40						0.2	984	-7.8	0.90	88	2.0			
11.0	221	-53.3	-0.10						0.5	948	-9.7	0.63	88	1.8			
11.65	200	-52.2							0.6	936	-10.1	0.40	88	1.7			
12.0	190	-50.1	-0.32					283	0.92	900	-7.4	-0.84	88	2.2			
13.0	163	-45.9	-0.42						1.0	881	-7.4		88	2.2			
14.0	141	-44.5	-0.14						1.37	850	-7.4	0.00	88	2.4			
15.0	121	-43.8	-0.07														

26.5 1329 φ = 76°56' λ = 190°00'
10/10 St (16)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.5	835	-7.6	0.15	98	2.4				14.0	142	-40.2	-0.13					231
1.83	800	-8.3	0.20	98	2.4				15.0	123	-39.4	-0.08					235
2.0	782	-8.6	0.20	98	2.4				16.0	106	-38.7	-0.07					239
2.5	733	-9.6	0.30	89	2.0			284	16.39	100	-38.5	-0.08					243
2.8	705	-10.1	0.17	81	1.9				17.0	92	-37.9	-0.15					246
2.87	700	-10.4	0.18	80	1.8				18.0	80	-36.4	-0.02					247
3.0	689	-11.1	0.50	76	1.7				19.0	69	-36.2	-0.07					
4.0	603	-14.7	0.36	66	1.2				20.0	60	-35.5	-0.07					
4.05	600	-14.9	0.42	66	1.1				21.0	52	-34.6	-0.09					
5.0	528	-18.9	0.42	49	0.7			235	21.22	50	-34.5	-0.07					
5.41	500	-21.2	0.60	47	0.6				22.0	45	-32.9	-0.18					
6.0	461	-24.9	0.73	43	0.4			219	23.0	39	-32.1	-0.13					
7.0	401	-32.2	0.73	43					24.0	34	-30.8	-0.13					
7.04	400	-32.4	0.73	43					25.0	30	-30.2	-0.06					
8.0	348	-40.4	0.82	43				25.36	29	-29.4	-0.22						
9.01	300	-47.4	0.69	43													
9.95	260	-50.7	0.35	43													
10.0	258	-50.7	0.35	43													
10.47	241	-50.7	0.00	43				216	0.0	016	-6.0	83	1.9	315	5		
11.0	221	-45.9	-0.91	43					0.12	000	-6.2	83	1.9	316	6		
11.67	200	-44.2	-0.22	43					0.2	989	-6.5	83	1.8	318	6		
12.0	190	-43.7	-0.22	43					0.5	953	-7.9	83	1.9				
13.0	164	-41.5	-0.22														

27.5 0129 φ=76°59' λ=190°02'

10/10 St (49)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.88	907	-11.1	0.84	93	1.5				0.2	994	-9.0	1.30	84	1.5			
0.94	900	-11.1	0.00	93	1.6				0.5	957	-12.1	1.03	84	1.2			
1.0	893	-11.1	0.00	93	1.5				0.97	900	-12.1	0.00	83	1.2			
1.37	850	-11.1	0.00	85	1.5				1.0	897	-12.1	-0.87	82	1.5			
1.5	837	-11.1	0.00	81	1.5				1.16	878	-10.7	0.00	81	1.5			
1.86	800	-11.1	0.00	71	1.4				1.41	850	-10.7	0.00	81	1.5			
2.0	785	-11.1	0.00	69	1.3				1.5	840	-10.7	0.00	80	1.5			
2.26	759	-11.1	0.00	65	1.3				1.7	817	-10.7	0.00	80	1.5			
2.5	735	-12.1	0.42	58	1.1				1.87	800	-11.6	0.58	79	1.4			
2.87	700	-13.5	0.42	57	1.0			340	1.94	793	-12.1	0.58	78	1.3			
3.0	687	-14.1	0.40	57	1.0				2.0	786	-12.3	0.20	77	1.3			
3.37	655	-15.7	0.43	50	0.7				2.5	736	-13.2	0.16	71	1.3			
4.0	602	-18.2	0.40	50	0.6				2.75	713	-13.6	0.16	71	1.3			274
4.03	600	-18.3	0.54	50	0.6				2.87	700	-14.3	0.52	71	1.1			
5.0	526	-23.6	0.48	50	0.4				3.0	688	-14.9	0.61	70	0.7			
5.38	500	-25.1	0.48	50	0.4				4.0	603	-21.0	0.61	70	0.7			
6.0	459	-28.4	0.48	50	0.3			335	4.04	600	-21.2	0.69	68	0.4			248
									5.0	525	-27.9	0.78	68				
									5.35	500	-30.9	0.78	68				
									6.0	456	-35.7	0.63	68				
									6.9	400	-41.5	0.63	68				
									7.0	353	-43.0	0.63	68				

27.5 1439 φ=77°01' λ=190°02'

10/10 St (36)

Продолж. приложения

28.5 0129 $\varphi = 77^{\circ}02'$ $\lambda = 190^{\circ}02'$

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
8.0	341	-48.2	0.63	68					0.0	023	-7.3	83	1.7	015			
8.24	339	-46.4	0.46						0.17	000	-8.0	85	1.6	054	1		
8.48	300	-46.4	0.00						0.2	997	-8.2	85	1.6	054	2		
8.72	282	-46.4	0.00				241		0.5	959	-10.2	87	89	1.5	053	2	
8.96	264	-47.2	0.29						0.6	939	-11.7	89	1.4				
9.20	246	-44.4	-0.28						0.66	899	-8.4	89	1.7				
9.44	200	-43.0					245		1.0	880	-5.9	-0.97	83	1.7			
9.68	185	-43.7	-0.07						1.33	850	-5.9	67	1.7				
9.92	169	-42.5	-0.11						1.45	830	-5.9	62	1.7				
10.16	151	-41.3	-0.07				243		1.5	814	-5.9	0.00	56	1.6			
10.40	137	-42.0	-0.06						1.91	800	-5.9	0.00	54	1.6			
10.64	122	-40.7	-0.06						2.0	790	-5.9	0.00	52	1.6			
10.88	108	-40.4	-0.03				265		2.2	769	-5.9	0.00	50	1.2			
11.12	94	-40.0	-0.04						2.5	741	-5.4	0.83	50	1.2			
11.36	80	-39.5	-0.05						2.92	700	-10.8	48	1.0				
11.60	65	-39.5	-0.05				276		3.0	693	-11.4	0.00	47	1.0			310
11.84	50	-38.0	-0.15						4.0	608	-17.2	0.58	40	0.6			
12.08	35	-37.2	-0.08						4.11	600	-18.1	0.80	36	0.3			
12.32	21	0	-0.06				275		5.0	531	-23.2	0.30	34	0.2			
12.56	8	-35.9	-0.07						5.44	500	-27.8	0.70	34				
12.80	38	-35.9	-0.07						6.6	462	-32.2	0.70	34				

Продолж. приложения

28.5 1344 $\varphi = 77^{\circ}03'$ $\lambda = 190^{\circ}02'$

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
7.02	400	-36.4	0.41	34					0.0	025	-6.2	77					
7.26	386	-42.9	0.66	34					0.19	000	-7.8	0.84			135	5	
7.50	369	-51.5	0.85	34			286		0.5	959	-10.6	0.90			125	7	
7.74	351	-51.2	0.85	34					0.6	947	-11.2	0.90					
7.98	336	-50.6	0.00						0.85	917	-11.2	0.00					
8.22	320	-50.0	-1.00				287		1.0	900	-9.0	-1.47					
8.46	304	-48.5	-0.74						1.33	863	-6.5	-0.76					
8.70	288	-46.0	-0.34				246		1.45	850	-6.5	0.00					
8.94	272	-44.2	-0.10						1.93	800	-6.5	0.00					
9.18	256	-42.8	-0.08						2.0	792	-6.5	0.00					
9.42	240	-41.6	-0.12				249		2.5	742	-8.5	0.40					
9.66	224	-41.4	-0.06						2.95	700	-10.9	0.36					
9.90	208	-41.0	-0.04						3.0	685	-11.3	0.63					
10.14	192	-40.2	-0.04				309		4.0	610	-17.6	0.63					
10.38	176	-39.7	-0.03						4.12	600	-18.3	0.67					
10.62	160	-39.1	-0.03						5.0	532	-24.3	0.67					
10.86	144	-38.5	-0.06						5.45	500	-26.6	0.57					
11.10	128	-38.4	-0.01						6.0	463	-30.0	0.57					
11.34	112	-38.4	-0.06														
11.58	96	-38.4	-0.06				313										
11.82	80	-38.4	-0.06														
12.06	64	-38.4	-0.06														
12.30	48	-38.4	-0.06														
12.54	32	-38.4	-0.06														
12.78	16	-38.4	-0.06														

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
7.0	403	-34.8	0.48					375	0.0	021	-8.1		88	1.6	131		
7.05	400	-35.2							0.16	000	-9.0		83	1.5			
8.0	348	-42.9	0.81					317	0.2	995	-9.4	0.63	85	1.4			
9.0	300	-49.3	0.64						0.5	657	-11.8	0.80	85	1.2			
10.0	259	-56.5	0.72						0.65	937	-12.8	0.67	84	1.1			
11.63	200	-47.6	-0.57					323	0.97	900	-7.1	-1.78	83	2.0			
12.0	189	-46.2	-0.46						1.0	895	-7.1		81	2.0			
13.0	162	-45.0	-0.12						1.41	850	-7.1		81	2.0			
14.0	139	-43.8	-0.12						1.5	842	-7.1		81	2.0			
15.0	121	-42.4	-0.11						1.9	809	-7.1		75	2.0			
16.0	105	-41.6	-0.08						2.0	798	-7.1		74	2.0			
17.0	90	-40.8	-0.08					316	2.28	761	-7.1		70	2.0			
18.0	77	-40.0	-0.06						2.3	740	-7.8		63	1.6			
19.0	66	-39.4	-0.06						2.80	700	-9.8		56	1.3			
20.0	58	-38.3	-0.11					378	3.0	668	-10.2	0.48	56	1.3			
21.0	50	-36.8	-0.15						4.0	608	-15.2	0.30	52	0.9			
22.0	42	-35.6	-0.12						4.09	600	-15.7		52	0.9			
23.0	37	-34.6	0.00					382	5.0	531	-22.0	0.68	52	0.5			
24.0	32	-33.6	0.00						5.44	400	-21.3		52	0.4			
25.0	28	-33.6	0.00														

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Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
6.0	461	-26.7	0.47	52	0.4			446	0.0	018	-9.2		79	1.3	133	10	
7.02	400	-33.2	0.64	52					0.14	000	-10.0		78	1.2	139	10	
8.0	348	-38.4	0.53	52					0.2	993	-10.5	0.65	77	1.2	138	10	
9.0	302	-46.6	0.82	52					0.5	954	-12.6	0.70	75	1.0			
9.04	300	-46.8		52					0.65	936	-13.3	0.47	75	1.0			
10.0	260	-54.6	0.80						0.96	900	-8.2		72	1.6			
10.25	231	-52.7	0.44						1.0	895	-7.8	-1.57	72	1.6			
10.8	231	-52.7	0.00						1.41	830	-6.4		64	1.7			
11.0	224	-51.7	-0.50					395	1.5	840	-6.5		63	1.6			
11.73	200	-49.7							1.87	800	-7.3		56	1.4			
12.0	192	-48.7	-0.60						2.0	786	-7.7	0.22	54	1.4			
13.0	164	-45.8	-0.29						2.5	737	-9.1	0.28	53	1.3			
14.0	142	-45.4	-0.04					390	2.91	700	-10.9		52	1.1			
15.0	121	-45.0	-0.04						3.0	690	-11.4	0.46	51	1.1			
16.0	104	-44.6	-0.04						4.08	600	-16.7		47	0.7			
16.3	100	-44.4							5.0	529	-21.5	0.54	47	0.5			
17.0	90	-43.1	-0.15					406	6.0	462	-27.3		47	0.4			
18.0	77	-42.2	-0.09						7.0	402	-30.6		47	0.3			
19.0	66	-41.7	-0.05														
20.0	57	-41.2	-0.05														
21.0	50	-40.7	-0.05														
22.0	43	-40.0	-0.07														
23.0	37	-39.4	-0.05														
24.0	32	-37.7	-0.17					494									

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Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
30.5 0120 φ = 77°09' λ = 189°51'																	
10/10 St (31)																	
7.04	400	-31.0		47				272	0.0	015	-9.8		89	1.4	135		6
8.0	349	-38.3	0.77	47					0.11	000	-10.6		88	1.4			
9.02	300	-46.4	0.79	47					0.2	989	-11.6	0.90	87	1.2			
10.0	258	-52.0	0.57					265	0.35	970	-12.8	0.80	86	1.1			
11.0	222	-47.3	-0.47					277	0.5	951	-12.8	0.00	85	1.1			
11.68	200	-44.3	-0.43						0.73	924	-12.8	0.00	84	1.2			
12.0	188	-43.0	-0.43					291	0.94	900	-9.7		84	1.6			
13.0	164	-41.4	-0.16						1.0	883	-9.0		77	1.5			
14.0	142	-40.3	-0.66						1.07	884	-8.3	-1.32	71	1.5			
15.0	123	-40.2	-0.66						1.38	850	-8.3		58	1.3			
16.0	105	-40.0	-0.92						1.5	836	-8.3	0.00	55	1.2			
17.0	82	-39.5	-0.14					314	1.84	800	-10.2		55	1.1			
18.0	59	-37.8	-0.08						2.0	783	-10.6	0.46	57	1.1			
19.0	69	-37.2	-0.06						2.2	783	-11.2	0.30	61	1.2			
20.0	58	-37.2	-0.00						2.5	785	-11.9	0.23	61	1.1			
21.0	50	-36.6	-0.06					354	2.87	700	-12.9		61	1.1			329
22.8	39	-34.2	-0.16						3.0	687	-13.5	0.32	61	1.0			
23.0	38	-34.2	0.00						4.0	602	-20.0	0.55	61	0.7			
24.0	33	-34.2	0.00					338	4.03	600	-20.2		61	0.7			
25.0	28	-34.2	0.00														
25.37	26	-34.2	0.00														

Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
30.5 1335 φ = 77°09' λ = 189°52'																	
10/10 St (43)																	
5.0	585	-25.1	0.51	61	0.5			330	0.0	016	-7.9		85	1.6	135	7	
5.36	500	-26.4		56	0.4				0.12	000			88		122	8	
6.0	456	-29.9	0.46	49	0.2				0.2	889			88		124	9	
6.93	400	-35.6		44					0.5	922			86				
7.0	385	-37.2	0.73	44					0.33	900			84				
8.0	342	-46.0	0.88	43					1.0	893			84				
8.28	327	-47.7	0.51	43					1.37	850			84				
8.88	300	-47.7	0.00	41				285	1.5	858			82				
9.0	295	-47.7	0.00	41					1.84	800			81	1.8			
9.32	281	-47.7	0.00	40					2.0	783	-9.3		81	1.8			
10.0	254	-44.3	-0.13	40					2.14	770	-9.4	0.07	79	1.2			
11.0	219	-43.0	-0.18	40				273	2.5	734	-11.0	0.44	78	1.2			
11.6	200	-41.6	-0.18	40					2.83	709	-14.0	0.91	77	1.3			
12.0	188	-41.2	0.00	40				280	3.0	691	-14.0	0.90	75	1.4			
13.0	163	-41.2	0.00						3.45	663	-14.9	0.99	71	1.0			
14.0	140	-41.2	0.00						4.0	600	-17.3		71	1.0			
15.0	121	-41.2	-0.04						5.0	614	-17.3		69	0.5			
16.0	104	-40.8	-0.04					302	5.38	500	-24.8	0.61	62	0.6			
16.25	100	-40.6	-0.08						6.0	459	-26.7	0.34	57	0.4			
17.0	90	-40.0	-0.08														
18.0	78	-39.5	-0.05														
18.92	67	-39.5	0.00														

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
6.98	400	-31.6	0.50	55					26.0	26	-30.0	-0.10					
8.0	346	-37.8	0.61	53					26.68	23	-29.4	-0.09					389
9.0	300	-44.0	0.62	52				302									
9.9	265	-44.0	0.00	46													
10.0	238	-43.2	-0.80	45													
11.0	222	-40.6	-0.26														
11.7	200	-39.8						307									
12.0	192	-39.5	-0.11						0.0	014	-5.8			96	112	5	
13.0	166	-38.8	-0.07						0.11	000	-6.6						
14.0	144	-38.4	-0.04						0.22	989	-7.4	0.80					
15.0	124	-38.0	-0.04					315	0.5	951	-8.2	0.27					
16.0	108	-37.6	-0.04						0.93	900	-9.4						
16.5	100	-37.4							1.0	892	-9.6	0.28					
17.0	93	-37.1	-0.05					314	1.37	850	-10.6						
18.0	80	-36.4	-0.07						1.5	838	-11.1	0.30					
19.0	70	-35.6	-0.08						1.84	800	-12.9						
20.0	60	-35.0	-0.06						2.0	783	-13.8	0.54					
21.0	52	-34.5	-0.05						2.5	734	-13.8	0.00					
21.3	50	-34.4						390	2.85	700	-13.8						
22.0	45	-33.7	-0.08						3.0	686	-13.8	0.00					
23.0	40	-32.5	-0.12						3.28	661	-13.8	0.00					
24.0	34	-31.8	-0.07						4.0	600	-18.2	0.61					
25.0	30	-31.0	-0.08						5.0	535	-24.0	0.58					

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Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.34	500	-25.5						312									
6.0	466	-30.2	0.62						0.0	009	-3.4			90	2.5	112	7
6.94	400	-33.3							0.07	000	-3.5			90	2.6		
7.0	386	-35.1	0.59						0.2	983	-3.9	0.35		90	2.5	100	10
8.0	344	-40.6	0.45						0.5	945	-5.2	0.43		89	2.3		
8.9	300	-44.6	0.42					320	0.89	900	-6.6			89	2.2		
9.0	285	-44.8							1.0	888	-7.5			89	2.0		
9.5	274	-46.0	0.24						1.0	878	-8.2	0.58		89	2.0		
10.0	255	-45.6	-0.08					380	1.35	850	-8.4			89	2.0		
11.0	221	-44.8	-0.08						1.5	833	-8.5	0.07		89	2.0		
15.0	78	-40.9							1.83	800	-8.8			89	2.0		
19.0	68	-40.0	-0.09						2.0	781	-9.0	0.10		89	2.0		
20.0	58	-39.2	-0.08						2.5	732	-9.4	0.08		88	2.0		
21.0	50	-38.6	-0.06					371	2.84	700	-9.6			88	2.1		
22.0	42	-38.0	-0.06						3.0	686	-9.7	0.06		88	2.2		
23.0	37	-37.4	-0.06						4.0	600	-14.7	0.50		87	1.6		
24.0	32	-37.0	-0.04						5.0	526	-19.6	0.49		85	1.1		
25.0	28	-36.6	-0.04					420	5.39	500	-21.3			83	0.9		
26.0	24	-36.2	-0.04						6.0	460	-24.8	0.52		81	0.7		
26.7	22	-35.9	-0.04						8.0	345	-32.2	0.78		69			

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
8.06	300	-46.0	0.71	64					0.04	000	-3.4	0.05	95	2.8				
9.0	298	-46.3	0.71	63					0.2	890	-3.5	0.07	95	2.8	037			
9.22	289	-46.0	0.77	62			298		0.5	842	-3.7	0.08	94	2.8				
10.0	237	-45.0	0.00	62					0.75	912	-3.9	0.08	94	2.8				
10.3	245	-45.0	0.00	62					0.85	900	-4.4	0.08	93	2.7				
11.0	221	-44.7	-0.57	62					1.0	884	-5.0	0.44	93	2.7				
11.7	200	-41.7	-0.29	62			270		1.31	850	-6.6	0.52	92	2.3				
12.0	185	-40.6	-0.03	60					1.8	800	-9.1	0.21	91	2.0				
14.0	141	-40.1	-0.03	58			280		2.0	779	-10.2	0.21	91	1.9				
15.0	121	-39.6	-0.03	58					2.3	749	-10.2	0.00	90	2.0				
16.0	106	-39.0	-0.06	55					2.5	730	-11.1	0.45	89	1.9				
16.42	100	-38.7	-0.06	55			281		2.81	700	-12.1	0.38	88	1.7			323	
17.0	92	-38.2	-0.06	55					3.0	683	-13.0	0.38	88	1.5				
18.0	79	-36.8	-0.14	55					3.98	600	-18.4	0.55	88	0.8				
18.54	74	-36.7	-0.30	55					5.0	522	-24.6	0.61	46	0.4				
19.0	69	-35.7	0.00	55					5.31	500	-27.3	0.71	39				298	
20.0	59	-35.7	0.00				285		6.0	453	-31.7	0.71	39					
21.0	50	-35.7	0.00						6.87	400	-38.0	0.71	35					
									7.0	392	-38.8	0.71	35					
									7.72	354	-43.1	0.60	34					338
									8.0	340	-43.1	0.00	33					
									8.84	300	-43.1	0.00	32					

1.6 0138 $\varphi = 77^{\circ}15'$ $\lambda = 189^{\circ}18'$
10,10 Ns (43), X^o

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
9.0	293	-43.1	0.00	32					0.07	000	-1.8	0.95	85	2.7			
9.84	260	-43.1	0.00	30					0.2	862	-3.2	0.77	91	2.3			2
10.0	254	-41.6	-0.94	30			235		0.5	846	-6.6	0.26	100	2.4			
11.0	219	-41.0	-0.06						1.0	808	-6.8	0.26	100	2.4			
11.62	200	-40.5	-0.07						1.35	800	-8.0	0.40	100	2.3			
12.0	189	-40.3	-0.07				238		1.5	833	-8.3	0.40	100	2.1			
13.0	163	-39.8	-0.05						1.81	800	-10.9	0.64	100	1.7			
14.0	140	-39.6	-0.02						2.0	780	-12.0	0.56	98	1.6			
15.0	121	-39.3	-0.03				241		2.5	731	-13.6	0.32	98	1.4			
16.0	105	-39.0	-0.03						2.83	700	-14.2	0.22	96	1.4			237
16.37	100	-38.9	-0.02						3.0	684	-14.7	0.22	95	1.4			
17.0	92	-38.8	-0.02						3.59	600	-19.6	0.49	77	0.8			232
18.0	78	-38.5	-0.03				268		5.0	522	-26.2	0.55	68	0.3			
19.0	68	-38.2	-0.03						5.31	500	-28.4	0.67	67	0.4			
20.0	60	-37.7	-0.05						6.0	454	-32.9	0.67	67	0.4			
21.0	52	-37.1	-0.06				267		6.89	400	-38.6	0.64	73				247
21.3	50	-36.9	-0.07						7.0	394	-39.3	0.64	73				
21.9	46	-36.4	-0.07						8.0	339	-46.4	0.71					
22.0	46	-35.5	-0.09						8.4	320	-46.4	0.00					
23.0	42	-35.5	-0.09				269		8.83	300	-45.8	-0.15					
23.3	40	-35.3	-0.07						9.0	292	-45.5	-0.15					
									10.0	251	-43.3	-0.22					

1.6 1328 $\varphi = 77^{\circ}15'$ $\lambda = 189^{\circ}18'$
10,10 Ss, X^o

0.0 | 008 | -1.3 | 84 | 2.8 | 0

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
11.0	217	-41.4	-0.19						1.83	800	-9.6		79	1.7			
11.55	200	-40.7	-0.09						2.0	782	-10.1	0.28	76	1.6			
12.0	187	-40.5	-0.09					266	2.5	733	-12.4	0.46	70	1.3			
13.0	162	-40.0	-0.05						2.86	700	-14.1		66	1.0			309
14.0	140	-39.6	-0.04					295	3.0	686	-14.8	0.48	65	1.0			
15.0	122	-39.2	-0.04						4.0	602	-19.0	0.42	51	0.6			
16.0	106	-39.2	0.00						4.03	600	-19.2		51	0.6			
16.39	100	-39.2	0.00						5.0	555	-24.6	0.56	49	0.4			
17.0	91	-39.2	0.00						5.35	500	-26.9		48	0.3			311
18.0	76	-39.2	0.00					318	6.0	455	-31.1	0.65	47				
18.32	73	-39.2	0.00						6.83	400	-38.2		45				
									7.0	396	-38.5	0.74	45				
									8.0	342	-45.4	0.69	45				
									8.76	305	-49.9	0.59	45				
									8.87	300	-49.9	0.00	45				309
0.0	011	-3.2		93	2.7	339	5		8.94	297	-49.7	-0.33	45				
0.09	000	-3.7		92	2.7	351	11		9.0	294	-49.7	-0.43	45				
0.2	894	-4.0	0.40	91	2.5				10.0	254	-45.4	-0.26	45				
0.5	948	-5.2	0.40	89	2.3				11.0	219	-42.8	-0.26	45				
0.92	900	-6.8	0.66	86	2.1				11.62	200	-41.5		45				382
1.0	889	-7.3	0.42	86	2.0				12.0	189	-41.0	-0.18	45				
1.37	850	-8.4		86	1.9				13.0	162	-40.5	-0.05	45				
1.5	838	-8.7	0.28	86	1.9				14.0	140	-40.1	-0.04	45				

2.6 0127 φ = 77°13' λ = 189°21'

10/10 St (18)

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
15.0	121	-39.6	-0.05					270	2.91	700	-13.1		65	1.2			
16.0	104	-39.1	-0.05						3.0	693	-13.3	0.26	64	1.1			
16.31	100	-38.8						288	4.0	606	-19.4	0.61	58	0.6			
17.0	91	-38.4	-0.07						4.07	600	-19.6		57	0.6			218
18.0	79	-37.8	-0.06					284	5.0	539	-23.6	0.42	52	0.5			
18.96	70	-37.8	-0.00						5.41	500	-30.0		50	0.3			205
									6.0	460	-37.2	0.73	47				
									6.99	400	-43.7	0.64	45				
									8.0	345	-48.2	0.73	43				
									8.62	316	-48.2		43				
									8.97	300	-48.2	0.00	43				219
0.0	017	-4.2		86	2.3	338	3		9.0	298	-48.2	0.00	42				
0.13	000	-4.9		86	2.2	348	3		9.32	285	-48.2	0.00	41				
0.2	990	-5.6	0.70	86	2.1	351	3		10.0	258	-45.6	-0.38	41				210
0.3	978	-6.3	0.70	85	2.0	334	5		11.0	223	-42.4	-0.32	41				
0.5	954	-5.7	-0.30	83	2.1	339	6		11.74	200	-40.5		40				
0.8	919	-4.9	-0.27	82	2.2	310	5		12.0	193	-40.4	-0.20	40				301
0.96	900	-5.5		82	2.2	304	4		13.0	166	-38.8	-0.06	39				
1.0	895	-5.7	0.40	82	2.2	302	4		14.0	144	-38.1	-0.07	38				320
1.39	850	-7.6	0.44	75	1.7	266	2		15.0	122	-38.4	-0.07	38				
1.5	840	-7.9		70	1.5				16.0	106	-37.7	-0.07	38				
1.87	800	-8.9		69	1.5				16.35	100	-37.4		38				
2.0	787	-9.4	0.30	69	1.5				17.0	92	-36.9	-0.08	37				
2.5	758	-12.0		67	1.2			258									

2.6 1342 φ = 77°12' λ = 189°22'

10/10 St (43)

Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W	
18.0	79	-31.9	-0.10	37			248	1.88	800	-8.8	76	1.7	342	6		
19.0	68	-35.2	-0.07	36				2.0	787	-9.2	75	1.7	338	6		
20.0	60	-34.6	-0.06	36				2.5	728	-12.5	63	1.1	335	6		
21.0	32	-31.8	-0.08	35			316	2.9	700	-15.3	61	0.9	332	6		
21.38	50	-33.7		35				3.0	689	-16.4	61	0.8	335	6	320	
22.0	46	-33.1	-0.07	35				3.35	638	-19.8	59	0.6	335	5		
23.0	40	-31.9	-0.12	34				3.76	624	-19.8	0.00	57	0.6	332	5	
24.0	34	-31.6	-0.03					4.0	604	-20.9	0.46	53	0.5	338	5	
25.0	30	-31.6	0.00					4.04	600	-31.0	52	0.5	339	5		
26.0	26	-31.6	0.00				302	5.37	500	-38.5	42	0.3	030	5		
								6.0	457	-32.9	0.65	41	0.3	030	5	298
								6.92	400	-38.6	40	0.41	031	6		
								7.0	395	-39.0	0.61	40	0.32	031	6	
								8.0	342	-45.6	0.66	39	0.41	5		
								8.24	331	-46.9	0.54	38	0.31	5		
								8.88	300	-46.9	0.00	38	0.03	4		
								9.0	305	-46.9	0.00	38	0.03	5	312	
								9.92	305	-46.9	0.00	37	0.35	8		
								10.0	353	-46.6	0.00	37	0.35	8		
								11.0	318	-45.1	-0.17	36	0.37	8		
								11.28	200	-44.6	0.00	36	0.33	8		
								12.0	187	-44.4	-0.07	35	0.16	7	342	

311

3.6 0132 $\varphi=77^{\circ}12'$ $\lambda=189^{\circ}22'$
 $8/3 \text{ Ac, S, M, H}$

H	B	t	U	q	d	V	W
0.0	018	-7.1	91	1.9			0
0.14	000	-7.1	91	1.9	333	3	
0.2	991	-7.0	-0.05	91	2.0	341	4
0.5	955	-6.9	-0.03	91	2.0	341	4
0.97	900	-7.4	85	2.0	338	4	
1.0	895	-7.5	0.12	85	2.0	330	3
1.41	850	-7.9	81	1.9	343	4	
1.5	841	-8.0	0.10	80	1.8	344	4
1.8	809	-8.4	0.13	77	1.8	345	6

312

Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
13.0	161	-43.8	-0.06	35			322	1.86	800	-10.3	85	1.7	288	4	
14.0	139	-43.8	0.00	34			322	2.0	783	-11.0	0.30	85	1.6	295	4
15.0	100	-43.8	0.00	33				2.5	735	-13.7	0.54	85	1.4	309	5
16.0	104	-43.4	-0.04					2.86	700	-14.6	0.51	85	1.3	341	5
16.26	100	-43.2					363	3.0	687	-15.2	0.20	85	1.3	341	5
17.0	90	-42.5	-0.09					4.0	650	-20.3	0.51	80	0.8	342	7
18.0	78	-41.9	-0.06					5.0	595	-26.2	0.59	75	0.5	345	6
19.0	67	-41.4	-0.05					5.36	500	-28.2	0.53	71	0.4	344	6
20.0	58	-40.8	-0.06					6.0	456	-31.5	0.55	67	0.4	346	7
21.0	50	-40.1	-0.07					6.93	400	-37.9	0.55	67	0.39	8	288
22.0	43	-38.6	-0.06				427	7.0	386	-37.0	0.55	67	0.33	7	
								8.0	342	-42.3	0.55	67	0.31	6	
								8.87	300	-46.9	0.64	67	0.32	7	
								8.92	288	-46.4	0.64	67	0.32	7	
								9.0	284	-46.4	0.64	67	0.32	7	
								9.16	267	-46.4	0.00	67	0.314	7	312
								10.0	253	-44.9	-0.42	67	0.312	6	
								11.0	219	-42.3	-0.25	67	0.312	6	
								11.6	200	-41.4	-0.11	67	0.307	6	
								12.0	188	-41.1	-0.12	67	0.304	6	
								13.0	163	-40.5	-0.06	67	0.305	5	313
								14.0	140	-39.7	-0.08	67	0.313	5	
								15.0	121	-39.2	-0.05	67	0.314	4	

3.6 1332 $\varphi=77^{\circ}12'$ $\lambda=189^{\circ}22'$
 $1/0 \text{ Cc}$

H	B	t	U	q	d	V	W
0.0	016	-3.6	73	2.0	338	1	
0.13	000	-4.5	70	1.9	338	2	
0.2	990	-5.0	74	1.9	324	2	
0.5	925	-6.0	0.63	74	1.6	331	2
0.84	900	-8.2	0.63	77	1.7	327	3
1.0	892	-8.4	0.30	78	1.6	332	3
1.39	850	-9.1	0.22	82	1.7	331	4
1.5	838	-9.5	0.22	83	1.7	329	3

Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
16.0	104	-38.6	-0.06	67					2.3	753	-13.8	0.60	79	1.2	307	4	
16.3	100	-38.4		67					2.5	734	-13.8	0.00	79	1.3	312	3	
17.0	90	-37.6	-0.10	67				369	2.6	725	-13.8	0.00	79	1.3	314	4	
18.0	78	-36.5	-0.11	67					2.86	700	-14.7		76	1.2	326	5	317
19.0	68	-35.8	-0.07	67					3.0	687	-15.2	0.35	74	1.1	333	5	
20.0	59	-34.7	-0.11						4.0	600	-20.4	0.52	57	0.6	352	7	
21.0	52	-33.9	-0.08						5.0	524	-25.9	0.55			353	7	
21.2	50	-33.7							5.24	500	-27.7						342
21.4	49	-33.6	-0.07					304	6.0	458	-32.6	0.57					
									6.9	400	-38.4						
									7.0	394	-39.0	0.64					
									8.0	340	-46.7	0.77					
									8.7	306	-51.8	0.73					

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4.6 0128 φ = 77°13' λ = 189°22'
10°0 Ac (2652)

H	B	t	γ	U	q	d	V	W
0.0	013	-4.9		95	2.4		0	
0.11	000	-5.2		94	2.3		1	
0.2	989	-5.6	0.35	92	2.2	223	1	
0.5	952	-6.7	0.37	86	2.0	304	2	
0.83	900	-7.5		70	1.8	304	2	
1.0	892	-7.6	0.18	70	1.8	299	3	
1.27	856	-8.8		70	1.7	293	5	
1.3	836	-9.4	0.36	70	1.6	292	5	
1.34	800	-11.1		70	1.5	298	7	
2.0	783	-12.0	0.52	70	1.3	295	6	

4.6 1327 φ = 77°14' λ = 189°22'
10°0 Ac (174)

H	B	t	γ	U	q	d	V	W
0.0	013	-2.6		94	2.9	225	3	
0.11	000	-3.4		94	2.7	226	4	
0.2	957	-3.9	0.65	93	2.6	226	4	
0.5	949	-5.3	0.47	93	2.3	240	4	
0.92	900	-6.4		92	2.3	282	5	
1.0	891	-6.7	0.28	92	2.3	284	5	

Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
1.30	850	-8.2		92	2.1	286	6		15.0	122	-20.5	-0.06					
1.5	838	-8.6	0.38	92	2.0				16.0	105	-26.7	-0.08					
1.86	800	-9.9		91	1.8				16.3	100	-26.3	-0.09					354
2.0	784	-10.4	0.35	91	1.8				17.0	92	-27.5	-0.11					
2.3	755	-12.2	0.36	91	1.6				18.0	80	-26.7	-0.11					
2.87	700	-13.5		91	1.5				19.0	70	-25.8	-0.09					366
3.0	687	-14.0	0.35	91	1.5				20.0	60	-24.8	-0.10					
4.02	600	-19.5	0.54	80	0.9			317	21.0	51	-33.6	-0.12					
5.0	535	-25.7	0.62	76	0.5				21.1	50	-33.5	-0.10					
5.36	500	-28.3		75	0.4				22.0	43	-32.6	-0.10					
6.0	438	-31.5	0.58	73				323	23.0	35	-31.6	-0.10					
6.99	400	-38.5	0.71	69					23.3	33	-31.3	-0.10					374
8.0	343	-47.3	0.88	69													
8.36	325	-50.2	0.75														
8.71	309	-50.2	0.00														
8.9	300	-48.8															
9.0	295	-48.4	-0.62														
10.0	253	-45.0	-0.34					352	0.0	009	0.00	-6.4	89	2.0	225	3	
11.0	218	-41.6	-0.34						0.2	984	-6.4	0.00	86	2.0	255	9	
11.6	200	-41.3							0.5	947	-6.4	0.00	81	1.9	261	11	
12.0	188	-41.1	-0.05						0.9	900	-6.4	0.00	76	1.9	255	15	
13.0	162	-40.6	-0.05					372	0.95	885	-6.4	0.00	75	1.9	255	15	
14.0	141	-40.1	-0.05														

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5.6 0927 φ = 77°12' λ = 189°27'
10°0 Ac (258)

H	B	t	γ	U	q	d	V	W
0.0	009	-6.4		89	2.0	225	3	
0.08	000	-6.4		88	1.9	248	8	
0.2	984	-6.4	0.00	86	2.0	255	9	
0.5	947	-6.4	0.00	81	1.9	261	11	
0.9	900	-6.4	0.00	76	1.9	255	15	
0.95	885	-6.4	0.00	75	1.9	255	15	

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.0	889	-6.6	74	1.8	254	14			14.0	140	-41.3	-0.02					278
1.35	890	-7.4		1.7	253	12			15.0	121	-40.8	-0.05					
1.5	833	-7.8	0.35	70	1.6	253	12		16.0	104	-40.4	-0.01					
1.81	800	-9.4		67	1.4	253	14		16.28	100	-40.2						274
2.0	780	-10.2	0.48	66	1.4	256	13		17.0	90	-39.4	-0.10					
2.5	732	-11.8	0.32	62	1.2				17.48	84	-38.5	-0.19					
2.84	700	-13.2		61	1.1			300									
3.0	685	-13.9	0.42	61	1.0												
4.01	600	-19.0	0.50	57	0.7												
5.0	524	-24.6	0.57	53	0.4												
5.33	500	-26.0		51	0.4												
6.0	455	-28.1	0.35	49	0.3			306	0.0	982	-0.2						
6.96	400	-33.9		40					0.2	958	-1.7	0.75					
7.0	398	-34.3	0.62	49					0.5	921	-3.1	0.47					
8.0	344	-42.0	0.77	49					0.68	900	-3.8						
8.92	300	-47.3	0.88	49					1.0	865	-5.4	0.46					
9.0	295	-47.3		49				298	1.14	850	-6.2						
9.64	269	-47.3	0.00	49					1.3	832	-7.4	0.67					
10.0	255	-45.6	-0.47	49					1.3	812	-7.8	0.20					
11.0	219	-44.0	-0.16	49					1.62	800	-8.0	0.14					
11.02	200	-41.8		49					2.0	761	-8.5						
12.0	189	-41.5	-0.25	49				278	2.38	734	-9.0	0.13					
13.0	182	-41.5	0.00						2.5	713	-9.5	0.42					
									2.64	700	-10.2						

315

6.6 0137 φ=77°08' λ=189°56'
10,10 St. (41), №°

100 292 7
319 11

316

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	668	-12.0	0.50					290	1.5	828	-9.0	0.36					
3.82	600	-15.9	0.49						1.77	800	-9.6						
4.0	585	-16.9							2.0	776	-9.8						
5.0	513	-24.0	0.71						2.5	728	-10.2	0.16					
5.18	500	-25.5						322	2.8	710	-10.7	0.08					291
6.0	445	-31.7	0.77						3.0	682	-11.3	0.22					
6.77	400	-37.9	0.81						3.98	600	-16.0	0.48					
7.0	387	-39.8							5.0	524	-21.4	0.53					
8.0	335	-39.8	0.00						5.33	500	-23.4						
8.75	300	-35.6						322	6.0	457	-27.5	0.61					321
9.0	289	-38.2	-0.16						6.94	400	-35.9	0.89					
10.0	249	-38.2	0.00						7.0	396	-36.4						
									8.0	343	-43.5	0.71					
									8.6	314	-47.4	0.65					
									8.91	300	-47.4						
									9.0	295	-47.4	0.00					
									9.15	289	-47.4	0.00					
0.0	064	-1.4					180	6	10.0	254	-42.8	-0.54					
0.02	000	-1.5							11.0	219	-40.3	-0.25					
0.2	977	-2.8	0.70						11.62	200	-39.2						
0.5	941	-5.2	0.80						12.0	190	-38.6	-0.17					
0.85	900	-6.7							13.0	164	-38.0	-0.06					
1.0	883	-7.2	0.40						14.0	142	-37.5	-0.05					
1.3	870	-8.5															

8.6 1333 φ=77°02' λ=190°40'

10,10 St. (19)

Пробок. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.0	122	-37.0	-0.05						2.5	724	-9.0	0.46	100	2.4			
16.0	105	-36.6	-0.04						2.75	707	-10.2	0.50	99	2.1			285
16.37	100	-35.4							3.0	677	-11.5	0.52	98	1.5			
17.0	92	-35.0	-0.05					283	3.93	600	-16.3	0.52	97	1.5			
18.0	79	-35.6	-0.04						4.0	594	-16.7	0.55	95	1.0			
19.0	68	-35.2	-0.04						5.0	520	-22.2	0.78	95	0.9			328
20.0	68	-34.4	-0.08						5.28	500	-24.2	0.78					
21.0	52	-33.6	-0.08					290	6.0	453	-30.0	0.77					
21.2	50	-33.5	-0.05						6.87	400	-36.5	0.77					
									7.0	392	-37.7	0.95					
									7.64	357	-43.8	0.95					
									8.0	340	-43.8	0.90					
									8.81	300	-43.8	0.90					349
0.0	996	-2.1		98	3.1		0		9.0	291	-43.8	0.90					
0.2	970	-3.0	0.45	98	3.0	183	3		9.1	286	-43.8	0.90					
0.5	954	-4.5	0.50	99	2.8	165	2		10.0	251	-41.2	-0.29					
0.65	916	-5.3	0.53	100	2.7	189	3		11.0	217	-39.4	-0.16					
0.79	900	-5.4		100	2.7	212	2		11.54	200	-39.0						336
1.0	877	-5.7	0.11	100	2.7	219	3		12.0	187	-38.9	-0.05					
1.24	850	-6.0	0.12	100	2.7	204	2		13.0	163	-38.7	-0.02					
1.5	823	-6.3	0.12	100	2.7	212	4		14.0	142	-38.5	-0.02					
1.71	800	-6.5	0.08	100	2.6				15.0	124	-38.3	-0.02					
2.0	771	-6.7	0.08	100	2.9				16.0	106	-38.1	-0.02					

9.6 0122 $\varphi = 77^{\circ}01'$ $\lambda = 190^{\circ}45'$
 10/0 As (146), χ°

Пробок. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
16.4	100	-38.0						340	1.75	800	-10.0	0.10	58	1.2	315	15	
17.0	92	-37.9	-0.02						2.0	774	-10.3	0.36	53	1.1	309	17	
18.0	79	-37.7	-0.03						2.5	735	-12.1	0.36	40	0.8	297	18	
19.0	68	-37.4	-0.04					332	2.77	700	-13.0	0.46	37	0.7	291	18	
20.0	60	-37.0	-0.04						3.0	679	-14.4	0.46	35	0.6	293	18	330
21.0	51	-36.5	-0.05						3.93	600	-19.1	0.49	34	0.4			
21.1	50	-36.5	-0.04						4.0	594	-19.3	0.63	34	0.4			
22.0	44	-36.1	0.00						5.0	518	-25.6	0.63	31	0.2			
23.0	38	-36.1	0.00						5.26	500	-27.3	0.54	30	0.2			
24.0	33	-36.1	0.00						6.0	450	-31.0	0.54	28				267
24.2	32	-36.1	0.00						6.82	400	-36.2	0.38					
									7.0	390	-36.8	0.38					
									7.14	382	-37.6	0.57					
									8.0	338	-37.6	0.00					340
									8.84	300	-35.9						
0.0	001	-4.0		81	2.2	282	9		9.0	293	-35.6	-0.20					218
0.2	975	-4.6	0.30	79	2.1	311	12		10.0	264	-33.9	-0.17					
0.5	938	-6.5	0.67	77	1.8	307	15		11.0	221	-33.3	-0.05					
0.8	903	-8.5	0.75	75	1.5	305	13		11.52	203	-33.3	0.00					
0.83	900	-8.7	0.64	75	1.5	293	13		11.7	200	-33.4						
1.0	880	-9.2	0.29	74	1.3	291	14		12.0	191	-33.7	0.08					229
1.28	850	-9.6	0.69	69	1.4	317	14		13.0	166	-34.6	0.09					
1.5	827	-9.8	0.12	64	1.3	316	15		14.0	144	-34.8	0.02					

9.6 1415 $\varphi = 77^{\circ}01'$ $\lambda = 190^{\circ}45'$
 0/0 Sc, χ°

Прилож. приложение

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
15.0	125	-34.8	0.00				231	3.97	600	-18.1	53	0.7			317
16.0	110	-34.8	0.00					4.0	597	-18.2	0.45	53	0.7		
16.79	100	-34.8	0.00					5.0	523	-23.5	0.53	51	0.5		
17.0	98	-34.8	0.00				220	5.33	500	-35.4	0.59	50	0.4		
18.0	85	-34.8	0.00					6.0	455	-29.4	0.59	50	0.3		
								9.91	400	-34.1	0.50	50			390
								7.0	365	-34.4	0.50	50			
								7.91	345	-39.6	0.57	49			
								8.0	341	-39.6	0.57	49			
								8.89	320	-39.6	0.00	48			
								9.0	295	-39.6	0.00	48			
								9.18	297	-39.6	0.00	48			
								10.0	235	-38.2	-0.17	47			298
								11.0	221	-36.8	-0.14	46			
								11.3	212	-36.4	-0.13	45			
								11.7	200	-35.4	0.00	44			
								12.0	191	-35.4	0.00	44			285
								13.0	165	-36.4	0.00	43			
								14.0	143	-36.4	0.00	43			
								15.0	124	-36.4	0.00	43			305
								16.0	108	-36.4	0.00	43			
								16.6	100	-36.4	0.00	43			
								17.0	91	-36.4	0.00	43			

10.6 0133 $\varphi = 76^{\circ}59'$ $\lambda = 190^{\circ}51'$
10/10 St (88), +

1 319 1

Прилож. приложение

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
18.0	81	-36.4	0.00	43			332	2.0	780	-3.3	00	3.3			215
19.0	70	-36.4	0.00	43				2.5	733	-5.4	0.41	30	3.0		
20.0	62	-36.4	0.00					3.0	687	-7.1	0.54	30	2.7		
21.0	53	-36.4	0.00					4.0	604	-14.4	0.63	29	1.4		
21.34	50	-36.4	0.00					4.05	600	-14.8	0.95	28	1.3		
22.0	45	-36.4	0.00				350	4.8	543	-22.0	0.00	27	0.5		237
22.2	43	-36.4	0.00					5.0	528	-22.0	0.00	27	0.3		
								5.24	511	-22.0	0.00	27	0.3		
								5.4	500	-22.9	0.00	26	0.7		284
								6.0	460	-26.6	0.61	63	0.4		
								7.0	400	-33.8	0.72	56			284
								8.0	346	-41.0	0.72	52			
								8.93	300	-47.2	0.65	51			
								9.0	298	-47.6	0.67	51			
								9.18	290	-48.8	0.00	50			179
								9.6	272	-48.8	0.00	50			
								10.0	265	-46.2	-0.65	50			
								11.0	221	-42.3	-0.39	48			
								11.65	200	-41.4		48			177
								13.0	190	-41.2	-0.11	47			179
								13.0	164	-40.5	-0.67	46			
								14.0	142	-39.9	-0.6	45			

11.6 0130 $\varphi = 77^{\circ}00'$ $\lambda = 199^{\circ}57'$
10/10 St (30)

1 320 1

Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
15.0	123	-39.1	-0.06	45			177	5.45	500	-20.5	54	0.6			
16.0	106	-38.9	-0.02					6.0	463	-23.1	51	0.6			310
11.6 1334 $\varphi = 77^{\circ}01'$, $\lambda = 190^{\circ}58'$															
10/10 St (16)															
0.0	006	-0.5		55	3.3	133	6	9.06	300	-43.6	46				310
0.05	000	-0.7		55	3.5	134	6	9.85	295	-48.4	45				310
0.2	979	-1.2	0.35	94	3.4			10.0	290	-47.5	-0.60	45			310
0.5	943	-2.4	0.40	93	3.1			11.0	224	-44.5	-0.30	44			310
0.78	912	-2.4	0.00	92	3.1			11.8	200	-41.6	-0.32	43			310
0.89	900	-1.4		91	3.4			12.0	194	-41.3	-0.32	42			310
1.0	887	-0.8	-0.73	91	4.2			12.0	167	-39.8	-0.15	42			310
1.33	850	0.6	-0.42	90	4.3			14.0	144	-38.8	-0.10				310
1.5	834	0.0	0.35	88	4.1			15.0	124	-38.0	-0.08				310
1.83	800	-1.0	0.35	88	3.9			16.0	108	-37.4	-0.06				310
2.0	782	-1.8	0.36	87	3.7			16.5	100	-37.0	-0.06				310
2.5	735	-3.5	0.34	80	3.1			17.0	54	-36.5	-0.09				310
2.87	700	-5.0	0.34	75	2.7			18.0	80	-35.9	-0.06				310
3.0	688	-5.8	0.46	71	2.4			19.0	70	-34.6	-0.13				310
4.0	606	-12.7	0.69	61	1.3			20.0	60	-33.5	-0.11				310
4.07	600	-13.1		61	1.3			21.0	52	-32.4	-0.11				310
5.0	530	-18.0	0.53	56	0.8			21.32	50	-32.2					310

Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
22.0	45	-32.1	-0.13				295	4.09	600	-11.2	69	1.7			
22.95	42	-29.9	-0.22					5.0	534	-16.2	64	0.9			
11.6 1334 $\varphi = 77^{\circ}03'$, $\lambda = 190^{\circ}58'$															
10/10 St (53)															
0.0	008	0.0		98	3.7	158	4	7.13	400	-31.7	67	0.9			402
0.06	000	-0.2		97	3.6	175	7	8.0	353	-37.7	67	0.9			402
0.2	882	-0.3	0.15	97	3.7	183	6	9.0	305	-45.3	65				402
0.5	846	-0.3	0.00	96	3.7	183	6	9.1	300	-46.1	65				402
0.85	807	-0.3	0.00	94	3.8			10.0	268	-53.2	64				402
0.91	800	0.2		94	3.9			10.4	242	-53.2	63				402
1.0	890	0.8		93	4.3			11.0	235	-51.3	62				402
1.06	883	1.2	-0.71	93	4.4			11.74	190	-47.6	60				402
1.37	850	1.2	0.00	91	4.4			12.0	162	-46.4	59				402
1.44	842	1.2	0.00	91	4.5			14.0	143	-44.0	58				402
1.5	837	1.0		89	4.1			15.0	122	-43.2	57				402
1.85	800	-0.3		89	4.0			16.4	100	-41.6	56				402
2.0	785	-0.9	0.37	89	4.0			17.0	91	-41.3	55				402
2.5	737	-2.7	0.36	83	3.5			18.0	78	-40.7	54				402
2.89	700	-4.4		79	3.0			18.0	68	-40.2	53				402
3.07	691	-4.5	0.12	77	2.8			19.0	54	-39.5	52				402
4.0	607	-10.8	0.60	70	1.8			21.32	50	-39.2	50				402

Продолж. приложения.

H	B	t	t	Y	U	q	d	V	W	H	B	t	t	Y	U	q	d	V	W	
20.0	58	-36.2	-0.10						346	2.5	737	-2.6	71	0.60	71	3.0				287
21.0	50	-37.9	-0.13							2.91	709	-6.1	70	0.82	69	2.2				
22.0	43	-36.7	-0.12							3.0	691	-6.7	69	0.82	69	2.2				
23.0	37	-35.7	0.00						329	4.0	690	-11.4	65	0.47	65	1.5				
23.51	34	-35.7	0.00							4.11	690	-12.1	65	0.55	63	1.0				273
12.6 1344 $\varphi = 77^{\circ}04'$ $\lambda = 190^{\circ}58'$																				
10/10 Ш. =																				
0.0	007	-0.1			98	3.7	180	4		7.0	405	-30.7	0.71	57	0.6					295
0.05	000	-0.4			99	3.7				7.1	400	-31.1	0.71	57	0.6					
0.16	986	-1.2	0.69		99	3.6				8.0	351	-36.4	0.57	48						
0.2	981	-1.2	0.00		99	3.6				9.0	300	-44.6	0.82	47						
0.45	951	-1.2	0.00		100	3.7				9.07	290	-45.0	0.82	47						
0.5	945	0.3	0.00		100	4.2				9.36	292	-51.8	0.75	47						
0.67	925	2.0	-1.45		100	4.7				10.0	290	-51.8	0.00							270
0.9	900	2.0	0.00		90	4.4				10.28	290	-47.3	-0.59							
1.0	889	2.0	0.00		85	4.2				11.0	224	-47.3	-0.59							
1.37	850	2.0	0.09		76	3.9				11.75	200	-47.3	-0.59							
1.46	840	2.0	0.09		74	3.8				12.0	193	-47.3	-0.59							
1.5	836	1.9	0.09		73	3.8				13.0	166	-47.3	-0.59							
1.85	800	0.8	0.30		72	3.7				14.0	143	-47.3	-0.59							
2.0	784	0.4	0.30		72	3.7				15.0	123	-47.3	-0.59							
					72	3.7				16.0	108	-47.3	-0.59							

Продолж. приложения.

H	B	t	t	Y	U	q	d	V	W	H	B	t	t	Y	U	q	d	V	W
16.55	100	-37.7	-0.08							1.35	850	1.0	84	0.00	84	4.0			
17.0	93	-37.4	-0.08							1.5	834	1.0	81	0.00	81	4.0			
18.0	81	-36.6	-0.08						272	1.68	815	1.0	79	0.00	79	3.9			
19.0	69	-35.9	-0.07							2.0	783	0.5	76	0.31	73	3.6			
20.0	60	-35.2	-0.07							2.5	783	0.0	73	0.0	73	3.6			
21.0	52	-34.2	-0.10							2.89	700	-4.7	65	2.2	65	2.9			
21.2	50	-34.0	-0.10							3.0	689	-5.4	60	2.2	60	2.2			
22.0	44	-33.2	-0.10						278	4.0	607	-10.7	53	44	1.1				
23.0	38	-32.2	-0.10							4.08	600	-11.0	53	44	1.1				
23.25	35	-31.8	-0.15							5.0	532	-17.3	66	37	0.6				
24.0	31	-31.8	0.00						278	5.46	500	-21.0	36	0.4					
24.5	27	-31.8	0.00							6.0	464	-24.3	36	0.4					
13.6 0124 $\varphi = 77^{\circ}05'$ $\lambda = 190^{\circ}52'$																			
10/10 Ш(6)																			
0.0	005	0.2			99	3.8	180	3		7.06	400	-31.6	0.79	35					
0.04	000	0.1			99	3.8				8.0	351	-39.0	0.64	34					
0.2	980	-0.4	0.30		97	3.6				9.04	300	-47.0	0.75	34					
0.37	890	-0.4	0.00		96	3.6				9.35	278	-50.0	0.60	34					
0.5	945	1.0	-1.08		94	4.0				10.0	258	-50.0	0.00	34					
0.89	900	1.0	0.00		90	4.1				11.0	222	-44.6	-0.54	33					
1.0	888	1.0	0.00		88	4.0				11.73	200	-41.8	-0.34	32					
					88	4.0				12.0	192	-41.2	-0.34	32					

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
13.0	166	-0.6	-0.06	32				250	0.8	912	3.3	0.00			217	8	
14.0	144	-0.2	-0.04	31					0.91	900	2.9	0.40			227	6	
15.0	120	-0.8	-0.04	30				288	1.0	899	2.5	0.40					
16.0	100	-0.3	-0.05	30					1.37	890	0.1						
17.0	83	-0.7	-0.06	30				306	1.5	885	-1.4	0.78					
18.0	69	-0.8	-0.04	30					1.85	890	-1.9	0.16					268
19.0	60	-0.7	-0.04	30					2.0	785	-2.2	0.14					
20.0	60	-0.7	-0.07	30					2.5	737	-2.9	0.14					
21.0	51	-0.6	-0.05	30				337	2.63	725	-3.1	0.15					
21.1	50	-0.6	-0.06	30					2.9	700	-4.3	0.63					
22.0	42	-0.5	-0.06						3.0	691	-5.4	0.80					
23.0	36	-0.5	-0.06					838	4.1	600	-13.4	0.80					
24.0	30	-0.5	-0.01						5.0	533	-17.5	0.42					268
24.4	25	-0.5	0.00						5.46	500	-20.9	0.74					
									7.0	405	-32.2	0.72					268
									7.08	400	-32.6	0.68					268
									8.0	350	-39.0	0.74					
									9.0	302	-46.4	0.74					
									9.04	300	-46.6						
									9.42	283	-49.4	0.71					
									(9.52)	263	-46.4	0.00					

13.6 1329 $\varphi = 77^{\circ}08'$ $\lambda = 191^{\circ}32'$

10/10 Sc (116)

H	B	t	T	U	q	d	V	W
0.0	007	1.2						225
0.05	000	0.8						4
0.2	381	0.1	0.55					221
0.5	946	3.3	-1.07					219

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
10.0	280	-0.1	-0.22					283	1.15	874		0.00					
11.0	224	-0.6	-0.35						1.37	850							
11.76	200	-0.6	-0.26						1.5	837							
12.0	193	-0.3	-0.26					281	1.86	800							
13.0	166	-0.2	-0.18						2.0	785							
14.0	143	-0.5	-0.06						2.5	738							
15.0	124	-0.1	-0.05					284	2.92	700							
16.0	107	-0.4	-0.07						3.0	692							
16.48	100	-0.2	-0.25						4.0	609							
17.0	93	-0.2	0.00					285	4.1	600							
18.0	82	-0.2	0.00						5.0	534							
18.44	78	-0.2	0.00						5.46	500							
									6.0	466							
									7.0	406							
									7.12	400							
									8.0	332							
									9.0	304							
									9.11	300							
									10.0	262							
									10.3	251							
									10.72	235							
									11.0	226							
									11.8	200							

14.6 0134 $\varphi = 77^{\circ}08'$ $\lambda = 191^{\circ}27'$

10/10 Sc (15)

H	B	t	T	U	q	d	V	W
0.0	008	0.6						225
0.07	000	0.7						5
0.2	983	(1.1)	-0.25					227
0.5	948	(2.0)						13
0.55	942	2.2	-0.31					
0.91	900	2.2	0.00					
1.0	890	2.2	0.00					

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
12.0	194	-44.3	-0.54					289	0.2	985	1.5	-0.30					
13.0	166	-41.6	-0.27						0.36	966	3.1	-1.00					
14.0	143	-41.1	-0.05					277	0.5	949	3.1	0.00					
15.0	123	-40.5	-0.06						0.85	908	3.1	0.00					
16.0	106	-40.0	-0.05						0.92	900	2.6						
16.4	100	-39.8							1.0	891	2.0	0.73					
17.0	92	-39.5	-0.05					283	1.39	850	1.0	0.24					
18.0	80	-39.0	-0.05						1.5	839	0.8						
19.0	70	-38.4	-0.06						1.88	800	0.0	0.20					
20.0	60	-37.6	-0.08					302	2.0	788	-0.2	0.32					
21.0	52	-36.8	-0.08						2.5	740	-1.8	0.32					
21.26	50	-36.5							2.94	700	-3.3	0.40					341
22.0	45	-35.9	-0.9						3.0	694	-3.8	0.40					
23.0	39	-35.5	-0.4						4.0	611	-10.5	0.57					
24.0	34	-35.1	-0.4					312	4.14	600	-11.3	0.58					
25.0	29	-34.7	-0.4						5.0	535	-16.3	0.58					
25.64	28	-34.5	-0.3						5.5	500	-19.8	0.83					538
									6.0	467	-24.6	0.43					
									7.0	408	-28.9	0.43					
									7.14	400	-30.5	0.84					
									8.0	354	-37.3	0.84					
									9.0	305	-46.0	0.87					
									9.13	300	-46.6						251

14.6 1336 $\psi = 77^{\circ}10'$ $\lambda = 191^{\circ}40'$
10/10 Ns, °

0.0	011	0.9						87									
0.09	000	1.3															6

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
9.2	266	-47.2	0.60						1.88	800	-1.5	0.22					
9.9	267	-47.2	0.00						2.0	787	-1.7	0.30					235
10.0	263	-46.4	-0.80					184	2.5	739	-3.2	0.50					
11.0	227	-40.4	-0.60						2.93	700	-5.5	0.47					
11.81	200	-38.3							3.0	693	-5.7	0.50					232
12.0	195	-38.1	-0.23					202	4.0	610	-10.4	0.47					
13.0	169	-37.0	-0.11						4.13	600	-11.0	0.60					
14.0	146	-37.0	0.00						5.0	535	-16.4	0.60					
15.0	126	-37.0	0.00					214	5.52	500	-19.7	0.66					
15.6	116	-37.0	0.00					155	7.0	408	-28.2	0.82					232

15.6 0257 $\psi = 77^{\circ}12'$ $\lambda = 191^{\circ}48'$
10/10 Ns (10), °

0.0	013	0.2						96									
0.1	000	0.2															5

0.2	987	0.2	0.60						7.14	400	-29.1	0.61					
0.5	950	0.1	0.03						8.0	353	-34.3	0.69					
0.94	900	0.0							9.0	306	-41.2	0.78					363
1.0	892	0.0	0.02						9.15	300	-42.4	0.80					
1.2	871	-0.1	0.05						10.0	264	-49.0	0.47					
1.4	850	-0.5	0.17						10.6	239	-51.8	0.00					
1.5	839	-0.6							11.9	205	-51.8	0.00					
									11.78	200	-47.5						
									12.0	188	-46.5	-0.53					
									13.0	166	-43.5	-0.30					
									14.0	144	-42.1	-0.14					
									15.0	123	-40.9	-0.12					365

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
16.0	105	-40.4	-0.05						1.4	850	-0.6		85	3.7			
16.37	100	-40.2							1.5	839	-1.1	0.48	80	3.4			
17.0	92	-39.8	-0.06						1.87	800	-2.9		75	2.8			
18.0	80	-39.0	-0.08					330	2.0	787	-4.0	0.38	75	2.6			
19.0	69	-38.0	-0.10						2.1	777	-4.6	0.00	74	2.5			
20.0	60	-37.5	-0.05						2.5	739	-4.6	0.00	74	2.6			
21.0	51	-37.0	-0.05						2.65	725	-4.6	0.00	74	2.7			285
21.22	50	-36.9							2.92	700	-5.5		73	2.6			
22.0	44	-36.5	-0.05						3.0	692	-6.0	0.40	73	2.5			
23.0	38	-36.0	-0.05						4.0	609	-10.8	0.48	72	1.8			
24.0	32	-35.4	-0.06						4.11	600	-11.4		72	1.7			
24.7	28	-35.0	-0.06					388	5.0	534	-16.8	0.60	71	1.1			275
									5.47	500	-20.6		70	0.8			
									6.0	466	-24.0	0.72	69	0.6			
									7.0	405	-29.7	0.57	68	0.4			
									7.03	400	-30.3		68				
									8.0	351	-35.5	0.68	67				279
0.0	0.13	0.8		97	4.0	225	4		9.0	304	-41.0	0.75					
0.1	1.00	0.8		98	4.0	223	10		9.09	300	-44.5						
0.2	887	0.8		99	4.1	230	12		10.0	261	-49.6	0.70					
0.5	951	0.8		99	4.3				10.1	257	-48.2	-1.40					285
0.95	900	0.8		99	4.6												
1.0	864	0.8		99	4.6												
1.1	883	0.8		99	4.7												

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15.6 1925 φ = 77°13' λ = 192°00'

10/10 St

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.0	0.14	0.4		97	3.8	302	3		5.0	533	-17.4	0.52	82	1.3			
0.11	0.00	0.5		96	3.8	214	10		5.47	500	-21.4	0.76	72	0.6			300
0.2	988	0.9		95	3.9	222	11		6.0	465	-25.0	0.67	69				
0.3	976	1.1		94	3.9	228	11		7.0	406	-31.7	0.67	68				
0.5	952	1.1		92	4.0	237	10		7.11	400	-32.2	0.60	66				
0.8	918	1.1		90	4.0	237	12		8.0	352	-37.7	0.60	63				
0.96	900	0.1		88	3.3	337	14		9.1	300	-45.3	0.72	63				272
1.0	885	-0.2		85	3.3	336	14		9.85	269	-49.8	0.58	60				
1.3	863	-1.7		80	3.0	334	14										
1.41	850	-2.4		78	2.8	327	15										
1.5	840	-3.0		75	2.6	325	16										
1.89	800	-4.9		73	2.3												
2.0	788	-5.3		73	2.0												
2.5	740	-7.5		73	1.9												
2.64	726	-8.6		72	1.9												
2.83	700	-9.6		70	1.9												
3.0	693	-9.8		69	1.9												
3.9	617	-11.8		68	2.0												
4.0	609	-12.2		68	2.0												
4.11	600	-12.7		68	2.3												

- 330 -

16.6 0125 φ = 77°14' λ = 192°16'

10/0 As, Ac (195)

16.6 1340 φ = 77°15' λ = 192°35'

10/10 St

5

Прилож. приложение:

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
1.5	841	-2.3	0.42	38	2.1			13.0	168	-39.0	-0.15	55			241
1.9	800	-4.3	0.54	34	1.8			14.0	146	-39.0	0.00	55			245
2.0	789	-4.8	0.50	33	1.7			15.0	125	-38.8	-0.02				
2.5	741	-7.2	0.48	49	1.4			16.0	109	-38.1	-0.07				
2.94	700	-9.2	0.46	46	1.2		262	16.58	100	-37.8					
3.0	684	-9.6	0.48	46	1.1			17.0	94	-37.6	-0.05				261
3.13	682	-10.1	0.38	46	1.1			18.0	81	-37.4	-0.02				
4.0	610	-12.0	0.22	50	1.1			19.0	70	-36.9	-0.05				
4.12	600	-12.5	0.22	51	1.2		262	20.0	61	-35.4	-0.15				274
5.0	535	-17.0	0.30	55	1.1			21.0	54	-34.6	-0.08				
5.49	500	-19.5	0.59	55	0.9			21.48	51	-34.2	-0.08				
6.0	467	-22.9	0.59	55	0.8										
7.0	407	-28.7	0.58	55	0.6		261								
7.12	400	-29.5	0.59	55	0.4										
8.0	353	-34.6	0.59	55	0.3										
9.0	305	-41.7	0.71	55											
9.12	300	-42.4	0.61	55			254	0.0	017	-2.7	96	2.9	225	4	
10.0	263	-47.8	0.61	55				0.14	000	-2.6	91	2.8			
10.24	254	-48.8	0.42	55				0.2	591	-2.3	-0.20	89	2.8		
10.43	246	-48.8	0.42	55				0.46	959	0.6	-1.12	80	3.3		
10.63	226	-48.3	0.40	55				0.5	955	0.6		80	3.3		
11.24	200	-46.3	-0.61	55				0.7	931	0.6	0.00	73	3.1		
11.84	200	-41.0	0.55	55				0.97	900	-0.3		67	2.7		
12.0	159	-40.3	-0.48	55				1.0	897	-0.4	0.33	66	2.7		
								1.43	850	-1.9		55	2.1		

17.6 0125 $\varphi = 77^{\circ}15'$ $\lambda = 192^{\circ}38'$

10/10 Ξ ζ

Прилож. приложение

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
1.5	842	-2.1	0.34	54	2.1			0.2	992	-1.7	0.45	94	3.2		
1.91	800	-3.8	0.42	48	1.7			0.28	884	-0.2	-2.30	93	3.6		
2.0	791	-4.2	0.50	39	1.2			0.5	954	-0.2	0.00	89	3.6		
2.5	742	-6.7	0.50	39	1.2		268	0.97	900	-0.2		71	3.0		
2.96	700	-8.0	0.50	39	1.1			1.0	896	-0.2		70	2.9		
3.0	696	-8.2	0.30	41	1.1			1.08	888	-0.2	0.00	68	2.9		
4.0	611	-11.7	0.35	49	1.0			1.43	850	-1.7	0.43	59	2.4		
4.14	600	-12.4	0.35	49	1.0			1.5	843	-2.0		56	2.2		
5.0	535	-17.6	0.59	66	1.0		281	1.91	800	-3.3	0.34	47	1.7		
5.5	500	-20.5	0.60	62	0.8			2.0	790	-3.7	0.24	37	1.3		
6.0	467	-23.6	0.60	59	0.3			2.5	742	-4.9	0.24	37	1.3		
7.0	406	-29.6	0.60	59	0.3			2.95	700	-6.0		41	1.4		
7.11	400	-30.4	0.61	54			294	3.0	696	-6.3	0.28	41	1.3		314
8.0	353	-35.7	0.61	54				4.0	611	-10.7	0.44	60	1.6		
9.0	305	-42.8	0.71	53				4.15	600	-11.4		66	1.6		
9.11	300	-43.7	0.53	53				4.4	580	-12.5	0.45	66	1.5		
10.0	262	-49.4	0.66	53				5.0	535	-16.0	0.58	61	1.1		
								5.53	500	-18.5		56	0.8		
								6.0	468	-21.3	0.53	53	0.6		
								7.0	409	-28.3	0.70	48	0.3		
								8.0	355	-35.6	0.73	45			
								9.0	306	-44.3	0.87	43			

17.6 1340 $\varphi = 77^{\circ}15'$ $\lambda = 192^{\circ}45'$

10/10 Ξ

Продолж. приложения

H	B	t	γ	U	d	V	W	H	B	t	γ	U	q	d	V	W	
9.16	300	-45.4		43				0.2	992	-3.0	0.85	94	2.8				
-9.9	208	-50.6	0.70	41				0.4	987	-1.3	-0.85	93	3.2				
10.0	254	-50.6	0.00	41				0.5	954	-1.3	0.00	91	3.2				
10.26	254	-50.6	0.00	41			270	0.98	900	-1.3	0.00	84	3.1				
11.0	227	-47.2	-0.46	40				1.45	850	-1.9	0.13	74	2.8				
11.88	200	-42.3	-0.49	38				1.5	845	-2.0	0.13	74	2.8				
12.0	195	-42.3	-0.49	38				1.93	800	-2.7	0.16	64	2.4				
13.0	169	-40.4	-0.19	37			279	2.0	783	-2.8	0.22	56	2.1				
14.0	146	-39.7	-0.07	37				2.5	744	-3.9	0.22	56	2.1				
15.0	128	-38.9	-0.08	37				2.97	700	-5.2	0.28	50	1.7				
16.0	108	-38.1	-0.08	37				3.0	697	-5.3	0.28	50	1.7				
16.57	100	-37.7	-0.08	37			248	4.0	613	-10.5	0.52	42	1.1				
17.0	94	-37.3	-0.08	37				4.17	600	-11.5	0.52	42	1.1				
18.0	82	-36.1	-0.12	37				5.0	538	-16.0	0.85	39	0.6				
19.0	70	-34.3	-0.18	37				5.55	500	-19.5	0.85	39	0.6				
20.0	61	-34.3	-0.00	37				6.0	470	-23.4	0.74	36	0.4				
20.5	57	-34.3	-0.00	37			248	7.0	409	-31.0	0.76	33					
								7.15	400	-32.2	0.80	32					
								8.0	354	-39.0	0.80	32					
								9.0	306	-46.8	0.78	32					
								9.13	300	-48.0	0.75	32					
								9.8	271	-52.8	0.75	32					
								10.0	264	-52.8	0.00	32					

18.6 0131 φ=77°15' λ=192°40'

10/10 ≡ (7)

97 3.2 | 068 2

95 3.0

0.0 019 -1.3

0.14 000 -2.4

Продолж. приложения

H	B	t	γ	U	d	V	W	H	B	t	γ	U	q	d	V	W
10.4	248	-52.8	0.00	32				0.28	982	-2.0	0.61	100	3.3			
11.0	226	-49.1	-0.62	32				0.46	960	-2.0	0.00	100	3.4			
11.79	200	-46.5		32			254	0.5	956	-1.2	-1.33	100	3.7			
12.0	184	-45.0	-0.41	32				0.35	950	-0.8	0.00	85	3.3			
13.0	166	-42.8	-0.22	32			235	1.0	900	-0.8	0.00	60	2.5			
14.0	154	-42.7	-0.01	32				1.46	850	-0.8	0.00	58	2.4			
15.0	124	-42.2	-0.05	32				1.5	846	-0.8	0.00	58	2.4			
16.0	107	-41.6	-0.05	32				1.95	800	-0.8	0.00	50	2.2			
16.46	100	-41.4		32				2.0	794	-1.0	0.25	40	1.7			
17.0	92	-41.0	-0.05	32			235	2.3	746	-2.2	0.28	37	1.2			
18.0	79	-40.0	-0.10	32				3.0	700	-1.7	0.28	37	1.2			
18.75	72	-39.5	-0.07	32			227	4.0	616	-7.5	0.28	37	1.2			
19.0	69	-39.5	0.00	32				5.0	541	-14.2	0.67	37	0.8			
20.0	59	-39.3	0.00	32				5.59	500	-18.3	0.69	37	0.5			
21.0	51	-39.3	0.00	32			224	6.0	473	-21.1	0.69	37	0.5			
21.3	50	-39.3	0.00	32				7.0	412	-28.5	0.74	37	0.3			
								7.21	400	-30.2	0.71	36				
								8.0	353	-35.6	0.82	34				
								9.0	307	-43.8	0.82	34				
								9.17	300	-45.5	0.75	33				
								10.0	263	-51.3	0.75	33				
								10.1	249	-51.3	0.00	33				

18.6 1341 φ=77°15' λ=192°41'

10/10 Sc (26)

99 3.6 | 112 2

100 3.5

100 3.4

100 4

0.0 020 -0.3

0.15 000 -1.0

0.2 983 -1.4

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
11.0	227	-45.6	-0.95	34					1.0	900	-1.0	0.00	73	2.8	165	2	
11.36	200	-42.4	-0.37	34					1.46	850	-1.0	0.00	66	2.7			
12.0	195	-41.9	-0.37	34				253	1.5	846	-1.0	0.00	65	2.7			
13.0	168	-39.8	-0.21	33					1.70	818	-1.0	0.00	52	2.2			
14.0	145	-39.0	-0.08	32				253	1.84	809	-1.5	0.25	47	2.0			
15.0	125	-38.4	-0.06	32					2.3	745	-2.0	0.28	46	1.8			203
16.0	108	-37.7	-0.07	31					3.0	702	-3.8	0.35	46	1.2			
16.6	100	-37.0	-0.09	30				273	4.0	615	-8.7	0.59	45	1.3			
17.0	95	-36.8	-0.09	30					4.2	600	-9.6	0.53	44	1.2			
18.0	82	-36.0	-0.08	30					5.0	539	-14.0	0.83	44	0.3			
18.0	71	-35.5	-0.05						5.26	500	-18.0	0.70	43	0.6			
20.0	61	-34.7	-0.08					283	6.0	412	-27.2	0.62	42	0.3			
21.0	53	-33.2	-0.13						7.21	400	-29.0	0.83	41	0.3			
									8.0	358	-33.5	0.69	40				
0.0	020	-2.4		94	2.8	112	3		9.0	308	-42.4	0.69	40				
0.15	000	-2.0		66	3.0	108	4		10.0	266	-50.5	0.81	39				130
0.2	994	-3.0	0.30	97	2.9	107	4		10.84	253	-53.3	0.82	39				
0.34	976	-3.8	0.37	97	2.7	113	2		10.9	232	-53.3	0.00	38				
0.5	857	-2.3		97	3.1	089	1		11.0	229	-52.3	-1.00	38				
0.58	948	-1.0	-1.17	97	3.6	137	1		11.86	200	-46.0		37				

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19.6 0140 $\varphi=77^{\circ}17'$ $\lambda=192^{\circ}38'$

10/10 St, Δ^*

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
12.0	155	-45.7	-0.86	37					0.75	931	1.0	-1.00	(72)	3.2			
13.0	168	-42.9	-0.29	37				217	0.93	910	1.0	0.00	67	3.0			
14.0	146	-42.0	-0.09	37				213	1.02	900	0.8	0.22	65	3.0			
15.0	126	-41.6	-0.04	37					1.47	850	-0.5	0.29	54	2.3			
16.0	109	-41.0	-0.06	37					1.5	847	-0.6	0.29	53	2.2			
16.55	100	-40.8	-0.04	37				237	1.85	800	-2.2	0.30	50	2.0			
17.0	94	-40.6	-0.04	37					2.0	794	-2.4	0.35	49	1.9			250
18.0	81	-40.2	-0.04	37					2.5	745	-3.9	0.30	46	1.7			
19.0	71	-39.7	-0.05	37				250	3.0	700	-5.4	0.20	44	1.5			241
20.0	61	-39.2	-0.05						4.0	616	-9.8	0.44	43	1.1			
21.0	52	-38.3	-0.09						4.19	600	-10.6	0.55	42	0.8			
21.2	50	-38.2							5.0	540	-15.3	0.79	40	0.4			
21.4	49	-37.9	-0.10					253	5.37	500	-19.7	0.74	38				247
22.0	46	-37.5	0.00						6.0	472	-23.2	0.74	38				
22.5	41	-37.9	0.00						7.0	411	-30.6	0.74	38				
									7.19	400	-32.4	0.76	38				
									8.0	356	-38.2	0.85	37				
									9.0	308	-44.7	0.85					
0.0	021	-1.8		94	3.0	158	3		9.17	280	-45.7	0.00					249
0.17	008	-3.3	0.88	93	2.7				10.0	265	-51.5	0.00					
0.2	995	-3.3		93	2.7				10.2	257	-51.5	0.00					
0.28	965	-3.3	0.00	93	2.7				11.0	228	-48.7	-0.35					
0.5	860	-1.5	-1.50	92	3.2				11.85	200	-46.1						

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19.6 1340 $\varphi=77^{\circ}18'$ $\lambda=192^{\circ}38'$

10/10 St (15), Δ^*

Продолж. приложение.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	
12.0	195	-44.7	-0.40					244	0.17	600	-2.6	0.00	92	2.8	178	4		
13.0	168	-42.4	-0.23						0.2	595	-2.6	0.00	92	2.8	199	3		
14.0	146	-41.9	-0.05					239	0.76	629	1.8	-1.13	90	3.9	224	5		
15.0	125	-41.4	-0.05						1.02	609	1.0	-0.38	87	4.1	225	5		
16.0	108	-41.1	-0.03					255	1.47	609	-1.2	0.31	86	4.0	219	4		
16.54	100	-40.8							1.47	609	-1.2	0.50	85	3.4	231	5		
17.0	93	-40.6	-0.05						1.5	647	-1.4	0.80	85	3.4	251	5		
18.0	81	-39.2	-0.14					277	1.63	631	-2.6	0.80	80	3.1				
19.0	70	-39.2	-0.00						1.50	609	-2.6	0.00	79	3.1				
20.0	60	-38.7	-0.05						2.0	794	-2.6	0.00	75	3.0				
21.0	52	-37.7	-0.10					279	2.2	774	-2.6	0.47	72	2.2				
21.35	50	-37.2							2.5	746	-1.0	0.47	72	2.2				
22.0	46	-36.0	-0.17						2.81	717	-0.9	0.61	68	2.2				
23.0	39	-35.4	-0.05						3.0	700	-0.2	0.15						
24.0	34	-34.8	-0.06					274	3.48	657	-7.0	0.17						
25.0	30	-33.7	-0.11						4.0	615	-10.0	0.38						
25.35	28	-33.0	-0.20						4.19	600	-10.8	0.53						
									5.0	539	-15.3						154	
									5.55	500	-18.8							157
0.0	021	-2.2		93	3.0	135	3		6.0	471	-21.9	0.65						159
0.06	014	-2.6	0.67	83	2.9	167	4		7.0	411	-27.3	0.54						
									8.0	3.7	-34.8	0.72						

20.6 0140 $\varphi = 77^{\circ}17'$ $\lambda = 192^{\circ}11'$

6/6 Sc

Продолж. приложение.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
9.0	390	-42.2	0.74						4.0	612	-8.8	0.56	85	2.5			
9.19	386	-43.3							4.15	600	-9.5		85	2.5			
10.0	285	-48.9	0.67				159		5.0	585	-14.7	0.59	82	1.6			
10.26	285	-50.8	0.73						5.32	500	-17.2		80	1.4			
									6.0	470	-20.3	0.56	77	1.0			
									7.0	410	-26.5	0.62	73	0.6			
									7.18	400	-27.6	0.75	69	0.6			
									8.0	356	-40.9	0.69	67				
									9.0	308	-49.1		66				
									9.18	300	-49.1	0.87	65				
									9.79	275	-47.8	0.00	65				
									10.0	265	-47.8	0.00	63				
									10.73	238	-46.0	-0.67	63				
									11.0	229	-46.0	-0.67	61				
									11.82	200	-40.8	-0.32	60				
									12.0	195	-40.8	-0.16	59				
									13.0	169	-39.2	-0.12	57				
									14.0	147	-38.0	-0.08	55				
									15.0	128	-37.4	-0.08	53				
									16.0	108	-36.0						
									16.56	100	-35.0						
									17.0	94	-33.2	-0.12					
									18.0	82	-33.3	-0.14					

20.6 1407 $\varphi = 77^{\circ}19'$ $\lambda = 192^{\circ}38'$

10/10 St

95 3.5 112 6

95 3.5 - 10

94 3.4 116 10

30 3.3 124 10

90 3.5 138 9

82 3.9 139 7

81 4.0 140 7

77 3.8 146 10

77 3.8 143 11

77 3.4 3.4

77 3.3 3.3

79 2.6 2.6

82 2.7 2.7

82 2.7 2.7

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Продолж. приложения

29*

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
18.0	71	-33.1	-0.07					3.0	689	-7.4	78	2.3			366
19.9	64	-32.4	-0.08					4.0	606	-12.8	78	1.6			
20.0	63	-32.4	0.00				305	4.08	600	-13.2					
21.0	55	-32.4	0.00					5.0	531	-19.4	0.66				
21.6 0145 $\varphi = 77^{\circ}22'$ $\lambda = 192^{\circ}31'$															
10/10 Ξ (13)															
0.0	007	0.2		100	3.8	133		7.0	403	-32.6	0.77				368
0.06	000	-0.1		99	3.8			8.0	348	-39.0	0.64				
0.1	995	-0.6	0.80	99	3.8			9.02	300	-45.6	0.65				
0.2	992	-0.6	0.00	99	3.7			9.47	280	-45.6	0.00				
0.32	957	-0.6	0.00	98	3.7			10.0	258	-44.4	-0.23				338
0.5	945	0.2	-0.44	98	3.9			11.0	223	-42.1	-0.23				
0.65	927	0.9	-0.47	97	4.3			11.71	200	-41.1					
0.89	900	0.9	0.00	97	4.5			12.0	192	-41.0	-0.11				
1.0	888	0.9	0.00	96	4.4			13.0	166	-40.9	-0.01				305
1.35	850	0.2	0.00	95	4.3			14.0	144	-40.7	-0.02				
1.5	835	-0.1	0.20	93	4.2			15.0	123	-40.6	0.00				
1.85	800	-1.2	0.00	90	4.0			16.0	107	-40.4	-0.02				
2.0	783	-1.7	0.32	89	3.8			16.48	100	-40.2					310
2.5	734	-4.3	0.62	84	3.0			17.0	93	-40.1	-0.01				
2.89	700	-6.7	0.79	79	2.5			18.0	80	-40.0	-0.01				
								19.0	69	-39.8	-0.02				

339

Продолж. приложения

30*

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
20.0	59	-39.6	-0.02				335	3.0	691	-5.5	49	1.7			
21.0	50	-39.4	-0.02					4.0	609	-9.1	0.35	46	1.3		213
22.0	44	-39.0	-0.04					4.12	600	-9.5	0.35	46	1.3		
23.0	38	-38.7	-0.03					5.0	535	-14.3	0.52	44	0.9		
24.0	33	-38.4	-0.03				338	5.51	500	-17.7	0.52	42	0.7		220
24.65	32	-38.1	-0.05					6.0	467	-20.9	0.66	41	0.5		
21.6 1325 $\varphi = 77^{\circ}27'$ $\lambda = 192^{\circ}29'$															
10/10 St. (5), Ξ															
0.0	005	0.2		97	3.7	133		7.0	407	-37.1	0.62	39			
0.05	000	-0.4		97	3.6			8.0	355	-33.1	0.60				235
0.2	981	-1.1	0.65	97	3.5			9.0	307	-39.8	0.67				
0.5	945	-1.0	0.00	90	4.9			10.0	285	-44.3	0.46				
0.55	938	4.6	87	4.9				10.76	237	-44.7	0.20				
0.9	900	4.6	75	4.3				11.0	229	-44.1	-0.25				227
1.0	889	4.6	0.00	69	4.1			11.91	200	-41.2					
1.37	850	3.3	0.00	62	3.6			12.0	196	-40.9	-0.32				235
1.5	836	2.7	0.38	60	3.2			13.0	170	-38.6	-0.23				220
1.85	800	1.0	0.54	55	2.9			14.0	147	-38.6	0.00				
2.0	785	0.9	0.00	54	2.5		210	15.0	127	-38.6	0.00				
2.3	757	-2.3	0.30	51	2.1			16.0	111	-38.6	0.00				
2.91	700	-5.0	0.50	50	1.8			16.7	100	-38.3	-0.05				

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Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
18.0	82	-37.6	-0.05						4.09	600	-10.6	0.54	61	1.6			
19.0	70	-37.0	-0.06						5.0	533	-14.1	0.40	53	1.2			
19.24	68	-37.0	0.00					222	5.47	500	-17.0	0.62	46	0.5			380
22.6 0130 φ = 77°30' λ = 192°26'																	
10/10 St (5)																	
0.0	006	0.0	0.50	99	3.8	133			8.0	354	-29.8	0.63	46	0.5			
0.04	000	-0.2	0.50	100	3.8				9.0	307	-37.0	0.72					
0.2	590	-0.2	0.00	100	3.9				9.15	300	-38.5	0.82					
0.24	975	-0.2	0.00	100	3.9				10.0	266	-45.2	0.82					
0.5	945	2.7		100	4.9				10.8	237	-48.4	0.40					
0.56	938	2.9	-0.97	100	5.0				11.0	231	-47.7	-0.35					375
0.9	900	2.9		81	4.3				11.93	200	-43.8	-0.40					
1.0	889	2.9	0.00	79	4.2				12.0	198	-43.7	-0.40					
1.37	850	1.5		73	3.6				13.0	171	-40.7	-0.30					
1.5	836	1.0	0.38	73	3.6				14.0	147	-39.6	-0.11					
1.88	800	-0.5		77	3.5				15.0	127	-39.0	-0.06					
2.0	784	-1.3	0.46	78	3.4				16.0	109	-38.4	-0.06					
2.5	737	-4.1	0.56	81	3.0				16.59	100	-37.8	-0.07					
2.9	700	-5.7		81	2.8				17.0	94	-37.7	-0.07					
3.0	680	-6.3	0.44	81	2.6			345	18.0	82	-36.5	-0.12					
4.0	668	-10.1	0.38	62	1.7				18.44	77	-36.2	-0.07					
									19.0	71	-36.2	0.00					233

Продолж. приложение

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
20.0	63	-36.2	0.00						5.0	536	-16.0	0.54					
20.89	55	-36.2	0.00					230	5.51	500	-18.0	0.46					287
6.0	488	-20.6	0.62						6.0	488	-20.6	0.62					
7.0	408	-26.8							7.0	408	-26.8						
7.15	400	-27.5							7.15	400	-27.5						
5.0	356	-32.4	0.56						5.0	356	-32.4	0.56					
5.0	308	-38.9	0.65						5.0	308	-38.9	0.65					
2.19	300	-40.4							2.19	300	-40.4						
10.0	266	-46.6	0.77						10.0	266	-46.6	0.77					
11.0	229	-50.6	0.71						11.0	229	-50.6	0.71					241
11.89	200	-44.9	0.00						11.89	200	-44.9	0.00					
12.0	197	-44.5	-0.61						12.0	197	-44.5	-0.61					
1.0	169	-42.2	-0.23						1.0	169	-42.2	-0.23					
13.83	150	-41.5	-0.08						13.83	150	-41.5	-0.08					
23.6 0155 φ = 77°31' λ = 192°25'																	
10/10 St (22)																	
0.0	006	0.0	0.50	95	3.6	380	3		8.0	354	-29.8	0.63	46	0.5			
0.07	000	-0.1	0.30	94	3.6	016	5		9.0	307	-37.0	0.72					
0.2	983	-0.6	0.30	93	3.4				9.15	300	-38.5	0.82					
0.5	947	-1.6	0.33	92	3.2				10.0	266	-45.2	0.82					
0.84	908	2.6	-1.24	90	4.5				10.8	237	-48.4	0.40					
0.91	900	2.6		89	4.6				11.0	231	-47.7	-0.35					
1.0	889	2.6	0.00	90	4.6				11.93	200	-43.8	-0.40					
1.32	856	2.6	0.00	88	4.7				12.0	198	-43.7	-0.40					
1.37	850	2.4		88	4.7				13.0	171	-40.7	-0.30					
1.5	836	1.8	0.44	85	4.4				14.0	147	-39.6	-0.11					
1.85	800	0.6	0.76	(76)	3.7				15.0	127	-39.0	-0.06					
2.0	785	0.1	0.34	(72)	3.5				16.0	109	-38.4	-0.06					
2.5	738	-2.5	0.52	59	2.5				16.59	100	-37.8	-0.07					
2.92	700	-4.4		59	2.2				17.0	94	-37.7	-0.07					
3.0	692	-4.7	0.44	59	2.2			299	18.0	82	-36.5	-0.12					
4.0	610	-10.6	0.59						18.44	77	-36.2	-0.07					
4.12	600	-11.6							19.0	71	-36.2	0.00					246

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	t	U	q	d	V	W
0.7	921	2.2	-1.35	95	4.5				11.0	229	-47.5	0.00				
0.89	900	2.2	0.00	85	4.7				11.37	209	-47.5	0.00				
1.0	887	2.2	0.00	85	4.7				11.69	200	-45.8					
1.34	850	2.2	0.00	94	4.5				12.0	196	-44.7	-0.65				
1.5	833	2.2	0.00	94	5.0				12.0	189	-42.0	-0.27				
1.7	812	2.2	0.00	89	5.0				14.0	147	-41.1	-0.69				396
1.83	809	1.7	0.40	92	4.9				15.0	126	-40.0	-0.11				
2.0	788	1.0	0.94	85	3.9				16.0	110	-39.1	-0.69				
2.3	755	-1.7	0.40	71	2.9			385	17.0	94	-38.5	-0.06				
3.0	690	-3.3	0.40	0.53					18.0	83	-37.7	-0.08				357
4.0	607	-9.0	0.53						19.0	72	-36.8	-0.09				
4.1	600	-9.4	0.42						20.0	62	-35.5	-0.13				
5.0	534	-13.2	0.48						21.0	53	-34.3	-0.12				
5.49	500	-15.5	0.48						21.45	50	-34.2					338
6.0	467	-18.0	0.57					334	22.0	47	-34.2	-0.01				
7.0	408	-23.7	0.57						23.0	42	-31.2	0.00				335
7.13	400	-24.2	0.66						24.6 0131 φ = 77°35' λ = 192°23'							
8.0	355	-30.3	0.66						10/10 St (12), Эз							
9.0	309	-37.6	0.73						0.0	009	-0.1	96	3.7	202	2	
9.21	300	-39.5							0.05	000	-0.4	97	3.6			
10.0	267	-44.8	0.72													
10.43	250	-47.5	0.63													

Продолж. приложения

H	B	f	T	U	q	d	V	W	H	B	t	U	q	d	V	W
0.2	892	-1.1	0.30	97	3.5	294			11.0	229	-45.2	0.00	65			300
0.5	847	-1.8	0.23	95	3.2				11.16	222	-45.2	0.00	65			
0.92	800	0.1	-0.41	93	3.9				11.9	200	-43.1		65			
1.0	800	0.4	-0.41	93	4.0				12.0	196	-43.0	-0.26	65			
1.37	830	1.4	-0.20	91	4.5				13.0	170	-42.2	-0.08	64			288
1.5	837	1.4	-0.20	90	4.6				14.0	148	-41.6	-0.06	63			
1.87	800	-0.2	0.42	89	4.3				15.0	126	-41.1	-0.05				
2.0	786	-0.7	0.46	88	4.0				16.0	109	-40.6	-0.05				
2.5	739	-3.0	0.46	86	3.5			278	16.6	100	-40.4					
3.0	693	-5.4	0.48	85	3.0				17.0	94	-40.1	-0.05				279
4.0	610	-11.5	0.61	86	2.0				18.0	81	-39.2	-0.09				
4.13	600	-11.9	0.49	86	2.0				19.0	70	-38.4	-0.08				309
5.0	535	-15.4	0.39	77	1.5				20.0	60	-37.4	-0.10				
5.5	500	-18.0	0.56	75	1.2			288	21.0	52	-36.4	-0.10				
6.0	467	-21.0	0.56	72	0.9				21.4	50	-36.4					
7.0	408	-26.7	0.57	69	0.6				22.0	46	-35.4	0.00				
7.13	400	-27.0	0.66	69	0.6				23.0	40	-35.4	0.00				305
8.0	354	-31.3	0.68	68	0.6			277	24.6 1300 φ = 77°35' λ = 192°23'							
9.0	306	-39.9	0.66	67					10/10 St (15), Эз							
9.14	300	-41.0	0.66	67					0.0	011	-0.3	99	3.9	338	2	
9.3	272	-45.2	0.66	66					0.09	000	-0.1	99	3.8	335	9	
10.0	254	-45.2	0.60	66												

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.2	885	-0.5	0.40	59	3.7				10.05	263	-46.4	0.80					
0.3	872	-1.0	0.30	59	3.6				10.76	236	-46.4	0.00					355
0.5	846	-1.0	0.00	59	3.7				11.0	228	-45.6	-0.33					
0.83	800	-1.0	0.00	59	3.9				11.92	200	-41.9						
1.0	891	-1.0	0.00	59	4.0				12.0	197	-41.7	-0.39					
1.29	850	-1.0	0.00	59	3.6				13.0	170	-40.0	-0.17					305
1.5	859	-1.0	0.00	56	3.6				13.0	147	-39.2	-0.08					
1.8	807	-1.0	0.00	56	3.7				13.0	127	-38.4	-0.08					
1.87	800	-1.5	0.55	56	3.5				16.0	111	-37.7	-0.07					270
2.0	787	-2.1	0.55	56	3.5				17.0	100	-36.8	-0.13					
2.5	739	-4.5	0.48	56	3.0				17.0	95	-36.4	-0.13					
3.0	694	-6.4	0.38	56	2.8			350	18.0	81	-35.4	-0.10					
4.0	610	-11.0	0.46	55	2.1				19.0	69	-34.7	-0.07					262
4.13	600	-11.9	0.46	53	1.9				20.0	59	-33.1	-0.16					
5.0	535	-15.2	0.42	72	1.4				21.0	50	-33.1	0.00					262
5.52	500	-18.5	0.63	63	0.9												
6.0	469	-21.0	0.58	61	0.8												
7.0	409	-27.3	0.63	58	0.5												
7.16	400	-28.6	0.57	57	0.4			355	0.10	10	0.1	100	3.8	180			1
8.0	335	-33.6	0.63	55					0.07	600	-0.2	100	3.8				
9.0	307	-38.9	0.53	54					0.2	583	-0.7	0.40	100	3.7			
9.17	300	-40.8															
10.0	265	-46.0	0.71														

25.6 0141 $\varphi = 77^{\circ}35'$ $\lambda = 192^{\circ}23'$

10/10 St (18), Ξ, φ

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.5	947	-1.6	0.30	100	3.5				10.53	282	-44.0	0.00					
0.53	900	-2.5	0.20	100	3.5				11.00	226	-42.5	-0.32					
1.0	891	-2.6	0.20	100	3.4				11.86	200	-39.6						251
1.15	875	-2.9	0.20	100	3.4				12.0	196	-39.1	-0.34					
1.39	850	-2.9	0.00	100	3.5				13.0	169	-36.0	-0.01					
1.5	838	-2.9	0.00	100	3.5				14.0	146	-36.0	0.00					240
1.86	800	-2.9	0.00	92	3.4				15.0	126	-35.0	0.00					
2.0	755	-3.1	0.14	89	3.4				16.0	109	-33.9	-0.04					
2.5	738	-4.5	0.28	73	2.6				16.6	100	-33.1						
2.91	700	-6.7	0.48	65	2.1				17.0	94	-37.8	-0.08					220
3.0	691	-6.9	0.48	63	2.0			311	18.0	82	-37.0	-0.08					
4.0	608	-11.4	0.45	52	1.2				19.0	71	-36.8	-0.02					220
4.11	600	-12.1	0.45	51	1.2				20.0	61	-33.7	-0.11					
5.0	532	-18.5	0.71	48					21.0	52	-33.7	0.00					
5.46	500	-20.7			0.7				21.3	50	-33.7						
6.0	464	-24.0	0.55					344	21.9	46	-33.7	0.00					245
7.0	404	-30.0	0.50														
7.07	400	-30.6															
8.0	350	-36.9	0.69														
9.0	304	-41.6	0.47														
9.09	300	-42.0	0.21					321	0.0	1008	0.0	96	3.6	100			1
10.0	262	-43.7	0.21						0.07	600	-0.2	95	3.6	100			2
10.17	253	-44.0	0.18						0.2	583	-0.7	95	3.5	108			

25.6 1360 $\varphi = 77^{\circ}35'$ $\lambda = 192^{\circ}24'$

10/10 St (42), Ξ

Проблж. приложенич

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.5	916	-2.3	0.53	94	3.1				0.5	943	-2.8	0.53					
0.9	900	-3.3	0.40	89	2.6				0.88	900	-4.0	0.30					
1.0	889	-3.8	0.30	82	2.8				1.0	885	-4.3	0.30					
1.26	859	-3.9	0.00	87	2.8				1.34	850	-5.2	0.26					
1.3	855	-3.9	0.00	84	2.8				1.5	832	-5.6	0.26					
1.84	800	-3.9	0.00	77	2.7				1.8	800	-6.7	0.36					
1.82	791	-4.4	0.00	70	2.7				2.0	779	-7.4	0.36					
2.0	783	-4.4	0.45	70	2.6				2.5	730	-9.8	0.48					
2.3	755	-6.4	0.45	70	2.3			332	2.83	700	-11.4						
2.88	700	-7.7	0.36	90	2.6				3.0	684	-11.4	0.52					
3.0	689	-8.2	0.36	89	2.5				4.0	600	-11.2	0.68					
4.0	605	-13.5	0.53	83	1.7				4.62	555	-20.6	0.23					
4.07	600	-13.8	0.36	82	1.6				5.0	524	-23.0	0.63					
5.0	530	-17.1	0.36						5.35	500	-21.5						
5.43	500	-19.9							6.0	451	-24.4	0.74					
6.0	462	-24.2	0.71					360	6.92	400	-27.2						
6.49	433	-27.8	0.74						7.0	395	-27.2	0.68					
									7.6	371	-31.2	0.67					
									8.0	345	-41.2	0.00					
									8.9	304	-41.2	0.00					
									9.0	305	-41.2	0.00					
									9.24	285	-41.2	0.00					
									10.0	235	-38.5	-0.36					

26.6 0145 $\varphi = 77^{\circ}37'$ $\lambda = 192^{\circ}27'$
10/10 Ns, *

Проблж. приложенич

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
11.0	240	-36.6	-0.19						2.83	700	-12.2		94	1.8			
11.68	200	-36.6	0.00					286	3.0	684	-13.4	0.74	93	1.7			353
12.0	191	-36.6	0.00						4.0	600	-18.4	0.50	91	1.2			
13.0	164	-36.6	0.00						5.0	524	-24.5	0.61	85	0.7			
14.0	142	-37.2	0.00						5.38	500	-25.8		82	0.6			
15.0	124	-37.8	0.00					274	6.0	455	-29.2	0.47	76	0.5			
15.62	113	-38.1	0.03						6.92	400	-34.5		71				
									7.0	385	-35.0	0.58	71				412
									7.93	345	-42.5	0.81					
									8.0	341	-42.5						
									8.75	305	-42.5	0.00					
									8.89	300	-41.8						
									9.0	295	-40.8	-0.68					
									10.0	256	-37.0	-0.38					
									11.0	222	-35.3	-0.17					
									11.66	200	-33.2						
									12.0	190	-35.1	-0.02					
									13.0	165	-35.0	-0.01					
									14.0	143	-34.8	-0.02					
									15.0	124	-34.7	-0.01					
									16.0	107	-34.5	-0.02					
									16.45	100	-34.5						
									17.0	93	-34.4	-0.01					

26.6 1325 $\varphi = 77^{\circ}38'$ $\lambda = 192^{\circ}28'$
10/10 Ns, Fs (41), *

Продолж. приложение.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
18.0	80	-34.2	-0.02						3.34	657	-12.6	0.21	88	1.8			
19.0	70	-34.0	-0.02						4.02	690	-18.0	0.79	77	1.0			
20.0	60	-33.9	-0.01				478		5.0	527	-23.0	0.51	62	0.6			298
20.6	53	-33.8	-0.01						5.37	500	-25.5		60	0.5			
									6.0	459	-30.5	0.76	56				
									6.95	400	-37.5		51				
									7.0	396	-38.0	0.74	51				
									8.0	342	-44.9	0.69	50				312
									8.89	300	-39.5		50				
									9.0	295	-38.9	-0.60	49				
									10.0	256	-36.3	-0.26	49				
									11.0	221	-35.6	-0.07	48				
									11.68	200	-35.1		47				276
									12.0	191	-34.8	-0.08	47				
									13.0	166	-34.4	-0.04	46				
									14.0	145	-34.4	0.00	45				
									15.0	126	-34.2	-0.02	44				246
									16.5	108	-33.8	-0.04	44				
									16.5	100	-33.7		44				
									17.0	93	-33.5	-0.03	44				240
									18.0	81	-33.2	-0.03	44				
									19.0	72	-32.4	-0.08					
									19.6	65	-31.5	-0.15					243

27.6 0152 φ=77°43' λ=191°47'

10/10 St (S), ρ

0.0	0.06	-0.1	98	3.7	112	8
0.05	0.00	-0.2	97	3.7		
0.2	980	-0.5	0.20	96	3.5	
0.5	944	-1.0	0.17	94	3.5	
0.87	900	-1.5	0.14	89	3.4	
1.0	887	-1.7	0.14	87	3.3	
1.35	850	-2.2	0.12	75	2.8	
1.5	834	-2.3	0.12	75	2.5	
1.83	800	-4.6	0.74	75	2.2	
2.0	782	-6.0	0.60	75	1.8	
2.5	733	-9.0	0.60	75	1.8	
2.72	713	-11.1	0.95	79	1.7	273
2.85	700	-11.4	0.82	1.6		
3.0	687	-11.9	0.29	87	1.7	

Продолж. приложение.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.0	987	-0.2		100	3.8	180	2		0.0	000	-0.3		100	3.7	158	8	
0.2	972	-1.2	0.59	100	3.6	187	3		0.2	975	-0.5	0.10	96	3.5	153	7	
0.5	936	-2.0	0.37	100	3.4	183	6		0.5	940	-1.0	0.17	92	3.4	170	9	
0.81	900	-2.9		100	3.3	209	8		0.85	900	-1.7		87	3.2			
1.0	879	-3.7	0.34	100	3.2	205	7		1.0	882	-1.8	0.16	86	3.2			
1.27	850	-5.2		100	2.9				1.23	857	-2.3	0.22	86	3.1			
1.5	825	-6.7	0.60	100	2.7				1.29	850	-2.7		86	3.2			
1.75	800	-8.1		100	2.4				1.5	828	-3.9	0.39	86	2.8			
2.0	773	-9.1	0.48	100	2.3				1.77	800	-5.1		86	2.7			
2.5	726	-11.3	0.44	100	2.0				2.0	777	-5.8	0.39	86	2.6			
2.77	700	-12.6		100	1.9				2.5	728	-8.3	0.50	86	2.2			
3.0	679	-13.8	0.50	100	1.7		240		2.81	700	-9.9		86	2.0			297
3.94	600	-20.3		87	0.9				3.0	683	-11.0	0.54	86	1.9			
4.0	585	-20.6	0.68	87	1.0				3.58	600	-16.6		86	1.3			
5.0	519	-26.0	0.54	82	0.6				5.0	523			86				
5.27	500	-27.8		82	0.5				5.33	500			86				
6.0	452	-32.1	0.61	78					6.0	476			86				
									6.93	400			86				
									7.0	396							

28.6 0127 φ=77°46' λ=191°40'

10/10 As, Ac, Ns, Δ, X°

28.6 1349 φ=77°49' λ=191°35'

10/10 St

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
8.0	343	-35.8						235	2.78	700	-11.7	0.44					327
8.93	300	-32.8							3.0	679	-12.9						
9.0	297	-32.6	-0.32						3.95	600	-18.2	0.55					
10.0	258	-30.8	-0.18					294	4.0	535	-18.4	0.84					
11.0	225	-30.6	-0.02						5.0	519	-26.8						
11.82	200	-30.6							5.27	500	-29.4						
12.0	185	-30.5	0.00					211	6.0	451	-35.2	0.84					316
13.0	168	-30.6	0.00						6.52	419	-39.1	0.75					
14.0	146	-31.8	0.12					214	6.83	400	-39.1						
29.6 0142 $\varphi = 77^{\circ}51'$ $\lambda = 101^{\circ}33'$																	
10/10 SN (S), Δ , Σ , ω																	
0.0	988	0.2							9.0	294	-32.5	-0.45					289
0.2	974	-0.6	0.40				180 3		10.0	254	-32.5	0.00					
0.5	938	-2.2	0.53						11.0	221	-32.5	0.00					
0.83	900	-3.6							11.7	200	-32.5						253
1.0	881	-4.3	0.42						12.0	192	-32.5	0.00					
1.27	850	-5.9							11.0	166	-32.5	0.00					
1.5	826	-7.2	0.38						11.0	145	-32.0	-0.05					251
1.75	800	-8.5							13.0	126	-30.9	-0.11					
2.0	774	-9.4	0.44						11.28	117	-26.3	-0.28					238
2.5	726	-10.7	0.26														

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
8.0	341	-37.6							8.0	341	-37.6	0.60	68				
8.5	318	-37.6							8.5	318	-37.6	0.60	68				
8.9	300	-36.9							9.0	295	-36.9	-0.18	67				292
10.0	258	-34.0	-0.27						10.0	258	-34.0	-0.27	66				
11.0	222	-32.8	-0.12						11.0	222	-32.8	-0.12	64				
11.15	216	-32.6	-0.13						11.15	216	-32.6	-0.13	64				
11.7	200	-32.6							11.7	200	-32.6	0.00	62				283
12.0	191	-32.6							12.0	191	-32.6	0.00	59				
12.8	166	-32.6							12.8	166	-32.6	0.00	59				
13.0	163	-32.9	0.15						13.0	163	-32.9	0.15	58				
14.0	144	-34.0	0.11						14.0	144	-34.0	0.11	58				
15.0	125	-34.0	0.00						15.0	125	-34.0	0.00	58				306
16.0	108	-34.0	0.00						16.0	108	-34.0	0.00	58				
16.5	100	-34.0							16.5	100	-34.0	0.00	58				
17.0	93	-34.0					324		17.0	93	-34.0	0.00	58				303
18.0	81	-34.0	0.00						18.0	81	-34.0	0.00	57				
19.0	70	-34.0	0.00						19.0	70	-34.0	0.00	57				
20.0	60	-33.7	-0.03						20.0	60	-33.7	-0.03	56				
21.0	52	-33.3						333	21.0	52	-33.3		56				306
21.3	50	-32.2							21.3	50	-32.2		56				
22.0	45	-32.8							22.0	45	-32.8		55				
23.0	38	-32.4							23.0	38	-32.4		55				
29.6 1341 $\varphi = 77^{\circ}52'$ $\lambda = 191^{\circ}47'$																	
3/3 Fs																	
0.0	004	0.0							98	3.7	180						
0.03	000	-0.4							98	3.6							
0.2	978	-1.2	0.60	97	3.5	187	10		11.0	222	-32.8	-0.12	64				
0.5	941	-3.0	0.60	96	3.1	197	8		11.15	216	-32.6	-0.13	64				
0.85	900	-4.6							11.7	200	-32.6						
1.0	883	-5.3	0.46	93	2.5	188	11		12.0	191	-32.6						
1.31	850	-7.4							12.8	166	-32.6						
1.5	830	-7.9	0.52	90	2.0	201	12		13.0	163	-32.9	0.15	58				
1.78	800	-8.5							14.0	144	-34.0	0.11	58				
2.0	779	-9.2	0.26	88	2.0	207	14		15.0	125	-34.0	0.00	58				
2.5	730	-11.1	0.38	83	1.7	220	14		16.0	108	-34.0	0.00	58				
2.83	700	-12.0							16.5	100	-34.0						
3.0	683	-12.9	0.36	80	1.4	221	16		17.0	93	-34.0	0.00	58				
3.38	690	-18.4	0.56	77	1.0	219	15		18.0	81	-34.0	0.00	57				
3.6	523	-24.0	0.55	74	0.7	225	16		19.0	70	-34.0	0.00	57				
5.33	500	-25.7							20.0	60	-33.7	-0.03	56				
6.0	454	-30.5	0.65	70	0.6	228	33		21.0	52	-33.3		56				
6.89	400	-36.4							21.3	50	-32.2		56				
7.0	394	-37.1							22.0	45	-32.8		55				
7.07	390	-37.6	0.66	69					23.0	38	-32.4		55				

ИРСОНАЛЪЕ ЕДИНОВЕРЕНЪ

H	B	I	T	Y	U	Q	D	V	W	H	B	I	T	Y	U	Q	D	V	W
24.0	33	-31.7	-0.07							5.0	322	-33.1	0.55	63	0.0				
25.0	28	-31.0	-0.07							5.3	300	-33.3	0.55						
26.0	24	-29.6	-0.14							6.0	433	-30.6	0.75						
27.0	23	-27.6	-0.20						385	6.89	400	-37.6	0.78						
27.74	22	-27.6	0.00							7.0	393	-38.4	0.78						
										7.4	471	-40.2	0.45						
										7.9	516	-40.2	0.60						
										8.0	311	-39.5	0.70						
										8.9	300	-35.0							
										9.0	335	-35.5	-0.40						
										10.0	258	-31.0	-0.25						
										10.25	240	-32.5	-0.20						
										11.0	221	-32.5	0.00						
										11.55	205	-32.5	0.00						
										11.71	200	-32.6	0.07						
										12.0	192	-32.8	0.07						
										13.0	168	-33.5	0.07						
										14.0	145	-34.0	0.05						
										15.0	126	-34.0	0.00						
										16.0	110	-34.0	0.00						
										17.0	95	-34.0	0.00						
										18.0	82	-34.0	0.00						

30.6 1327 $\rho = 78^{\circ}00'$ $\lambda = 191^{\circ}12'$
 9/2 Cl, Fs

Пробоек. приковену

H	B	I	T	Y	U	Q	D	V	W	H	B	I	T	Y	U	Q	D	V	W
19.0	70	-34.0	0.00							6.0	453	-31.1	0.55	52					
20.0	58	-34.0	0.00						272	6.87	400	-38.6	0.85	51					
20.6	50	-34.0	0.00							7.0	393	-39.6	0.85	50					
										7.2	381	-40.7	0.55	50					
										7.85	348	-40.7	0.00	50					422
										8.0	340	-40.3	-0.27						
										8.88	300	-35.6							
										9.0	294	-35.2	-0.51						
										10.0	255	-33.8	-0.14						
										10.7	231	-33.0	-0.11						
										11.0	221	-33.0	0.00						
										11.79	200	-33.0	0.00						
										12.06	195	-33.1	0.08						
										12.0	192	-33.8	0.07						
										13.0	162	-34.5	0.14						
										14.0	145	-34.5	0.00						
										15.0	128	-34.3	0.00						
										16.0	108	-34.5	0.00						
										16.52	100	-34.5	0.00						
										17.0	94	-34.5	0.00						
										18.0	82	-34.5	0.00						
										19.0	71	-34.5	0.00						

1.7 0128 $\rho = 77^{\circ}59'$ $\lambda = 191^{\circ}53'$
 9/9 Fs, III

Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
20.0	62	-34.5	0.00				238	4.0	595	-20.4	0.58	75	0.8		
21.0	53	-34.5	0.00					5.0	519	-27.6	0.72	67	0.4		
21.5	50	-34.5	0.00					5.27	500	-28.5	0.58	65	0.4		308
22.0	47	-34.5	0.00					6.0	451	-33.4	0.58	59			
23.0	40	-34.5	0.00				235	6.85	400	-37.8	0.60	53			
23.5	38	-34.5	0.00					7.0	391	-39.4	0.60	48			
								8.0	339	-39.4	0.00	48			
								8.85	300	-35.5	0.00	44			
								9.0	294	-35.8	-0.35	43			
								10.0	255	-32.6	-0.32	36			
								10.31	244	-32.2	-0.13	35			
								11.0	221	-32.2	0.00	33			
								11.72	200	-32.2	0.00	31			
								12.0	192	-32.2	0.00	30			
								12.16	188	-32.2	0.00	30			
								13.0	167	-32.7	0.60	29			
								14.0	144	-33.7	0.15	26			
								15.0	125	-33.7	0.15	25			
								16.0	108	-33.7	0.00				
								16.56	100	-33.7	0.00				
								17.0	94	-33.7	0.00				
								18.0	81	-33.7	0.00				
								19.0	71	-33.7	0.00				

1.7 1351 $\varphi = 78^{\circ}02'$ $\lambda = 192^{\circ}05'$

10/10 St(41), Sc, Δ

H	B	t	U	q	d	V	W
0.0	002	-0.4	87	3.2	302	6	
0.2	976	-1.4	87	2.9	194	8	
0.5	940	-3.5	0.70	87	2.6		
0.85	900	-5.0	0.70	87	2.4		
1.0	883	-5.7	0.44	87	2.2		
1.29	850	-7.1	0.44	87	2.0		
1.5	827	-7.9	0.44	87	1.9		
1.76	800	-9.1	0.42	87	1.8		
2.0	775	-10.0	0.36	86	1.6		
2.5	727	-11.8	0.36	86	1.4		
3.0	680	-13.4	0.56	82	1.3		325
3.95	600	-20.0	0.56	75	0.8		

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Продолж. приложения

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
20.0	62	-33.7	0.00					2.5	726	-14.2	0.60	72	1.2	220	280
21.0	54	-33.7	0.00					2.77	700	-15.8	0.58	72	1.0		
21.5	50	-33.7	0.00				445	3.0	679	-17.1	0.58	72	0.9		
22.0	48	-33.5	-0.05					3.83	600	-23.5	0.67	68	0.5		
23.0	42	-33.3	-0.02					4.0	594	-23.8	0.67	68	0.5		
24.0	35	-33.0	-0.03					5.0	517	-29.9	0.61	64	0.3		
25.0	31	-32.8	-0.02				449	5.24	500	-31.4	0.79	61			269
26.0	28	-32.5	-0.03					6.56	413	-37.8	0.68	59			
27.0	25	-32.2	-0.03					6.79	400	-41.6	0.68	59			
								7.0	387	-41.6	0.00	59			
								7.05	385	-41.6	0.00	57			
								8.0	334	-37.4	-0.42	56			
								8.77	300	-34.5	0.55	55			
								9.0	291	-33.9	-0.35	54			
								9.61	266	-32.6	-0.21	53			
								10.0	259	-29.6	0.00	52			
								10.37	239	-29.6	0.00	51			
								11.0	218	-33.0	0.05	50			
								11.61	200	-32.5	0.08	49			
								12.0	189	-32.8	0.08	49			
								13.0	164	-35.1	0.18	48			
								14.0	142	-35.9	0.08	46			

2.7 0133 $\varphi = 78^{\circ}02'$ $\lambda = 192^{\circ}12'$

10/0 Cc, Ct, Ac, Σ

H	B	t	U	q	d	V	W
0.0	002	-1.8	65	3.1	202	1	
0.03	000	-1.9	65	3.0	229	3	
0.2	977	-2.4	0.30	59	2.6	224	4
0.5	941	-3.8	0.47	64	2.3	227	4
0.85	900	-5.5	0.44	63	2.1	232	4
1.0	882	-6.4	0.32	63	1.8	233	2
1.29	850	-7.8	0.30	63	1.7	219	2
1.5	828	-8.9	0.30	77	1.5	213	3
1.75	800	-10.1	0.46	73	1.4	208	3
2.0	775	-11.2					

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Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.0	121	-36.4	0.05	46					2.0	780	-10.2	0.32	83	1.7	278		
16.0	106	-37.0		46				231	2.5	732	-12.7	0.50	80	1.4			272
16.06	104	-37.1	0.07	46					2.84	700	-14.2		78	1.2			
16.37	100	-37.1		46					3.0	684	-14.8	0.42	77	1.2			
17.0	91	-37.1	0.00	46					4.0	600	-20.6	0.58	73	0.7			
18.0	80	-37.1	0.00	46					5.0	522	-26.8	0.82	71	0.4			267
19.0	69	-37.1	0.00						5.3	500	-29.0		71	0.4			
20.0	60	-37.1	0.00						6.0	453	-34.2	0.74	69				
21.0	53	-37.1	0.00					232	6.88	400	-39.6		66				
21.4	50	-37.1	0.00						7.0	393	-40.1	0.59	65				240
									7.24	380	-41.2	0.46	65				
									8.0	340	-37.5	-0.49	62				
									8.89	300	-33.4		59				
									9.0	295	-33.2	-0.43	59				
0.0	007	-0.3		95	3.4	292	4		10.0	255	-31.7	-0.15	57				231
0.08	000	-1.0		95	3.3	—	—		10.1	252	-31.6	-0.10	57				
0.2	983	-1.6	0.55	94	3.2	295	5		11.0	221	-31.6	0.00	57				
0.5	945	-3.4	0.60	92	2.8	303	6		11.71	200	-31.6	0.00	56				
0.89	900	-6.1		90	2.3	274	6		12.0	192	-31.7	0.03	55				262
1.0	886	-6.8	0.68	89	2.1	272	7		13.0	167	-32.9	0.13	51				
1.34	850	-8.2		87	2.0	271	6		14.0	145	-33.9	0.10	51				
1.5	833	-8.6	0.36	86	1.9	271	6		15.0	135	-34.6	0.07	52				260
1.82	800	-9.4		84	1.8	272	7		15.28	120	-34.6	0.07	52				

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2.7 1324 φ = 78°02' λ = 102°13'
10/10 Sc (50)

3.7 0141 φ = 78°00' λ = 192°16'
10/10 Sc (40)

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
16.0	108	-34.8	0.00	52					2.5	735	-11.4	0.52	71	1.4			
16.58	100	-34.8	0.00					288	2.87	700	-13.3		69	1.2			317
17.0	94	-34.8	0.00						3.0	688	-14.0	0.52	68	1.2			
18.0	81	-34.8	0.00						4.0	602	-19.1	0.51	63	0.8			
19.0	70	-34.8	0.00						4.03	600	-19.3		63	0.7			
20.0	60	-34.8	0.00						5.0	525	-24.9	0.58	61	0.5			
21.0	52	-34.8	0.00					286	5.35	500	-26.8		61	0.4			299
21.3	50	-34.8	0.00						6.0	455	-30.4	0.55	61				
									6.95	400	-37.5	0.75	61				
									7.0	395	-37.5	0.00	53				296
									8.0	343	-37.5	0.00	53				
									8.94	300	-37.5	0.00	48				
									9.0	297	-37.5	0.00	47				
0.1	006	-2.2		87	2.5	292	5		9.4	280	-37.5	0.00	46				
0.2	987	-2.7	0.60	85	2.7				9.86	262	-35.8	-0.37	43				
0.5	948	-4.4	0.57	80	2.5				10.0	257	-35.8	0.00	42				221
0.7	925	-5.6	0.60	80	2.3				11.0	222	-35.8	0.00	38				
0.91	900	-6.0		80	2.3				11.71	200	-35.8	0.00	37				
1.0	890	-6.1	0.17	80	2.3				12.0	192	-35.8	0.00	37				
1.37	860	-6.8		80	2.2				13.0	167	-35.8	0.00	36				217
1.5	837	-7.1	0.20	80	2.2				14.0	144	-35.8	0.00	34				
1.85	800	-8.0		78	1.9				15.0	124	-35.8	0.00	32				229
2.0	764	-8.8	0.34	76	1.8				16.0	108	-35.8	0.00	31				

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Продолж. приложение.

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
16.55	100	-35.8	30					1.88	800	-6.4	76	2.1			
17.0	94	-35.8	0.00	29			228	2.0	787	-6.5	0.30	74	2.1		
18.0	81	-35.8	0.00	28				2.5	739	-7.7	0.22	56	1.5		130
18.35	78	-35.8	0.00	28				2.92	700	-10.2	0.55	55	1.3		
19.0	70	-35.6	-0.03	27			266	3.0	692	-10.5	0.56	55	1.3		125
20.0	60	-35.1	-0.05					4.0	608	-11.8	0.43	51	0.9		130
21.0	53	-34.6	-0.05					4.1	500	-11.6	0.58	48	0.6		
21.3	50	-34.2	-0.04					4.5	500	-22.5	0.48	45	0.4		
22.0	45	-34.5	-0.07				270	4.1	464	-25.4	0.48	41	0.3		137
23.0	40	-33.5	-0.07					4.0	403	-31.9	0.65				
24.0	34	-32.8	-0.07				270	4.0	350	-32.2	0.72				143
25.0	30	-32.6	-0.02					4.0	330	-43.3	0.80				
3.0	015	-2.0	85	3.0	292	3		0.4	303	-43.3	0.00				
0.13	000	-3.0	93	2.8				0.16	285	-42.3	0.00				138
0.2	991	-3.4	0.70	2.7				10.0	261	-38.6	-0.44				140
0.5	855	-3.7	0.10	88	2.6			11.0	225	-36.6	-0.20				
0.97	800	-4.3	0.12	77	2.2			11.84	200	-33.9	-0.06				
1.0	880	-4.3	0.12	77	2.2			12.0	195	-33.9	0.00				
1.41	850	-4.3	0.16	71	2.1			13.0	169	-35.9	0.00				
1.5	840	-5.1	0.16	70	2.1		145	13.75	152	-35.9	0.00				137

3.7 1409 $\phi = 77^{\circ}59'$ $\lambda = 192^{\circ}16'$
10:10 S4. *.

Продолж. приложение.

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
5.45	500	-21.0	48	0.6				5.45	500	-21.0	48	0.6			268
6.0	463	-24.3	46	0.4				7.0	404	-31.7	0.74	46			
7.07	400	-32.3	45					8.0	351	-39.0	0.73	38			258
8.7	317	-42.7	0.00					9.0	304	-42.7	0.00				
9.09	300	-42.7	0.00					9.35	288	-42.7	0.00				
10.0	262	-40.3	0.00					11.0	226	-37.5	-0.23				230
11.2	217	-36.8	-0.23					11.2	217	-36.8	-0.23				
11.87	200	-36.8	0.00					11.87	200	-36.8	0.00				
12.0	169	-36.8	0.00					12.0	169	-36.8	0.00				
13.0	147	-36.8	0.00					13.0	147	-36.8	0.00				
14.0	128	-36.8	0.00					15.0	128	-36.8	0.00				
16.0	109	-36.8	0.00					16.0	109	-36.8	0.00				
16.6	100	-36.8	0.00					16.6	100	-36.8	0.00				
17.0	95	-36.8	0.00					17.0	95	-36.8	0.00				
18.0	88	-36.8	0.00					18.0	88	-36.8	0.00				
19.0	72	-36.4	-0.04					19.0	72	-36.4	-0.04				
20.0	62	-35.3	-0.06					20.0	62	-35.3	-0.06				

4.7 0139 $\phi = 77^{\circ}59'$ $\lambda = 192^{\circ}14'$
10:10 Ac (227)

317

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
21.0	53	-35.3	-0.05						2.94	700	-8.3		52	1.4			
21.45	50	-35.1							3.0	695	-8.4	0.18	51	1.4			
22.0	46	-34.9	-0.04						4.0	610	-12.7	0.43	43	1.0			331
23.0	41	-34.5	-0.04						4.12	600	-15.3		42	0.8			
24.0	35	-34.1	-0.04						5.0	534	-18.4	0.57	38	0.5			
24.4	33	-34.0	-0.02					237	5.49	500	-21.2		38				
									6.0	465	-24.6	0.66	38				
									7.0	405	-28.3	0.73	38				
									7.1	400	-28.2		38				
									8.0	351	-32.2	0.56					
									9.0	304	-37.9	0.41					
									9.1	300	-42.3						
									9.27	292	-42.3	0.22					
									10.0	263	-42.6	0.00					
									10.43	247	-42.6	0.00					
									11.0	227	-41.6	-0.18					
									11.86	200	-40.7	-0.09					
									12.0	185	-40.7	-0.09					
									13.0	160	-40.4	-0.03					
									14.0	146	-40.0	-0.04					
									15.0	126	-39.4	-0.06					
									16.0	109	-39.2	-0.02					
									16.53	100	-39.0						

4.7 1859 $\varphi = 78^{\circ}00'$ $\lambda = 192^{\circ}15'$
9/9 Ps

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	
0.0	018	-1.2							89	3.0	045							
0.15	009	-2.2							90	2.9								
0.2	992	-2.3	0.55	91	2.8				91	2.8								
0.5	954	-3.2	0.30	91	2.8				92	2.8								
0.82	917	-5.1	0.59	91	2.5				93	2.5								
0.97	900	-5.1	0.00	91	2.5				94	2.5								
1.0	897	-5.1	0.00	91	2.5	065	2		95	2.5	065	2						
1.36	858	-5.1	0.00	86	2.5	068	2		96	2.5	068	2						
1.43	850	-5.2	0.14	82	2.4	069	3		97	2.4	069	3						
1.5	843	-5.3	0.14	82	2.4	072	4		98	2.4	072	4						
1.91	800	-6.3	0.24	68	1.9	073	4		99	1.9	073	4						
2.0	790	-6.5	0.20	60	1.6	071	3		100	1.6	071	3						
2.5	741	-7.5																

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
17.0	94	-38.6	-0.05						1.5	845	-2.6	0.11	55	2.0	137	6	
18.0	82	-37.5	-0.11					239	1.92	800	-3.0	0.10	51	1.9	142	6	
19.0	72	-36.7	-0.08						2.0	792	-3.1	0.12	46	1.8	145	6	
20.0	62	-36.0	-0.07					243	2.3	743	-3.7	0.18	45	1.7	177	5	
21.0	54	-35.1	-0.09						2.61	733	-3.9	0.18	45	1.7	177	5	
21.5	50	-34.5	-0.12						2.98	700	-5.4	0.41	44	1.5	198	4	330
22.0	46	-34.3	-0.12					242	4.0	612	-9.8	0.43	39	1.1			
23.0	40	-33.9	-0.10						4.17	600	-10.9	0.62	37	0.7			
23.38	37	-32.9	-0.13						5.0	537	-16.0	0.56	35	0.5			
24.0	35	-32.4	0.00					235	5.55	500	-19.8	0.56	35	0.4			
24.15	34	-32.4	0.00						6.0	470	-21.6	0.59	34	0.3			
									7.0	410	-27.5	0.59	34	0.2			
									7.19	400	-28.3		33				
									8.0	357	-32.5	0.50	32				
									9.0	310	-38.9	0.64					
									9.21	300	-40.7	0.64					
									10.0	257	-45.3	0.39					
									10.28	256	-46.4	0.00					
									10.94	232	-46.4	0.00					
									11.0	229	-45.9						
									11.83	200	-41.8						
									12.0	198	-41.7	-0.44					
									13.0	171	-41.0						

5.7 0146 $\varphi = 78^{\circ}00'$ $\lambda = 192^{\circ}13'$
0/0 Ps

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	
0.0	020	-5.2							96	2.4	060							
0.15	000	-4.2							95	2.6								
0.2	993	-4.0	-0.60	93	2.6	111	3		94	2.6								
0.5	957	-4.8	-0.73	87	2.9	114	3		93	2.9	114	3						
0.7	934	-4.5	-0.50	83	3.1	127	3		92	3.1	127	3						
1.0	900	-4.5	0.23	65	2.4	127	4		91	2.4	127	4						
1.23	874	-4.3	0.35	57	2.1	139	5		90	2.1	139	5						
1.45	850	-4.5							89	2.0	138	6						

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H
14.0	147	-00.4	-0.06						4.0	616	-7.6	0.41	84	2.8													
15.0	127	-00.2	-0.01					251	4.2	600	-8.6		84	2.6													
16.0	110	-00.5	-0.06						5.0	540	-11.7	0.41	83	2.2													
16.65	100	-00.9	-0.06						5.59	500	-14.7		71	1.5													
17.0	95	-00.8	-0.07					259	6.0	473	-17.0	0.53	70	1.3													317
18.0	82	-00.8	0.00					262	7.0	414	-24.9	0.79	65	0.7													
18.82	73	-00.8	0.00						8.0	359	-29.7		65	0.6													
									9.0	312	-37.0	0.73	64	0.4													
									9.27	300	-39.0																269
0.0	019	-1.2		91	3.1	090	4		10.0	269	-43.1	0.61															
0.14	000	-1.7		90	3.1	127	7		10.8	239	-46.1	0.37															
0.2	991	-1.7	0.25	90	3.1	127	7		11.0	232	-46.1	0.00															
0.5	953	-1.3	-0.13	88	3.2	132	8		11.55	213	-46.1	0.00															
0.59	900	-0.6	-0.14	84	3.4	136	8		12.0	200	-44.8	0.29															309
1.45	850	-0.1	-0.11	75	3.4	160	6		13.0	172	-42.5	0.23															
1.5	845	-0.1		73	3.3	161	6		14.0	149	-41.6	0.09															
1.94	800	-0.1		73	3.3	161	6		15.0	128	-41.1	0.05															308
2.0	793	-0.1	0.00	73	3.5	162	6		16.0	110	-40.8	0.03															
2.16	778	-0.1	0.00	73	3.5	161	6		16.55	100	-40.4																
2.5	745	-1.6	0.44	73	3.4	162	6		17.0	95	-40.2	0.06															
3.0	700	-3.5	0.38	84	3.4			320	18.0	82	-39.5	0.07															
									19.0	71	-38.5	0.10															354

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5.7 1326 φ=78°03' λ=192°12'

10/10 As (280)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H
20.0	61	-37.3	-0.12						5.0	539	-13.0	0.60	63	1.4													
21.0	53	-36.2	-0.11						5.57	500	-15.6	0.45	60	1.2													303
21.4	50	-35.7						384	6.0	471	-17.5	0.52	43	0.5													
22.0	46	-35.2	-0.10						7.0	412	-22.7	0.52	43	0.5													
									8.0	359	-23.7	0.60	43	0.3													
									9.0	311	-36.0	0.73	43														346
									9.27	300	-37.7																
									10.0	269	-41.8	0.38															
									11.0	233	-47.9	0.51															
									11.57	214	-53.0	0.50															
									12.02	200	-50.3	0.60															
									13.0	172	-43.6	0.68															
									14.0	147	-43.6	0.00															
									15.0	127	-42.8	0.08															
									16.0	110	-41.9	0.09															
									16.63	100	-41.1																
									17.0	95	-41.2	0.07															
									18.0	82	-40.6	0.05															
									19.0	70	-39.8	0.08															
									20.0	60	-39.0	0.08															
								302	21.0	53	-38.2	0.08															
									21.3	50	-38.0																

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6.7 0145 φ=78°04' λ=192°13'

10/10 B (8)

Продолж. приложения.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	
22.0	45	-37.5	-0.07					300	4.21	600	-7.1	0.52	74	2.6				
23.0	39	-36.8	-0.07						5.0	541	-10.3	0.52	72	2.1				
24.0	34	-36.3	-0.05						5.6	590	-13.9	0.58	70	1.5			288	
25.0	30	-35.7	-0.05						6.0	473	-16.1	0.58	69	1.4				
26.0	25	-35.1	-0.05						7.0	416	-21.3	0.54	65	0.8				
6.7 1839 $\varphi=78^{\circ}05'$ $\lambda=192^{\circ}13'$																		
10/10 III																		
0.0	014	0.6		95	1.3	7	112	3	9.31	990	-35.1	0.62	61	0.4			365	
0.1	000	0.4		97	3.9				10.0	272	-41.3	0.80	59					
0.2	989	0.4	0.10	100	4.0				11.0	234	-49.5	0.82	57					
0.5	953	4.0	-1.20	100	5.3				11.7	211	-54.5	0.71	56					
0.75	924	4.9	-0.36	100	5.9				12.0	202	-53.7	-0.37	55				300	
0.97	900	4.8		98	6.0				12.07	200	-53.3							
1.0	895	4.7	0.08	98	6.0				13.0	174	-46.6	-0.7					392	
1.44	850	4.0		89	5.4				14.0	150	-44.1	-0						
1.5	844	3.9	0.16	88	5.4				15.0	129	-43.9							
1.93	800	2.9	0.24	82	4.8				16.0	110	-42.7							
2.0	793	2.7	0.24	82	4.8				16.65	100	-41.8						250	
2.5	743	0.9	0.36	80	4.5				17.0	95	-41.2							
3.0	700	-0.7	0.32	78	4.0				18.0	82	-39.6							
4.0	617	-5.1	0.44	75	3.1				19.0	71	-38.1							
									20.0	61	-36.5							258

Продолж. приложения.

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
21.0	53	-35.1	-0.14	47					2.5	747	1.2	0.10	67	3.7			
21.4	50	-34.6	-0.12	46				258	3.0	702	0.1	0.22	63	3.5			366
22.0	46	-33.9	-0.11	45					3.08	700	0.0	0.45	52	2.2			
23.0	40	-32.8	-0.11	45					4.0	619	-4.4	0.45	52	2.0			
24.0	35	-31.7	-0.11	45					4.24	600	-5.9	0.59	48	1.4			
25.0	30	-29.7	-0.20					258	5.0	544	-10.3	0.59	48	1.0			
25.27	29	-29.1	-0.22						5.96	500	-14.2	0.65	44	0.8			
7.7 0128 $\varphi=78^{\circ}06'$ $\lambda=192^{\circ}14'$																	
10/10 III																	
0.0	018	-0.9		100	3.4	225	3		7.0	417	-23.0	0.82	42	0.5			376
0.15	000	-0.8		100	3.3				7.28	400	-25.0	0.78	38				
0.2	994	-0.8	-0.05	100	3.6				8.0	364	-30.8	0.78	38				
0.5	957	4.0	-1.60	100	5.3				9.0	315	-38.1	0.73	36				
0.85	917	5.2	-0.34	88	5.2				9.33	300	-41.8	0.87	36				372
1.0	900	5.2	0.00	88	5.1				10.0	271	-46.8	0.87	35				
1.13	886	5.2	0.00	83	5.1				11.0	232	-52.2	0.54					
1.46	850	4.0	0.43	77	4.7				11.58	213	-54.4	0.3					
1.5	846	3.6	0.54	76	4.4				11.78	207	-54.4	-0.54					
1.72	813	2.2	0.64	73	3.9				12.0	200	-53.0	-0.54					296
1.95	800	1.8	0.64	72	4.0				13.0	171	-49.4	-0.3					
2.0	795	1.7	0.18	71	3.8				14.0	147	-47.7	-0.17					
									15.0	126	-46.6	-0.11					
									16.0	109	-44.4	-0.22					
									16.6	100	-43.4						

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	D	t	γ	U	q	d	V	W
17.0	95	-42.9	-0.15					300	3.04	700	-1.9	0.42	72	3.3			
18.0	82	-41.3	-0.16					630	4.0	630	-6.0	0.42	63	2.3			
19.0	70	-39.2	-0.21					4.25	600	6.7	-6.7	0.28	58	2.1			
20.0	61	-37.6	-0.16					5.0	545	-8.8	-8.8	0.28	51	1.7			
21.0	53	-37.6	0.00					5.66	500	-11.2	-11.2	0.46	47	1.4			315
21.2	52	-37.6	0.00					7.0	418	-19.3	-19.3	0.65	44	0.7			
								7.34	400	-22.4	-22.4	0.67	44	0.6			
								8.0	385	-26.6	-26.6	0.67	42	0.4			
								9.0	317	-33.9	-33.9	0.73	40				341
								9.39	300	-36.7	-36.7	0.75	39				
								10.0	275	-41.4	-41.4	0.75	39				
								11.0	237	-49.1	-49.1	0.77					331
								12.0	202	-55.0	-55.0	0.59					
								12.07	200	-55.2	-55.2	0.27					
								12.3	193	-55.8	-55.8	0.00					
								12.8	178	-55.8	-55.8	0.00					
								13.0	173	-54.0	-54.0	-0.90					
								14.0	149	-48.4	-48.4	-0.56					309
								15.0	127	-46.4	-46.4	-0.20					
								16.0	109	-45.2	-45.2	-0.12					
								16.6	109	-44.3	-44.3						
								17.0	94	-43.7	-43.7	-0.15					

7.7 1850 φ = 78°07' λ = 192°16'

10/10 3 (8)

0.0 021 -1.1 07 3.3 270 2

0.16 000 -1.7 97 3.3 270

0.2 996 -1.7 97 3.3 270

0.3 939 3.4 -1.70 97 4.3

0.83 921 5.2 -0.55 82 4.7

1.02 900 5.2 0.00 82 3.0

1.26 874 5.2 0.00 80 3.0

1.47 850 6.6 -0.58 79 3.6

1.5 847 6.6 -0.58 79 3.6

1.97 800 4.3 0.32 77 5.1

2.0 797 4.0 0.32 77 4.9

2.5 749 1.1 0.58 74 4.1

3.0 703 -1.8 0.58 72 3.3

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	D	t	γ	U	q	d	V	W
18.0	82	-42.8	-0.09					360	1.48	850	6.2	0.30	76	5.2	177	6	
19.0	71	-41.7	-0.11						1.98	800	4.1	0.42	76	4.8	205	7	263
20.0	60	-40.9	-0.08						2.5	750	1.5	0.50	76	4.3	209	7	
21.0	50	-40.0	-0.09						3.0	705	-3.1	0.92	76	3.2			
21.36	46	-39.4	-0.16						3.62	700	-3.0	0.85	76	3.1			
22.0	46	-38.4	-0.16						3.7	644	-7.1	0.90	75	2.4			
23.0	40	-37.5	-0.09						4.0	621	-7.7	0.20	71	2.3			
24.0	34	-36.7	-0.08						4.26	600	-8.4	0.45	69	1.5			277
25.0	30	-36.0	-0.07						5.0	545	-12.2	0.45	69	1.2			
26.0	27	-35.2	-0.08						5.66	500	-14.5	0.40	64	1.1			
27.0	25	-34.7	-0.05						6.0	477	-16.2	0.40	64	1.1			
									7.0	417	-23.9	0.77	52	0.6			
									7.31	400	-25.3	0.61					277
									8.0	353	-30.0	0.72					
									9.0	315	-37.2	0.75					
									9.35	300	-39.8	0.72					
									10.0	271	-44.7	0.89					265
									11.0	233	-51.9	0.72					
									11.37	211	-55.2	0.89					
									11.72	210	-55.2	0.00					
									12.02	200	-52.8	-0.80					
									13.0	173	-47.1	-0.58					269

8.7 0149 φ = 78°08' λ = 192°15'

0/0 Cl. Ac

0.4 021 0.4 94 3.7 180 2

0.17 000 2.4 85 3.9 202 8

0.2 996 2.8 84 4.0 205 8

0.38 974 6.8 -2.22 81 5.3 207 10

0.5 960 6.8 0.00 76 5.1 212 10

1.0 903 6.8 0.00 76 5.3 195 7

1.08 900 6.8 0.00 76 5.3 199 7

1.28 871 6.8 0.00 76 5.3 175 7

Продолж. приложения

H	B	t	l	U	q	d	V	W	H	B	t	l	U	q	d	V	W
14.0	149	-45.8	-0.13						4.25	600	-8.5	65	2.0	188	15		
15.0	123	-45.0	-0.05						5.0	545	-11.9	0.52	62	1.6	202	13	
16.0	110	-43.7	-0.13				242		5.65	500	-15.2	0.53	61	1.1	206	13	310
16.63	100	-42.8							6.0	476	-17.2	0.70	60	0.7	219	16	
17.0	94	-42.2	-0.15						7.0	416	-24.2	0.51	59		222	18	
17.53	87	-41.2	-0.19						8.0	361	-29.3	0.74	58		218	25	295
									9.0	314	-35.7	0.74	57		221	27	
									9.32	300	-38.7	0.75	56		223	29	
									10.0	272	-44.2	0.75	55		229	26	
									11.0	234	-51.6	0.74	54		221	28	283
									11.14	230	-52.8	0.85	53		220	29	
0.0	019	1.6		94	3.9	158	4		12.0	200	-52.8	0.00	52		221	18	
0.14	000	1.7		92	4.0				13.0	172	-47.8	-0.50	50		230	12	270
0.2	983	2.7	-0.55	91	4.2	192	11		14.0	146	-46.0	-0.18	48		239	7	
0.5	958	6.3	-1.20	87	5.5	194	12		15.0	127	-44.8	-0.12	46		243	4	
1.0	900	6.3	0.00	81	5.4	190	13		16.0	110	-43.2	-0.16	44		236	4	
1.47	850	6.3	0.00	76	5.4	187	13		16.63	100	-42.2		43		230	3	252
1.5	847	6.3	0.00	75	5.3	187	13		17.0	95	-41.6	-0.16	42		262	3	
1.97	800	6.0	0.46	73	5.3	190	15		18.0	81	-39.6	-0.20	40		039		
2.0	795	4.0	0.46	73	4.6	190	15		19.0	70	-38.0	-0.16	38				238
2.5	749	1.2	0.56	71	3.3	188	15		20.0	60	-36.7	-0.13	36				
3.02	700	-1.5	0.52	69	3.3	187	17	313									
4.0	619	-6.7	0.53	65	2.3	197	15										

8.7 1331 $\varphi=78^{\circ}11'$ $\lambda=192^{\circ}15'$
6/0 Сс

Продолж. приложения

H	B	t	l	U	q	d	V	W	H	B	t	l	U	q	d	V	W
0.0	016	0.9		91	3.6	158	4		9.0	313	-38.6	0.61	43				
0.13	000	2.4		88	4.0	169	11		9.29	300	-41.3	0.65	43				
0.2	990	4.0	-1.64	86	4.4	169	11		10.0	270	-45.1	0.64	42				
0.34	974	6.3	-1.64	83	5.1	169	11		11.0	232	-51.0	0.64	41				243
0.5	955	6.3	0.00	77	4.9	159	10		11.42	218	-46.7	0.00	41				
0.88	913	6.3	0.00	69	4.2	168	10		12.0	200	-46.7	-0.74	40				218
0.99	900	6.2	0.09	61	4.0	168	10		13.34	163	-43.9	-0.24	40				
1.45	850	5.1	0.24	57	3.7	159	12		14.0	148	-43.9	0.00	39				
1.5	845	5.0	0.24	57	3.7	159	12		14.73	139	-43.6	-0.11	38				215
1.95	800	3.2	0.35	54	3.2	153	13		15.0	110	-42.7	-0.09	38				
2.0	795	3.1	0.35	54	3.2	153	13		16.62	100	-41.6	0.00	33				
2.5	747	1.1	0.40	52	2.9	192	14		17.0	82	-40.9	-0.15	33				244
3.02	700	-1.3	0.46	49	2.4	193	15	283	18.0	62	-39.6	-0.13	33				
4.0	617	-6.5	0.53	45	1.6	198	19		19.0	51	-38.6	-0.10	33				
4.23	600	-7.7	0.53	45	1.5	201	17		19.25	48	-38.3	-0.12	33				247
5.0	543	-13.1	0.66	45	1.0	203	17										
5.63	500	-17.5	0.67	45	0.8	205	16										
6.0	475	-19.5	0.67	45	0.6	204	15	274									
7.0	415	-25.9	0.61	45	0.4	200	20										
7.27	400	-27.4	0.44	44	0.4	199	19										
8.0	361	-32.5	0.65	44													

9.7 1344 $\varphi=78^{\circ}16'$ $\lambda=192^{\circ}17'$
10,10 St (4)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.2	986	-0.8	0.00	100	3.6				10.0	285	-51.5	0.72	60				
0.3	975	-0.8	0.00	100	3.7				10.2	297	-53.0	0.75	60				
0.5	951	3.2	-2.00	100	5.1				11.0	228	-46.7	-0.79	57				238
0.64	935	4.6	-1.00	90	5.0				11.88	200	-43.6		53				
0.96	900	4.6	0.00	64	3.7				12.0	196	-43.4	-0.33	53				238
1.0	895	4.6	0.00	63	3.6				13.0	169	-42.3	-0.11	49				
1.43	850	4.6	0.00	55	3.5				14.0	146	-42.0	-0.03	47				
1.5	842	4.6	0.00	55	3.5				15.0	127	-41.6	-0.04	45				
1.82	810	4.6	0.00	51	3.3				16.0	109	-41.2	-0.04	43				238
1.91	800	4.2	0.39	49	3.2				16.58	100	-40.0		43				
2.0	791	3.9	0.39	49	3.1				17.0	94	-39.1	-0.21	41				202
2.3	743	1.0	0.38	49	2.7				18.0	81	-37.6	-0.15	40				201
2.99	700	-2.6	0.73	60	2.6			317	19.0	70	-35.9	-0.07	40				
4.0	615	-9.5	0.68	75	2.1				20.5	56	-34.5	-0.15	40				
4.19	600	-10.3	0.50	75	2.6				20.5	56	-34.5	-0.15	40				
5.0	539	-14.5	0.50	75	1.5				21.0	53	-33.6	-0.18	40				
5.55	500	-19.5	0.79	75	1.0				21.5	50	-33.6	-0.18	40				
6.0	471	-22.4	0.79	75	0.8				22.0	47	-33.6	0.00					210
7.0	412	-29.5	0.71	73	0.4												
7.19	400	-30.7	0.68	68													
8.0	355	-36.3	0.68	68													
9.0	308	-44.3	0.80	64													
9.17	300	-45.4	0.80	63													

10.7 1329 $\varphi = 78^{\circ}20'$ $\lambda = 192^{\circ}41'$

10° 0' Ac

0.0 011 1.2 92 3.8 180 4

0.09 000 1.4 90 3.9 206 10

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.2	986	2.5	-0.65	82	3.8	208	11		10.0	270	-44.5	0.81					
0.5	951	7.3	-1.60	57	3.9	212	11		10.52	240	-49.5	0.61					374
0.82	914	8.2	-0.28	48	3.6	222	8										
0.95	900	8.0	0.22	46	3.4	218	10										
1.0	894	7.8	0.22	46	3.4	218	10										
1.42	850	6.5	0.34	44	3.1	202	14										
1.5	841	6.1	0.34	41	2.5	207	16										
1.91	800	3.7	0.54	41	2.5	210	16										
2.0	791	3.4	0.54	40	2.1	226	12										
2.5	744	0.7	0.54	40	2.0												
2.99	700	-2.3	0.61	45	2.1												
3.3	672	-4.8	0.51	59	2.3												
3.76	635	-4.8	0.00	59	2.3												
4.0	616	-5.7	0.37	61	2.4												
4.2	600	-6.7	0.37	62	2.3												
5.0	541	-10.7	0.50	50	1.5												
5.61	500	-14.1	0.53	48	1.1												
6.0	475	-16.0	0.53	45	0.9												
7.0	415	-23.2	0.72	42	0.5												
7.26	400	-24.6	0.72	42	0.4												
8.0	381	-29.0	0.58	42	0.3												
8.0	313	-36.4	0.74	42													
8.31	300	-39.9	0.74	42													

11.7 1831 $\varphi = 78^{\circ}24'$ $\lambda = 192^{\circ}48'$

10° 10' E (6)

0.0 014 1.4 96

0.09 000 0.9 0.56

0.2 957 2.8 -1.73

0.5 951 3.9 -2.25

0.57 900 10.3 0.00

1.0 896 10.9 0.00

1.26 869 10.9 0.00

1.45 850 10.3 0.33

1.5 845 10.1 0.33

1.95 800 7.6 0.56

2.0 794 7.3 0.56

2.3 747 4.4 0.38

3.0 703 1.6 0.36

3.04 700 1.5 0.37

3.7 643 -2.4 0.57

4.0 620 -3.0 0.20

Продолж. приложение.

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
4.27	800	-3.6	0.84						19.0	72	-38.0	-0.13					247
4.5	582	-4.0	0.20						20.0	62	-36.2	-0.18					
5.0	546	-7.4	0.68						21.0	54	-35.3	-0.09					
5.7	500	-11.2						288	21.5	50	-34.8						244
6.0	480	-12.6	0.52						21.7	48	-34.6	-0.10					
7.0	430	-19.3	0.67														
7.36	400	-22.4															
8.0	366	-27.0	0.77														
9.0	317	-33.3	0.63														
9.4	300	-36.9						271									
10.0	274	-40.9	0.76						0.0	019	1.4			94.1	3.9	158	3
11.0	235	-46.7	0.58						0.2	992	6.5	-2.55		92	5.2	215	8
11.7	213	-51.8	0.73					276	0.5	956	9.1	-0.87		88	6.6	226	7
12.0	203	-51.8	0.00						0.7	934	10.2	-0.55		85	7.0	230	6
12.1	200	-51.8							1.0	900	10.2	0.00		85	7.2	219	10
12.4	191	-51.8	0.00						1.3	869	10.2	0.00		85	7.5	215	10
13.0	175	-60.4	-0.40					263	1.49	850	8.9	0.68		85	7.2	214	11
14.0	150	-65.8	-0.36						1.68	800	6.1	0.57		92	6.1	211	14
15.0	129	-44.2	-0.16					265	2.5	750	3.9	0.42		100	6.8	215	14
16.0	112	-42.7	-0.15					265	3.0	705	1.4	0.50		100	6.0	222	17
16.75	100	-41.2							3.05	700	1.2					221	17
17.0	97	-40.8	-0.19						4.0	622	-5.4	0.68				207	17
18.0	83	-38.3	-0.15						4.29	600	-7.7					206	16

12.7 0146 $\varphi=78^{\circ}25'$ $\lambda=192^{\circ}55'$
10.0 Ac (430)

Продолж. приложение.

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
4.5	584	-9.6	0.84						19.0	71	-39.4	-0.16					237
4.68	570	-8.2	-0.78						20.0	61	-37.5	-0.19					
5.0	547	-8.2	0.00						21.0	52	-36.2	-0.13					263
5.7	500	-12.0						295	21.4	50	-35.7						
6.0	480	-13.0	0.48						22.0	46	-34.9	-0.13					
7.0	430	-19.8	0.68						23.0	39	-34.8	-0.01					
7.36	400	-22.6							24.0	34	-34.8	0.00					254
8.0	366	-29.0	0.92						24.6	30	-34.8	0.00					
9.0	317	-36.3	0.73														
9.4	300	-39.6															
10.0	275	-43.5	0.72														
11.0	237	-52.3	0.88														
11.8	210	-56.3	0.40					297	0.0	023	2.0			84	3.6	138	2
12.0	204	-56.3	0.00						0.17	000	6.8			75	4.7	197	11
12.1	200	-56.3							0.2	995	7.9	-2.95		73	4.9	196	10
12.2	196	-56.3	0.00						0.22	981	9.5	-1.33		66	5.0	197	10
13.0	175	-50.2	-0.76					251	0.3	960	9.5	0.00		61	4.8	196	10
14.0	149	-48.0	-0.21						0.3	905	9.5	0.00		52	4.3	192	10
15.0	127	-45.9	-0.21						1.05	900	6.3	0.00		52	4.3	190	10
16.0	112	-44.6	-0.13					200	1.16	888	9.5	0.00		52	4.4	187	10
16.69	100	-43.7							1.22	869	9.0	0.42		51	4.0	188	13
17.0	95	-43.1	-0.15						2.01	800	6.2	0.37		51	3.7	193	15
18.0	82	-41.0	-0.21						2.5	753	3.	0.65		50	3.2	201	14

12.7 1331 $\varphi=78^{\circ}27'$ $\lambda=192^{\circ}59'$
0.0 Cs

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	708	-0.1	0.62	49	2.6	207	14		17.0	84	-41.3	-0.17					218
3.09	700	-0.7	0.55	45	1.7	205	14	316	18.0	82	-39.6	-0.17					230
4.0	624	-5.3	0.42	42	1.5	210	12		19.0	71	-37.5	-0.21					
4.31	600	-7.0	0.41	38	1.2	218	11	248	20.0	61	-36.4	-0.11					
5.0	548	-9.7	0.41	37	0.8	224	11		21.0	53	-35.6	-0.08					
5.68	500	-14.4	0.66	35	0.7	222	11		21.5	50	-35.6	0.00					204
6.0	479	-16.3	0.78	33	0.4	217	15		22.0	46	-35.6	0.00					
7.0	419	-24.1	0.78	32	0.3	218	16	233	22.4	44	-35.6	0.00					
7.35	400	-26.5	0.61	32		222	17										
8.0	365	-30.2	0.77			222	18										
8.13	338	-31.0	0.77			222	20										
9.0	317	-37.9	0.85			222	20	235	0.0	053	2.0		86	3.7	180	4	
9.38	300	-41.0	0.85			221	25		0.19	000	5.7	-1.85	83	4.7	193	11	
10.0	274	-46.5	0.71			226	30		0.4	975	8.6	-1.38	79	5.7	193	11	
11.0	234	-53.6	0.48			230	30	236	0.5	964	8.6	0.00	78	5.6	192	10	
11.44	219	-55.7	-0.30						1.0	907	8.6	0.00	64	4.9	190	11	
12.0	201	-54.0	-0.37						1.07	900	8.6	0.00	64	4.9	190	11	
13.04	209	-54.0	-0.37						1.47	857	8.6	0.00	58	4.7	189	10	
13.0	172	-48.3	-0.19					212	1.5	854	8.5		58	4.8	189	10	
14.0	149	-46.4	-0.14						1.54	850	8.4		58	4.8	189	10	
15.0	130	-45.0	-0.20						2.0	805	7.4	0.23	57	4.4	183	11	
16.0	113	-46.0	-0.20						2.05	800	7.3		57	4.5	183	11	
16.9	100	-41.4															

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13.7 0150 $\varphi = 78^{\circ}27'$ $\lambda = 192^{\circ}57'$

0/0

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.5	757	5.2	0.44	56	4.0	188	8		16.73	100	-45.2						229
3.0	711	2.2	0.60	55	3.4	196	7	333	17.0	95	-44.7	-0.20					232
3.13	700	1.3	0.58	52	2.3	197	7		18.0	85	-43.2	-0.15					226
4.0	627	-3.6	0.51	51	2.1	200	7		19.0	71	-42.2	-0.10					200
4.36	600	-5.0	0.46	50	1.7	204	7		20.0	62	-41.5	-0.07					156
5.0	553	-8.2	0.46	46	1.2	194	7	312	21.0	53	-40.7	-0.08					156
5.76	500	-12.1	0.51	46	1.2	194	7		21.44	50	-39.6	-0.11					054
6.0	484	-13.3	0.51	46	1.2	198	7		22.0	46	-38.4	-0.12					054
7.0	424	-19.2	0.59	41	0.7	214	10		23.0	39	-37.3	-0.06					051
7.44	400	-21.2	0.59	41	0.6	221	10		24.0	34	-37.1	-0.07					051
8.0	371	-24.5	0.53	40		221	10		25.0	30	-37.1	-0.08					058
9.0	322	-30.9	0.64			229	11		26.0	26	-36.3	-0.08					065
9.49	300	-33.7	0.64			229	11	313	27.0	23	-35.8	-0.10					065
10.0	278	-37.4	0.65			231	11										
11.0	240	-46.5	0.91			236	12										
12.0	207	-52.8	0.63			238	13										
12.2	200	-53.5	0.63			238	14		0.0	026	2.4		81	3.6	138	2	
12.5	191	-55.4	0.52			238	15		0.2	000	4.8	-1.20	73	3.9	178	8	
13.0	177	-55.4	0.00			236	12	314	0.4	977	7.3	-1.35	67	4.4	175	6	
13.12	174	-55.4	0.00			236	11		0.5	965	7.3	0.00	65	4.4	175	7	
14.0	150	-50.5	-0.49			232	8		1.0	907	7.3	0.00	52	3.7	173	8	
15.0	130	-48.5	-0.20			226	6	310	1.06	900	7.5		52	3.7	173	8	
16.0	112	-46.7	-0.18			221	4										

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13.7 1402 $\varphi = 78^{\circ}29'$ $\lambda = 192^{\circ}58'$

0/0

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.5	853	7.5	0.00	49	3.7	172	8		13.0	175	-54.6	-1.40			205	3	
1.53	850	7.3	0.00	49	3.7	173	8		14.0	150	-49.4	-0.52			203	2	363
2.0	803	5.5	0.40	45	3.2	176	8		15.0	129	-47.0	-0.24			222	1	
2.03	800	5.4	0.44	3.1	176	8			16.0	111	-45.4	-0.16			199	1	
2.5	755	3.7	0.36	37	2.4	173	9		16.65	100	-44.2				169	2	
3.0	709	1.4	0.46	35	2.1	167	10	305	17.0	95	-43.3	-0.21			149	2	
4.0	625	-3.4	0.48	34	1.6	159	9		18.0	83	-40.6	-0.27			265	1	255
4.33	600	-5.6	0.43	33	1.3	161	9		19.0	71	-38.6	-0.20			145	2	
5.0	551	-7.7	0.43	32	1.2	160	8		20.0	62	-37.9	-0.07			118	1	257
6.0	484	-13.5	0.58	31	0.8	171	10		21.0	53	-37.9	0.00			044	2	
7.0	424	-19.4	0.59	30	0.5	168	8		21.4	50	-37.9						
7.42	400	-22.3	0.59	29	0.4	172	11		22.0	46	-37.9	0.00					252
8.0	370	-25.9	0.65	29	0.3	172	12										
9.0	322	-32.8	0.69			179	9	316									
9.48	300	-37.2	0.79			179	10		0.0	095	1.2			85	3.4	135	3
10.0	278	-40.7	0.81			177	9		0.2	000	5.5	-2.20		76	4.3		
11.0	240	-48.8	0.81			177	9		0.41	975	7.2	-0.76		65	4.2		
12.0	205	-55.7	0.69			184	6		0.5	965	7.1			62	4.0	156	10
12.16	200	-56.5	0.60			184	6		1.0	907	6.5	0.12		52	3.5	149	10
12.4	159	-58.1	0.60			190	5		1.07	900	6.4			49	3.3	149	10
12.75	132	-58.1	0.00			199	4	296	1.3	853	5.7	0.16		42	2.8	139	11

14.7 0142 φ=78°30' λ=192°44'

0.0

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.33	850	5.6	0.38	41	2.7	160	11		15.0	128	-47.4	-0.21			151	3	271
2.0	803	3.2	0.38	33	2.1	163	11		16.0	110	-45.9	-0.15			074	3	
2.03	800	3.1	0.35	30	1.8	168	10	293	16.6	100	-44.5			102	2		
2.5	753	2.0	0.50	28	1.5	168	10		17.0	94	-43.4	-0.25			120	1	
3.0	709	-0.5	0.50	28	1.4	169	11		18.0	81	-41.9	-0.15			000	3	279
3.09	700	-1.0	0.43	25	1.0	169	10		19.0	70	-40.9	-0.10			000	3	
4.0	624	-4.8	0.43	22	0.9	171	10		20.0	60	-40.1	-0.05			003	5	282
4.31	600	-6.0	0.42	20	0.6	168	11		21.0	52	-39.4	-0.07			089	5	
5.0	549	-9.0	0.42	19	0.3	176	10		21.25	50	-39.2				105	5	
5.73	500	-13.4	0.59			177	10		22.0	44	-38.4	-0.10			086	5	
6.0	482	-14.9	0.72			173	11	294	23.0	38	-37.4	-0.10					
7.0	423	-22.1	0.72			175	14		24.0	32	-35.8	-0.16					
7.39	400	-25.8	0.89			175	15										
8.0	367	-31.0	0.89			172	15	302									
9.0	317	-39.0	0.80			171	15		0.0	022	2.0			54	3.6	133	5
9.39	300	-42.4	0.80			173	13		0.17	000	2.5			81	3.7	170	12
10.0	274	-47.0	0.80			171	10		0.2	997	3.0	-0.50		81	3.8	171	13
11.0	235	-56.5	0.95			169	10	323	0.5	961	8.5	-1.93		78	3.8	170	12
11.6	213	-59.7	0.93			162	9		1.0	905	8.5			56	4.5	171	13
12.02	200	-59.7	0.00			162	9		1.05	900	8.8	0.00		54	4.3	172	12
12.06	199	-59.7	0.00			162	9		1.52	850	7.3	0.32		42	3.2	174	13
13.0	172	-51.8	-0.84			160	8		2.02	800	6.2	0.22		31	2.3	173	13
14.0	149	-49.5	-0.23			158	5										

14.7 1442 φ=78°32' λ=192°49'

0.0

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W		
2.2	783	5.7	0.28	27	2.0	176	14		17.0	101	-41.2	-0.09							
2.5	754	3.9	0.60	26	1.8	180	13	255	17.07	100	-41.2	-0.11					291		
3.0	709	1.7	0.44	25	1.5	179	13		18.0	87	-40.1	-0.14							
3.09	700	1.2		25	1.5	178	12		19.0	75	-38.7	-0.18							
4.0	695	-3.1	0.48	23	1.1	176	11		20.0	65	-36.9	-0.18					288		
4.33	600	-4.2		22	1.0	178	12		21.0	56	-35.4	-0.15							
5.0	551	-6.5	0.34	21	0.8	180	12	237	22.0	50	-34.6	-0.08							
5.74	500	-11.6		19	0.6	172	12		22.8	44	-34.1	-0.05					284		
7.0	423	-19.5	0.64	18					15.7 0132 $\varphi = 78^{\circ}33'$ $\lambda = 192^{\circ}32'$										
7.41	400	-29.3	0.66						0'0										
8.0	359	-26.1	0.66						0.0	022	-0.4		92	3.3	180				
9.48	300	-36.2	0.65						0.13	006	-0.4	0.00	91	3.3	—	2			
10.0	278	-40.4	0.77					246	0.18	000	0.4	0.00	91	3.6	201	6			
11.0	239	-48.4	0.80						0.5	952	5.6	-1.62	88	5.2	200	8			
11.79	212	-53.4	0.63						0.6	950	7.0	-1.40	82	5.4	200	9			
12.0	205	-53.4	0.00						1.0	903	7.0	0.00	73	5.1	196	8			
12.16	200	-53.4	0.00					251	1.03	900	7.0	0.00	72	5.0	195	8			
12.49	190	-53.4	0.00						1.24	877	7.0	0.00	68	4.8	194	8			
13.0	176	-49.6	-0.75						1.5	850	4.6	0.82	63	3.9	189	8			
14.0	153	-45.5	-0.41						1.89	800	2.4	0.45	50	2.8	184	9			
15.0	132	-43.6	-0.19					277	2.5	750	-0.2	0.31	43	2.2	185	9			
16.0	116	-42.1	-0.15																

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	705	-2.5	0.46	41	1.8	193	9		18.0	81	-41.9	-0.10			148	5	
3.05	700	-2.8		40	1.7	192	10	337	19.0	70	-40.7	-0.12			159	6	
4.0	690	-6.5	0.40	37	1.3	183	12		20.0	60	-39.7	-0.10			100	6	408
4.27	646	-7.4		35	1.2				21.0	52	-38.6	-0.11			106	5	
5.0	546	-11.1	0.46						21.3	50	-38.5				096	4	
5.67	500	-14.5							22.0	45	-38.2	-0.04			081	4	
6.0	478	-16.7	0.56						23.0	39	-37.7	-0.05			071	5	
7.0	418	-23.6	0.69						24.0	34	-37.3	-0.04			063	5	397
7.31	400	-26.0							25.0	30	-37.0	-0.03			058	5	
8.0	384	-28.0	0.73														
8.0	384	-28.0	0.81														
9.32	300	-42.0	0.85														
10.0	270	-47.3	0.77					353									
11.0	233	-52.2	0.55						0.0	020	1.0		96	3.8	138	3	
11.64	210	-55.6		170	22				0.16	000	3.1		92	4.3	167	7	
11.97	200	-56.4		171	18				0.2	995	3.5	-1.25	92	4.5	160	8	
12.0	199	-56.1	-0.69						0.5	958	8.0	-1.50	84	5.9	166	10	
13.0	171	-50.0	-0.61				369		0.6	946	8.7	-0.70	81	5.8	166	10	
14.0	146	-47.5	-0.25						0.88	915	8.7	0.00	76	5.8	174	9	
15.0	125	-46.1	-0.14						1.02	900	8.1	0.43	73	5.5	161	8	
16.0	108	-44.2	-0.19						1.5	850	6.3	0.37	67	4.8	191	8	
16.52	100	-43.2							2.0	800	3.8	0.50	64	4.0	161	7	
17.0	83	-42.5	-0.13					381	2.5	750	1.8	0.40	61	3.6	175	6	

Продолж. приложения

Table with columns H, B, t, T, U, q, d, V, W, H, B, t, T, U, q, d, V, W. Includes data for 16.7 0181 and 100 Ac (412) and 16.7 1351 and 100 Ac (412).

Продолж. приложения

Table with columns H, B, t, T, U, q, d, V, W, H, B, t, T, U, q, d, V, W. Includes data for 16.7 1351 and 100 Ac (412) and 16.7 1351 and 100 Ac (412).

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
7.0	415	-25.4	0.62	65	0.6				24.0	38	-34.8	-0.05	57				431
7.28	400	-26.7		65	0.6				25.0	30	-34.8	0.00	57				
8.0	381	-31.5	0.61	65				262	26.0	27	-34.3	0.00	57				
9.0	313	-39.4	0.79	64					27.0	23	-31.8	0.00					
9.31	300	-41.5		64					28.0	20	-31.8	0.00					
10.0	272	-45.6	0.62	63					29.0	17	-31.8	0.00					456
10.22	263	-46.6	0.45	63					30.0	15	-31.8	0.00					
10.9	237	-46.6	0.00	62				261	17.7 0136 $\varphi = 78^{\circ}36'$ $\lambda = 192^{\circ}47'$								
11.0	234	-45.6	-1.00	62					9.9 \equiv C1								
12.0	200	-41.9	-0.37	61					0.0	020	-1.8		99	3.2	180	2	
13.0	174	-41.2	-0.07	60				268	0.17	000	-0.8		97	3.4			
14.0	150	-40.8	-0.04	60					0.2	905	-0.7	-0.55	96	3.5			
15.0	130	-40.5	-0.03	60					0.5	960	4.4	-1.70	88	4.8			
16.0	112	-40.1	-0.04	60					0.65	943	5.9	-1.00	87	5.4			
17.0	96	-39.6	-0.05	59				292	1.0	903	5.9	0.00	81	5.5	237	3	
18.0	83	-38.9	-0.07	59					1.03	900	5.9	0.00	81	5.5	237	3	
19.0	72	-38.2	-0.07	58				328	1.15	887	5.9	0.00	81	5.5	235	3	
20.0	62	-37.3	-0.09	57					1.29	850	4.3	0.41	82	5.1	331	4	
21.0	54	-36.4	-0.09	57					1.37	800	2.3	0.50	80	4.6	332	6	
21.5	50	-36.2	-0.06	57					2.0	797	2.2	0.45	79	4.3	334	6	
22.0	47	-35.8	-0.06	57					2.3	749	0.3	0.38	78	4.1	237	6	
23.0	40	-35.3	-0.05	57													

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	702	-1.8	0.42	75	3.4	217	8	328	18.0	81	-60.0	-0.08					318
3.03	700	-1.9		75	3.4	216	8		19.0	71	-39.3	-0.07					
4.0	619	-7.8	0.60	71	2.3	217	12		20.0	61	-38.2	-0.11					
4.24	600	-9.0		70	2.1	218	12		21.0	52	-35.7	-0.26					
5.0	544	-12.4	0.46	68	1.6			283	21.3	50	-35.1	-0.12					322
5.63	500	-15.6		60	1.2				22.0	46	-34.5	-0.12					
6.0	475	-18.8	0.64	58	0.9				23.0	40	-33.8	-0.07					
7.0	415	-26.7	0.79	56	0.5				17.7 1401 $\varphi = 78^{\circ}37'$ $\lambda = 192^{\circ}46'$								
7.28	400	-29.0		57	0.4				10/5 Ac. F8 \equiv								
8.0	381	-34.5		54				309	0.0	020	-0.1		98	3.4	135	1	
9.0	312	-42.0	0.75	54					0.16	000	0.4		98	3.9	110	3	
9.27	300	-43.8		54					0.2	595	0.5	-0.30	100	4.0	113	3	
10.0	268	-49.2	0.72	53					0.5	960	5.5	-1.67	87	5.1	134	3	
10.6	244	-52.7	0.59	50					0.58	950	6.1	-0.75	87	5.4	139	3	
11.0	220	-50.5	-0.55						1.0	903	6.1	0.00	87	5.7	146	3	
11.93	200	-45.2						308	1.03	900	6.1	0.00	86	5.7	147	2	
12.0	197	-44.9	-0.56						1.1	891	6.1	0.00	86	5.7	147	2	
13.0	170	-43.4	-0.15						1.1	850	5.2	0.23	86	5.1	136	2	
14.0	146	-42.8	-0.06					294	1.49	850	3.6	0.23	86	4.0	162	5	
15.0	126	-42.4	-0.04						1.97	800	3.5	0.33	86	4.0	167	6	
16.0	110	-41.7	-0.07						2.0	797	3.5	0.33	86	4.0	167	6	
16.62	100	-41.1	-0.09						2.5	749	0.0	0.70	86	3.4	166	5	
17.0	94	-40.8															

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Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
3.0	703	-3.0	0.60	70	3.0	168	5	322	18.0	80	-39.0	-0.09	65				311
3.04	700	-3.3		70	2.9	168	5		19.0	69	-38.1	-0.09	65				
4.0	619	-10.0	0.70	87	2.3	181	7		20.0	60	-37.3	-0.08	65				
4.23	600	-11.4		87	2.1	187	7		21.0	52	-36.8	-0.05	65				305
5.0	542	-14.6	0.46	87	1.7	202	9		21.3	50	-36.7		65				
5.59	500	-19.4		87	1.2			283	22.0	45	-35.3	-0.05	65				
6.0	472	-23.6	0.80	86	0.9				23.0	40	-35.1	-0.02	65				
7.0	411	-31.1	1.2	82					24.0	34	-35.8	-0.03	65				
8.0	357	-35.8	0.56	79					25.0	28	-35.3	-0.05	65				
9.0	308	-42.1	0.63	77				304	25.36	23	-34.2	-0.08					373
9.17	300	-43.4		76													
10.0	265	-49.7	0.76	75													
10.32	252	-51.2	0.47	74													
11.0	227	-59.3	-0.28	73					0.0	019	-0.2		93	3.4	068	3	
11.85	200	-65.6		72				304	0.15	000	2.0	-1.40	90	4.0	069	7	
12.0	156	-82.2	-0.41	72					0.2	932	2.6	-1.73	81	5.7	116	6	
13.0	138	-92.3	-0.31	70					0.5	857	7.8	-0.70	79	5.9	125	6	
14.0	125	-101.4	-0.64	68				284	0.0	815	8.3	0.60	74	5.7	128	5	
15.0	123	-11.6	-0.66	66					1.0	809	8.5	0.00	73	5.7	123	5	
16.0	108	-80.7	-0.69	65					1.12	888	8.5	0.00	69	5.1	117	6	
16.5	100	-80.2		65					1.48	850	6.9	0.44	69	5.1	117	6	
17.0	95	-82.9	-0.08	65					1.88	800	5.1	0.36	69	4.7	127	6	

18.7 0201 φ = 78°38', λ = 192°41'

5/0 Δс (395)

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
2.5	749	2.7	0.46	69	4.2	169	5		17.0	95	-39.0	-0.09	34				295
3.0	704	0.0	0.54	69	3.8			300	18.0	82	-38.2	-0.08	38				
3.05	700	-0.3		69	3.6				19.0	71	-37.4	-0.08	37				
4.0	621	-6.9	0.59	69	2.6				20.0	61	-37.0	-0.04					
4.9	600	-6.7		64	2.4				21.0	53	-37.0	0.00					330
5.0	546	-10.1	0.42	63	1.6			292	21.4	50	-37.0	0.00					
5.68	500	-14.7	0.77	50	1.1				22.0	46	-36.8	-0.33					
6.0	477	-17.8	0.77	50	0.8				23.0	40	-36.2	-0.06					
7.0	416	-24.2	0.64	48	0.5				24.0	34	-35.8	-0.04					330
7.25	400	-25.2		47	0.4				25.0	29	-35.1	-0.07					
8.0	362	-32.6	0.84	45					26.0	27	-34.0	-0.11					
9.0	314	-40.3	0.77	43													
9.5	300	-42.6		43													
10.0	271	-47.2	0.69	42					0.0	017	0.8		93	3.7	090	5	
10.92	235	-53.9	0.73	42				261	0.14	000	1.2	-0.30	91	3.9	105	11	
11.0	232	-53.4		41					0.2	991	1.4	-0.87	88	4.7	113	11	
11.97	200	-60.0		41					0.5	956	4.0	-1.06	80	5.0	130	9	
12.0	171	-66.4	-0.69	41				269	1.0	900	9.3	-1.00	60	5.0	139	9	
13.0	147	-83.6	-0.28	41					1.4	858	9.3	0.00	57	5.0	129	9	
14.0	127	-102.7	-0.09	40					1.48	850	9.0	0.00	57	4.8	131	10	
15.0	110	-113	-0.14	40					1.97	800	6.6	0.55	53	3.9	131	10	
16.0	110	-89.9	-0.14	39					2.0	797	6.0		53	3.9	131	10	
16.64	100	-89.4		39													

18.7 1331 φ = 78°39', λ = 192°33'

9/0 Cl, Cs

Предлож. приложениа

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.5	749	3.3	0.54	51	3.3	133	7		17.0	97	-33.4	-0.11					
3.0	703	0.0	0.55	49	2.7	136	8	322	18.0	84	-37.2	-0.12					
3.04	700	-0.3	0.50	44	2.5	138	8		19.0	73	-36.2	-0.10					328
4.0	620	-6.0	0.50	44	1.6	143	7		20.0	63	-35.2	-0.10					
4.26	600	-7.2	0.43	43	1.3	143	7		21.0	55	-34.3	-0.09					
5.0	545	-10.5	0.46			136	9		21.7	50	-33.7						285
5.65	500	-14.7				135	11		22.0	48	-33.4	-0.09					
6.0	477	-17.5	0.70			130	10	313	23.0	41	-32.5	-0.09					
7.0	417	-24.7	0.71			125	10		24.0	35	-31.2	-0.13					290
7.82	400	-26.7				125	10		24.37	33	-30.5	-0.19					
8.0	383	-32.4	0.77			140	12										
9.0	314	-39.5	0.71			149	14										
9.33	300	-41.9				154	15	328									
10.0	272	-46.3	0.68			160	15										
10.96	235	-52.5	0.65			161	18		0.0	019	0.1						
11.0	234	-52.6	0.00			162	17		0.15	000	0.7						
11.53	214	-52.6	0.00			163	12		0.2	593	1.1	-0.50	93	3.8	132	8	
11.98	200	-47.0	-1.24			159	10	335	0.5	957	6.7	-1.87	79	5.1	144	9	
13.0	172	-42.5	-0.43			151	8		0.61	945	7.7	-0.91	79	5.4	145	8	
14.0	150	-41.5	-0.11			138	6		1.0	900	7.7	0.00	75	5.5	133	9	
15.0	129	-40.7	-0.08			164	5		1.49	850	6.0	0.35	71	4.9	137	9	
16.0	111	-39.5	-0.12			138	7	313	1.97	800	4.2		66	4.2	137	10	
16.75	100	-38.6							2.0	797	4.1	0.37	66	4.2	137	10	

19.7 0181 $\varphi = 78^{\circ}41'$ $\lambda = 192^{\circ}11'$
10/8 Cs, Fs

Предлож. приложениа

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.5	719	1.5	0.50	60	3.4	131	10		17.0	94	-42.4	-0.07					248
3.0	704	-0.7	0.46	54	2.8	130	10	278	18.0	82	-41.5	-0.08					
3.05	700	-0.0	0.50	54	2.7	130	10		19.0	71	-40.5	-0.10					292
4.0	630	-6.0	0.33	54	2.0	127	10		20.0	61	-40.0	-0.06					
4.27	600	-8.1	0.55			125	10		21.0	53	-39.4	-0.06					
5.0	516	-11.3	0.55			122	12	247	21.35	50	-39.2						308
5.67	500	-16.5				118	11		22.0	46	-38.9	-0.05					
6.0	478	-18.1	0.66			121	10		22.2	44	-38.7	-0.10					
7.0	417	-25.1	0.70			124	12										
7.31	400	-27.7	0.66			133	12	225									
8.0	392	-31.7	0.65			135	14										
9.0	314	-38.5	0.68														
9.31	300	-40.5						267	0.0	018	0.6						
10.0	271	-45.2	0.67						0.13	090	1.4						
10.87	238	-50.4	0.60						0.2	991	2.8	-1.10	92	4.4	133	11	
11.0	233	-50.4	0.00						0.2	955	7.0	-1.40	80	5.3	144	13	
11.5	213	-50.4	0.00						0.2	943	7.5	-0.60	63	4.3	144	13	
11.6	213	-50.4	0.00						0.29	900	7.5	0.00	50	3.5	152	11	
12.02	200	-48.9	-0.38					225	0.29	872	7.5	0.00	47	3.5	152	11	
13.0	172	-45.9	-0.31					218	1.24	870	7.0	0.00	44	3.3	152	11	
14.0	148	-44.8	-0.11						1.46	850	6.3	0.27	43	3.2	151	11	
15.0	128	-43.9	-0.09						1.3	846	5.0	0.27	37	3.1	143	13	
16.0	110	-43.1	-0.08						1.37	800	5.0	0.27	37	3.1	143	13	
16.53	100	-42.7							2.0	796	4.3	0.40	37	2.6	143	13	

19.7 1325 $\varphi = 78^{\circ}44'$ $\lambda = 192^{\circ}06'$
3/2 Fs, Cs

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
2.5	750	1.8	0.62	34	2.3	149	11		17.0	95	-41.2	-0.10					
3.0	704	-1.3	0.62	33	1.6	148	10	294	18.0	82	-39.7	-0.15					260
3.05	700	-1.5		32	1.5	149	10		19.0	70	-39.7	-0.90					
4.0	630	-7.1	0.58	30	1.0	146	10		20.7 0131 $\varphi = 78^{\circ}46'$ $\lambda = 191^{\circ}46'$								
4.27	600	-8.4		30	0.9	144	10	292	6/6 Fs, Cs								
5.0	545	-12.3	0.32	28	0.8	135	6		0.0	019	-1.3		99	3.3	112	5	
5.66	500	-16.8		26	0.4	133	6		0.15	000	-1.2		95	3.4			
6.0	477	-18.6	0.63	25	0.4	130	7		0.2	992	-1.0		-0.15	94	3.4		
7.0	416	-24.2	0.56	22	0.2	108	4	234	0.5	955	4.6		-1.87	74	4.1		
8.0	369	-30.9	0.67	21	0.2	114	4		0.7	934	6.7		-1.05	69	4.4		
9.0	315	-37.8	0.69			315*	4		1.0	900	6.7		0.00	61	4.1		
9.36	300	-40.2				322	4	286	1.47	859	5.5		0.28	59	4.0		
10.0	272	-45.4	0.76						1.5	847	2.4		0.28	57	3.2	119	2
10.75	244	-49.7	0.57						1.85	800	2.2		0.63	56	3.1	118	8
11.0	234	-49.7	0.00					289	2.0	795	2.2		0.44	55	3.3	189	2
11.63	212	-49.7	0.00						2.5	747	0.0		0.60	54	2.3	189	3
12.02	200	-48.2	-0.38					280	3.02	700	-3.1		0.60	50	1.4	110	3
13.0	174	-44.9	-0.31						4.0	613	-0.3		0.63	48	1.2	108	3
14.0	149	-44.1	-0.05						4.24	600	-10.3		0.50	45	0.9	112	4
15.0	127	-43.1	-0.10						5.0	513	-14.3		0.50	44	0.7	114	5
16.0	100	-41.6	-0.09						5.61	500	-17.7						

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
6.0	475	-19.8	0.55	42	0.4	115	6	307	1.5	844	0.4		0.33				
7.0	414	-26.2	0.64	40	0.4	117	7		1.98	800	-0.9		0.28				
7.24	400	-27.4				120	7		2.0	793	-1.0		0.28				
8.0	369	-31.0	0.48			127	6	274	2.5	744	-3.7		0.54				
9.0	311	-38.8	0.76			169	6		2.98	700	-5.8		0.46			329	
9.26	300	-40.4				169	7		3.0	698	-6.0		0.46				
10.0	270	-45.1	0.62			169	11		4.0	613	-13.1		0.71				
11.0	232	-49.8	0.47			169	11		4.17	600	-16.2		0.31				
11.4	218	-49.8	0.00						5.0	589	-19.4		0.31				
12.0	200	-48.0	-0.30					246	5.55	500	-22.6		0.64			333	
12.36	190	-46.5	-0.36						6.0	471	-26.0		0.74				
20.7 1333 $\varphi = 78^{\circ}48'$ $\lambda = 191^{\circ}37'$																	
10/10																	
0.0	019	-0.4		92		111	3		7.18	400	-31.0		0.78				282
0.14	000	-2.4							8.0	395	-37.5		0.92				
0.2	992	-2.4	1.00						9.0	305	-47.0		0.92				
0.5	955	1.5	-1.30						9.53	300	-48.6		0.79				
0.97	900	1.5							10.0	265	-51.2		0.00				
1.0	897	1.5	0.00						11.0	227	-46.7		-0.45				
1.17	879	1.5	0.00						11.85	200	-45.3		-0.14				300
1.44	850	0.6							12.0	195	-45.3		-0.14				
									13.0	168	-44.7		-0.06				
									14.0	145	-44.1		-0.06				

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.0	124	-42.1	-0.20					265	2.98	700	-7.2	0.60	63	1.9	019	2	316
16.0	108	-40.4	-0.17						4.0	614	-11.8	0.45	55	1.2	069	3	
16.5	100	-39.5						242	4.18	690	-12.9	0.42	50	1.1	062	8	
17.0	92	-39.0	-0.14						5.0	538	-16.0	0.42	50	0.9		1	305
18.0	80	-37.6	-0.14					242	5.55	590	-19.2	0.56	47	0.9	357	2	
19.0	69	-36.5	-0.11						6.0	470	-21.6	0.56	43	0.5	311	3	
20.0	59	-35.0	-0.05					242	7.0	411	-27.7	0.61	43	0.3	308	4	
									7.2	400	-28.9	0.62	43	0.3	301	6	315
									8.0	357	-33.9	0.62			210	9	
									9.0	309	-39.5	0.56			209	8	
									9.2	300	-40.6				208	3	
									10.0	265	-44.8	0.53			207	2	
									10.9	231	-49.6	0.53			207	2	
									11.0	228	-49.6	0.00			207	2	
									11.3	218	-49.6	0.00			207	2	
									11.9	200	-46.2	0.00			208	1	
									12.0	197	-45.4	-0.60			208	2	335
									13.0	170	-43.4	-0.20			204	1	
									14.0	148	-42.3	-0.11			202	2	
									15.0	126	-42.0	-0.03			206	1	
									16.0	111	-41.8	-0.02			211	1	354
									16.7	100	-41.4				207	2	
									17.0	90	-41.2	-0.08			203	2	

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21.7 0145 $\varphi = 78^{\circ}48'$ $\lambda = 191^{\circ}37'$

3/0 Cc

H	B	t	Y	U	q	d	V	W
0.0	018	-2.4						0
0.15	000	-1.5						
0.2	992	-1.1	-0.05					1
0.5	955	1.5						1
0.58	946	2.1	-0.84					2
0.99	900	2.1	0.00					3
1.42	854	2.1	0.00					3
1.45	850	1.8						3
1.5	845	1.7	0.50					3
1.94	800	-0.8						2
2.0	794	-1.2	0.58					2
2.5	745	-4.3	0.62					2

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
18.0	65	-40.6	-0.08					332	1.45	800	0.9	0.23	74	3.6	287	2	
19.0	72	-40.1	-0.05					001	1.5	845	0.8	0.23	74	3.6	282	3	
20.0	62	-39.5	-0.06					029	1.94	800	-1.3	0.54	71	2.9	289	4	
21.0	58	-39.0	-0.05					069	2.0	794	-4.9	0.60	69	2.3	336	3	295
21.5	50	-38.9						072	2.5	745	-4.9	0.46	67	2.0	346	3	
22.0	46	-38.5	-0.05					055	2.89	700	-7.1	0.48	62	1.4	302	3	
23.0	40	-38.0	-0.05					048	4.0	614	-12.0	0.48	59	1.2	310	3	
24.0	33	-37.6	-0.04					065	4.17	600	-12.8	0.62	57	0.9	335	1	
25.0	30	-37.0	-0.06					102	5.0	537	-18.2	0.54			288	2	305
26.0	24	-36.3	-0.07					116	6.0	468	-23.6	0.49			277	4	
27.0	21	-35.4	-0.09					120	7.0	409	-29.5	0.67			261	4	284
28.0	19	-34.2	-0.12					123	7.15	400	-29.4	0.62			252	4	
28.9	17	-32.9	-0.14						8.0	353	-35.2	0.62			233	4	
									9.0	306	-41.4	0.78			229	3	
									9.15	300	-43.0	0.30			232	4	
									10.0	263	-49.2	0.00			225	2	
									10.27	253	-50.0	-0.72			225	2	275
									10.75	235	-50.0	0.00			225	2	
									11.0	225	-48.2	-0.72			225	2	
									11.83	200	-42.8	-0.55			208	6	
									12.0	195	-42.7	-0.55			208	6	
									13.0	167	-43.4	-0.03			203	4	

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21.7 1387 $\varphi = 78^{\circ}51'$ $\lambda = 191^{\circ}40'$

4/0 Cc, Cc

H	B	t	Y	U	q	d	V	W
0.0	017	0.4						0
0.13	000	0.4						0
0.2	991	0.5						0
0.5	955	1.9						0
0.53	952	2.1	-0.46					1
0.99	900	2.1	0.00					1

Проблеск, присоединения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
14.0	144	-42.0	-0.04			313	3	244	1.0	900	2.6	0.57	65	3.3	046	1	
15.0	126	-41.7	-0.03			295	4		1.46	850	1.5		64	3.2	389	1	
16.0	109	-41.4	-0.03			283	4		1.5	846	1.4	0.24	64	3.2	330	1	
16.55	100	-41.1				300	4	238	1.95	800	-0.4		62	2.9	333	3	
17.0	93	-40.9	-0.05			309	4		2.0	795	-0.7	0.42	62	2.9	334	2	280
18.0	80	-40.4	-0.05			330	3		2.5	746	-3.3	0.82	60	2.3	295	2	
19.0	70	-39.8	-0.06			301	2	255	3.0	700	-5.3	0.40	58	2.0		0	
20.0	60	-38.9	-0.09			006	3		4.0	616	-10.7	0.54	49	1.2		1	
21.0	51	-37.9	-0.10				1		4.2	600	-11.4		49	1.2		1	
21.2	50	-37.7							5.0	539	-16.9	0.62	49	0.8	002	3	
22.0	45	-37.2	-0.07				2	258	5.57	500	-20.0		57	0.7	044	2	278
23.0	39	-36.8	-0.04			168	1		6.0	471	-22.3	0.54	54	0.6	046	2	
24.0	34	-36.2	-0.06			178	2		7.0	410	-29.5	0.62	49	0.3	015	2	
24.7	31	-35.8	-0.06					270	7.17	400	-29.6		49	0.3	009	2	

22.7 0122 $\phi = 78^{\circ}50'$ $\lambda = 191^{\circ}34'$
510, Ac, Cc

H	B	t	t	U	q	d	V	W
0.0	019	-1.8		91	2.9	090	3	
0.14	000	-1.4		84	2.9	100	5	
0.2	991	-1.0	-0.40	81	2.9	103	4	
0.5	935	2.1	-1.03	68	3.1	134	2	
0.7	932	2.8	-0.35	67	3.4	127	3	

Проблеск, присоединения

H	B	t	t	U	q	d	V	W	H	B	t	t	U	q	d	V	W
14.0	147	-40.7	0.10			330	6		1.94	800	2.0		50	2.8			
15.0	128	-40.8	0.01			332	5		2.0	793	1.5	0.36	50	2.7			
16.0	110	-40.3	-0.05			331	4	236	2.5	745	-1.0	0.50	44	2.1			
16.55	100	-40.0				327	4		3.0	700	-3.2	0.44	41	1.8			356
17.0	95	-39.7	-0.06			328	3		4.0	615	-7.4	0.42	37	1.2			
18.0	82	-39.0	-0.07			347	4	230	4.19	600	-8.3		36	1.1			
19.0	72	-37.7	-0.13			040	2		5.0	540	-13.0	0.55	35	0.8			
20.0	62	-37.7	0.00						5.59	500	-15.8		32	0.6			
20.8	55	-37.7	0.00					233	6.0	474	-18.7	0.57	31	0.5			

22.7 1337 $\phi = 78^{\circ}52'$ $\lambda = 191^{\circ}24'$

H	B	t	t	U	q	d	V	W
0.0	018	-0.6		95	3.4	112	3	
0.1	004	-1.4		80	3.4			
0.13	000	-1.4		94	3.2			
0.2	990	-1.4		94	3.2			
0.37	970	-1.4		0.00	93	3.2		
0.5	933	0.5	-1.46	92	3.9			
0.87	900	3.3	-0.60	82	4.4			
1.0	866	3.3		81	4.4			
1.44	833	3.3		59	3.4			
1.5	844	3.3	0.00	58	3.1			

10/10 St, Fs

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
16.8	100	-37.4	-0.06	99	3.5	022			1.0	896	1.1	0.00	70	3.2			
17.0	97	-37.3	-0.05	98	3.5	022			1.2	874	1.1	0.00	64	3.0			
18.0	83	-36.8	-0.05	98	3.5	022			1.43	850	0.7	0.20	60	3.0			
19.0	73	-36.2	-0.06	98	3.5	022			1.5	841	0.5	0.20	59	2.8			
20.0	62	-35.5	-0.07	98	3.5	022			1.9	800	-0.4	0.22	55	2.5			
21.0	54	-34.8	-0.07	98	3.5	022			2.0	790	-0.6	0.22	55	2.5			
21.5	50	-34.5	-0.07	98	3.5	022			2.5	742	-2.1	0.30	55	2.4			
22.0	46	-34.2	-0.06	98	3.5	022			2.96	700	-4.2	0.48	54	2.1			
23.0	40	-33.6	-0.05	98	3.5	022			3.0	686	-4.5	0.48	54	2.1			
24.0	35	-33.0	-0.05	98	3.5	022			4.0	613	-10.4	0.59	52	1.4			
24.0	32	-32.3	-0.07	98	3.5	022			4.177	600	-11.4	0.61	52	1.2			
25.0	29	-31.6	-0.07	98	3.5	022			5.0	538	-16.5	0.61	50	1.8			
26.2	28	-31.5	-0.05	98	3.5	022			5.55	500	-19.6	0.58	49	0.5			
				99	3.5	022			6.0	470	-22.3	0.58	49	0.5			
				99	3.5	022			7.0	411	-27.4	0.51	48	0.4			
				99	3.5	022			7.2	400	-28.4	0.73	46	0.3			
				99	3.5	022			8.0	357	-34.7	0.84	46				
				99	3.5	022			9.0	309	-43.1	0.84	46				
				99	3.5	022			9.2	300	-44.3	0.73	45				
				99	3.5	022			10.0	266	-50.4	0.73	45				
				99	3.5	022			10.28	255	-50.4	0.00	45				
				99	3.5	022			11.0	230	-66.9	-0.49	44				
				99	3.5	022			11.9	200	-84.2	-0.49	44				

23.7 0127 $\varphi = 78^{\circ}52'$ $\lambda = 191^{\circ}18'$

10/10 Sc (26)

315

335

318

318

2

2

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
13.0	197	-44.1	-0.28	44					0.2	888	-2.8	0.00	95	2.9	033	3	
13.0	170	-43.8	-0.03	43					0.35	970	-2.8	-1.47	94	2.9	018	3	
14.0	146	-43.6	-0.02	42					0.5	953	-0.6	-1.11	94	3.6	029	2	
15.0	126	-43.2	-0.04	42					0.68	933	1.4	0.00	94	4.3	005	4	
16.0	109	-42.9	-0.03	41					0.85	900	1.4	0.00	94	4.4	006	4	
16.0	100	-42.8	-0.03	41					1.3	862	1.4	0.00	94	4.4	007	4	
17.0	94	-42.6	-0.03	40					1.41	859	0.8	0.45	89	4.3	007	4	
18.0	80	-41.8	-0.03	39					1.5	844	0.3	0.45	88	4.1	007	4	
19.0	70	-41.2	-0.03	38					1.9	800	-0.9	0.40	80	3.4	003	4	
20.0	60	-40.5	-0.07	38					2.0	790	-1.3	0.40	80	3.4	001	4	
21.0	52	-40.0	-0.05	38					2.5	741	-4.0	0.50	75	2.8	000	5	
22.0	45	-39.2	-0.08	38					2.95	700	-6.0	0.44	69	2.3	014	7	
23.0	39	-38.6	-0.05	38					3.0	695	-6.2	0.44	69	2.3	015	7	
24.0	34	-38.2	-0.04	38					3.18	690	-7.0	0.44	65	2.0	030	8	
25.0	30	-38.2	0.00	38					3.5	653	-7.0	0.00	60	2.0	022	9	
26.0	26	-38.2	0.00	38					4.0	611	-9.6	0.65	58	1.6	030	11	
				38					4.15	600	-10.7	0.65	55	1.5			
				38					5.0	538	-15.6	0.60	51	1.0			
				38					5.52	500	-18.5	0.46	48	0.7			
				38					6.0	469	-22.2	0.66	46	0.5			
				38					7.0	410	-30.0	0.68	43	0.3			
				38					7.17	400	-30.2	0.68	43	0.3			

23.7 1336 $\varphi = 78^{\circ}52'$ $\lambda = 191^{\circ}15'$

7/7 Fs

2

3

2

2

3

Продолж. приложения

24.7 0140 φ=78°51' λ=191°05'

0/0

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
8.0	354	-35.4	0.54	41				248	0.0	015	-2.2	015	93	3.0	1	360	3
9.0	308	-44.2	0.88	39					0.11	000	-2.4	0.20	94	2.9	021	4	
9.17	300	-45.2	0.88	38					0.2	989	-2.6	0.10	95	3.0	019	4	
9.9	289	-50.4	0.62	37				246	0.4	963	-2.8	-0.10	95	3.0	017	4	
10.0	264	-50.4	0.00	37					0.5	951	-2.0	-0.80	87	4.1	009	4	
10.7	238	-48.5	-0.63						0.95	900	1.6	-0.80	85	4.1	006	5	
11.0	227	-48.5	-0.63					241	1.0	894	2.0	-0.80	85	4.2	006	5	
11.84	200	-45.8	-0.30						1.16	877	3.2	-0.75	89	4.3	004	4	
12.0	195	-45.3	-0.30					227	1.41	850	3.2	0.00	79	4.1	011	6	
13.0	168	-44.7	-0.08						1.5	841	3.2	0.00	70	3.9	011	6	
14.0	144	-43.6	-0.11						1.82	809	3.2	0.00	62	3.6	346	6	
15.0	124	-42.8	-0.08					218	1.91	800	2.6	0.67	60	3.4	346	6	
16.0	108	-42.2	-0.06						2.0	790	2.0	0.67	58	3.2	341	5	
17.0	93	-41.4	-0.08					213	2.5	742	-0.6	0.32	48	2.4	330	5	
18.0	80	-40.5	-0.09						2.96	700	-2.3	0.48	44	1.9	332	6	
19.0	70	-39.6	-0.09					214	3.0	686	-3.0	0.48	44	1.9	331	6	330
20.0	60	-39.1	-0.05						4.0	613	-7.0	0.40					
21.0	52	-39.1	0.00						4.17	600	-7.5						
21.11	51	-39.1	0.00						5.0	588	-11.1	0.41					
									5.57	300	-14.2						

Продолж. приложения

24.7 1329 φ=78°51' λ=190°58'

10/10 Sc (46)

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
6.0	472	-16.9	0.58				10	310	0.0	018	-0.3	018	90	3.2	022	3	
7.0	412	-21.9	0.30				9		0.14	000	-1.0	0.14	93	3.2			469
7.2	400	-23.9	0.78				8		0.2	992	-2.2	0.95	94	3.1	024	6	
8.0	359	-29.7	0.78				6		0.3	980	-3.1	0.90	95	2.9	024	6	
9.0	311	-37.7	0.80				10	337	0.5	954	-3.1	0.00	98	3.0			444
9.25	300	-40.0					8		0.6	943	-3.1	0.00	100	3.2			
10.0	269	-45.8	0.81				7		0.97	909	1.1	-1.14	100	4.0			
10.54	248	-51.0	0.56				8		1.0	897	1.1	0.00	99	4.4			
11.0	230	-51.0	0.00				9		1.3	864	1.1	0.00	99	4.0			
11.2	224	-51.0	0.00				10	380	1.44	800	0.6	0.25	79	3.6			
11.55	200	-46.8	-0.55				12		1.5	843	0.6	0.25	70	3.3			
12.0	198	-46.6	-0.55				12		1.92	800	-0.3	0.22	63	2.9			
13.0	172	-44.3	-0.23				10	380	2.0	792	-0.5	0.22	63	2.9			
14.0	148	-43.9	-0.04				9		2.5	744	-1.3	0.16	57	2.6			
15.0	126	-43.4	-0.05				7		3.0	700	-3.1	0.36	52	2.2			
16.0	109	-43.0	-0.04				8										
16.56	100	-42.8	-0.04				8	406									
17.0	94	-42.6	-0.04				7										
18.0	81	-41.5	-0.11				7										
19.0	70	-40.3	-0.12				5										
20.0	60	-39.2	-0.11				5										
21.0	52	-38.6	-0.06				6										
21.2	50	-38.5					6										327

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
4.0	615	-6.1	0.30	42	1.5				20.0	62	-38.4	-0.10					
4.19	600	-7.2	0.28	42	1.5				21.0	54	-37.2	-0.12					
5.0	541	-10.7	0.46	40	1.2				21.5	50	-36.5						385
5.39	500	-14.1	0.39	39	0.9				22.0	47	-36.3	-0.09					
6.0	474	-17.5	0.68	38	0.7				23.0	40	-35.9	-0.04					
7.0	415	-23.6	0.61	36	0.4			313	24.0	34	-35.5	-0.04					
7.26	400	-26.0	0.61	35	0.3				25.0	30	-35.1	-0.04					
8.0	361	-31.7	0.81	34					25.6	28	-34.9	-0.03					384
9.0	313	-40.4	0.87	33													
9.29	300	-42.6	0.89														
10.0	269	-49.3	0.89														
10.72	241	-53.6	0.60														
11.0	232	-53.6	0.00					402	0.0	018	-3.0						
11.96	200	-67.0	0.00						0.14	000	-3.2	0.15	58	2.8	338	1	
12.0	198	-66.8	-0.68						0.2	993	-3.3	0.00	57	2.9	016	5	
13.0	170	-64.5	-0.23						0.38	971	-3.3	0.00	56	2.8	011	4	
14.0	148	-63.8	-0.07					387	0.5	955	-1.4	-1.58	90	3.1	011	7	
15.0	127	-63.1	-0.07						0.6	943	-0.4	-1.00	83	3.2	023	8	
16.0	110	-62.3	-0.08						0.58	900	-0.4	0.00	81	3.3	025	7	
16.6	100	-61.6	-0.11						1.38	857	-0.4	0.00	79	3.4	010	7	
17.0	95	-61.2	-0.11					400	1.44	850	-0.6	0.00	79	3.4	008	7	
18.0	82	-60.2	-0.10						1.5	844	-0.8	0.33	79	3.3	005	7	
19.0	71	-59.4	-0.08						1.92	800	-2.0		77	3.1	355	7	

— 399 —

25.7 0139 φ = 78°50' λ = 190°47'

0/0

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
2.0	791	-2.4	0.32	76	3.0	382	7		16.53	100	-63.0						
2.5	743	-3.8	0.28	74	2.7	385	9		17.0	93	-62.7	-0.07					
2.97	700	-5.2	0.30	67	2.3	392	11	384	18.0	80	-60.9	-0.18					
3.0	689	-5.3	0.17	56	2.0	347	14		18.2	76	-60.9	0.00					316
4.0	614	-7.0	0.17	55	1.9	345	14										
4.19	600	-7.4	0.34	50	1.5	337	14										
5.0	541	-10.4	0.34	47	1.0	331	13										
5.39	500	-13.0	0.55	46	0.9	325	12		0.0	016	-0.4						
6.0	474	-15.9	0.64	43	0.5	321	12	403	0.11	000	-1.0	0.92	94	3.3			
7.0	413	-22.3	0.64	42	0.4				0.2	989	-1.8	0.70	94	2.7			
7.23	400	-24.5	0.76	41					0.5	951	-1.8	0.00	94	3.2	018	2	
8.0	359	-31.2	0.89						0.64	900	-1.8	0.00	94	3.4	011	3	
9.0	311	-33.8	0.76						1.0	893	-1.8	0.00	94	3.4	007	4	
9.25	300	-41.0	0.67						1.12	884	-1.8	0.00	94	3.5	357	6	
10.0	267	-45.5	0.84					454	1.4	850	-2.7	0.37	94	3.3	352	6	
11.0	231	-53.9	0.84						1.5	840	-3.2	0.00	94	3.3	350	6	
11.52	224	-55.2	0.25						1.89	800	-5.0						
11.93	200	-51.4	0.25						2.0	788	-5.8	0.52	94	2.8			
12.0	188	-51.0	-0.88						2.28	768	-7.9	0.75	94	2.4			
13.0	171	-46.8	-0.42						2.5	740	-7.9	0.00	94	2.4			
14.0	147	-45.0	-0.18						3.0	700	-7.9	0.00	71	2.0			
15.0	135	-41.1	-0.09					325	3.04	694	-8.0	0.00	70	2.0			
16.0	108	-60.4	-0.07						3.0	684	-8.0		70	2.0			321

— 400 —

25.7 1334 φ = 78°50' λ = 190°45'

10/10 Sc, Fs

Продолж. приложения

H	B	t	o	l	Y	U	q	d	V	W	H	B	t	l	Y	U	q	d	V	W
4.0	610	-11.6			0.35	55	1.4				18.0	80	-38.5		-0.05	41				317
4.14	600	-12.0			53	1.2					19.0	68	-38.5		0.00	41				
5.0	535	-15.0			0.34	52	1.0				20.0	60	-37.6		-0.09	41				
5.51	600	-18.5			51	0.8					21.0	52	-36.5		-0.11					
6.0	467	-22.0			0.70	50	0.5			278	21.2	50	-36.4							333
7.0	407	-29.0			0.70	49	0.3				22.0	44	-35.9		-0.05					
7.13	400	-29.5			0.84	48					23.0	36	-35.4		-0.05					
8.0	353	-37.4			0.84	48				278	24.0	29	-35.0		-0.04					
9.0	305	-44.2			0.68	47					25.0	24	-34.6		-0.04					418
9.11	300	-45.0			0.68	47					26.0	22	-34.2		-0.04					
10.4	247	-52.1			0.78	46					27.0	20	-33.8		-0.04					
11.0 [*]	224	-48.2			-0.65	45					28.0	18	-33.4		-0.04					
11.78	200	-44.7			-0.65	45					28.4	17	-33.3		-0.03					
12.0	194	-44.2			-0.40	45				308										
13.0	168	-41.8			-0.24	44														
13.34	160	-40.2			-0.47	44														
14.0	144	-40.2			0.00	44				305	0.0	017	0.0							
15.0	124	-40.2			0.00	44					0.11	000	-0.5							
15.5	115	-40.2			0.00	43					0.2	988	-0.8	0.40						
16.0	107	-39.8			-0.08	42					0.5	951	-2.0	0.40						
16.5	100	-39.4			-0.08	42					0.95	900	-3.0							
17.0	93	-39.0			-0.08	42					1.0	894	-3.1	0.22						

26.7 0134 φ = 78°50' λ = 190°33'
10/10 St (16), 9

— 401 —

Продолж. приложения

H	B	t	o	l	Y	U	q	d	V	W	H	B	t	l	Y	U	q	d	V	W	
1.41	850	-3.7									13.0	169	-38.3	0.00							255 J
1.5	841	-3.8			0.14						14.0	147	-38.3	0.00							
1.89	800	-4.7			0.24						15.0	127	-38.3	0.00							257
2.0	788	-5.0			0.24						16.0	110	-38.3	0.00							
2.5	739	-6.0			0.20						16.63	100	-38.3								257
2.93	700	-7.0			0.28					238	17.0	95	-38.3	0.00							
3.0	693	-7.4			0.28																
4.0	609	-12.1			0.47																
4.11	600	-12.6			0.51																
5.0	534	-17.2			0.51					268											
5.5	500	-19.3			0.43						0.0	018	0.0								
6.0	468	-21.5			0.50						0.12	000	-0.5								
7.0	408	-26.5			0.50						0.22	988	-1.9	0.85							
7.13	400	-27.3			0.55						0.5	953	-1.9	0.00							
8.0	354	-32.0			0.72					250	0.9	907	-1.9	0.00							
9.0	306	-39.2			0.72						0.97	900	-2.3	0.50							
9.15	300	-40.0			0.86						1.0	895	-2.4	0.50							
9.35	271	-44.0			0.86						1.43	850	-3.7	0.32							
10.0	265	-44.0			0.80						1.5	842	-4.0	0.32							
10.54	244	-44.0			0.80					250	1.91	800	-6.2	0.54							
11.0	223	-41.3			-0.59						2.0	790	-6.7	0.64							
11.88	200	-38.3			-0.54						2.5	741	-9.9	0.64							
12.0	195	-38.3			-0.40						2.95	700	-12.0	0.78							

26.7 1332 φ = 78°51' λ = 190°28'
5/5 Fs

— 402 —

Продолж. приложения

— 403 —

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
3.0	695	-12.3	0.48	79	1.5			348	20.0	60	-38.5	-0.05					
4.0	699	-18.4	0.61	74	0.9				20.73	54	-38.2	-0.04					330
5.0	531	-23.0	0.46	70	0.6												
5.43	500	-25.9	0.85	68	0.3												
6.0	461	-29.5	0.73	59	0.1												
7.0	409	-35.6															
7.03	409	-37.0						377	0.0	019	-0.0		100	3.7	360	4	
7.55	379	-41.0	0.75						0.2	992	-0.6	0.30	58	3.7			
8.0	346	-41.0	0.60						0.5	957	-0.6	0.00	58	3.6			
9.0	300	-41.0	0.60						1.0	900	-0.6	0.00	52	3.8			
10.0	259	-39.6	-0.12					396	1.1	889	-0.6	0.00	91	3.7			
11.0	224	-38.2	-0.16						1.45	850	-1.6	0.30	85	3.4			
11.8	200	-38.3							1.5	845	-1.8	0.30	85	3.2			
12.0	194	-38.4	0.02						1.93	800	-4.3	0.62	80	2.6			
13.0	158	-38.3	0.04					371	2.0	792	-4.9	0.62	80	2.6			
14.0	144	-39.3	0.05						2.5	743	-10.2	1.06	80	1.7			
15.0	124	-39.6	0.03						2.64	730	-11.3	0.79	80	1.6			
16.0	107	-39.6	0.00						2.97	700	-11.3	0.00	80	1.6			
16.43	100	-39.6							3.0	697	-11.3	0.00	80	1.6			
17.0	82	-39.6	0.04					376	3.14	685	-11.3	0.00	78	1.6		330	
18.0	80	-39.4	-0.02						4.0	611	-15.9	0.54	69	1.1			
19.0	70	-39.0	-0.04						4.14	600	-16.8		67	0.9			

27.7 0122 φ=78°50' λ=190°20'
10/10 St (9)

Продолж. приложения

— 404 —

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
5.0	535	-21.6	0.37	63	0.6				21.45	50	-35.9	-0.04					
5.49	500	-24.2	0.56	60	0.5				22.0	46	-35.7	-0.05					284
6.0	465	-27.2	0.79	57	0.4			328	23.0	40	-35.2	-0.05					
7.0	405	-35.1	0.79	56					24.0	35	-34.9	-0.03					
7.09	400	-35.6							25.0	30	-34.4	-0.05					286
8.0	350	-42.4	0.73	55													
8.37	317	-42.4	0.60	54				314									
9.0	304	-41.7	-0.21	53													
9.07	300	-41.6							0.0	018	0.2		03	3.4	338	3	
10.0	261	-39.4	-0.23	52					0.15	000	-0.3		82	3.4	380	5	
11.0	225	-37.5	-0.19	50					0.2	898	-0.9	0.55	91	3.3	382	6	
11.21	200	-37.5							0.45	892	-3.1	0.85	90	2.8			
12.0	195	-37.5	0.00	49				278	0.5	896	-3.1	0.00	88	2.8			
13.0	169	-37.5	0.00	48					0.62	942	-3.1	0.00	88	2.8			
14.0	146	-37.5	0.00	46				274	0.81	920	-1.7	-0.74	87	3.2			
15.0	125	-37.5	0.00	45					1.0	900	-1.7	0.00	82	3.0			
16.0	109	-37.5	0.00	44					1.45	850	-1.7	0.00	75	3.0			
16.6	100	-37.5						277	1.5	845	-1.7	0.00	63	2.5			
17.0	95	-37.5	0.00	43					1.77	816	-1.7	0.00	62	2.1			
18.0	82	-37.2	-0.03	42					1.93	800	-3.0	0.65	50	1.8			
19.0	72	-36.8	-0.04	41				284	2.0	792	-3.2	0.65	50	1.9			
20.0	62	-36.4	-0.04	40					2.5	743	-7.7	0.90	50	1.4			
21.0	54	-36.1	-0.03														

27.7 1832 φ=78°48' λ=190°11'
10/9 Fs (47), Cl, Δ

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.96	700	-11.2		50	1.0				16.65	100	-37.0	-0.07					245
3.0	695	-11.4	0.74	50	1.0				17.0	95	-36.7	-0.07					
3.44	657	-15.3	0.89	50	0.7				18.0	82	-35.9	-0.08					247
4.0	611	-16.6	0.23	50	0.7				19.0	71	-35.8	-0.01					
4.13	600	-16.7	0.08	49	0.7				20.0	62	-34.8	-0.10					352
5.0	533	-21.8	0.59	48	0.5				21.0	53	-33.8	-0.10					
5.46	500	-24.6		47	0.4												
6.0	463	-28.4	0.66	46	0.3												
7.0	403	-34.6	0.62	44													
7.05	400	-34.8		44													
8.0	350	-40.3	0.57	43					0.0	019	-2.0		59	3.1	338		
9.0	303	-45.3	0.50	41					0.08	008	-2.7	0.88	97	3.0			
9.06	300	-45.6		40					0.15	000	-2.7		96	3.0			
9.18	295	-46.1	0.44	40					0.2	893	-2.7	0.00	95	3.0			
9.5	281	-46.1	0.00	40					0.3	891	-2.7	0.00	94	3.0			
10.0	260	-43.8	-0.46	39					0.5	857	-1.3	-0.70	91	3.3			
11.0	224	-39.7	-0.41	38					0.99	800	-1.3	0.00	82	3.1			
11.76	200	-38.8		37					1.24	872	-1.3	0.00	74	2.9			
12.0	193	-38.8	-0.09	37					1.44	850	-2.2	0.42	71	2.6			
13.0	167	-38.5	-0.03	36					1.5	843	-2.4		67	2.1			
14.0	145	-38.2	-0.03	35					1.91	800	-5.0	0.62	66	2.0			
15.0	125	-37.8	-0.04						2.0	790	-5.5		60	1.6			
16.0	109	-37.4	-0.04						2.5	734	-8.1	0.52	60	1.6			

— 405 —

28.7 0121 $\varphi = 78^{\circ}46'$ $\lambda = 190^{\circ}05'$

10/10 Sc (12), Ξ

4

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.95	700	-10.0		56	1.3				17.0	92	-39.0	-0.06					200
3.0	695	-10.1	0.40	55	1.3				18.0	80	-38.6	-0.04					
4.0	611	-14.3	0.42	54	1.0				19.0	69	-38.2	-0.04					220
4.14	600	-15.0	0.64	54	0.9				20.0	60	-37.7	-0.05					
5.0	535	-20.5	0.62	54	0.6				21.0	51	-37.6	-0.01					
5.48	500	-23.6		54	0.5				21.15	50	-37.6						
6.0	465	-26.1	0.56	54	0.4				21.5	47	-37.6	0.00					223
7.0	405	-33.3	0.72	54													
7.09	400	-34.0		54													
8.0	353	-40.9	0.76	53													
8.9	338	-46.6	0.63	49					0.0	018	0.2		96	3.5	338		
9.0	334	-46.6	0.00	48					0.15	000	-0.5		95	3.5			
9.03	300	-46.6		48					0.2	899	-0.9	0.55	93	3.4			
10.0	260	-46.6	0.00	46					0.42	867	-2.5	0.73	94	2.9			
10.2	252	-46.6	0.00						0.5	857	-2.5	0.00	93	3.1			
11.0	224	-42.6	-0.50						0.6	845	-2.5	0.00	91	3.5			
11.74	200	-41.3							0.8	821	-1.1	-0.70	91	3.5			
12.0	192	-41.0	-0.16						0.99	800	-1.1	0.00	90	3.5			
13.0	166	-40.6	-0.04						1.43	850	-1.1	0.00	83	3.4			
14.0	143	-40.6	0.00						1.5	844	-1.1	0.00	81	3.4			
15.0	122	-40.2	-0.04						1.91	800	-3.6	0.62	76	2.8			
16.0	106	-39.6	-0.06						2.0	790	-4.2	0.82	75	2.6			
16.49	100	-39.4							2.5	743	-8.3	0.62	71	1.8			

— 406 —

28.7 1940 $\varphi = 78^{\circ}45'$ $\lambda = 190^{\circ}04'$

10/10 St (14)

5

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
2.84	711	-6.8	-0.44	68	2.0				17.0	53	-37.4	-0.03	40				
2.96	700	-7.1	0.31	66	2.0				18.0	80	-36.5	-0.09	40				
3.0	695	-7.3	0.31	66	1.9		398		19.0	70	-35.8	-0.07	39				380
4.0	611	-10.9	0.38	56	1.4				20.0	59	-35.4	-0.04	38				
4.14	600	-11.7	0.55	55	1.3				21.0	50	-34.9	-0.05	38				
5.0	535	-17.0	0.61	52	0.8				22.0	43	-34.7	-0.02	37				
5.51	500	-20.2	0.51	0.7					23.0	37	-34.7	0.00	37				
6.0	469	-22.7	0.57	50	0.5		342		24.0	32	-34.2	-0.05	37				
7.0	408	-29.3	0.66	47	0.3				25.0	28	-33.7	-0.05	36				
7.14	400	-30.2	0.66	46					26.0	25	-33.3	-0.04	35				443
8.0	353	-35.3	0.60	45					26.1	24	-33.2	-0.10	35				
9.0	306	-44.3	0.30	45													
9.13	300	-45.3		45													
10.0	253	-50.0	0.57	45													
10.3	251	-50.8	0.27	44													
11.0	226	-46.7	-0.50	41													
11.8	200	-42.3		43					0.0	620	-0.4		100		338	3	
12.0	194	-41.5	-0.52	43					0.13	600	-1.5						
13.0	168	-40.2	-0.13	43			335		0.2	594	-1.8	0.70					
14.0	144	-39.4	-0.08	42					0.25	575	-2.7	0.60					
15.0	124	-38.7	-0.07	42					0.5	557	-2.7	0.00					
16.0	108	-38.2	-0.05	41					1.0	500	-2.7	0.00					
16.5	100	-37.8		41			337		1.41	454	-2.7	0.00					

29.7 0121 φ = 78°44' λ = 190°03'

10/10 ≡ (6), 9

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W
1.5	844	-3.0							15.0	124	-40.6	-0.05					
1.93	800	-5.3							16.0	107	-39.3	-0.13					282
2.0	792	-5.9	0.54						16.46	100	-38.8						
2.5	743	-5.9	0.00						17.0	92	-38.4	-0.09					
2.8	716	-5.9	0.00						18.0	80	-38.0	-0.04					
2.97	700	-5.6					371		19.0	70	-37.5	-0.05					255
3.0	697	-5.8	0.45						19.3	65	-37.3	-0.07					
4.0	611	-11.8	0.50														
4.13	600	-12.5															
5.0	535	-17.9	0.61														
5.53	500	-21.6															
6.0	469	-25.4	0.75														
7.0	407	-33.2	0.78														
7.12	400	-34.0					353										
8.0	352	-39.8	0.66														
9.0	304	-47.1	0.73														
9.09	300	-47.6					337										
10.0	251	-52.3	0.52														
11.0	224	-45.0	-0.72														
11.77	200	-42.3															
12.0	193	-42.1	-0.20														
13.0	167	-41.7	-0.04				297										
14.0	144	-41.1	-0.06														

29.7 1326 φ = 78°48' λ = 190°00'

10/10 Sc (68)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	695	-5.4	0.30	70	2.4			316	18.0	82	-35.4	-0.11					
4.0	613	-10.0	0.46	58	1.6				20.0	72	-34.6	-0.68					216
4.17	600	-10.8	0.57	57	1.4				20.0	62	-33.6	-0.68					
5.0	539	-16.3	0.63	53	0.9				21.0	54	-33.2	-0.86					182
5.55	500	-18.2	0.63	52	0.7			319	21.4	50	-32.6	-0.86					
6.0	471	-22.6	0.63	51	0.6				22.0	46	-32.3	-0.80					
7.0	410	-29.2	0.66	49	0.3				23.0	41	-30.7	-0.16					185
7.2	400	-30.5	0.66	49	0.3				23.25	40	-30.7	-0.40					
8.0	355	-37.2	0.80	47					30.7	0141	φ=78°43' λ=190°01'						
9.0	308	-44.4	0.72	45					10/10 Sc (79)								
9.17	300	-46.3	0.68	44					0.0	020	0.0	3.5	248	1			
9.9	298	-50.5	0.68	44					0.14	000	-0.6	95	3.5	—			
10.0	255	-50.5	0.00	44					0.2	922	-1.0	93	3.4	261	5		
10.6	242	-50.5	0.00	44					0.5	955	-3.0	89	2.8	263	4		
11.0	228	-47.5	-0.75						0.8	920	-5.2	0.73	89	2.4			
11.87	200	-42.2	-0.75					285	0.8	920	-5.2	0.73	89	2.4			
12.0	196	-41.9	-0.56						0.98	900	-3.7	-0.83	89	2.8			
13.0	168	-40.4	-0.15					292	1.44	850	-2.6	-0.23	79	2.9			
14.0	146	-39.3	-0.11						1.5	844	-2.5	-0.23	78	2.8			
15.0	127	-38.6	-0.07						1.83	800	-3.2	0.16	63	2.4			
16.0	110	-37.8	-0.08					227	2.0	793	-3.3	0.16	63	2.3			
16.6	100	-37.0	-0.13						2.5	744	-4.3	0.20	46	1.6			
17.0	95	-36.5	-0.13														

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.89	700	-6.0	0.35	36	1.2			384	18.0	80	-38.0	-0.15					316
4.0	614	-12.0	0.59	31	0.7				19.0	70	-37.0	-0.10					
4.19	600	-12.5	0.30	0.7					20.0	60	-36.7	-0.03					297
5.0	538	-17.8	0.58	27	0.4				21.0	52	-36.7	0.00					
5.55	500	-21.0	0.59	27	0.3				21.3	50	-36.7	0.00					
6.0	470	-23.7	0.59	26	0.3				22.0	46	-36.7	0.00					297
7.0	408	-31.2	0.75	25	0.3				23.0	40	-36.7	0.00					
7.15	400	-32.6	0.74	23				400	30.7	1311	φ=78°43' λ=190°01'						
8.0	353	-38.6	0.73	23					10/10 Sc (48)								
9.0	305	-45.9	0.73	23					0.0	021	-0.8	97	3.4	270	3		
9.13	300	-46.7	0.74	23					0.17	000	-2.0	96	3.1	268	4		
9.84	270	-52.1	0.74	23					0.2	995	-2.2	0.70	96	3.1	265	4	
10.0	253	-52.1	0.00	23				391	0.5	959	-5.3	1.03	100	2.6			
10.2	256	-52.1	0.00	23					0.7	935	-5.3	0.00	100	2.6			
11.0	225	-47.4	-0.59	23					1.47	850	-0.5	-1.55	97	4.0			
11.8	200	-43.6	-0.30	23					1.01	900	-0.5	0.00	84	3.6			
12.0	194	-43.5	-0.30	23					1.47	850	-0.5	0.00	83	3.6			
13.0	168	-42.8	-0.07	23				340	1.5	847	-0.5	0.00	68	2.7			
14.0	144	-42.0	-0.08	23					1.95	800	-1.8	0.00	67	2.7			
15.0	124	-41.2	-0.08	23					2.0	794	-2.0	0.30	61	2.4			
16.0	107	-39.5	-0.07						2.5	745	-3.5	0.20	61	2.4			
16.6	100	-39.5	-0.07						3.0	700	-6.6	0.62	57	1.8			
17.0	93	-39.5	0.00														310

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
4.0	615	-12.3	0.57	48.	1.0				0.4	973	-5.0	0.86	93	2.4			
4.19	600	-13.0							0.5	951	-5.0	0.00	94	2.4			
5.0	538	-17.3	0.50						0.54	956	-5.0	0.00	94	2.4			
5.53	500	-21.8				267			0.72	935	-0.2	-2.67	90	3.5			
6.0	469	-25.6	+0.83						1.0	903	-0.2	0.00	83	3.4			
7.0	408	-32.6	0.70						1.03	900	-0.2	0.00	82	3.4			
7.13	400	-32.7							1.49	859	-0.2	0.00	69	3.1			
8.0	354	-40.3	0.77			228			1.97	800	-1.7	0.00	65	2.7			
9.0	305	-49.0	0.87						2.0	797	-1.8	0.53	64	2.6			
9.5	292	-51.7	0.54						2.5	748	-3.7	0.38	55	2.0			
10.0	292	-51.7	0.00			222			3.0	702	-5.9	0.44	53	1.7			307
10.24	252	-51.7	0.00						3.03	700	-6.0	0.00	53	1.7			
11.0	224	-46.7	-0.66						4.0	618	-11.7	0.88	48	1.1			
11.76	200	-44.2							4.23	600	-12.6	0.00	47	1.0			
12.0	193	-43.7	-0.30			217			5.0	541	-16.4	0.47	46	0.8			290
12.4	182	-42.8	-0.23						5.6	500	-19.1	0.00	45	0.8			
									6.0	473	-23.2	0.60					
									7.0	412	-29.5	0.62					
									7.2	400	-30.9	0.80					
									8.0	358	-37.5	0.80					
0.0	000	-2.6		80	2.7	270	2		9.0	309	-44.2	0.67					250
0.19		-3.2		0.32	0.1	2.7			9.21	300	-45.3						

31.7 0130 $\varphi = 78^{\circ}43'$ $\lambda = 190^{\circ}04'$
10/10 Sc (30)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
10.0	266	-50.6	0.64						0.5	953	-5.6	0.73	91	2.3	186		
10.1	262	-50.7	0.10						0.8	928	0.0	-1.87	86	3.5	124	2	
10.8	235	-50.7	0.00			263			1.0	905	0.0	0.00	83	3.5	102	2	
11.0	228	-49.5	-0.60						1.05	900	0.0	0.00	83	3.5	103	2	
11.85	200	-44.7							1.3	871	0.0	0.00	80	3.4	106	2	
12.0	195	-44.3	-0.52						1.5	850	-0.6	0.30	73	3.1	106	3	
13.0	169	-42.8	-0.15						1.98	800	-2.2	0.33	68	2.7	099	2	
14.0	146	-41.9	-0.09						2.5	745	-4.0	0.35	63	2.4			268
15.0	126	-41.3	-0.05						3.01	700	-7.2	0.63	63	1.9			
16.0	108	-40.8	-0.05			240			4.0	617	-11.9	0.47	60	1.3			
16.6	100	-40.5							4.2	600	-13.0	0.00	59	1.2			
17.0	94	-40.0	-0.08						5.0	540	-16.7	0.48	57	1.0			257
18.0	81	-38.9	-0.11						5.6	500	-21.6	0.77	55	0.6			
19.0	70	-38.2	-0.07			268			6.0	472	-24.4	0.77	55	0.6			
20.0	60	-37.6	-0.06						7.0	410	-31.2	0.68	53				260
21.0	52	-37.1	-0.05						7.21	400	-32.4	0.68	53				
21.3	50	-37.1							8.0	357	-38.3	0.71	51				
22.0	45	-37.1	0.00			250			9.0	307	-45.8	0.75	50				
									9.19	300	-47.1	0.62	50				
									10.0	265	-52.0	0.62					
									10.23	256	-53.7	0.74					
									10.61	242	-53.7	0.00					
									11.0	228	-51.4	-0.53					

31.7 1325 $\varphi = 78^{\circ}44'$ $\lambda = 190^{\circ}08'$
10/10 Sc (44) $\frac{1}{2}$

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
11.85	200	-47.0							0.5	967	-2.0		-0.10	84	2.8		
12.0	105	-46.5	-0.40				240		0.75	938	-1.8		-0.08	78	2.6		
13.0	168	-44.5	-0.20						0.89	922	-0.3		-1.07	67	2.7		
14.0	146	-43.7	-0.68						1.0	909	-0.3		0.00	65	2.6		
15.0	125	-42.8	-0.69				240		1.08	900	-0.3		0.00	63	2.6		
16.0	107	-41.7	-0.11						1.35	870	-0.3		0.00	60	2.5		
16.52	100	-41.2							1.3	853	-0.6		0.20	55	2.4		
17.0	83	-40.8	-0.09						1.53	850	-0.7		0.20	54	2.3		
18.0	70	-39.4	-0.07				270		2.0	800	-1.6		0.20	48	2.0		
20.0	60	-37.9	-0.15						3.0	705	-3.0		0.28	45	1.8		
21.0	51	-37.0	-0.09				270		3.05	700	-5.7		0.48	39	1.3		
21.12	50	-36.9							4.0	620	-10.6		0.52	32	0.8		
22.0	44	-36.5	-0.05						4.25	600	-11.8		0.00	30	0.7		
23.0	38	-36.5	0.00				272		5.0	544	-17.4		0.68	30	0.4		
24.0	33	-36.5	0.00						5.63	500	-20.7		0.00	30	0.3		
24.73	29	-36.5	0.00				67		6.0	475	-23.0		0.55	30	0.3		
									7.0	414	-30.4		0.74	30	0.3		
									7.24	400	-31.6		0.72				
									8.0	359	-37.6		0.71				
0.0	029	-2.4							9.0	310	-44.7		0.71				
0.2	004	-2.3							9.2	300	-46.2		0.68				
0.23	000	-2.3							10.0	285	-51.5						

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302

300

1.8 0156 $\varphi = 78^{\circ}45'$ $\lambda = 190^{\circ}10'$
10/10 St (96) Δ°

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
10.44	248	-55.1	0.82						1.05	900	0.4		79	3.5			
10.8	235	-55.1	0.00						1.52	850	0.4		0.00	72	3.4		
11.0	228	-53.5	-0.80						1.8	820	0.4		0.00	65	3.2		
11.87	200	-48.0					316		2.0	800	-0.2		0.20	62	3.0		
12.0	196	-47.5	-0.59						2.5	780	-0.2		0.36	54	2.3		
13.0	168	-44.0	-0.36						3.0	765	-3.3		0.20	49	2.0		
14.0	145	-43.0	-0.10				313		3.05	700	-3.7		0.64	49	2.0		
15.0	125	-43.0	0.00						4.0	620	-9.9		0.00	52	1.2		
16.0	107	-41.9	-0.11						4.25	600	-11.3		0.60	56	1.0		
16.53	100	-41.2							5.0	544	-15.9		0.00	50	0.8		
17.0	92	-40.7	-0.12						5.63	500	-19.1		0.47	50	0.7		
18.0	80	-39.6	-0.11						6.0	476	-20.6		0.59	54	0.4		
19.0	69	-38.5	-0.11						7.0	415	-26.5		0.70	53			
19.9	61	-38.5	0.00				323		7.27	400	-28.0		0.70	53			
									8.0	360	-33.5		0.57	51			
									9.0	312	-42.2		0.57	51			
									9.28	300	-44.2		0.59	49			
									10.0	268	-49.1		0.00				
0.0	029	-1.0							10.7	241	-53.0		0.00				
0.21	009	-2.0	0.48				3		11.0	229	-53.0		0.00				
0.3	024	-3.0	0.50				6		11.52	200	-44.9		-0.84				
0.9	016	0.4	-1.03				3		12.0	197	-46.6		-0.84				
1.0	507	0.4	0.00				3		13.0	171	-62.3		-0.23				

312

312

329

302

1.8 1341 $\varphi = 78^{\circ}46'$ $\lambda = 190^{\circ}10'$
10/10 St

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
14.0	147	-41.4	-0.00					285	1.99	890	0.5	0.12	65	3.2												
15.0	127	-40.0	-0.14						2.5	794	-0.8	0.23	63	3.0												331
16.0	110	-39.0	-0.10						3.0	794	-3.6	0.36	63	2.6												
16.62	100	-38.5							3.05	700	-3.9		63	2.5												
17.0	95	-38.2	-0.08					260	4.0	619	(-8.6)	0.32	70	2.0												
18.0	82	-37.5	-0.07						4.24	619	-9.7		68	2.0												
19.0	71	-36.4	-0.11						5.0	514	-13.7	0.49	62	1.4												
20.0	61	-35.5	-0.09					259	5.64	508	-15.7		61	1.2												
21.0	54	-34.6	-0.09						6.0	475	-18.2	0.75	60	0.7												
21.4	50	-34.3							7.0	415	-23.2	0.70	59	0.4												332
22.0	46	-33.8	-0.08					259	7.27	408	-23.4		57	0.3												
22.3	44	-33.6	-0.07						8.0	390	-33.6	0.54	55													
									9.0	312	-40.5	0.69	54													
									10.0	289	-47.5	0.70	54													378
									11.0	259	-50.7	0.64	54													
									12.0	222	-50.7	0.00	54													
									13.0	200	-46.4															
									14.0	170	-46.1	-0.61														383
									15.0	147	-43.6	-0.25														
									16.0	126	-42.0	-0.11														
									17.0	102	-42.0	-0.05														
									18.0	79	-42.0	-0.05														
									19.0	58	-42.0	-0.05														
									20.0	38	-42.0	-0.05														
									21.0	19	-42.0	-0.05														
									22.0	10	-42.0	-0.05														
									23.0	5	-42.0	-0.05														

2.8 0133 φ = 78°50' λ = 190°02'

10/10 St (10)

H	B	t	Y	U	q	d	V	W
0.0	028	-1.2		92	3.1	112		
0.2	000	-1.5	0.15	90	3.1			5
0.5	*955	0.7	-0.73	89	3.6			
0.75	835	1.8	-0.44	87	4.1			
1.0	905	1.8	0.00	83	4.0			
1.05	900	1.7	0.00	81	3.8			
1.5	850	1.1	0.14	70	3.4			

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	
16.0	109	-41.4	-0.06						4.0	616	-10.5	0.58	46	1.2	172	15											
16.6	100	-41.0						216	4.2	690	-11.7		45	1.1	172	15											
17.0	94	-40.7	-0.07						5.0	540	-17.5	0.70	42	0.6	181	12											
18.0	82	-39.8	-0.09					215	5.57	500	-21.3		42	0.5	183	10										377	
19.0	71	-39.2	-0.06						6.0	471	-23.8	0.63	41	0.4	185	10											
20.0	61	-39.2	0.00						7.0	411	-31.2	0.74	41														
21.0	53	-39.2	0.00						7.2	400	-32.7		41														
21.4	50	-39.2							8.0	356	-38.3	0.71	40														
22.0	46	-39.2	0.00					209	8.0	306	-46.6	0.70	39														
									9.15	300	-46.6		39														
									10.0	285	-52.0	0.67	39														388
									10.25	255	-52.0	0.00	39														
									11.0	227	-48.3	-0.49	38														
									11.9	200	-43.8		37														
									12.0	196	-43.6	-0.47	37														
									13.0	168	-42.2	-0.14	36														386
									14.0	145	-41.4	-0.08	35														
									15.0	125	-40.8	-0.06	34														
									16.0	108	-39.8	-0.10	34														272
									16.5	100	-39.4		34														
									17.0	93	-39.0		34														
									18.0	81	-38.0	-0.08	34														
									19.0	69	-37.0	-0.10	34														262

2.8 1321 φ = 78°52' λ = 190°00'

5/0 Cc, Ci, Cs

H	B	t	Y	U	q	d	V	W
0.0	022	0.6		92	3.6	135		5
0.17	000	0.9		91	3.7	150		10
0.2	996	1.0	-0.20	91	3.7	153		11
0.5	959	2.6	-0.33	91	4.4	167		12
0.9	913	2.6	0.00	79	3.7	167		13
1.02	900	2.3	0.23	74	3.8	165		13
1.5	850	0.8	0.31	66	3.2	164		14
1.98	800	-1.2	0.42	56	2.5	164		15
2.5	719	-2.5	0.25	54	2.2	169		14
3.02	700	-4.8		50	1.8	170		14

Проблеск, приложение

H	B	t	T	U	q	d	V	W	H	B	T	t	U	q	d	V	W
3.8 0120 $\varphi = 78^{\circ}54'$ $\lambda = 190^{\circ}03'$																	
10/10 St (8)																	
0.0	020	-0.2	08	3.6	138	8			9.0	307	-47.7	0.52					292
0.16	000	-0.5	69	3.7					9.16	300	-49.0						
0.2	985	-0.6	0.20	89	3.7				9.75	274	-83.2	0.73					
0.36	975	3.5	-2.55	100	3.0				10.0	264	-83.2	0.00					
0.5	658	3.5	0.00	80	4.6				10.36	250	-83.2	0.00					
1.0	900	3.5	0.00	69	3.7				11.0	226	-47.5	-0.89					
1.47	859	1.2	0.00	61	2.9				11.82	200	-44.2						253
1.5	847	1.0	0.50	61	2.9				12.0	194	-44.1	-0.34					
1.95	800	-1.3	0.48	70	2.0				13.0	188	-63.4	-0.07					260
2.0	794	-1.4	0.48	70	2.0				14.0	144	-62.0	-0.07					
2.5	748	-3.9	0.50	70	2.6				15.0	124	-62.0	-0.07					
3.0	700	-6.0	0.54	70	2.2		325		15.9	108	-41.4	-0.06					
4.0	615	-11.4	0.46	54	1.2				16.3	100	-40.3						
4.2	606	-12.4	0.46	54	1.2				17.0	93	-40.3	-0.11					
5.0	590	-18.3	0.69	50	0.7				18.0	80	-39.8	-0.05					
5.27	500	-20.7	0.50	48	0.6				18.45	75	-39.8	0.00					280
6.0	471	-23.3	0.50	46	0.5		330		3.8 1335 $\varphi = 78^{\circ}59'$ $\lambda = 190^{\circ}05'$								
7.0	412	-29.9	0.56	45	0.3				10/10 St (8)								
7.2	400	-31.4							0.0	017	0.4		94	3.7	158	9	
8.0	355	-38.5	0.86						0.08	007	0.1	0.38	93	3.5			
									0.14	000	0.1		93	3.5			
									0.2	992	0.1		92	3.6			

Проблеск, приложение

H	B	t	T	U	q	d	V	W	H	B	T	t	U	q	d	V	W
0.27	984	0.1	0.00	80	3.5				9.15	300	-44.5						
0.5	957	4.3	-1.87	88	4.3				10.0	264	-47.9	0.42					
0.84	917	4.4	0.60	83	4.7				10.13	250	-48.3	0.31					239
0.99	900	3.7	0.47	82	4.6				10.65	240	-48.3	0.00					
1.45	850	1.3	0.77	77	3.8				11.0	228	-47.1	-0.34					
1.5	845	1.0	0.53	76	3.6				11.88	200	-44.0						
1.65	829	0.1	0.60	74	3.4				12.0	196	-43.8	-0.33					245
1.93	800	-0.6	0.33	74	3.4				13.0	169	-42.4	-0.14					
2.0	793	-0.7	0.33	74	3.4				14.0	146	-41.3	-0.05					
2.21	755	-1.3	0.29	74	3.3				15.0	135	-41.3	-0.05					
2.5	745	-2.5	0.41	74	3.0				16.0	108	-40.8	-0.05					
2.99	700	-5.3	0.57	74	2.6		289		16.28	100	-40.4						
4.0	614	-13.2	0.78	76	1.6				17.0	84	-40.1	-0.07					
4.18	600	-14.1	0.50	79	1.5				18.0	81	-39.4	-0.07					254
4.5	576	-14.7	0.19	84	1.6				19.0	71	-38.9	-0.05					
4.8	554	-15.5	0.27	82	1.5				20.0	61	-38.3	-0.05					
5.0	539	-16.4	0.45	80	1.4				21.0	53	-37.5	-0.08					285
5.56	500	-20.5	0.76	76	0.9				21.46	48	-37.2						
6.0	471	-24.2	0.78	72	0.6		332		22.0	39	-36.8	-0.07					
7.0	411	-31.0	0.68	64					23.0	29	-36.8	0.00					313
7.18	400	-32.0							24.0	23	-36.8	0.00					
8.0	355	-37.3	0.63						24.94	23	-36.8	0.00					309
9.0	307	-43.7	0.64														

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	T	t	U	q	d	V	W
4.8 0125 $\varphi = 79^{\circ}00'$ $\lambda = 190^{\circ}06'$																	
10/10 St (4)																	
0.0	015	0.0	0.0	39	3.7	158	7		3.15	528	-18.1	0.53	51	0.8			
0.11	020	-0.3	0.45	90	3.5				5.35	500	-19.1	0.23	51	0.7			
0.2	899	-0.3	0.00	94	3.4				5.8	483	-19.6	0.23	51	0.7			821
0.35	892	-0.3	0.00	89	3.4				7.0	470	-20.6	0.20	51	0.7			
0.5	893	4.6	0.00	88	4.8				7.19	400	-27.1	0.39	51	0.7			
0.56	896	5.2	-1.90	88	5.0				8.0	357	-31.0	0.45					
0.80	900	5.2	0.00	81	4.9				9.24	300	-35.5	0.68					
0.85	900	4.8	0.00	80	4.9				10.0	267	-47.1	0.53					322
1.0	899	4.5	0.00	80	4.7				11.32	219	-54.0	0.60					
1.42	850	2.3	0.63	76	4.1				11.91	200	-49.6	0.00					
1.5	841	1.5	0.63	75	3.8				12.0	197	-49.1	-0.72					
1.9	800	-0.6	0.54	71	3.3				13.0	169	-45.0	-0.41					
2.0	789	-1.2	0.54	71	3.2				14.0	146	-43.9	-0.11					
2.5	742	-3.1	0.38	49	2.0				15.0	125	-42.8	-0.11					
2.86	700	-4.7	0.34	41	1.6				16.0	108	-42.1	-0.07					
3.0	697	-4.8	0.34	41	1.5				16.59	100	-41.6	-0.07					300
3.5	655	-7.1	0.46	37	1.2				17.0	94	-41.4	-0.07					
4.0	613	-10.3	0.64	39	1.0				18.0	83	-40.8	-0.06					
4.17	600	-11.3	0.64	42	1.0				19.0	72	-40.1	-0.07					
5.0	539	-17.3	0.70	51	0.8				20.0	62	-39.4	-0.07					

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	T	t	U	q	d	V	W
4.8 1320 $\varphi = 79^{\circ}08'$ $\lambda = 190^{\circ}10'$																	
10/10 Ns, Es, °																	
0.0	010	0.4	0.00	100		158	7		4.0	610	-11.5	0.60					
0.07	000	0.8	-0.60						4.14	600	-12.5	0.46					
0.2	984	1.6	-3.00						5.0	535	-16.1	0.46					
0.3	971	4.6	0.00						5.52	500	-17.9	0.34					277
0.5	948	4.6	0.00						6.0	468	-19.5	0.41					
0.75	920	4.6	0.00						7.0	409	-23.6	0.41					
0.89	900	4.0	0.36						7.17	400	-24.9	0.69					
1.0	891	3.7	0.36						8.0	355	-30.5	0.86					311
1.39	850	1.9	0.46						9.0	309	-39.1	0.86					
1.5	839	1.4	0.46						9.2	300	-40.7	0.82					
1.87	800	-0.2	0.43						9.93	269	-46.7	0.82					
2.0	797	-0.5	0.33						10.0	265	-46.7	0.00					
2.5	740	-1.7	0.24						10.8	236	-45.7	0.00					
2.94	700	-4.9	0.16						11.0	228	-45.7	-0.50					
3.0	694	-5.5	0.16						11.91	200	-44.8	-0.40					
									12.0	198	-44.8	-0.09					
									13.0	171	-40.8	-0.11					
									14.0	148	-39.7	-0.11					
									15.0	128	-38.3	-0.14					
									16.0	110	-37.0	-0.13					
									16.35	100	-36.6	-0.08					
									17.0	93	-36.2	-0.08					
									17.5	84	-35.6	-0.10					

Продолж. приложения

5.8 1330 $\varphi = 79^{\circ}14'$ $\lambda = 190^{\circ}17'$
10/10 St. 9

H	B	t	Y	U	q	d	V	W	H	B	T	t	U	q	d	V	W
0.0	005	0.2		100	3.8	302	4		5.0	534	-15.6	0.58	51	1.0			
0.05	000	0.1	0.30	100	3.8				5.49	500	-18.7		51	0.8			275
0.1	985	-0.1	0.00	100	3.9				6.0	467	-22.4	0.68	51	0.6			
0.2	840	-0.1	0.00	100	4.0				7.0	407	-27.5	0.51	51	0.4			
0.3	945	-0.1	0.00	100	4.0				8.0	353	-33.7	0.62	50				
0.45	965	-0.1	0.00	100	4.2				9.0	306	-39.9	0.62	48				
0.5	860	0.2	-0.60	100	4.2				9.15	300	-40.7		46				318
0.65	890	0.8	-0.45	88	4.2				10.0	254	-45.9	0.60	46				
1.0	855	1.3	0.00	100	4.6				10.2	256	-47.3	0.70	46				
1.11	870	1.3	-0.45	88	4.2				10.6	241	-47.3	0.00	46				
1.26	820	1.3	0.00	81	4.0				11.0	227	-44.7	-0.65	45				
1.5	832	1.3	0.00	76	3.9				11.85	200	-41.4		43				290
1.7	814	1.3	0.00	66	3.6				12.0	195	-40.9	-0.38	43				
1.84	809	1.0	0.27	64	3.3				13.0	169	-39.7	-0.12	41				
2.0	793	0.5	0.27	60	3.1				14.0	147	-39.3	-0.04	41				283
2.5	778	-1.5	0.40	51	2.3				15.0	126	-38.9	-0.04	41				
2.9	760	-3.1	0.46	31	2.2			292	16.0	108	-38.6	-0.03	41				
3.0	690	-3.8	0.46	31	2.0				17.0	94	-38.1	-0.05	41				
4.0	605	-9.8	0.60	31	1.4				18.0	82	-37.4	-0.07	41				312
4.11	600	-10.3		31	1.3				19.0	70	-36.7	-0.07	41				
									20.0	61	-35.6	-0.11	41				

I 421 -

Продолж. приложения

6.8 0141 $\varphi = 79^{\circ}13'$ $\lambda = 190^{\circ}20'$
10/10 St (57)

H	B	t	Y	U	q	d	V	W	H	B	T	t	U	q	d	V	W
21.0	53	-35.2	-0.04	41				303	3.0	689	-7.3	0.46	59	1.7			312
21.6	50	-35.1		41					4.0	605	-12.8	0.55					
22.0	46	-34.6	-0.06	41					4.07	600	-13.1						
23.0	39	-34.2	-0.04	41					5.0	530	-19.1	0.63					
23.17	38	-34.2	0.00	41				295	5.42	500	-21.4						320
									6.0	462	-26.3	0.72					
									7.0	402	-31.7	0.54					
									7.03	400	-31.8						
									8.0	348	-37.4	0.57					
									9.02	300	-43.8	0.63					322
									10.0	259	-43.8	0.00					
									10.37	245	-43.8	0.00					
									11.0	224	-41.1	-0.43					
									11.77	200	-39.7						
									12.0	193	-39.4	-0.17					270
									13.0	167	-38.9	-0.05					
									14.0	144	-38.9	0.00					293
									15.0	125	-38.9	0.00					
									16.0	109	-38.9	0.00					
									16.76	100	-38.9	0.00					
									17.0	94	-38.9	0.00					267
									18.0	81	-38.8	-0.01					
									19.0	70	-38.4	-0.04					

I 422 -

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
20.0	60	-38.0	-0.04					265	2.57	700	-9.2		71	1.8			
21.0	52	-37.6	-0.04						3.0	688	-9.6	0.37	69	1.7			285
21.25	50	-37.6	-0.04						4.0	604	-16.4		53	0.9			
22.0	45	-37.3	-0.03						4.05	600	-16.4	0.65	54	0.8			
23.0	38	-36.8	-0.05					270	5.0	529	-18.3	0.25	52	0.7			339
24.0	32	-36.2	-0.06						5.15	517	-19.1	0.13	51	0.7			
25.0	27	-35.7	-0.05					270	5.42	500	-21.3	0.13	50	0.6			
									6.0	481	-25.5	0.72	46	0.4			
									7.02	400	-29.0	0.79	46				
									8.0	348	-40.3	0.73	44				
									8.81	309	-44.2	0.56	44				
									9.01	300	-44.7	0.00	42				
									9.72	269	-44.7	0.00	41				
									10.0	238	-46.4	0.00	41				
									11.0	223	-50.4	-0.46	41				
									11.42	210	-59.6	-0.58	39				
									11.73	200	-58.7	-0.21	38				
									12.0	192	-58.7	0.00	37				
									13.0	166	-58.7	0.00	37				
									14.0	144	-58.7	0.00	37				
									15.0	124	-58.7	0.00	37				
									16.0	107	-58.7	0.00	37				
									16.42	100	-58.7	0.00	37				
									17.0	92	-58.9	-0.04					

6.8 1944 $\varphi = 79^{\circ}13'$ $\lambda = 190^{\circ}22'$
10/10 St. (45), $\rho = 0$

100 3.8 292 2

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
17.0	52	-38.3	-0.07	37				268	3.71	631	-11.7	0.51	38	0.9			365
18.0	80	-37.4	-0.09	37					4.0	608	-13.3	0.45	38	0.8			
19.0	70	-37.2	-0.02						4.1	600	-13.7	0.67	37	0.7			
20.0	61	-37.2	0.00					271	5.0	532	-20.0	0.67	36	0.4			
									5.46	500	-22.0	0.55	35	0.3			
									6.0	464	-25.5	0.77	34				
									7.0	404	-33.2	0.77	34				
									7.07	400	-33.7	0.60	32				
									8.0	350	-39.2	0.64	31				
									9.0	302	-45.6	0.64	31				
									9.03	300	-45.9	0.42	30				
									9.5	280	-47.7	0.42	30				
									10.0	260	-46.2	-0.30	28				
									11.0	224	-41.4	-0.48	28				
									11.78	200	-40.5	-0.10	26				
									12.0	183	-40.4	-0.10	26				
									12.64	176	-39.8	-0.00	24				
									13.0	166	-39.8	0.00	23				
									14.0	144	-39.8	0.00	22				
									15.0	125	-39.8	0.00	22				
									16.0	108	-39.3	-0.05	19				
									16.48	100	-39.1						
									17.0	92	-38.9						

7.8 0196 $\varphi = 79^{\circ}13'$ $\lambda = 190^{\circ}25'$
10/10 St. Sc (109)

97 3.7 270 2

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
18.0	81	-38.6	0.03					269	2.5	740	-4.1	0.32	77	2.8	269	1	
19.0	70	-38.2	-0.04						2.195	700	-6.3	0.48	66	2.1	261	3	
20.0	60	-37.9	-0.03						4.0	655	-6.5	0.47	64	1.6	258	3	
21.0	52	-37.6	-0.03					272	4.0	611	-11.2	0.47	63	1.5	207	4	
21.4	50	-37.4							4.13	600	-11.7	0.42	58	1.1	203	4	
22.0	46	-37.2	-0.04					264	3.0	555	-18.1	0.42	57	0.9	213	6	
23.0	40	-36.9	-0.03						3.33	500	-18.1	0.65	55	0.6	218	8	
									7.0	468	-21.9	0.69	52	0.4	240	15	
									7.14	400	-29.2	0.33	51	0.4	242	15	
									9.0	354	-32.1	0.33	49		250	20	
									9.17	307	-38.8	0.67	48		254	24	
									10.0	300	-40.0	0.68			254	26	
									11.0	264	-45.6	0.77			258	29	
									11.3	228	-53.3	0.77			253	30	
									11.8	218	-53.3	0.00			250	18	
									11.85	200	-67.7				252	14	
									13.0	150	-67.7	-0.94			252	13	
									13.0	167	-62.8	-0.39			246	13	
									14.0	144	-61.7	-0.11			243	12	
									15.0	125	-60.6	-0.11			243	12	
									16.0	108	-59.6	-0.10			243	12	
									16.3	100	-59.2				243	12	

7.8 1335 $\varphi=79^{\circ}18'$ $\lambda=190^{\circ}29'$
 8'0 Cs, Cc
 100 3.8 1 158 3
 0.1 0.1
 0.2 0.1
 0.2 989 0.0
 0.3 969 0.0
 0.5 953 -0.4
 0.8 917 -0.4
 0.85 900 -0.6
 1.0 894 -0.7
 1.41 850 -1.4
 1.5 840 -1.5
 1.89 800 -2.2
 2.0 788 -2.5

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
17.0	98	-39.0	-0.06						3.0	691	-7.1	0.28	74	2.3			
18.0	80	-38.6	-0.04						4.0	697	-12.1	0.50	73	1.6			
19.0	68	-38.2	-0.04						4.08	600	-12.7	0.56	72	1.2			
20.0	59	-37.8	-0.04						5.0	539	-17.7	0.56	72	1.2			
20.3	56	-37.6	-0.07					385	5.47	500	-19.1	0.34	70	0.9		324	
									6.0	465	-21.1	0.32	69	0.6			
									7.0	405	-25.3	0.77	67	0.5			
									7.1	369	-27.0	0.77	66				
									8.0	332	-34.0	0.77	66				
									9.0	300	-41.7	0.77	66				
									9.1	269	-42.3	0.80					
									10.0	233	-49.7	0.00					
									10.5	244	-49.7	-0.04					
									11.0	220	-46.3	-0.04					
									11.6	200	-46.6	-0.40					
									12.0	184	-42.3	-0.19					
									13.0	168	-40.6	-0.19					
									13.25	154	-38.8	-0.11					
									14.0	149	-38.8	0.00					
									15.0	123	-39.6	-0.02					
									16.3	100	-39.4	-0.02					
									17.0	93	-39.1	-0.03					

8.8 0142 $\varphi=79^{\circ}14'$ $\lambda=190^{\circ}29'$
 10'10 St, (63)
 98 3.6 112 7
 98 3.5
 0.1 996 -0.5
 0.2 984 -0.5
 0.5 948 -0.5
 0.68 900 -0.5
 1.0 891 -0.5
 1.1 880 -0.5
 1.38 850 -1.6
 1.5 837 -2.2
 1.86 800 -3.4
 2.0 785 -4.1
 2.5 737 -5.7
 2.89 700 -6.7

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
18.0	81	-38.8	-0.03						5.0	529	-16.4	0.54	93	1.6			
19.0	70	-38.6	-0.02						5.43	500	-18.6	0.52	85	1.4			
19.24	68	-38.3	-0.04					262	6.0	463	-21.7	0.53	85	1.0			375
8.8 1322 $\varphi=79^{\circ}15'$ $\lambda=190^{\circ}29'$																	
10/10 St (29)																	
0.0	063	-0.5		89	3.7	112	5		9.0	303	-41.6	0.79	74				
0.04	060	-0.7		89	3.7				9.07	300	-42.2	0.78	74				
0.2	978	-1.4	0.45						9.35	295	-43.9	0.86	72				
0.37	957	-2.3	0.33	89	3.2				10.0	292	-46.0	-0.69	71				273
0.5	942	-2.3	0.00	89	3.3				11.0	292	-42.1	-0.59	62				
0.86	900	-2.3	0.00	89	3.3				12.0	290	-40.1	-0.51	59				
1.0	885	-2.3	0.00	89	3.3				13.0	194	-40.0	-0.21	56				291
1.32	850	-2.8	0.16	89	3.3				14.0	145	-38.8	-0.05	54				
1.5	832	-3.2	0.22	89	3.6				15.0	125	-38.4	-0.04					
1.8	800	-3.8	0.20	89	3.5				16.0	107	-38.4	0.00					297
2.0	780	-4.2	0.20	89	3.6				16.5	100	-38.3						
2.5	732	-5.8	0.32	98	3.1			347	17.0	83	-35.9	-0.04					
2.85	700	-7.5	0.30	97	2.8				18.0	80	-37.6	-0.04					
3.0	686	-8.3	0.30	97	2.6				19.0	69	-37.2	-0.04					
4.0	604	-11.0	0.37	95	2.4				20.0	60	-38.7	-0.05					
4.05	600	-11.3		95	2.3				20.45	57	-38.7	0.00					336

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.0	000	-0.2		100	3.8	180	3		0.0	004	0.0						
0.2	975	-0.6	0.30	89	3.6	211	6		0.04	000	-0.1						
0.37	954	-1.4	0.35	88	3.4				0.2	979	-0.9	0.45					
0.5	939	-1.4	0.00	88	3.5				0.7	941	-2.9	0.68					
0.85	900	-1.4	0.00	86	3.5				0.78	909	-3.1	0.82					
1.0	883	-1.4	0.00	85	3.6				0.85	892	-5.1						
1.3	850	-2.5		84	3.5				1.0	862	-5.1	0.00					
1.5	829	-3.4	0.40	83	3.2				1.21	859	-3.9						
1.77	800	-5.0	0.60	82	3.8				1.38	843	-3.6	-0.39					
2.0	777	-6.5	0.62	81	2.5				1.5	830	-3.6	0.00					
2.35	743	-8.6	0.60	80	2.0				1.8	800	-3.6	0.00					
2.5	729	-8.9	0.20	80	2.1				2.0	779	-3.6	0.00					
2.81	700	-9.6		87	2.1			295	2.5	731	-3.1	0.30					225
3.0	683	-9.9	0.20	87	2.1				2.84	700	-6.7	0.46					
3.1	674	-10.0	0.10	86	2.1				3.0	686	-7.4	0.46					190
4.0	600	-14.7	0.52	74	1.3				4.0	603	-12.5	0.51					
5.0	504	-20.7	0.60	57	0.7				4.08	600	-12.7	0.68					
5.33	500	-22.9		51	0.5			298	5.0	527	-19.3	0.68					
6.0	455	-28.3	0.76	48	0.3				6.0	459	-28.7	0.64					222

Продолж. приложения

H	B	t	T	U	q	d	V	W	II	B	t	l	T	U	q	d	V	W	350
7.02	400	-31.0	0.32						0.5	940	-11.5	0.37	90	2.7					
8.0	348	-35.4	0.45					244	0.7	917	-5.1	0.90	87	2.3					
9.02	300	-41.8	0.63						0.85	990	-2.1	0.90	87	2.4	186				
9.7	272	-46.8	0.74						1.0	883	-2.4	-1.13	87	2.8					
10.0	260	-46.8	0.00						1.3	850	-2.4	0.00	87	2.0					
10.22	253	-46.3	0.00						1.5	828	-1.7	0.05	87	2.8					
11.0	224	-42.0	-0.62					333	1.77	890	-6.4	0.05	87	2.4					
11.74	200	-40.3							2.0	776	-8.2	0.70	87	2.2					
12.0	152	-40.1	-0.19						2.5	728	-9.6	0.28	86	2.6					
13.0	166	-39.8	-0.03					210	2.8	760	-10.5	0.28	86	1.9					
14.0	142	-39.4	-0.04						3.0	681	-12.0	0.48	85	1.7					
15.0	123	-39.0	-0.04					201	3.97	600	-16.0	0.41	83	1.3					
16.0	108	-38.6	-0.04						4.0	598	-16.1	0.41	83	1.3					
16.5	100	-38.5	-0.02						5.0	523	-20.0	0.30	81	1.1					
17.0	92	-38.5	0.00						5.35	500	-20.7	0.20	80	1.0					
18.0	79	-38.5	0.00						5.8	470	-21.6	0.20	80	1.0					
18.8	68	-38.5	0.00					197	6.0	457	-22.6	0.50	79	0.9					
									6.97	400	-28.0	0.55	77	0.5					
									7.0	398	-28.1	0.55	77	0.5					
									8.0	346	-34.5	0.64	75						
									8.99	300	-41.2	0.68	72						
									9.9	262	-47.2	0.66	67						
									10.0	258	-47.2	0.60	67						

10.8 0127 $\varphi = 79^{\circ}19'$ $\lambda = 190^{\circ}40'$

10/10 St (79), Δ°

0.0	001	-1.0	59	3.3	0
0.01	000	-1.1	59	3.3	0
0.2	970	-1.8	59	3.1	181

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	l	T	U	q	d	V	W	393		
10.37	244	-47.2	0.00	64				319	0.5	933	-2.5	0.30	90	3.0							
11.0	222	-42.8	-0.70	59					0.82	900	-3.1	0.20	90	2.9							
11.7	200	-40.4	0.56						1.0	881	-3.5	0.40	88	2.7							
12.0	191	-39.8	-0.30	55				282	1.27	850	-4.6	0.55	86	2.5							
13.0	165	-39.0	-0.03	52					1.5	827	-5.5	0.40	83	2.4							
14.0	143	-38.6	-0.04	49					1.76	800	-6.2	0.28	80	2.2							
15.0	123	-38.6	0.00	46					2.0	776	-6.9	0.28	80	2.2							
16.0	108	-38.6	0.00	44				286	2.5	727	-9.3	0.48	74	1.7							
16.44	100	-38.6	0.00						2.79	700	-10.3	0.70	1.5								
17.0	92	-38.6	0.00						3.0	680	-10.6	0.26	68	1.6							
18.0	80	-38.6	0.00					279	3.97	600	-15.0	0.35	1.0								
19.0	69	-38.6	0.00						4.0	588	-15.1	0.45	57	1.0							
20.0	59	-38.6	0.00						5.0	524	-19.7	0.46	49	0.6							
21.0	52	-38.6	0.00						5.34	500	-21.3	0.53	41	0.4							
21.22	50	-38.6	0.00					280	6.05	400	-29.7	0.50	39	0.3							
22.0	45	-38.6	0.00						7.0	395	-30.0	0.50	39	0.2							
23.0	39	-38.6	0.00						8.0	345	-34.0	0.40	33								
24.0	34	-38.6	0.00					270	8.96	300	-39.3	0.36	36								
									9.0	298	-39.6	0.56	36								
									9.64	272	-43.0	0.53	35								
									10.0	258	-43.0	0.00	34								
									10.14	253	-43.0	0.00	34								

11.8 0141 $\varphi = 79^{\circ}18'$ $\lambda = 191^{\circ}00'$

10/10 Fs (29), Δ°

0.0	000	-1.0	91	3.1	248	5
0.2	975	-1.6	90	3.1	181	1

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W	
11.0	222	-60.4	-0.30	33					2.5	722	-8.9	0.36	58	1.4	263	4	270	
11.74	200	-39.2		32					2.75	700	-10.0		53	1.3	255	5		
12.0	192	-39.0	-0.14	31			243		3.0	676	-11.7	0.42	58	1.3	248	5	303	
13.0	166	-38.2	-0.08	29			251		3.93	600	-14.0		58	1.0				
14.0	144	-38.0	-0.02						4.0	594	-15.0	0.40	58	1.0				
15.0	124	-37.8							5.0	520	-19.5	0.45	58	0.8				
16.0	107	-37.5	-0.03						5.29	500	-21.1		57	0.77				
16.5	100	-37.4							6.0	454	-24.4	0.49	53	0.5				
93		-37.3	-0.02				285		6.9	400	-30.0		50	0.3				
11.8	1331	φ=79°18'	λ=191°15'						7.0	394	-30.6	0.62	50					
									8.0	342	-38.5	0.79	49					
									8.7	308	-45.0	0.93	48					
0.0	584	-3.0		92	1.8	360	1		8.87	300	-45.0	0.00	48					
0.2	970	-4.0	0.50	90	2.5	334	2		9.0	295	-45.0	0.00	48					
0.28	950	-4.7	0.88	89	2.4	324	2		9.4	278	-45.0	0.00	47					
0.5	934	-4.7	0.00	87	2.4	311	2		10.0	254	-39.9	-0.85	47					
0.8	900	-4.7	0.00	84	2.4	292	3		11.0	220	-36.5	-0.34	46					
1.0	877	-4.7	0.06	82	2.5	302	3		11.64	200	-35.8		45					
1.24	850	-5.1		77	2.3	291	4		12.0	190	-35.8	-0.07	45				289	
1.5	822	-5.7	0.20	73	2.1	272	4		13.0	165	-35.0	0.02	44					
1.71	800	-6.1		68	2.0	258	4		14.0	142	-37.2	0.12	43					
2.0	770	-7.1	0.28	65	1.8	270	4		15.0	123	-37.3	0.01	43					
									16.0	108	-37.3		43					292

Продолж. приложения

H	B	t	γ	U	q	d	V	W	H	B	t	γ	U	q	d	V	W	
16.55	100	-37.3		43					3.95	600	-16.6		65	1.0				
17.0	94	-37.3	0.00	43			254		4.0	596	-16.8	0.44	65	0.9				
18.0	80	-37.3	0.00	43			251		5.0	522	-23.0	0.62	62	0.6				
19.0	68	-37.3	0.00	43					5.31	500	-25.2		61	0.5			309	
20.0	60	-37.3	0.00						6.0	454	-28.8	0.38	60	0.4				
21.0	52	-37.3							6.89	400	-32.0		59					
21.32	50	-37.3	0.00				263		7.0	393	-32.5	0.37	59					
									8.0	341	-37.6	0.51	58					
									8.89	300	-43.3	0.64	58					
									9.0	295	-43.3	0.00	57					
									9.3	283	-43.3		57					
									10.0	255	-39.7	-0.51	57				287	
									11.0	220	-36.8		56					
									11.67	200	-36.2		55					
									12.0	191	-36.0	-0.08	55					
									13.0	165	-35.2	-0.08	55				289	
									14.0	143	-35.2	0.00	54					
									15.0	124	-35.2	0.00	53				311	
									16.0	108	-35.2	0.00	52					
									16.55	100	-35.2		52					
									17.0	93	-35.2	0.00	52					
									18.0	81	-35.2	0.00	51					
									19.0	70	-35.2	0.00	51					
																		293

Продолж. приложение

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W
20.0	61	-35.2	0.00	51			304	3.97	600	-17.0	59	0.8			
21.0	52	-35.2	0.00	51				4.0	597	-17.1	0.46	59	0.8		
21.35	50	-35.2	0.00	51				5.0	522	-21.6	0.45	59	0.6		
22.0	45	-35.2	0.00	51				5.31	500	-22.7	0.56	59	0.4		277
23.0	38	-35.2	0.00					6.0	455	-27.2	0.56	59			
23.9	34	-35.2	0.00				297	6.93	400	-31.7	0.50	58			
13.8 0145 $\varphi = 79^{\circ}11'$ $\lambda = 192^{\circ}00'$															
10/10 Ξ (14)															
0.0	001	-2.8	0.9	2.8	270			9.12	291	-45.4	0.68	50			227
0.1	000	-2.9	0.9	2.8				9.7	287	-46.1	0.58	50			
0.2	976	-3.0	0.9	2.8				10.0	285	-42.5	-1.20	48			
0.5	939	-3.7	0.23	89	2.7			11.0	220	-37.7	-0.48	46			206
0.85	900	-4.7	0.1	2.3				11.66	200	-36.8	0.00	44			
1.0	882	-5.5	0.35	79	2.1			11.74	197	-36.7	-0.14	44			
1.29	850	-6.6	0.6	7.1	1.9			12.0	190	-36.7	0.00	42			191
1.5	828	-7.1	0.32	71	1.8			13.0	164	-36.7	0.00	42			
1.77	800	-7.7	0.24	62	1.5			14.0	143	-36.7	0.00	42			221
2.0	776	-8.3	0.24	62	1.5			15.0	124	-36.7	0.00	42			
2.5	728	-9.8	0.30	56	1.2			16.0	107	-36.7	0.00	42			224
2.8	700	-11.4	0.53	53	1.1			16.37	102	-36.7	0.00	42			
3.0	681	-12.5	0.54	52	1.0		330								

Продолж. приложение

H	B	t	U	q	d	V	W	H	B	t	U	q	d	V	W		
0.0	000	-0.8	0.9	3.5	292			6.99	400	-34.0	0.67	65					
0.05	000	-1.2	0.55	99	3.3			8.0	345	-40.2	0.61	62					
0.2	892	-1.9	0.63	96	3.8			8.88	303	-47.6	0.84						
0.5	845	-3.8	0.07	2.9				9.36	300	-47.6	0.00				382		
0.89	800	-3.8	0.00	57	3.0			9.7	298	-47.6	0.00						
1.0	888	-3.8	0.00	57	3.0			10.0	296	-45.4	-0.73						
1.38	850	-3.8	0.00	57	3.0			11.0	230	-49.5	-0.49						
1.5	835	-3.8	0.00	93	3.1			11.07	200	-39.3	-0.15						
1.85	800	-5.8	0.50	86	2.4			12.0	190	-39.0	-0.10						
2.0	785	-6.3	0.50	86	2.4			13.0	165	-38.9	-0.10						
2.5	736	-8.8	0.50	82	2.0			14.0	142	-37.4	-0.06						
2.89	700	-11.5	0.78	76	1.6			15.0	123	-36.8	-0.06						
3.0	689	-12.2	0.68	77	1.5			16.0	107	-36.2	-0.06				322		
3.5	645	-16.2	0.80	74	1.0			16.46	100	-36.3	-0.09						
4.0	603	-17.1	0.18	74	1.0			17.0	93	-36.3	-0.09				301		
4.04	600	-17.2	0.17	72	1.0			17.54	84	-34.7	-0.09						
4.3	579	-17.6	0.17	72	1.0												
5.0	528	-21.0	0.49	70	0.8												
5.41	500	-23.4	0.64	67	0.5												
6.0	460	-27.4															
15.8 1406 $\varphi = 79^{\circ}00'$ $\lambda = 193^{\circ}00'$																	
10/10 Ξ , \times																	
	0.0	018	0.0											96	3.5	270	4
		0.15	0.00	-0.6											96	3.5	

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.2	992	-0.8	0.40	96	3.3				10.08	956	-41.8	0.00	47				253
0.3	955	-2.4	0.53	95	3.1				11.0	223	-40.8	-0.11	46				
0.38	900	-5.0	0.65	94	2.6				11.77	200	-40.2	-0.06	46				254
1.05	892	-6.0	0.85	94	2.4				12.0	193	-40.2	0.00	46				
1.44	850	-6.0	0.89	89	2.4				13.0	167	-40.2	0.00	44				242
1.5	843	-6.0	0.90	87	2.4				14.0	144	-40.2	0.00	43				
1.82	809	-6.0	0.90	78	2.3				15.0	125	-40.2	0.00	43				
1.91	800	-6.3	0.90	76	2.1				15.73	113	-40.2	0.00	43				
2.0	780	-6.7	0.89	74	2.1				16.0	109	-40.0	-0.07	43				282
2.5	741	-8.5	0.86	67	1.7				16.53	100	-39.8						
2.94	700	-10.3	0.82	62	1.4				17.0	92	-39.6	-0.04					
3.0	694	-10.5	0.80	62	1.4				18.0	80	-39.2	-0.04					
4.0	609	-17.3	0.68	57	0.8			291	19.0	69	-38.9	-0.03					
4.11	600	-17.7	0.67	57	0.8				20.0	60	-38.5	-0.04					
5.0	532	-23.5	0.62	53	0.5				21.0	52	-38.5	0.00					
5.45	500	-26.8	0.61	51	0.3				21.2	50	-38.5	0.00					
6.0	463	-29.6	0.61	51	0.3				22.0	44	-38.5	0.00					338
7.0	402	-35.5	0.59	50													
7.03	400	-35.7	0.59	50													
8.0	347	-39.4	0.59	48													
8.72	313	-41.8	0.58	48													
9.01	300	-41.8	0.58	47													
10.0	259	-41.8	0.56	47													

16.8 0137 $\rho=7901'$ $\lambda=193^{\circ}10'$
 10/10 Sc (62), Σ , Δ
 0.0 017 -0.6 98 3.6 248 3
 0.13 000 -1.0 97 3.4 274 6
 0.2 591 -1.2 96 3.5 282 6

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.5	955	-2.5	0.43	92	3.0				10.52	240	-51.6	0.00	43				
0.8	920	-4.7	0.73	(65)	2.5				11.0	223	-47.3	-0.50	43				
0.97	900	-3.2	0.88	81	3.7				11.75	200	-44.0	-0.37	42				225
1.0	897	-3.2	0.90	81	2.7				12.0	192	-43.6	-0.12	41				
1.2	875	-3.2	0.90	79	2.7				13.0	166	-42.4	-0.04	41				217
1.43	850	-4.5	0.87	77	2.4				14.0	143	-42.0	-0.04	41				
1.5	842	-4.5	0.87	76	2.3				15.0	123	-41.8	-0.02	40				
1.91	800	-6.9	0.82	73	2.0				16.0	106	-41.6	-0.02					
2.0	790	-7.3	0.82	72	1.9				16.41	100	-41.5						
2.5	741	-8.7	0.78	66	1.6				17.0	92	-41.3	-0.03					209
2.94	700	-9.9	0.76	60	1.4				18.0	80	-41.0	-0.03					
3.0	694	-10.0	0.76	59	1.4				19.0	68	-40.9	-0.01					206
4.0	609	-14.4	0.64	53	1.0			264	20.0	58	-40.9	0.00					
4.12	600	-15.2	0.63	53	0.9				21.0	51	-40.9	0.00					
5.0	538	-20.4	0.60	50	0.6				21.67	50	-40.9	0.00					
5.47	500	-23.3	0.58	48	0.4				21.97	50	-40.9	0.00					
6.0	465	-25.9	0.55	47	0.4				22.0	43	-40.9	0.00					202
7.0	404	-31.4	0.55	46													
7.07	400	-31.7	0.55	46													
8.0	350	-37.5	0.61	45													
9.0	303	-45.0	0.75	44													
9.06	300	-45.3	0.75	44													
10.0	259	-51.6	0.66	44													

16.8 1833 $\rho=76^{\circ}58'$ $\lambda=193^{\circ}25'$
 10/10 Sc (9), ρ
 0.0 018 0.4 96 3.7 248 5
 0.13 000 0.4 96 3.7 248 5
 0.2 593 0.4 96 3.8 252 6

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.5	877	0.4	0.00	96	3.9				11.9	200	-42.8	-0.68					218
0.99	900	0.4	0.00	96	4.2				12.0	197	-42.6	-0.15					
1.23	874	0.4	0.00	96	4.3				13.0	170	-41.1	-0.09					224
1.45	850	-0.2	0.26	96	4.3				14.0	147	-40.2	-0.06					
1.5	845	-0.3	0.26	96	4.1				15.0	127	-39.6	-0.04					230
1.93	800	-1.2	0.22	87	3.7				16.0	109	-39.2	-0.04					
2.0	792	-1.4	0.22	86	3.7				16.61	100	-38.9	-0.04					
2.5	744	-3.7	0.46	55	2.1			270	17.0	95	-38.8	-0.04					232
2.97	700	-5.9	0.46	48	1.6				19.0	71	-38.0	-0.04					
3.0	698	-6.0	0.46	48	1.6				19.0	71	-38.0	-0.04					
4.0	615	-10.9	0.49						21.0	53	-37.2	-0.04					
4.18	600	-12.3	0.66					237	21.5	50	-37.0	-0.04					
5.0	539	-17.5	0.59						22.0	45	-36.8	-0.04					
5.55	500	-21.0	0.59						22.64	41	-36.6	-0.03					232
6.0	470	-23.4	0.48														
7.0	411	-28.2	0.48														
7.2	400	-29.2	0.66					254									
8.0	358	-34.8	0.72														
9.0	308	-42.0	0.61					246	0.0	019	0.0	0.00	100	3.7	248	7	
9.18	300	-43.0	0.57						0.15	000	0.0	0.00	100	3.8			
10.0	266	-48.1	0.00						0.2	583	0.0	0.00	100	3.9			
10.23	257	-49.4	0.00						0.5	587	2.6	-0.87	96	4.6			
11.0	229	-49.4	0.00						0.7	934	3.1	-0.25	94	4.8			

17.8 0153 $\varphi=78^{\circ}57'$ $\lambda=193^{\circ}40'$

10/10 Ξ (6)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.01	900	2.0	0.16	89	4.5				0.2	600	1.0	0.00	88	3.6	275	13	
1.47	850	1.5	0.24	81	4.0				0.5	954	1.0	0.00	87	3.7	284	16	
1.5	846	1.4	0.24	81	4.0				0.97	900	1.0	0.00	87	4.0	276	18	
1.94	800	-0.4	0.44	74	3.4				1.0	897	1.0	0.00	87	4.1	277	20	
2.0	783	-0.8	0.44	73	3.3				1.18	878	1.0	0.00	87	4.1	277	20	
2.5	745	-4.0	0.64	70	2.6			384	1.44	843	-0.9	0.49	87	3.7	279	21	
3.0	700	-6.5	0.50	67	2.1				1.5	800	-3.0	0.46	82	3.0	280	19	
4.0	615	-12.8	0.63	62	1.3				1.92	700	-3.2	0.46	80	3.0	280	20	
4.19	600	-13.8	0.49	62	1.2				2.0	741	-5.0	0.36	72	2.4	278	18	
5.0	539	-17.7	0.49	62	0.9				2.3	745	-8.0	0.36	68	1.8	282	18	
5.55	500	-20.8	0.64	72	0.9			385	2.97	700	-8.1	0.62	65	1.8	283	18	317
6.0	470	-24.1	0.64	72	0.6				3.0	697	-13.9	0.63	66	1.4	284	21	
7.0	410	-30.3	0.62	72	0.6				4.16	600	-13.9	0.63	68	1.3	284	22	
7.2	400	-31.2	0.67	72					5.0	585	-13.2	0.63	58	0.8	282	23	
8.0	355	-35.0	0.67	72					5.31	500	-24.8	0.65	56	0.6	281	24	
9.0	307	-42.8	0.68	72					6.0	467	-25.7	0.65	53	0.4	279	25	316
9.15	300	-43.7	0.57	72				418	7.0	407	-31.3	0.55	51				
9.75	274	-47.1	0.57						7.13	400	-32.9	0.72					
									8.0	353	-36.3	0.51					
									9.0	306	-43.5	0.29					
									9.15	300	-43.5	0.29					
									9.35	292	-41.6	0.29					

17.8 1353 $\varphi=78^{\circ}56'$ $\lambda=194^{\circ}00'$

2/1 Ac, Es

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
18.8 0126 $\varphi = 78^{\circ}55'$ $\lambda = 194^{\circ}30'$																	
10/10 Sc (16)																	
0.0	015	-0.2		100	3.7	248	8		7.0	404	-31.0	0.67					230
0.12	009	-1.5	0.65	98	3.5				7.08	400	-31.4	0.73					
0.2	889	-1.5	0.65	98	3.3				8.0	351	-38.3	0.69					
0.4	864	-2.4	0.45	95	3.1				9.0	304	-45.2	0.69					
0.5	853	-2.4	0.60	91	3.2				10.0	251	-45.2	0.00					220
0.96	806	-2.4	0.00	91	3.2				10.27	225	-41.9	-0.45					
1.0	855	-2.4	0.00	90	3.1				11.0	206	-40.4	-0.25					
1.42	850	-2.4	0.00	83	3.1				11.8	200	-40.4	0.00					
1.5	841	-3.0	0.00	78	2.7				12.0	194	-40.4	0.00					225
1.9	789	-4.4	0.40	67	2.2				13.0	168	-40.4	0.00					200
2.0	789	-4.7	0.40	66	2.2				14.0	145	-40.4	0.00					200
2.5	740	-7.9	0.64	61	1.6			277	15.0	125	-40.4	0.00					
2.83	700	-9.3	0.57	57	1.4				16.0	109	-40.4	0.00					
3.0	694	-9.4	0.30						16.5	102	-40.4	0.00					200
4.0	609	-14.0	0.46						18.8 1342 $\varphi = 78^{\circ}55'$ $\lambda = 194^{\circ}10'$								
4.11	600	-14.3							10/10 Ns (82), %								
5.0	533	-19.1	0.51					250	0.0	014	0.2	96	3.6	248	4		
5.47	500	-21.7							0.11	000	-0.3	96	3.5				
6.0	464	-24.3	0.52						0.2	988	-0.5	96	3.5				

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
19.8 0136 $\varphi = 78^{\circ}52'$ $\lambda = 194^{\circ}40'$																	
10/10 Ns, Ξ , η																	
0.5	932	-1.1	0.20	96	3.5				12.0	197	-48.0	0.00	44				307
0.95	900	-1.8	0.16	96	3.5				13.0	169	-48.0	0.00	44				
1.0	893	-1.9	0.16	96	3.5				13.94	147	-48.0	0.00	44				290
1.41	850	-2.5	0.14	96	3.5				14.0	145	-47.9	-0.94	44				
1.5	840	-2.6	0.14	96	3.5				15.0	126	-47.0	-0.86	44				
1.88	800	-3.4	0.25	96	3.5				15.7	114	-46.4	0.00	44				
2.0	788	-3.9	0.25	96	3.4				16.0	109	-46.4	0.00	44				
2.5	739	-5.3	0.28	96	3.2			293	16.58	100	-46.4	0.00					
2.93	700	-6.7	0.33	96	3.1				17.0	93	-46.4	0.00					288
3.0	693	-7.2	0.33	96	3.0				18.0	80	-46.4	0.00					
4.0	610	-12.4	0.52	87	1.9				18.48	74	-46.4	0.00					
4.13	600	-13.0	0.52	87	1.9				19.8 0136 $\varphi = 78^{\circ}52'$ $\lambda = 194^{\circ}40'$								
5.0	534	-17.9	0.55	(79)	1.1			310	10/10 Ns, Ξ , η								
5.49	500	-21.0	0.60	(79)	0.9				0.0	012	0.2	96	3.6	248	3		
6.0	465	-23.9	0.60	(68)	0.7				0.1	000	0.3	96	3.6				
7.0	405	-31.2	0.73	(59)				309	0.2	987	0.4	-0.10	95	3.9			
7.09	400	-31.7	0.76	50					0.4	963	0.5	-0.05	95	3.9			
8.0	353	(-38.8)		50					0.5	951	0.5	0.00	95	4.0			
9.0	307			49					0.7	927	0.5	0.00	94	3.8			
9.16	300			49					0.84	900	-0.3	0.37	93	3.8			
10.0	265			48					1.0	893	-0.6		93	3.8			
11.0	229			46													
11.9	200			46													

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
0.97	800	-1.3	88	3.3	305	9			0.2	591	-1.5	0.35	86	2.9	315	6		
1.0	806	-1.5	81	3.0	304	9			0.5	554	-3.6	0.70	85	2.6				
1.2	841	-2.7	80	2.8	307	9			0.55	537	-4.5	0.60	84	2.4				
1.3	800	-3.9	74	2.6	299	10			0.97	900	-1.5	-0.94	83	3.1				
2.0	741	-5.9	72	2.4	295	10			1.0	897	-1.5		81	3.1				
2.5	711	-7.8	65	2.0	293	12	273		1.4	853	-1.5	0.00	67	2.7				
2.8	700	-8.1	59	1.7	297	16			1.43	850	-1.6		65	2.4				
3.0	658	-12.0	54	1.2	300	17			1.5	842	-1.9	0.40	65	2.4				
4.0	609	-12.6	53	1.2	302	17			1.72	819	-3.0	0.50	62	2.2				
4.13	608	-17.4	52	0.8	305	16			1.9	800	-3.0	0.00	58	2.1				
5.0	558	-23.5	52	0.5	309	14			2.2	770	-3.0	0.00	54	2.1				
5.32	549	-30.4	52	0.5	309	14			2.5	742	-3.6	0.20	50	1.9				
6.0	468	-30.2	52	0.5	302	12	305		3.0	685	-5.0	0.28	43	1.5				
7.0	407	-30.9	52		299	12			4.0	612	-9.4	0.44	35	1.0			311	
7.12	400	-36.0	52						4.16	600	-10.6							
8.0	353	-43.8	52					287	5.0	537	-16.3	0.69						
8.56	303	-43.8	52						5.55	500	-20.0	0.69					287	
									6.0	470	-23.2	0.64						
									7.0	409	-29.6							
									7.17	400	-30.5							

20.8 1330 φ=78°49' λ=195°37'
 10/10 St (44), 3³
 87 3.0 | 315 | 4
 86 3.0 | 312 | 5

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
8.0	355	-35.5	0.59						0.0	020	-1.4		91	3.0	338	1	
9.0	307	-43.0	0.75					338	0.16	000	-2.0	0.35	90	3.0	333	5	
9.17	300	-44.3	0.54						0.2	983	-2.1		90	2.6			6
9.54	284	-45.9	0.00						0.5	957	-3.7	0.55	89	2.6			
10.0	284	-45.9	0.00						0.58	947	-4.2	0.60	89	2.7			
10.94	229	-45.9	0.00						1.0	900	-4.2	0.60	88	2.8			
11.0	227	-45.7						310	1.45	850	-4.2	0.60	88	2.9			
11.86	200	-45.6	-0.25						1.5	844	-4.2	0.60	88	2.9			
12.0	195	-43.2	-0.08						1.6	834	-4.2	0.60	88	2.9			
13.0	169	-42.4	-0.07					284	1.8	813	-3.8	-0.70	79	2.9			
14.0	146	-41.5	-0.02						1.92	800	-2.8	0.00	77	2.9			
15.0	127	-41.5	0.00						2.0	792	-2.8	0.00	77	3.0			
16.0	110	-41.4						280	2.25	767	-2.5	0.56	75	2.8			
16.57	100	-41.1	-0.04						2.5	744	-4.2	0.60	74	2.1			
17.0	94	-40.4	-0.07						2.87	700	-3.0	0.80	73	2.0			
18.0	81	-39.8	-0.05						3.0	697	-3.0	0.85	72	1.7			
19.0	70	-39.3	-0.05						3.2	679	-3.9	0.00	70	1.8			
20.0	60	-38.7	-0.06						3.7	637	-11.0	0.37	69	1.7			
21.0	52	-38.6						285	4.0	613	-11.9		68	1.6			
21.25	50	-38.5							4.16	600	-11.9						
21.4	49	-38.5															

21.8 0130 φ=78°50' λ=195°35'
 10/10 St (51)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.0	535	-17.4	0.64	60	1.0				21.0	51	-40.4	0.00					
5.51	530	-20.4		59	0.7		270		21.1	50	-40.4						257
6.0	498	-24.0	0.65	58	0.5				21.27	48	-40.4	0.00					
7.0	468	-30.5	0.65	55													
7.15	364	-37.5	0.70	53			235										
8.0	305	-43.1	0.55	53					0.0	022	-1.8		89	2.8	158		2
9.15	200	-43.7							0.16	000	-2.5		91	2.8	176		3
9.44	265	-45.1	0.45						0.2	595	-2.8	0.50	91	2.7	179		
10.0	264	-45.1	0.00				275		0.3	959	-4.7		94	2.5			
11.0	277	-45.1	0.00						0.35	952	-5.0	0.63	96	2.5			
11.16	292	-45.1	0.00						0.77	927	-5.0	0.00	96	2.6			
11.85	200	-43.5							0.94	908	-3.4	-0.94	96	3.0			
12.0	135	-43.4	-0.20				263		1.01	900	-3.4	0.00	94	3.0			
13.0	168	-43.2	-0.02						1.35	862	-3.4	0.00	87	2.9			
14.0	145	-42.9	-0.03						1.47	850	-3.0	0.00	84	2.9			
15.0	128	-42.6	-0.03				255		1.5	846	-2.7	-0.50	83	3.1			
16.0	100	-42.4	-0.02						1.65	830	-1.8	-0.60	80	3.1			
16.5	100	-42.2							1.84	800	-1.8	0.00	79	3.2			
17.0	94	-42.1	-0.03						2.0	794	-2.2	0.00	79	3.2			
18.0	61	-41.6	-0.05				235		2.5	745	-4.6	0.50	78	2.7			
19.0	70	-41.0	-0.05						2.59	700	-6.9	0.47	76	2.3			305
20.0	60	-40.4	-0.05														

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
4.0	614	-13.2	0.62	74	1.6				14.0	146	-41.8	-0.05					278
4.17	600	-13.6		73	1.5				15.0	126	-41.4	-0.04					
5.0	537	-16.6	0.34	71	1.2				16.0	108	-40.9	-0.05					
5.56	500	-20.6		70	0.8		305		16.51	100	-40.7						
6.0	471	-24.0	0.74	69	0.6				17.0	93	-40.4	-0.05					270
7.0	410	-29.2	0.52	65	0.5				18.0	82	-39.3	-0.11					
7.18	400	-30.8		64													
8.0	355	-35.2	0.60	61			331		0.0	024	-3.8		87	2.3	135		3
9.0	307	-42.6	0.74						0.17	000	-4.4		87	2.3			
9.15	300	-43.5							0.2	997	-4.5	0.35	87	2.3			
9.57	269	-47.5	0.56						0.4	971	-5.6	0.50	86	2.2			
10.0	264	-47.5	0.00						0.5	959	-5.4	-0.20	85	2.1			
10.52	244	-47.5	0.00						0.9	912	-2.5	-0.73	78	2.6			
11.0	228	-45.6	-0.40				293		1.01	900	-2.5	0.00	75	2.6			
11.89	200	-43.6							1.24	874	-2.5	0.00	70	2.5			
12.0	196	-43.4	-0.22						1.46	850	-3.3		67	2.3			
13.0	169	-42.3	-0.11														

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.5	846	-3.5	0.38	67	2.3				0.7	536	-8.0	0.56	80	1.7			
1.62	833	-4.0	0.42	65	2.3				1.01	500	-6.1	-0.61	78	2.0			
1.95	800	-4.0	0.40	64	2.3				1.45	850	-4.8		69	2.1			
2.0	794	-4.0	0.00	63	2.3				1.5	845	-4.7	-0.29	68	2.1			
2.14	790	-4.0	0.00	63	2.3				1.85	808	-3.3	-0.40	64	2.2			
2.5	746	-5.2	0.33	60	2.0			296	1.93	800	-3.3		63	2.2			
3.0	700	-7.0	0.35	57	1.4				2.0	783	-3.3	0.00	62	2.3			
4.0	614	-11.2	0.42	56	1.3				2.2	773	-3.3	0.00	60	2.2			
4.17	600	-12.1	0.65	55	0.8				2.5	745	-4.8	0.50	58	2.0			294
5.0	538	-17.7	0.85	54	0.5				2.98	700	-6.6	0.37	55	1.1			
5.57	500	-22.4	0.78	53	0.4				4.0	614	-12.0	0.53	51	1.0			
5.91	477	-24.8	0.8	53	0.4			295	4.17	600	-13.4	0.55					
6.0	471	-25.1	0.26	52	0.4				5.0	538	-17.5						
6.52	439	-26.4	0.26	52	0.4				5.54	500	-19.5	0.19					
7.0	410	-29.4	0.63	51	0.3				6.0	468	-22.4	0.91					
7.17	400	-30.3	0.56					292	7.0	409	-29.0	0.91					
7.32	391	-31.2	0.56						8.0	355	-35.7	0.67					
									9.0	306	-44.4	0.87					
									9.14	300	-49.0						
									10.0	264	-50.7	0.63					
									10.2	257	-51.4	0.35					

22.8 1344 $\varphi = 76^{\circ}52'$ $\lambda = 195^{\circ}18'$
 10/10 Fs (34), Δ°

0.0	093	-2.1	0.63	88	2.8	133	4
0.19	000	-6.3	0.80	85	2.5		
0.5	961	-6.1	0.90	82	2.0		

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
0.0	026	-3.6	0.88	2.6	133				7.25	400	-26.4						221
0.2	000	-5.0	0.70	88	2.3				8.0	360	-31.1	0.64					
0.42	972	-0.7	-1.96	80	3.0				9.0	310	-39.0	0.79					
0.5	962	-0.7	0.00	62	2.5				9.25	300	-40.7	0.68					220
1.0	905	-0.7	0.00	62	2.5				10.0	258	-45.8						
1.04	900	-0.7	0.00	48	2.1				10.87	235	-52.7	0.79					
1.5	850	-0.7	0.00	48	2.1				11.0	231	-52.7	0.00					
1.98	800	-0.7	0.00	44	2.0				11.93	200	-52.2	0.00					186
2.04	794	-0.7	0.00	44	2.0				12.0	197	-52.2	-0.45					
2.5	749	-3.3	0.57	40	1.3				13.0	169	-47.9	-0.11					
3.0	703	-5.2	0.38	39	1.4				14.0	145	-46.8	-0.11					
3.04	700	-5.4	0.49					207	14.6	132	-45.3	-0.25					162
4.0	618	-10.1	0.49														
4.23	600	-11.4	0.58														
5.0	541	-16.9	0.58														
5.59	500	-19.3	0.61														
6.0	474	-22.0	0.60														
6.1	467	-22.6	0.60														
6.83	418	-24.2	0.19														
7.0	414	-24.7															

24.8 0106 $\varphi = 79^{\circ}10'$ $\lambda = 195^{\circ}10'$
 10/7 Fs (30), AC

0.0	026	-1.3							0.0	026	-1.3						
0.14	009	-1.4							0.14	009	-1.4	0.07					10
0.21	000	-1.4							0.21	000	-1.4						
0.35	982	-1.4						214	0.35	982	-1.4	0.00	81	2.7			
0.5	963	0.1							0.5	963	0.1	-1.00	77	3.1			
1.0	906	0.1							1.0	906	0.1	0.00	58	2.4			
1.05	900	0.1							1.05	900	0.1	0.00	57	2.4			

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.51	850	0.1	0.00	46	2.1				14.0	147	-48.8	-0.13	57				
1.7	880	0.1	0.00	45	2.1				15.0	127	-48.2	-0.06	53				244
2.0	900	-0.7	0.37	34	1.6				16.0	110	-47.5	-0.07	51				
2.5	920	-3.1	0.48	34	1.4				16.67	100	-46.7		51				
3.0	940	-5.0	0.38	34	1.2				17.0	95	-46.4	-0.11	51				276
3.04	794	-5.2							18.0	81	-45.1	-0.13	51				
3.33	650	-9.1	0.65	34	1.0			363	19.0	71	-44.4	-0.07					
4.0	620	-10.4	0.24	34	0.9				20.0	60	-44.4	0.00					311
4.23	600	-10.4							20.43	56	-44.4	0.00					
4.54	576	-10.8	0.15	34	0.9				25.8 0151 $\varphi = 79^{\circ}17'$ $\lambda = 194^{\circ}40'$								
5.0	544	-12.7	0.41	59	1.4				10.5 P8 (67), Ac								
5.64	500	-16.5							0.0	028	-2.8		95				135
6.0	476	-17.7	0.50	68	1.2			400	0.22	000	-1.7	-0.50					10
7.0	416	-21.5	0.58	68	0.7				0.4	978	1.4	-1.72					
7.28	400	-24.9	0.71	68					0.5	956	1.4	0.00					
8.0	383	-27.9	0.73	68					1.0	908	1.4	0.00					
9.0	314	-40.4						308	1.07	900	1.4	0.00					
9.33	300	-40.4	0.71	67					1.34	870	1.4	0.00					
10.0	272	-45.9	0.72	65					1.52	850	0.8						
11.0	233	-52.2	0.80	64					1.54	807	-0.1	0.25					
11.5	217	-50.2						257									
12.0	200	-54.7	-0.30	62													
13.0	172	-50.1	-0.46	60													

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.5	752	-0.1	0.00						16.0	111	-47.7	-0.12					
2.71	732	-0.1	0.00					311	16.53	100	-47.0						298
3.0	707	-0.8	0.24						17.0	95	-46.7	-0.10					
3.07	700	-1.2							25.8 1420 $\varphi = 79^{\circ}19'$ $\lambda = 194^{\circ}50'$								
4.0	623	-5.2	0.44						10.0 Cc, Ac								
4.29	600	-7.7							0.0	030	-0.5		78	2.8	135		6
5.0	548	-10.3	0.51						0.2	005	0.3	-0.40	73	2.8	158		15
5.69	500	-13.7	0.53				316		0.23	000	0.3		72	2.8	159		15
6.0	481	-15.6	0.60						0.4	990	2.1	-0.30	67	2.9	166		17
7.0	421	-21.6							0.5	957	2.1	0.00	60	2.7	188		18
7.37	400	-24.2							1.0	909	2.1	0.00	40	1.9	191		13
8.0	365	-29.4	0.78				288		1.07	900	2.1	0.00	39	1.9	159		14
9.41	300	-36.0	0.46						1.15	892	2.1	0.00	38	1.9	158		14
10.0	275	-40.4	0.64						1.5	824	0.5	0.46	33	1.9	161		13
11.0	237	-48.0	0.76						1.54	820	0.4	0.10	32	1.9	161		13
11.73	213	-53.5	0.00						2.0	803	0.0	0.10	23	1.2	168		12
12.0	203	-53.5	0.00				242		2.04	800	-0.1	0.12	21	1.0	168		12
12.13	200	-53.5	0.00						2.5	754	-0.6	0.12	21	1.0	170		12
13.0	189	-53.5	0.00						3.0	708	-1.9	0.26	18	0.8	171		12
13.0	175	-51.8	-0.34						3.09	700	-2.2						342
14.0	150	-50.5	-0.13						4.0	624	-5.4	0.70					
15.0	129	-48.9	-0.16														

Предлож. приложени

H	B	I	T	U	q	d	V	W	H	B	I	T	U	q	d	V	W
4.31	600	-7.1					174	10	0.2	006	-1.8	-1.20	87	2.0	163	13	
5.0	548	-11.0	0.50				174	10	0.24	000	-0.8		87	3.0	164	13	
5.7	500	-14.7					184	10	0.3	591	0.3	-2.10	86	3.4	164	14	
6.0	480	-16.2	0.52				191	10	0.5	387	0.3		80	3.3	161	17	
7.0	420	-22.2	0.60						1.0	010	0.3	0.00	66	2.8	169	16	
7.35	400	-25.4							1.09	000	0.3	0.00	64	2.8	169	17	
8.0	385	-20.7	0.75						1.5	856	0.3	0.00	54	2.5	169	17	
9.0	318	-35.7	0.60					303	1.55	850	0.3	0.00	43	2.0	161	17	
9.4	300	-38.3							1.86	818	2.0	-0.77	45	2.4	169	16	
10.0	274	-43.6	0.79						2.03	804	2.0	0.00			151	15	
11.0	237	-50.0	0.64					280	2.03	800	2.0	0.00			132	15	
11.4	224	-52.2	0.55						2.26	777	2.0	0.00			148	14	
12.0	205	-52.2	0.00						2.5	755	0.8	0.50			137	13	330
12.17	200	-52.2	0.00						3.0	710	-2.1	0.58			147	13	
12.22	198	-52.2	0.00						3.1	700	-2.8				147	13	
13.0	176	-50.9	-0.17						4.0	624	-6.3	0.42			132	12	
14.0	150	-49.2	-0.17					279	4.31	600	-7.4						
15.0	128	-48.0	-0.12						5.0	548	-11.6	0.53					
15.84	113	-47.1	-0.11						5.7	500	-14.4						
									6.0	480	-15.0	0.43					
									7.0	421	-22.6	0.67					
									7.36	400	-25.3						

26.8 0158 φ = 79°23' λ = 194°47'
3/0 Cc

0.0 | 032 | -4.2 | 90 | 2.4 | 135 | 6 |

Предлож. приложени

H	B	I	T	U	q	d	V	W	H	B	I	T	U	q	d	V	W
8.0	366	-29.3	0.67						3.09	700	-3.9		45	1.7	145	9	
9.0	318	-34.4	0.51						4.0	623	-9.2	0.47	45	1.4	144	7	
9.4	300	-37.5							4.3	600	-12.2	0.40	45	1.3	136	7	
10.0	274	-42.1	0.77					384	5.0	548	-10.5		45	0.9	104	5	
10.63	250	-46.5	0.70						5.69	500	-10.5	0.51	45	0.8	085	4	295
									6.0	479	-17.3	0.65	45	0.5			
									7.0	419	-23.3						
									7.36	400	-25.7	0.48					
									8.0	385	-26.6	0.54					
									9.0	316	-34.0	0.61					
									9.38	300	-36.3	0.65					
									10.0	274	-40.1	0.65					
									11.0	237	-46.6	0.64					
									12.0	203	-53.0	0.70					
									12.11	200	-53.8						
									12.23	196	-54.6						
									12.61	185	-54.6						
									13.0	175	-52.6						
									14.0	150	-50.4						
									15.0	129	-49.0						
									16.0	111	-47.7						
									16.72	100	-47.0						
									17.0	96	-46.7						

26.8 1400 φ = 79°26' λ = 194°43'
2/0 Cc

H	B	I	T	U	q	d	V	W
0.0	030	-2.0						
0.2	005	-0.9						
0.23	000	-0.8						
0.33	988	-0.4						
0.5	968	-0.4						
1.0	911	-0.4						
1.09	900	-0.4						
1.5	855	-0.4						
1.55	850	-0.4						
1.97	806	-0.4						
2.0	803	-0.5						
2.03	800	-0.6						
2.5	753	-1.7	0.25					
3.0	708	-3.5	0.36					

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	U	q	d	V	W
18.0	83	-45.6	-0.11			116	5	289	5.0	545	-15.3	0.59	59	1.1	083	13
19.0	71	-44.1	-0.15			133	4		5.63	500	-18.3		53	0.8	079	14
20.0	61	-43.4	-0.07			145	2	312	6.0	476	-20.4	0.51	45	0.6	075	14
21.0	52	-42.7	-0.07			119	3		7.0	416	-27.0	0.66	45	0.4	078	19
21.23	50	-42.0				112	3	287	7.27	400	-28.2		45	0.3	077	18
22.0	45	-42.0	-0.07			116	3		8.0	381	-33.3	0.63	45	0.74	074	18
									9.0	312	-40.5	0.72	45	0.61	081	18
									9.28	300	-42.6		45	0.65	085	19
									9.86	274	-46.6	0.71				354

27.8 0144 $\varphi = 79^{\circ}28'$ $\lambda = 194^{\circ}30'$
I/O Ac

H	B	t	T	U	q	d	V	W	H	B	t	U	q	d	V	W
0.0	028	-4.0		01	2.5	090	6		0.0	027	-5.4		87	2.1	009	4
0.21	000	-3.0	-0.48	83	2.5	100	11		0.21	000	-2.7	-1.29	83	2.6	130	9
0.5	963	0.5	-1.21	70	2.9	102	13		0.34	983	-1.0	-1.31	80	2.9	131	8
1.0	907	0.5	0.00	52	2.2	098	18		0.5	963	-1.0	0.00	76	2.8	138	8
1.06	900	0.5	0.00	52	2.3	098	18		1.0	905	-1.0	0.00	53	2.1	133	8
1.44	850	0.5	0.00	52	2.3	093	16		1.05	900	-1.0		53	2.1	134	8
1.52	850	0.2	0.38	52	2.2	095	14		1.56	843	-1.0	0.00	50	2.1		
2.0	800	-1.6	-0.34	52	2.0	094	14	312	1.58	800	-2.7	0.40	48	1.9		
2.5	751	-3.3	0.34	60	2.2	094	10		2.5	748	-4.8	0.40	47	1.6		
3.0	705	-5.0	0.34	60	2.2	094	10									
3.06	700	-5.2														
4.0	681	-9.4	0.44	60	1.7	083	13									
4.23	680	-11.2		60	1.5	079	14									

27.8 1322 $\varphi = 79^{\circ}29'$ $\lambda = 194^{\circ}24'$
I/O Fs

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	U	q	d	V	W
3.02	700	-7.6	0.54	43	1.2			229	0.0	023	-5.4		76	1.8	068	7
4.0	617	-11.2	0.37	37	0.9			206	0.19	000	-3.0	-1.26	69	2.1	088	14
4.22	600	-11.9		35	0.8				0.5	961	1.0	-1.29	53	2.3	089	16
5.0	500	-15.8	0.46	34	0.6			201	0.6	949	1.5	-0.30	51	2.3	084	16
5.6	473	-19.7	0.65	31	0.4				1.02	900	0.1	0.33	46	1.9	084	16
6.0	413	-28.1	0.88	30	0.3				1.48	850	-1.1	0.26	46	1.9	087	16
7.0	400	-39.6	0.68					220	1.95	800	-2.9		46	1.7	085	16
8.0	310	-41.5	0.65						2.0	795	-3.0	0.37	46	1.6	085	16
9.0	310	-43.0							2.5	747	-5.0	0.40	46	1.6	087	14
10.0	265	-47.8	0.64					220	3.02	700	-7.0	0.38	46	1.4	081	12
10.08	262	-48.4							4.0	617	-10.8	0.39	41	1.0	082	13
11.0	233	-48.4	0.00						4.21	600	-11.6		39	0.9	103	10
11.18	200	-46.7						192	5.0	540	-14.0	0.32	36	0.8	104	9
12.0	199	-46.6	-0.22						5.58	500	-16.3		36	0.6	103	7
13.0	170	-46.3	-0.03					200	6.0	473	-18.2	0.42	36	0.6	107	7
14.0	146	-46.0	-0.03						7.0	413	-23.8	0.56	36	0.4	124	10
15.0	126	-45.7	-0.03						8.0	359	-30.3	0.65	36	0.4		
16.0	108	-45.4	-0.03					204	9.0	312	-38.0	0.77	36			
16.54	100	-43.2														
17.0	93	-41.9	-0.05													

28.8 0156 $\varphi = 79^{\circ}29'$ $\lambda = 194^{\circ}55'$
I/O Cl. Cs

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
9.26	300	-39.9		36					5.0	506	-14.0	0.37	47	1.0	085	15	
10.0	269	-46.8	0.88	36					5.30	506	-16.2	0.46	46	0.7	085	18	305
10.02	244	-52.7	0.95				385		6.1	469	-18.6	0.42	46	0.7	085	20	
									6.38	434	-20.2	0.40	46	0.7	083	20	
									7.0	434	-20.2	0.40	46	0.7	083	20	
									7.19	400	-23.7	0.60	45	0.5	081	20	
									8.0	357	-27.9	0.53	45	0.4	080	16	203
									9.0	311	-35.0	0.71	44				
									9.24	300	-36.5		44				
									10.0	267	-40.8	0.58	43				
									11.0	230	-48.4	0.76	42				
									11.06	200	-53.1	0.71	41				
									11.56	200	-53.1	0.71	41				
									12.0	198	-57.7		41				
									13.0	170	-67.0	-0.58					317
									14.0	147	-61.0	-0.10					
									15.0	127	-41.5	-0.15					
									16.0	109	-31.8	-0.17					
									16.6	100	-45.3						
									17.0	94	-45.4	-0.04					
									18.0	82	-42.0	-0.04					
									19.0	71	-41.7	-0.03					

28.8 1409 $\varphi=79^{\circ}28'$ $\lambda=193^{\circ}40'$
810 Ci, Cc

H	B	t	Y	U	q	d	V	W
0.0	016	-2.1		78	2.5	045	10	
0.12	000	-2.0		76	2.4			
0.2	990	-1.9		-0.10	76	2.5	076	
0.5	932	0.0		-0.63	76	3.0	076	
0.6	940	1.1		-1.10	76	3.3	078	
0.95	900	1.1		68	3.5	075	18	
1.0	885	1.1		0.00	65	3.0	075	
1.41	850	1.1		56	2.7	082	15	
1.5	840	1.1		55	2.7	085	16	
1.91	800	1.1		54	2.7	088	15	
2.0	790	1.5		53	2.3	088	15	
2.5	742	-4.2		52	1.9	082	17	
2.96	700	-6.0		51	1.7	085	19	341
3.0	695	-6.1		0.38	51	1.7	085	
4.0	612	-10.3		0.42	49	1.3	087	16
4.15	600	-10.9		48	-1.2	086	16	

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
20.0	61	-41.3	-0.04						2.88	700	-6.6		80	2.6			
21.0	32	-40.1	-0.12						3.0	698	-7.5	0.70	81	2.3			
21.25	50	-40.1							3.62	698	-11.7	0.68	84	1.8			
22.0	45	-40.1	0.00						4.0	698	-12.6	0.24	86	1.9			
22.4	42	-40.1	0.00				410		4.07	698	-12.7	0.24	87	1.9			249
									5.0	691	-14.5	0.19	93	2.0			
									5.14	691	-14.4	0.21	94	1.9			
									5.46	500	-18.8	0.47	76	1.2			
									6.0	466	-25.5	0.67	66	0.6			
									7.0	400	-33.3	0.78	65	0.6			
									8.0	332	-41.3	0.83	64				
									9.0	305	-41.6		64				
									10.0	283	-42.3	0.69	62				
									10.96	227	-52.9	0.47	62				
									11.0	226	-52.9	0.47	61				
									11.5	209	-52.9	0.00	60				
									11.78	200	-50.1		59				
									12.0	194	-48.9	-0.80	59				
									13.0	166	-46.4	-0.25	58				
									14.0	144	-46.1	-0.13	57				
									15.0	122	-44.3	-0.08					

30.8 0135 $\varphi=79^{\circ}26'$ $\lambda=192^{\circ}50'$
1010 St, X

H	B	t	Y	U	q	d	V	W
0.0	006	-0.5		94	3.4	022	4	
0.05	000	-0.6		94	3.5			
0.2	981	-1.6		0.35	94	3.0		
0.36	962	-2.4		0.30	94	3.0		
0.5	945	-2.4		0.00	94	3.1		
0.54	941	-2.4		-0.00	94	3.1		
0.90	900	-0.8		0.44	65	2.5		
1.0	887	-0.8		0.00	62	2.5		
1.34	850	-0.8		0.00	57	2.3		
1.5	834	-0.8		0.00	57	2.4		
1.74	809	-0.8		0.00	57	2.5		
1.83	800	-1.3		0.57	2.4			
2.0	783	-2.3		0.58	2.3			206
2.5	734	-4.0		0.34	68	2.6		

Прилож. приложение

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
30.8 1435 $\varphi=79^{\circ}24'$ $\lambda=192^{\circ}40'$ 10/10 St (26)																	
0.0	007	-3.6		82	5.7	082	6		5.47	500	-18.0		51	0.8			
0.05	000	-3.8		83	5.5				6.0	485	-21.1	0.54	51	0.7			214
0.2	891	-4.6	0.30	85	5.9				7.0	400	-26.0	0.49	51	0.5			
0.46	950	-4.6	0.00	85	5.7				9.0	306	-38.2	0.68	50				213
0.5	946	-4.3		85	5.6				9.14	300	-39.2		51				
0.8	911	-1.8	-0.82	81	5.8				10.0	254	-43.1	0.69	49				
0.9	900	-1.8		80	5.9				11.0	227	-50.8	0.57	48				203
1.0	889	-1.8	0.00	79	5.8				11.85	200	-47.8		47				
1.36	850	-1.8	0.00	74	5.8				12.0	185	-46.4	-0.70	47				190
1.5	835	-1.8	0.00	72	5.8				13.0	168	-43.6	-0.28	46				
1.84	800	-1.8	0.00	65	5.9				14.0	145	-42.8	-0.08	45				226
1.96	787	-1.8	0.00	62	5.9				15.0	126	-41.8	-0.10	44				
2.0	783	-1.9	0.33	61	5.6				16.0	108	-41.0	-0.08	44				
2.5	735	-3.6	0.33	51	5.0			247	16.5	100	-41.0	0.00	44				231
2.89	700	-6.1	0.72	51	1.7				17.0	83	-41.0	0.00	44				
3.0	689	-7.2	0.72	51	1.6				18.0	70	-41.0	0.00	44				
4.0	607	-11.4	0.42	51	1.2			223	19.0	60	-41.0	0.00	44				
4.09	600	-11.9		51	1.2				20.0	60	-41.0	0.00					232
5.0	532	-15.7	0.43	51	1.0				21.0	52	-41.0	0.00					

Прилож. приложение

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
31.8 0200 $\varphi=79^{\circ}21'$ $\lambda=192^{\circ}20'$ 10/10 St, Δ																	
0.0	009	-3.2		90	2.6	380	8		6.0	463	-22.0	0.52	47	0.6			333
0.06	000	-3.8		92	2.5				7.0	404	-27.9	0.59	47	0.3			
0.2	892	-4.9		93	2.4				8.0	351	-34.6	0.67	47				
0.28	973	-5.3	0.75	94	2.4				9.0	303	-43.4	0.88	46				325
0.5	946	-5.3	0.00	97	2.4				10.0	261	-51.5	0.81	42				
0.91	900	-5.3	0.00	100	2.7				10.59	238	-54.7	0.54	40				
1.0	889	-5.3	0.00	100	2.7				10.9	228	-54.7	0.00	40				
1.35	850	-5.3	0.00	99	2.6				11.0	224	-52.8	-1.90	40				
1.5	835	-5.3	0.00	98	2.6				11.73	200	-48.1						
1.84	800	-5.3	0.00	98	2.8				12.0	192	-47.0	-0.58					285
2.0	783	-5.3	0.00	95	3.0				13.0	165	-45.6	-0.14					
2.06	777	-5.3	0.00	95	3.0				14.0	142	-44.6	-0.10					
2.5	735	-7.2	0.43	92	2.7				15.0	122	-44.4	-0.02					
2.89	700	-6.8	0.42	89	2.2				16.0	105	-44.4	0.00					
3.0	689	-9.3	0.42	89	2.2				16.32	100	-44.4						
3.76	624	-14.2	0.04	87	1.6			382	17.0	91	-44.4	0.00					273
4.0	604	-14.2	0.00	86	1.4												
4.05	600	-14.2	0.00	84	1.4												
4.38	574	-14.2	0.00	84	1.3												
5.0	520	-16.8	0.42	88	0.9				0.0	014	-5.1		90	5.2	360	8	
5.42	500	-19.0		84	0.8				0.11	000	-6.1		89	2.0	331	10	

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
0.2	989	-6.2	0.55	88	2.0	356	11		9.88	259	-47.3	0.00					
0.5	522	-6.7	0.17	86	2.0	355	11		10.0	254	-46.4	-0.75					205
0.94	900	-7.3	0.14	81	1.9	356	11		11.0	219	-42.2	-0.42					
1.0	892	-7.4	0.00	79	1.8	353	11		11.61	200	-42.0	-0.03					
1.22	888	-7.4	0.00	75	1.7	353	11		12.0	189	-42.0	0.00					
1.39	850	-7.8	0.00	75	1.7	353	11		13.0	182	-42.0	0.00					
1.5	837	-8.0	0.21	74	1.7	353	12		13.4	153	-42.0	0.00					208
1.85	800	-9.2	0.69	69	1.5	353	14										
2.0	784	-9.8	0.36	67	1.4	353	15										
2.5	735	-12.6	0.56	66	1.2	343	13										
2.88	700	-14.6	0.54	64	1.0	346	14	304	0.0	012	-2.1		94	3.0	292		
3.0	689	-15.3	0.54	63	0.9	345	13		0.1	000	-2.7		94	2.3			
4.0	603	-19.4	0.41	58	0.6	333	9	197	0.2	987	-3.2		0.55	94	2.8		
4.03	600	-19.6	0.58	58	0.6	333	9		0.5	951	-4.4		0.40	93	2.6		
5.0	526	-24.4	0.50	48	0.4				0.65	932	-4.7		0.20	93	2.6		
5.37	500	-27.2	0.69	32					0.93	900	-5.0		0.11	93	2.6		
6.0	458	-31.3	0.67	318	12				1.0	892	-5.1		0.18	93	2.6		
6.95	400	-37.6	0.67	317	12	188			1.28	850	-5.7		0.18	93	2.6		
7.0	397	-38.0	0.56	323	14				1.5	837	-6.0		0.15	92	2.5		
8.0	343	-43.6	0.47						1.7	815	-6.3		0.15	92	2.5		
8.78	306	-47.3	0.00						1.85	800	-6.8		0.43	92	2.4		
8.9	300	-47.3	0.00					200	2.0	784	-7.6		0.43	92	2.4		
9.0	296	-47.3	0.00														

2.9 1405 $\rho = 79707$, $\lambda = 191^{\circ}41'$
10/10 St (88), Δ^*

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
2.5	736	-11.0	0.68	89	1.8				16.3	100	-40.3	0.00					256
2.88	700	-11.0	0.00	86	1.8				17.0	90	-40.3	0.00					
3.0	689	-11.0	0.00	83	1.9				18.0	78	-40.3	0.00					
3.3	683	-11.0	0.00	79	1.3			263	19.0	67	-40.3	0.00					272
4.0	604	-14.8	0.54	79	1.3				20.0	58	-40.3	0.00					
4.65	600	-15.1	0.79	79	1.3				21.0	50	-40.3	0.00					274
5.0	529	-20.8	0.60	73	0.8				21.66	46	-40.3	0.00					
5.42	500	-23.3	0.70	73	0.7												
6.0	461	-27.8	0.69	67	0.4												
7.01	400	-34.7	0.69	67				321									
8.0	345	-42.3	0.77	64													
8.95	300	-48.3	0.62	61					0.0	009	-1.4		98	3.3	292		
9.0	298	-48.5	0.64	60					0.08	000	-1.5		(98)	3.2			
9.28	286	-50.3	0.64	60					0.15	992	-1.8		0.27	(98)	3.3		
10.0	257	-50.3	0.00	57				282	0.2	985	-1.8		0.00	(96)	3.2		
10.14	251	-50.3	0.00	57					0.5	949	-1.8		0.00	(91)	3.1		
11.0	220	-44.6	-0.06	54					0.91	900	-0.4		-0.34	(82)	3.4		
11.64	200	-43.0	0.00	52					1.0	889	-0.4		0.00	(81)	3.3		
12.0	189	-42.3	-0.23	51				242	1.37	850	-0.4		0.00	(74)	3.2		
13.0	163	-41.4	-0.09	47					1.5	835	-0.4		0.00	(72)	3.2		
14.0	140	-40.7	-0.07	44				248	1.85	800	-0.4		0.00	58	2.7		
15.0	121	-40.3	-0.04						2.0	785	-0.4		0.00	58	2.7		
16.0	105	-40.3	0.00						2.5	737	-2.8		0.46	58	2.4		

3.9 1430 $\rho = 79707$, $\lambda = 192^{\circ}00'$
10/10 St (8)

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.91	700	-5.2		58	2.1				18.0	78	-41.8	-0.06					332
3.0	693	-6.3	0.70	57	1.8		326		19.0	67	-41.5	-0.03					
4.0	697	-12.4	0.61	57	1.2				20.0	58	-41.2	-0.03					
4.1	690	-13.0		57	1.2				21.0	50	-40.9	-0.03					332
5.0	531	-18.6	0.62	55	0.8				22.0	42	-40.6	-0.03					
5.47	500	-21.3		55	0.6		332										
6.0	468	-23.8	0.52	55	0.5												
7.0	404	-31.3	0.75	55					0.0	010	-2.0		91	2.9	270		
7.68	400	-31.9		55					0.08	000	-2.3		93	2.9			
8.0	348	-38.0	0.67	55			311		0.2	985	-2.8	0.40	96	2.9			
9.0	300	-44.9	0.69	54					0.5	949	-4.2	0.50	99	2.8			
10.0	260	-51.1	0.82	54					0.56	942	-4.6	0.00	90	2.6			
10.76	233	-55.4	0.70	53					0.78	917	-4.6	0.00	90	2.6			
11.0	216	-55.4	0.00	53					0.93	900	-3.4		82	2.6			
11.2	200	-52.4	0.00	52					1.0	892	-3.0	-0.73	78	2.6			
11.7	191	-50.4	-0.75	52			270		1.38	850	-2.1		67	2.6			
12.0	165	-47.0	-0.34	52					1.5	837	-2.0	-0.20	64	2.3			
14.0	141	-45.8	-0.12	51					1.86	800	-3.6		57	2.1			
15.0	122	-44.8	-0.10	50			307		2.0	785	-3.9	0.38	56	2.0			
16.0	105	-43.6	-0.12	50					2.5	737	-5.4	0.30	55	1.8			
16.36	100	-43.2		50					2.89	700	-7.6		54	1.6			
17.0	91	-42.6	-0.10	50													

4.9 1346 $\varphi = 79^{\circ}06'$ $\lambda = 192^{\circ}10'$
10/10 St (30), Δ°

5

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.0	690	-5.5	0.62	54	1.5				16.31	100	-42.3						332
4.0	695	-13.8	0.73	51	0.8				17.0	90	-41.8	-0.07					
4.07	600	-16.8		51	0.6				18.0	78	-41.1	-0.07					
4.54	564	-20.2	0.81	50	0.6				18.37	74	-40.9	-0.05					
5.0	530	-20.2	0.00	49	0.6				19.0	68	-40.9	0.00					338
5.12	522	-20.2	0.00	49	0.6				20.0	58	-40.9	0.00					
5.43	500	-21.4	0.43	49	0.5				21.0	50	-40.9	0.00					
6.0	462	-24.0	0.65	48	0.5				22.0	43	-40.9	0.00					337
7.0	403	-30.5	0.65	46					23.0	38	-40.9	0.00					
7.06	400	-31.0		46			360		23.46	36	-40.9	0.00					
8.0	350	-37.6	0.71	46													
9.0	302	-44.2	0.66	46													
9.05	300	-44.6		46													
10.0	260	-50.5	0.63	46													
10.44	243	-53.7	0.73	43													
11.0	223	-53.7	0.00	43													
11.34	212	-53.7	0.00	43													
11.7	200	-50.9		43													
12.0	191	-48.0	-0.71	43													
13.0	164	-45.3	-0.37	43													
14.0	141	-44.2	-0.11	43													
15.0	122	-43.3	-0.09	43													
16.0	105	-42.5	-0.06	43													

5.9 1401 $\varphi = 78^{\circ}58'$ $\lambda = 192^{\circ}30'$
10/10 St (21), Δ°

3

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.5	835	-10.2	0.26	70	1.4				14.0	139	-41.5	0.00	26				
1.83	800	-11.0	0.00	60	1.1				13.0	119	-41.5	0.00	29				245
2.0	782	-11.6	0.28	57	1.0				16.0	102	-41.5	0.00	26				
2.5	734	-13.3	0.34	51	0.8				16.12	100	-41.5	0.00	26				
2.85	700	-15.4	0.48	48	0.7			340	17.0	88	-41.5	0.00	26				274
3.0	687	-16.2	0.58	47	0.7				19.0	68	-41.5	0.00	26				
4.02	600	-20.4	0.41	41	0.4				20.0	58	-41.5	0.00	26				276
5.0	524	-25.0	0.47	37	0.3												
5.35	500	-27.6	0.72	36	0.2				6.9	1330	φ - 78°57'	λ = 192°42'					
6.0	456	-32.2	0.72	36					9/0	Ac (208)							
6.92	400	-38.8	0.74	35					0.0	013	-7.2	90	1.9	292			7
7.0	395	-39.6	0.74	35					0.0	000	-7.4	90	1.8	280	10		
8.0	340	-45.7	0.61	33					0.2	987	-7.4	0.10	90	1.9	310	12	
8.35	323	-47.2	0.43	32					0.5	949	-6.4	-0.33	90	2.0	320	10	
8.87	300	-47.2	0.00	32					0.7	925	-5.9	-0.25	89	2.2	321	10	
9.0	294	-47.2	0.00	32					0.92	900	-5.9	0.00	88	2.3	323	10	
9.28	281	-47.2	0.00	32				230	1.0	880	-5.9	0.00	88	2.3	323	10	
10.0	252	-44.9	-0.22	31					1.3	857	-5.9	0.00	84	2.3	324	10	
11.0	218	-42.9	-0.20	30					1.36	850	-6.3	0.50	76	2.0			
11.54	200	-42.5	-0.07	29					1.53	835	-6.9	0.50	70	1.6			
12.0	187	-42.2	-0.07	28				232	1.83	800	-8.1	0.52	67	1.5			
13.0	161	-41.6	-0.07	27					2.0	783	-9.5	0.52	67	1.5			
13.04	160	-41.5	-0.07	27													

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.4	744	-11.7	0.55	61	1.2				16.0	102	-41.5	-0.06	51				
2.5	735	-12.1	0.40	63	1.1				16.15	100	-41.4	0.00	50				
2.87	700	-13.9	0.54	70	1.2				17.0	89	-40.9	-0.06	49				
3.0	688	-14.8	0.50	77	1.3			392	18.0	77	-40.2	-0.07	47				289
3.1	679	-15.3	0.52	70	0.8				19.0	66	-39.6	-0.06	45				
4.01	600	-20.0	0.52	70	0.5				19.95	57	-38.0	-0.17					
5.0	524	-26.5	0.66	69	0.5												
5.34	500	-28.8	0.69	69	0.3												
6.0	455	-32.0	0.55	66													
6.92	400	-37.8	0.62	64													
7.0	395	-38.2	0.62	64				371	0.0	011	-4.6	91	2.4	295		4	
8.0	341	-45.0	0.66	61					0.09	000	-4.8	0.20	90	2.3	282	8	
8.82	300	-50.5	0.65	60					0.2	985	-5.0	0.23	87	2.2	272	13	
9.0	292	-51.5	0.65	60					0.5	948	-5.7	0.23	87	2.2	272	13	
9.2	283	-52.4	0.46	60					0.8	913	-7.2	0.50	83	1.9	259	14	
9.85	256	-55.4	0.30	59					0.91	900	-7.2	0.00	81	1.9	249	15	
10.0	251	-50.7	-1.19	58				290	1.0	890	-7.2	0.00	80	1.9	239	12	
11.0	216	-46.3	-0.44	56					1.33	854	-7.2	0.00	77	1.8	233	11	
11.51	200	-44.9	-0.21	56				254	1.5	835	-8.3	0.61	74	1.8	244	8	
12.0	185	-43.4	-0.06	55					1.56	809	-8.6	0.61	74	1.7	217	7	
13.0	159	-43.4	-0.06	55					1.83	800	-8.6	0.00	70	1.7	216	5	
14.0	138	-42.7	-0.07	54				282	2.0	782	-8.6	0.00	70	1.7	216	5	
15.0	119	-42.1	-0.06	53													

7.9 1321 φ = 78°53' λ = 193°02'

7/2 Ci, Cc, Sc

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.4	743	-8.6	0.00	55	1.4	235	5		16.0	104	-39.9	-0.07					
2.5	723	-9.0	0.40	52	1.2	238	5	256	16.28	100	-39.7						203
2.86	700	-10.8	0.55	52	1.1	244	6		17.0	90	-39.2	-0.07					
3.0	687	-11.3	0.55	52	1.0	245	6		17.07	89	-39.1	-0.07					204
4.0	602	-17.6	0.58	61	0.9	250	8		18.0	79	-39.1	0.00					
4.03	600	-17.8	0.58	61	0.8	250	8		18.64	72	-39.1	0.00					
5.0	525	-22.8	0.62	61	0.3	254	5	211									
5.35	500	-25.7	0.61	0.3	255	5											
6.0	458	-28.8	0.50	61	0.4	272	4										
6.95	400	-35.0	0.65	60		272	4	209	0.0	005	-3.4		50	2.5	202	7	
7.0	397	-35.4	0.65	60		273	5		0.03	000	-3.6		91	2.6			
8.0	344	-42.3	0.69	58		273	5		0.2	978	-4.6	0.60	58	2.6			
8.9	300	-48.1	0.63	56				210	0.5	941	-6.2	0.33	58	2.4			
9.0	295	-48.6	0.63	56					0.86	900	-7.5	0.22	55	2.2			
9.88	298	-52.2	0.41	54					1.0	883	-8.2	0.40	55	2.1			
10.0	284	-52.2	0.00	54					1.3	859	-9.7	0.52	93	1.7			
10.06	251	-52.2	0.00	54				211	1.5	829	-10.8	0.38	90	1.5			
11.0	219	-45.1	-0.75	52					1.77	800	-11.8	0.38	90	1.5			
11.58	200	-43.4	-0.23					204	2.0	776	-12.7	0.40	86	1.3			
12.0	188	-42.8	-0.10						2.5	727	-14.7	0.40	84	1.2			
13.0	162	-41.8	-0.10					203	3.0	680	-17.0	0.46	83	1.1			
14.0	140	-41.2	-0.06														
15.0	121	-40.6	-0.06														

83.9 1343 $\rho = 78^{\circ}53'$ $\lambda = 193^{\circ}12'$
10/10 St, \times

Продолж. приложение

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
3.94	600	-22.5	0.60	77	0.7				18.0	78	-40.1	0.00					234
4.0	595	-23.0	0.60	77	0.6				19.0	67	-40.1	0.00					
5.0	519	-29.2	0.62	72	0.4				20.0	57	-40.1	0.00					239
5.25	500	-30.6	0.62	71				282	20.7	51	-40.1	0.00					
6.0	450	-34.4	0.52	65													
6.81	400	-38.9	0.54	59													
7.0	389	-39.8	0.54	57													
8.0	335	-45.2	0.40	55													
8.6	306	-47.6	0.40	55													
8.75	300	-47.6	0.40	55													
9.0	289	-47.6	0.00	54				251	0.0	002	-11.6		180				
9.3	276	-47.6	0.00	54					0.02	000	-11.8	0.30	211	4			
10.0	249	-43.4	-0.60	52					0.5	937	-12.6	0.00	203	4			
11.0	214	-40.2	-0.52	48					0.81	900	-12.6	0.00	202	5			
11.2	208	-40.1	-0.05	48					1.0	877	-12.6	0.00	203	5			
11.49	200	-40.1	0.00	46					1.24	850	-12.6	0.00	215	3			
11.9	185	-40.1	0.00	46					1.5	823	-13.5	0.45	219	3			
12.0	185	-40.1	0.00	46					1.72	800	-14.4	0.50	199	6			
13.0	160	-40.1	0.00						2.0	770	-16.0	0.40	206	9			
14.0	138	-40.1	0.00						2.5	720	-18.0	0.68	207	10			
15.0	120	-40.1	0.00						2.71	700	-19.1	0.68	204	11		313	
16.0	103	-40.1	0.00						3.0	673	-24.5		198	14			
16.22	100	-40.1							3.84	600	-26.5		188	14			
17.0	89	-40.1	0.00						4.0	587	-27.4	0.60	188	14			

9.9 1330 $\rho = 78^{\circ}53'$ $\lambda = 193^{\circ}56'$
9/0 St

Продолж. приложения

H	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
5.0	510	-33.6		0.62					322	0.0	000	-3.5							
5.13	506	-33.7								0.2	574	-4.6				158	6		
6.0	462	-30.5		0.59						0.5	938	-6.1				171	11		
6.68	409	-29.0								0.82	900	-7.7							
7.0	381	-29.4		0.59						1.0	879	-8.6							
7.82	337	-26.1		-0.17						1.26	850	-10.3							
8.0	327	-26.1								1.5	824	-11.8							
8.38	300	-27.6		-0.34						1.72	800	-12.7							
9.0	282	-25.7		-0.43						2.0	771	-12.7							
10.0	243	-21.4		-0.43						2.06	765	-12.7							
11.0	209	-21.4		0.09						2.5	723	-14.3							
11.3	200	-21.4		0.00						2.75	700	-15.4							
12.0	180	-21.4		0.00						3.0	676	-16.6							
13.0	158	-21.4		0.00						3.89	600	-21.7							311
14.0	133	-21.4		0.00						4.0	591	-22.2							
15.0	115	-21.4		0.00						5.0	516	-28.1							
16.0	100	-21.4		0.00						5.22	500	-29.2							
17.0	86	-21.4		0.00						6.0	448	-31.0							
18.0	74	-21.4		0.00						6.79	400	-33.0							
19.0	64	-21.4		0.00															285
20.0	54	-21.4		0.00															
20.55	50	-21.4		0.00															
21.0	47	-21.4		0.00															

Продолж. приложения

H	B	t	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W	
7.0	388	-39.1		0.51					242	0.0	005	-11.7							
8.0	335	-45.2		0.61						0.04	000	-11.8				85	1.2		
8.74	300	-48.2		0.41						0.2	979	-12.2				85	1.2	262	3
9.0	288	-47.2		-0.38						0.5	942	-14.1				85	1.0	264	5
10.0	248	-41.8		-0.54						0.75	911	-15.6				85	0.9		
10.46	232	-40.5		-0.28						0.85	900	-14.4				85	1.0		
11.06	214	-40.5		0.00						1.0	882	-13.3				85	1.2		
11.46	200	-40.5		0.00						1.12	869	-12.7				83	1.2		
12.0	184	-40.5		0.00						1.28	850	-13.0				80	1.2		
13.0	169	-40.5		0.00						1.5	826	-13.3				72	1.0		
14.0	138	-40.5		0.00						1.73	800	-15.0				62	0.8		
15.0	119	-40.5		0.00						2.0	772	-16.6							
16.0	103	-40.5		0.00						2.5	722	-19.2							
16.2	100	-40.5		0.00						2.73	700	-20.2							281
17.0	89	-40.5		0.00						3.0	674	-21.8							
18.0	78	-40.5		0.00						3.87	600	-26.7							
19.0	66	-40.5		0.00						4.0	589	-27.3							
20.0	57	-40.5		0.00						5.0	512	-31.8							
21.0	50	-40.5		0.00						5.17	500	-32.5							
21.19	49	-40.5		0.00															258

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
13.9 1346 $\varphi = 79^{\circ}05'$, $\lambda = 194^{\circ}20'$																	
6.0	444	-37.0	0.52						0.0	002	-10.2				225	5	
6.71	400	-41.8	0.65					269	0.01	000	-10.2				233	10	
7.0	333	-45.6	0.80						0.2	977	-10.3	0.05			233	10	
8.0	330	-49.6	0.96						0.45	946	-11.7	0.56			232	11	
8.38	311	-48.6	0.26						0.5	940	-11.7	0.00			231	11	
8.64	300	-48.6	0.00						0.64	923	-11.7	0.00			227	11	
8.74	285	-47.2	-0.54					234	0.83	900	-12.8	0.53			219	12	
9.0	264	-47.2	-0.54						1.0	880	-13.6	0.53			219	12	
10.0	245	-42.2	-0.24						1.27	850	-14.3	0.53			209	12	
11.0	210	-41.2	0.00						1.5	824	-15.1	0.30			205	12	
11.36	200	-41.2	0.00					230	1.72	800	-15.3	0.58			202	12	
12.0	182	-41.2	0.00						2.0	770	-18.0	0.58			205	12	
13.0	156	-41.2	0.00						2.5	721	-21.1	0.62			204	13	
14.0	138	-41.2	0.00					246	2.72	700	-21.7	0.42			203	15	320
15.0	117	-41.2	0.00						3.0	674	-23.2	0.42			196	13	
16.0	101	-41.2	0.00						3.84	600	-27.0	0.44			193	15	
16.04	100	-41.2	0.00						4.0	587	-27.6	0.44			189	16	
17.0	86	-41.2	0.00					244	5.0	510	-32.8	0.52			189	19	
18.0	76	-41.2	0.00						5.14	500	-33.6	0.52			188	19	
18.42	71	-41.2	0.00														

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
15.9 1430 $\varphi = 78^{\circ}58'$, $\lambda = 196^{\circ}00'$																	
6.0	442	-39.4	0.66			188	21	332	7.0	391	-47.2	0.54					276
6.4	417	-41.7	0.58						8.0	335	-50.6	0.70					
									8.35	319	-50.5	0.00					
									8.75	300	-48.5	-0.42					
									9.0	289	-47.9	-0.42					
									10.0	247	-45.8	-0.21					
									11.0	211	-44.8	-0.10					
									11.18	205	-44.7	-0.06					202
15.9 1342 $\varphi = 78^{\circ}57'$, $\lambda = 196^{\circ}14'$																	
0.0	024	-8.0		56					0.16	009	-9.7	0.00			270	1	
0.18	000	-8.4	0.22						0.23	003	-8.1	-1.00					
0.5	660							259	0.23	000	-8.1	0.00			304	4	
1.0	900								0.5	964	-8.1	0.00			288	5	
1.45	850								1.0	905	-8.1	0.00			287	5	
1.5	844								1.04	800	-10.2	0.46			257	4	
1.91	800								1.5	690	-11.6	0.32			254	6	
2.0	789	-12.9	0.64						2.0	630	-11.8	0.60			250	6	
2.5	739	-16.1	0.64						2.3	745	-14.8	0.60			258	6	
3.0	700	-19.1	0.84														
3.0	691	-20.3	0.84					305									
4.0	604	-26.8	0.65														
4.05	600	-27.2	0.73														
5.0	595	-34.1															
5.35	500	-36.7															
6.0	454	-41.8	0.77														
6.85	400	-46.4															

Пробок. прикован

H	B	t	T	U	q	d	V	W	H	B	T	U	q	d	V	W
2.97	700	-17.3				269	6		16.13	100	-66.1					
3.0	697	-17.4	0.32			270	6		16.75	91	-45.6	-0.08				
4.0	610	-21.0	0.38			280	8		17.0	88	-45.6	0.00				196
4.12	600	-21.6				282	9	211	17.47	82	-45.6	0.00				
5.0	532	-26.1	0.51													
5.45	500	-27.9														
6.0	463	-31.1	0.50													
7.02	400	-37.4	0.62					224	0.0	025	-6.4		92	2.0	135	4
8.0	346	-44.7	0.75						0.2	000	-6.4	0.00	92	2.0	100	6
8.95	300	-50.3	0.59						0.5	951	-6.4	0.00	91	2.1	100	6
9.0	297	-50.6	0.59				220		1.02	900	-6.4	0.00	90	2.2	174	4
9.46	277	-54.1	0.76						1.46	850	-6.4	0.00	89	2.3	190	3
10.0	255	-54.1	0.00						1.5	846	-6.4	0.00	89	2.3	191	2
10.47	237	-54.1	-0.47				217		1.88	838	-6.4	0.00	89	2.3	193	2
11.0	219	-51.6							1.93	800	-7.7	0.00	88	2.2	202	2
11.57	200	-50.0							2.0	793	-8.0	0.28	88	2.2	206	2
12.0	188	-48.9	-0.27						2.5	743	-10.4	0.48	86	1.8		
13.0	161	-47.8	-0.11				213		2.96	700	-12.6	0.48	84	1.5		
13.52	149	-47.3	-0.10						3.0	695	-12.8	0.48	84	1.5		
14.0	138	-47.3	0.00						4.0	610	-16.5	0.37	80	1.2		
14.7	125	-47.3	0.00						4.12	600	-17.0	0.00	79	1.1		
15.0	113	-47.0	-0.10				196		5.0	533	-21.9	0.54	77	0.8		
16.0	103	-46.2	-0.08													

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17.9 1437 $\varphi = 78^{\circ}57'$ $\lambda = 196^{\circ}13'$
10/10 Sc

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Пробок. прикован

H	B	t	T	U	q	d	V	W	H	B	T	U	q	d	V	W
5.47	500	-25.9							21.0	48	-46.6	0.00				
6.0	465	-30.3	0.84	74				323	22.0	41	-46.6	0.00				288
7.0	403	-35.7	0.54	71												
8.0	348	-42.9	0.72	70												
8.99	300	-51.0	0.82					291	0.0	018	-10.0					135
9.77	266	-55.9	0.63						0.13	000	-9.6					147
10.0	257	-55.9	0.00						0.2	991	-9.2	-0.40				139
10.68	232	-53.6	-0.72						0.5	955	-6.3	-0.37				181
11.0	220	-53.6							0.97	900	-6.3	0.00				178
11.62	200	-51.0							1.0	895	-6.3	0.00				183
12.0	188	-50.4	-0.32						1.41	850	-6.9	0.15				159
13.0	161	-48.8	-0.16						1.5	800	-7.1	0.00				152
14.0	139	-47.9	-0.09						1.87	800	-8.5	0.44				127
15.0	119	-47.4	-0.09						2.0	786	-9.3	0.44				117
16.0	102	-47.0	-0.04						2.2	766	-10.5	0.60				079
16.12	100	-46.9	-0.04						2.5	738	-11.8	0.17				004
16.9	89	-46.6	0.00						2.9	700	-13.1	0.22				320
17.0	88	-46.6	0.00						3.0	690	-13.3	0.35				317
18.0	76	-46.6	0.00						3.33	681	-18.3	0.75				309
19.0	65	-46.6	0.00						4.0	660	-18.3	0.75				292
20.0	56	-46.6	0.00						4.07	600	-18.6					289
20.78	50	-46.6	0.00													305

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18.9 1411 $\varphi = 79^{\circ}03'$ $\lambda = 196^{\circ}20'$
0/0 Sc

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.97	700	-17.3				269	6		16.13	100	-46.1						
3.0	697	-17.4	0.52			270	6		16.75	91	-45.6	-0.08					
4.0	610	-21.0	0.36			280	8		17.0	88	-45.6	0.00					196
4.12	600	-21.6				282	9	211	17.47	82	-45.6	0.00					
5.0	532	-26.1	0.51														
5.45	500	-27.9															
6.0	463	-31.1	0.50														
7.02	400	-37.4	0.62														
8.0	346	-44.7	0.75														
8.95	300	-50.3	0.59														
9.0	297	-50.6	0.59														
9.46	277	-54.1	0.76														
10.0	255	-54.1	0.00														
10.47	237	-54.1	0.00														
11.0	219	-51.6	-0.47														
11.57	200	-50.0															
12.0	188	-48.9	-0.27														
13.0	161	-47.8	-0.11														
13.52	140	-47.3	-0.10														
14.0	138	-47.3	0.00														
14.7	125	-47.3	0.00														
15.0	119	-47.0	-0.10														
16.0	103	-46.2	-0.68														

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17.9 1437 $\varphi = 78^{\circ}57'$ $\lambda = 196^{\circ}13'$
10/10 Sc

2.0 023 -6.4 0.00 52 2.0 135 4
0.2 000 -6.4 0.00 52 2.0 - - 6
0.5 951 -6.4 0.00 91 2.1 160 6
1.02 900 -6.4 0.00 90 2.2 174 4
1.46 850 -6.4 0.00 89 2.3 190 3
1.5 846 -6.4 0.00 89 2.3 191 3
1.58 838 -6.4 0.00 89 2.3 193 2
1.63 830 -7.7 0.38 88 2.2 202 2
2.0 793 -8.0 0.48 86 1.8 205 2
2.5 743 -10.4 0.48 84 1.6
2.95 700 -12.6 0.48 84 1.5
3.0 695 -12.8 0.48 80 1.2
4.0 610 -16.5 0.37 79 1.1
4.12 600 -17.0 0.54 77 0.8
5.0 533 -21.9 0.53

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.47	500	-25.9							21.0	48	-46.6	0.00					
6.0	465	-30.3	0.84	74					22.0	41	-46.6	0.00					288
7.0	403	-35.7	0.54	71													
8.0	348	-42.9	0.72	70													
8.99	300	-51.0	0.82														
9.77	268	-55.9	0.63														
10.0	257	-55.9	0.00														
10.68	232	-59.9	0.00														
11.0	200	-53.6	-0.72														
11.62	198	-51.0															
12.0	188	-50.4	-0.32														
13.0	161	-48.8	-0.16														
14.0	139	-47.9	-0.09														
15.0	119	-47.4	-0.05														
16.0	102	-47.0	-0.04														
16.12	100	-46.9	-0.04														
16.9	89	-46.6	0.00														
17.0	88	-46.6	0.00														
18.0	76	-46.6	0.00														
19.0	65	-46.6	0.00														
20.0	56	-46.6	0.00														
20.78	50	-46.6	0.00														

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18.9 1411 $\varphi = 79^{\circ}03'$ $\lambda = 196^{\circ}20'$
0/0 Sc

0.0 018 -10.0 0.00 155 2
0.13 000 -9.6 0.00 147 4
0.2 591 -9.2 -0.40 130 4
0.5 585 -6.3 -0.97 161 2
0.97 500 -6.3 0.00 178 2
1.0 895 -6.3 0.00 198 2
1.41 850 -6.9 0.16 192 2
1.5 840 -7.1 0.16 192 2
1.87 800 -8.5 0.44 117 3
2.0 785 -10.5 0.60 073 1
2.2 738 -11.0 0.17 604 2
2.5 700 -11.8 0.00 320 1
2.9 690 -12.1 0.22 317 2
3.0 680 -13.3 0.36 369 3
3.33 661 -13.3 0.75 292 5
4.0 605 -18.3 0.00 289 4
4.07 600 -18.6

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
5.0	528	-24.2	0.59			280	7		21.0	47	-47.1	0.00					208
5.39	500	-26.6				276	7	270	22.0	40	-47.1	0.00					
6.0	459	-30.0	0.55			280	8										
6.98	400	-36.0	0.61			201	12										
8.0	345	-43.4	0.73			304	19	287									
8.93	300	-50.0				300	23										
9.0	296	-50.3	0.69			300	23		0.0	011	-4.4		92	2.4	248	3	
9.87	259	-56.5	0.71			304	21		0.09	000	-4.4		93	2.4			
10.0	254	-56.5	0.00			304	19	229	0.2	985	-4.4	0.00	96	2.5	284	5	
10.55	234	-56.5	0.00			296	17		0.5	949	-4.4	0.00	96	2.7	281	4	
11.0	218	-54.0	-0.55			294	14		0.52	900	-4.4	0.00	96	2.8			
11.55	200	-51.7				295	12	225	1.0	891	-4.6		96	2.8			
12.0	186	-50.6	-0.34			298	10		1.38	850	-6.0		96	2.6			
13.0	159	-48.7	-0.19			298	10		1.5	837	-6.8	0.41	96	2.4			
14.0	136	-48.0	-0.07			293	8	257	1.82	803	-8.5	0.53	96	2.2			
15.0	118	-47.3	-0.07			295	6		1.85	800	-8.5	0.00	96	2.2			
16.0	102	-47.1	-0.02			291	6		2.0	784	-9.5	0.20	76	1.8			
16.17	100	-47.1				290	6		2.5	735	-9.5	0.00	76	1.6			
17.0	87	-47.1	0.00			293	5		2.88	700	-10.9	0.36	76	1.6			
18.0	75	-47.1	0.00					296	3.0	689	-11.3	0.00	76	1.6			
19.0	64	-47.1	0.00						4.0	604	-16.2	0.49	76	1.2			
20.0	55	-47.1	0.00						4.05	600	-16.5		76	1.1			
20.5	50	-47.1							5.0	528	-22.1	0.59	69	0.7			

Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
5.4	500	-22.1		65	0.7				3.0	684	-15.8	0.36	68	1.0			283
5.46	495	-22.1	0.00	64	0.7				3.98	600	-18.4	0.28	63	0.8			
5.72	479	-23.4	0.50	55	0.6			298	4.0	598	-18.6	0.28	63	0.8			282
6.0	460	-25.3	0.68	55	0.4				5.0	523	-24.0	0.34					
7.0	400	-32.6	0.73	55					5.33	500	-26.3	0.66					
8.0	347	-40.7	0.81	55				311	6.0	455	-30.6	0.66					241
8.82	307	-48.1	0.90						7.0	394	-38.2	0.88					
									8.0	339	-46.3	0.99					
									8.85	300	-49.0	0.48					
									9.0	293	-49.6	0.48					
									9.15	286	-50.4	0.35					
									10.0	250	-50.4	0.00					210
									10.17	244	-50.4	0.00					
									11.0	215	-47.3	-0.37					176
									11.48	200	-46.4	-0.16					
									12.0	185	-45.7	-0.16					205
									13.0	160	-43.1	-0.25					
									14.0	138	-41.9	-0.12					228
									15.0	119	-41.9	0.00					
									16.0	102	-41.9	0.00					
									16.1	100	-41.9	0.00					
									17.0	88	-41.9	0.00					

Продолж. приложения

H	B	t	l	T	U	q	d	V	W	H	B	t	l	T	U	q	d	V	W
18.0	77	-41.9	0.00						281	4.0	585	-22.2	0.49	82	0.77	230			
19.0	66	-41.9	0.00							5.0	519	-28.9	0.67	79	0.4			10	
20.0	57	-41.9	0.00						288	5.26	500	-30.6	0.53	76					288
20.2	55	-41.9	0.00							0.0	450	-34.2	0.53	76					
										0.82	400	-38.8	0.56	73					
										7.0	389	-39.8	0.56	71					
										8.0	335	-46.5	0.67	71					
										8.74	300	-50.0	0.47	69					
										9.0	288	-50.0	0.00	69					285
										9.17	281	-50.0	0.00	69					
										9.75	257	-48.4	0.00	68					
										10.0	248	-48.4	0.00	68					
										10.09	244	-48.4	0.00	67					229
										11.0	213	-45.4	-0.33	65					
										11.42	200	-45.4	0.00	64					
										12.0	184	-45.4	0.00	63					
										13.0	158	-45.4	0.00	62					
										14.0	136	-45.4	0.00	60					233
										15.0	117	-45.4	0.00	58					
										16.0	101	-45.4	0.00	56					236
										16.95	100	-45.4	0.00	55					
										17.0	87	-45.4	0.00	54					
										18.0	75	-45.4	0.00	53					

211.9 1409 $\varphi = 79^{\circ}03'$ $\lambda = 195^{\circ}46'$
 10/6 Fs, Cs, As, X^o

H	B	t	l	T	U	q	d	V	W
0.0	009	-9.9			85	1.4	158	1	
0.07	000	-9.9			85	1.4	151	3	
0.2	984	-10.0	0.05	85	1.4	138	1	3	
0.5	946	-10.1	0.03	85	1.4	138	1	3	
0.88	900	-10.3	0.05	85	1.4	138	1	3	
1.0	886	-10.9	0.50	84	1.4	138	1	3	
1.32	850	-12.6	0.50	84	1.3	138	1	3	
1.5	830	-13.4	0.50	84	1.2	138	1	3	
1.77	800	-14.8	0.50	84	1.1	138	1	3	
1.96	780	-15.7	0.50	84	1.1	194	3		
2.0	776	-15.8	0.15	83	1.0	161	5		
2.5	727	-16.5	0.15	83	1.0	161	5		
2.79	700	-16.9	0.16	83	1.0	189	5		
3.0	680	-17.3	0.16	83	1.0	200	6		335
3.94	600	-21.6		83	0.7	230	10		

Продолж. приложения

H	B	t	l	T	U	q	d	V	W	H	B	t	l	T	U	q	d	V	W
19.0	64	-45.4	0.00						285	3.0	679	-21.0	0.14						
20.0	55	-45.4	0.00							3.32	642	-21.7	0.17						326
20.66	50	-45.4								4.0	593	-24.7	0.50						
21.0	48	-45.4	0.00						283	5.0	515	-25.1	0.75						
21.68	43	-45.4	0.00							5.21	500	-34.2	0.73						304
										6.0	446	-39.9	0.73						
										6.76	400	-43.4	0.45						
										7.0	385	-44.4	0.45						
										7.78	344	-47.9	0.46						
										8.0	332	-47.9	0.00						
										8.68	300	-47.9	0.00						311
										9.0	286	-47.9	0.00						
										9.24	276	-47.9	0.00						
										10.0	265	-45.6	-0.36						
										10.34	233	-44.3	-0.36						
										11.0	211	-44.3	0.00						
										11.36	200	-44.3	0.00						274
										12.0	182	-44.3	0.00						
										13.0	157	-44.3	0.00						
										14.0	136	-44.3	0.00						276
										15.0	117	-44.3	0.00						
										16.01	100	-44.3	0.00						

22.9 1355 $\varphi = 79^{\circ}02'$ $\lambda = 195^{\circ}50'$
 10/0 As (223)

H	B	t	l	T	U	q	d	V	W
0.0	011	-10.0			98				
0.09	000	-10.5			88				
0.2	987	-10.8	0.40		88				
0.5	948	-11.4	0.20		88				
0.9	900	-12.6	0.30		88				
1.0	888	-12.9	0.30		88				
1.33	850	-14.3			88				
1.5	831	-15.1	0.44		88				
1.78	800	-16.4			88				
2.0	777	-17.5	0.48		88				
2.35	742	-20.0	0.71		88				
2.5	727	-20.3	0.20		88				
2.78	700	-20.7			88				

Продолж. приложения

H	B	t	Y	U	Q	d	V	W	H	B	t	Y	U	Q	d	V	W
1.5	628	-11.6	0.32	80	1.4				11.0	211	-50.6	-0.47					220
1.75	600	-12.4		80	1.3				11.38	200	-19.3						
2.0	774	-12.9	0.26	79	1.3				12.0	182	-17.3	-0.37					220
2.45	730	-15.7	0.62	78	1.1				12.75	162	-16.3	-0.15					
2.5	726	-15.9		78	1.0				13.0	156	-16.3	0.00					
2.77	700	-16.4		77	1.0			346	14.0	134	-16.3	0.00					
3.0	678	-16.9	0.22	77	1.0				15.0	115	-16.3	0.00					230
3.16	664	-17.1	0.12	76	1.0				15.59	100	-16.3	0.00					
3.92	600	-22.8		74	0.6				16.0	99	-16.8	0.00					
4.0	593	-23.6	0.77	74	0.5												
4.23	576	-25.8	0.96	73	0.4												
4.43	559	-25.8	0.00	72	0.4												
5.0	517	-27.6	0.32	70	0.4												
5.23	500	-28.9		68	0.3				0.0	007	-1.5		95	2.5	225	7	
6.0	449	-32.4	0.48	61				382	0.06	000	-4.5		95	2.5	233	11	
6.8	400	-37.8	0.66	58					0.2	951	-6.1	0.80	93	2.8	231	10	
7.0	389	-39.0	0.66	58					0.5	944	-7.2	0.37	95	2.2			
8.0	335	-45.8	0.63	55					0.88	900	-8.6		94	2.0			
8.73	300	-50.1		53					1.0	886	-9.0	0.35	94	1.9			
9.0	288	-51.4	0.56	52				231	1.32	850	-9.5		94	1.9			
9.54	265	-54.3	0.54						1.5	831	-9.8	0.16	94	1.9			
10.0	247	-54.3	0.00						1.79	800	-10.2		94	1.9			
10.21	239	-54.3	0.00						2.0	778	-10.6	0.16	94	1.9			
									2.5	729	-11.7	0.22	93	1.9			

Продолж. приложения

H	B	t	Y	U	Q	d	V	W	H	B	t	Y	U	Q	d	V	W
2.8	700	-13.2		93	1.7			297									
3.0	682	-14.6	0.55	91	1.5												
3.96	600	-23.3		76	0.6												
4.0	596	-23.5	0.59	76	0.6												
5.0	520	-27.1	0.35	68	0.4			224									
5.23	500	-28.6		67	0.4												
6.0	452	-32.5	0.54	63					0.08	012	-11.8		92	1.2	135	8	
6.86	400	-38.2		59					0.2	985	-11.6		92	1.3	144	9	
7.0	392	-39.0	0.65	58				190	0.38	962	-10.1	-0.10	92	1.3	182	12	
8.0	337	-44.8	0.65	55					0.5	948	-10.1	0.00	91	1.5	187	12	
8.77	300	-49.0	0.65	53					0.9	900	-10.1	0.00	90	1.6	187	10	
9.0	290	-50.2	0.54	52				174	1.0	889	-10.5	0.40	90	1.6	193	10	
10.0	248	-56.5		48					1.34	850	-11.4		89	1.5	200	9	
10.09	244	-57.0	0.62						1.5	832	-11.8	0.26	89	1.4	203	9	
10.73	221	-57.0	0.00						1.8	800	-12.4	0.20	88	1.4	211	11	
11.0	212	-55.3	-0.63					176	2.0	779	-12.8	0.20	88	1.4	206	13	
11.34	200	-53.3							2.14	765	-13.2	0.29	87	1.4	207	13	
12.0	182	-51.0	-0.45					177	2.5	730	-15.7	0.09	84	1.2	209	11	
13.0	156	-49.0	-0.20						2.81	700	-17.8		81	0.9	208	14	
14.0	133	-47.7	-0.13					187	3.02	682	-19.1	0.68	79	0.9	212	14	
15.0	114	-47.2	-0.05						3.62	628	-24.0	0.79	73	0.5			
15.87	100	-46.8							3.96	600	-24.5	0.16	69	0.5			
16.0	98	-46.6	-0.06					181	4.0	596	-24.6	0.16	69	0.5			
									4.5	556	-25.6	0.20	62	0.4			
									5.0	519	-28.2	0.52	57	0.3			

Продолж. приложения

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H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
5.27	500	-29.9		56	0.3				0.2	990	-7.5	-0.30	07	2.0			
6.0	452	-33.8	0.26	35				309	0.39	966	-5.8	-0.00	08	2.1			
6.86	400	-39.4		54					0.5	953			09				
7.0	392	-40.4	0.66	53					0.95	900			06				
8.0	337	-47.2	0.68	52					1.0	853			06				
8.76	300	-50.9						265	1.38	850	-10.6		04	1.7			
9.0	289	-51.6	0.44						1.5	837	-11.6		04	1.6			
9.5	268	-52.8	0.24						1.84	800	-13.4		02	1.4			
9.82	255	-52.8	0.00						2.0	783	-14.3	0.54	02	1.3			
10.0	248	-52.3	-0.28					245	2.5	734	-16.4	0.42	09	1.1			
11.0	213	-48.3	-0.40						3.0	686	-19.4	0.60	07	0.9			263
11.4	200	-47.2							3.99	600	-27.6	0.83	07	0.4			
12.0	183	-46.1	-0.22						4.12	589	-28.8	0.92	07	0.4			
13.0	157	-43.5	-0.05					247	4.34	572	-28.8	0.00	85	0.4			
14.0	135	-44.8	-0.07						4.91	528	-31.8	0.53	79				
14.2	131	-44.7	-0.05						5.0	521	-32.1		77				
15.0	116	-44.7	0.00					255	5.3	500	-32.8		71				
16.0	100	-44.7	0.00						6.0	452	-35.4	0.29	61				275
									6.84	400	-40.8	0.70	60				
0.0	016	-1.8		94	1.8	158	5		7.0	390	-42.0	0.65	54				
0.13	000	-7.8		95	1.8				8.0	336	-48.3	0.63	53				264

283.9 1438 φ = 79°03', λ = 198°33'
10/10 Ns, *

Продолж. приложения

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H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
8.75	300	-52.4		51				183	1.5	831	-16.0	0.46	79	0.9			
9.0	289	-53.2	0.49	51					1.78	800	-17.8	0.60	78	0.7			
9.12	284	-53.5	0.25	51					2.0	776	-19.0	0.38	73	0.6			
9.78	255	-58.5	0.00	49					2.5	727	-20.9	0.38	73	0.6			
10.0	247	-59.0	-0.68	49					2.78	700	-22.4	0.56	64	0.4			
11.0	212	-48.5	-0.35	48					3.0	679	-23.7	0.56	63	0.4			
11.39	200	-47.9		48				204	3.89	600	-30.6	0.79	59				388
12.0	182	-47.3	-0.12	48					4.0	590	-31.6	0.85	55				
12.15	178	-47.2	-0.07	48					5.0	512	-37.4	0.95	54				
13.0	156	-47.2	0.00	48					5.16	500	-38.2	0.49	51				
14.0	134	-47.2	0.00					207	6.0	442	-42.3	0.49	51				
14.26	129	-47.2	0.00						6.56	408	-45.0	0.48	50				
									6.69	400	-45.0	0.00	48				
									7.0	382	-45.0	0.00	48				312
									7.84	337	-45.0	0.00	46				
									8.0	329	-44.7	-0.19	46				
									8.62	300	-43.3		44				
0.0	011	-10.2		82	1.3	225	12		9.0	283	-42.5	-0.21	42				
0.09	000	-10.3		81	1.3				10.0	245	-41.8	-0.08	40				285
0.2	985	-10.6	0.20	81	1.1				11.0	210	-41.8	0.00	37				
0.5	947	-12.1	0.50	80	1.0				11.35	200	-41.8	0.00	37				
0.9	900	-13.4		80	1.0				12.0	182	-41.8	0.00	35				
1.0	887	-13.7	0.32	79	0.9				13.0	157	-41.8	0.00	33				369
1.33	850	-15.1															

30.9 1409 φ = 79°06', λ = 198°00'
10/10 Fs, *

Продолж. приложение

H	B	t	l	γ	U	q	d	V	W	H	B	l	γ	U	q	d	V	W
14.0	135	-42.2	0.04	32						3.6	631	-25.8	0.21	100	0.6			
15.0	117	-43.1	0.09							3.96	600	-27.8	0.55	91	0.5			
16.02	100	-43.4	0.33							4.0	595	-28.0	0.48	90	0.4			296
17.0	86	-43.4	0.00						319	5.0	518	-32.8	0.48	78				
17.36	81	-43.4	0.00							5.24	500	-34.5	0.51	77				
										6.0	447	-37.9	0.51	75				
										6.77	400	-41.4	0.51	73				227
										7.0	387	-43.0	0.51	72				
										7.76	345	-46.7	0.49	70				
										8.0	333	-47.3	0.25					
										8.5	309	-48.2	0.18					
										8.69	300	-48.2	0.00					
										9.0	285	-48.2	0.00					
										9.19	278	-48.2	0.00					
										10.0	247	-45.7	-0.31					
										10.1	243	-45.1	-0.60					215
										11.0	212	-45.1	0.00					
										11.39	200	-45.1	0.00					232
										12.0	182	-45.1	0.00					
										12.6	166	-45.1	0.00					
										13.0	157	-45.2	0.02					
										14.0	135	-45.7	0.05					296
										15.0	115	-46.2	0.05					

1.10 1405 φ=79°04' λ=199°30'
10/10 St. (39)

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Продолж. приложение

H	B	t	l	γ	U	q	d	V	W	H	B	l	γ	U	q	d	V	W
16.0	100	-46.6	0.04							4.02	600	-21.8	0.50	92	0.8			
16.31	96	-46.7	0.03							4.13	591	-22.2	0.36	92	0.8			
17.0	86	-46.7	0.00						242	5.0	525	-24.0	0.21	91	0.7			
18.0	74	-46.7	0.00							5.37	500	-26.0	0.87	87	0.6			284
18.75	65	-46.7	0.00							6.0	458	-30.2	0.62	78				
										6.54	400	-35.4	0.65	74				
										7.0	396	-36.7	0.65	74				
										8.0	342	-45.1	0.84	71				
										8.57	300	-51.2	0.69	69				291
										9.0	294	-52.0	0.48	66				
										10.0	252	-56.8	0.48	65				
										10.3	240	-58.1	0.43	65				
										10.67	227	-58.1	0.00	65				
										11.0	215	-56.8	-0.39	64				206
										11.45	200	-53.4	0.63	63				
										11.87	188	-51.9	-0.56	62				
										12.0	184	-51.9	0.00	62				
										13.0	157	-51.9	0.00	59				191
										14.0	135	-51.9	0.00					
										15.0	116	-51.9	0.00					197
										15.55	100	-51.9	0.00					
										16.0	99	-51.9	0.00					197

2.10 1425 φ=79°05' λ=199°48'
10/10 St. *

I 484

Продолж. приложения

H	B	l	Y	U	q	d	V	W	H	B	l	Y	U	q	d	V	W
3.10 1402 $\varphi = 79^{\circ}09'$ $\lambda = 199^{\circ}55'$																	
7/1 Ac, Fs																	
0.0	025	-12.8		100					8.0	347	-40.8	0.61					205
0.18	000	-12.2							8.98	300	-46.7	0.60					
0.5	559	-9.7							9.9	260	-51.6	0.53					
0.8	923	-7.4							10.0	255	-51.6	0.00					201
1.0	900	-7.4							11.0	220	-51.6	0.00					
1.04	895	-7.4							11.61	200	-51.6	0.00					198
1.45	850	-8.8							12.0	189	-51.6	0.00					
1.5	844	-8.0							13.0	162	-51.6	0.00					
1.91	800	-10.8							14.0	138	-51.6	0.00					
2.0	790	-11.1							15.0	118	-51.6	0.00					
2.5	741	-13.6							15.24	114	-51.6	0.00					201
2.59	700	-16.3							5.10 1417 $\varphi = 79^{\circ}15'$ $\lambda = 200^{\circ}10'$								
3.0	693	-16.7							10/10 St (20), φ								
3.0	693	-16.7							0.0	020	-6.8	0.00	100	2.1	315		
4.0	607	-20.3							0.15	000	-6.9	0.05	100	2.1			1
4.09	600	-20.6							0.2	594	-8.9	0.05	100	2.1			
5.0	530	-24.8							0.5	957	-8.4	0.50	100	1.9			
5.42	500	-25.7							0.98	900	-8.4	0.00	38	1.8			
6.0	460	-29.8							1.18	877	-8.4	0.00	77	1.0			
7.01	400	-34.8							1.42	850	-8.8	0.00	72	1.5			
									1.5	812	-8.9	0.16	71	1.3			

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Продолж. приложения

H	B	l	Y	U	q	d	V	W	H	B	l	Y	U	q	d	V	W
6.10 1421 $\varphi = 79^{\circ}20'$ $\lambda = 200^{\circ}20'$																	
10/10 St (22), φ																	
1.88	800	-9.7		67	1.4				12.0	186	-50.2	0.00	100	1.2			174
2.0	788	-10.0		0.22	1.4				13.0	159	-50.2	0.00	100	1.2			
2.5	738	-12.7		0.54	1.1				13.79	141	-50.2	0.00	100	1.6			167
2.57	731	-13.1		0.67	1.1				5.10 1421 $\varphi = 79^{\circ}20'$ $\lambda = 200^{\circ}20'$								
2.91	700	-13.9		0.67	1.1				10/10 St (22), φ								
3.0	691	-14.2		0.25	0.6				0.0	025	-11.9	0.00	100	1.2			2
3.18	675	-14.6		0.22	0.6				0.18	000	-12.9	0.56	100	1.2			
4.0	606	-19.2		0.56	0.6				0.34	580	-12.9	0.00	100	1.2			
4.07	600	-19.7		0.65	0.6				0.46	564	-11.2	0.42	100	1.6			
5.0	529	-25.7		0.65	0.3				0.5	560	-11.2	0.00	97	1.7			
5.4	500	-28.2		0.65	0.3				1.0	500	-11.2	0.00	93	1.7			
6.0	460	-32.2		0.65	0.3				1.43	850	-11.2	0.00	90	1.7			
6.97	400	-38.9		0.69					1.9	800	-11.2	0.00	89	1.7			
7.0	398	-39.1		0.69					2.0	789	-11.2	0.00	89	1.7			
8.0	344	-46.9		0.78					2.09	780	-11.2	0.00	89	1.7			
8.8	305	-52.2		0.66					2.5	740	-13.4	0.54	86	1.4			
8.9	300	-52.2		0.00					2.65	725	-14.5	0.69	85	1.3			
9.0	295	-52.2		0.00					2.94	700	-14.5	0.00	82	1.3			
9.97	254	-52.2		0.00					3.0	683	-14.5	0.00	81	1.3			292
10.0	252	-52.1		0.00					3.16	680	-14.5	0.00	81	1.3			
11.0	217	-50.5		-0.16													
11.15	212	-50.2		-0.20													
11.52	200	-50.2															

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
4.0	607	-19.2	0.56	74	0.9				2.94	700	-14.4	0.32					
4.09	600	-19.9		73	0.8				3.0	694	-14.6	0.44					334
5.0	530	-25.4	0.62	63	0.4				4.1	607	-19.0	0.50					
5.42	500	-27.8		63	0.4		290		5.0	530	-24.0	0.50					
6.0	461	-31.1	0.57	63					5.43	500	-26.9	0.61					
6.39	400	-37.6	0.66	63					6.0	462	-30.1	0.74					361
8.0	343	-46.4	0.87				291		7.02	400	-37.6	0.82					
8.12	337	-47.5	0.92						8.0	343	-46.6	0.82					
									8.52	329	-50.1	0.87					362

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7.10 1413 $\varphi = 79^{\circ}22'$ $\lambda = 200^{\circ}02'$

10/10 Sc (145)

H	B	t	Y	U	q	d	V	W
0.0	027	-14.2		100	1.1	133	2	
0.2	000	-13.6	-0.30	99	1.2			
0.5	962	-12.1	-0.50	98	1.4	144	7	
0.81	925	-10.0	-0.68	95	1.7	137	7	
1.01	900	-10.0	0.00	92	1.7	136	6	
1.46	850	-10.0	0.00	84	1.6			
1.5	845	-10.0	0.00	83	1.6			
1.82	800	-10.0	0.00	79	1.6			
2.0	791	-10.0	0.00	77	1.6			
2.16	775	-10.0	0.00	75	1.6			
2.5	741	-12.0	0.59	75	1.4			

9.10 1416 $\varphi = 79^{\circ}30'$ $\lambda = 200^{\circ}03'$

10/10 Sc (93), λ^*

H	B	t	Y	U	q	d	V	W
0.0	024	-13.4		100	1.2	158	5	
0.18	000	-14.0	0.33	100	1.1			
0.5	960	-15.3	0.41	100	1.0			
0.84	919	-9.4	-1.74	100	1.9			
1.0	900	-9.4	0.00	96	1.8			
1.27	869	-9.4	0.00	85	1.7			
1.44	850	-9.6	0.00	81	1.6			
1.5	843	-9.7	0.13	81	1.6			
1.9	800	-10.3		78	1.6			

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
2.0	789	-10.4	0.14	77	1.5				1.2	869	-9.7	-0.75					
2.22	767	-10.8	0.18	76	1.5				1.37	850	-10.0	0.17					
2.5	739	-11.9	0.39	74	1.3				1.5	838	-10.2	0.17					
2.92	700	-14.2					338		1.83	800	-10.8	0.20					
3.0	692	-14.7	0.56						2.0	783	-11.2	0.20					
4.0	606	-20.5	0.58						2.5	733	-13.0	0.36					
4.07	600	-20.9							2.86	700	-14.4						
5.0	529	-25.2	0.57						3.0	686	-15.0	0.40					
5.4	500	-28.1							4.0	600	-20.3	0.53					
6.0	460	-31.6	0.54						5.0	523	-27.0	0.67					
6.95	400	-38.3							5.33	500	-29.0						
7.0	397	-38.7	0.71						6.0	455	-32.9	0.59					
7.4	374	-42.1	0.85						6.9	400	-39.0						
									7.0	394	-39.6	0.67					
									8.0	340	-46.0	0.64					
									8.82	300	-51.9						
									9.0	291	-53.2	0.72					
									10.0	250	-58.9	0.57					
									10.2	242	-59.5	0.30					
									10.68	224	-59.5	0.00					
									11.0	213	-58.3	-0.38					
									11.39	200	-55.7						
									12.0	181	-53.4	-0.49					

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10.10 1401 $\varphi = 79^{\circ}35'$ $\lambda = 200^{\circ}15'$

10/10 St (93)

H	B	t	Y	U	q	d	V	W
0.0	018	-17.2					158	5
0.14	000	-17.7						
0.2	992	-18.0	0.40					
0.5	953	-18.0	0.00					
0.53	900	-12.2						
1.0	892	-11.2	-1.36					

Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
1.0	888	-10.3	0.88	100	1.8				0.0	014	-7.9	0.11	92	1.2				0.0	014	-7.9	0.11	92	1.2			
1.12	875	-10.7	0.83	100	1.8				0.2	053	-8.0	0.35	95	1.8				0.2	053	-8.0	0.35	95	1.8			
1.34	830	-10.7	0.83	100	1.7				0.5	061	-7.4	-0.40	100	2.1				0.5	061	-7.4	-0.40	100	2.1			
1.5	833	-10.7	0.80	91	1.7				0.7	063	-5.3	-0.79	100	2.6				0.7	063	-5.3	-0.79	100	2.6			
1.81	800	-10.9	0.80	79	1.5				0.7	063	-5.3	-0.79	100	2.6				0.7	063	-5.3	-0.79	100	2.6			
2.0	780	-11.2	0.15	79	1.5				0.7	063	-5.3	-0.79	100	2.6				0.7	063	-5.3	-0.79	100	2.6			
2.5	731	-12.2	0.20	79	1.3				0.7	063	-5.3	-0.79	100	2.6				0.7	063	-5.3	-0.79	100	2.6			
2.89	700	-13.6		79	1.3				0.7	063	-5.3	-0.79	100	2.6				0.7	063	-5.3	-0.79	100	2.6			
3.0	684	-14.2	0.40	79	1.3			315	1.0	082	-5.3	0.12	100	2.6				1.0	082	-5.3	0.12	100	2.6			
3.62	631	-16.0	0.29	79	1.2				1.0	082	-5.3	0.12	100	2.6				1.0	082	-5.3	0.12	100	2.6			
4.0	600	-17.6	0.42	77	1.1				1.5	037	-6.6	0.15	99	2.0				1.5	037	-6.6	0.15	99	2.0			
5.0	523	-24.3	0.07	75	0.6				1.77	003	-7.9	0.15	96	2.5				1.77	003	-7.9	0.15	96	2.5			
5.33	500	-27.0		75	0.4				1.85	000	-7.4	0.15	96	2.5				1.85	000	-7.4	0.15	96	2.5			
6.0	455	-31.4	0.71	73	0.4			329	2.0	784	-10.6	0.43	94	2.4				2.0	784	-10.6	0.43	94	2.4			
6.0	400	-37.0		71					2.5	726	-10.6	0.52	90	1.9				2.5	726	-10.6	0.52	90	1.9			
7.0	394	-38.0	0.75	71					3.0	699	-13.0	0.64	89	1.6				3.0	699	-13.0	0.64	89	1.6			
8.0	340	-46.8	0.70	68					4.0	603	-13.8	0.44	80	1.0				4.0	603	-13.8	0.44	80	1.0			
8.83	300	-52.1	0.60	66				200	4.04	600	-16.3	0.60	79	1.0				4.04	600	-16.3	0.60	79	1.0			
9.0	292	-53.4	0.60	66					5.0	627	-25.0	0.68	66	0.5				5.0	627	-25.0	0.68	66	0.5			
10.0	240	-60.5	0.01						6.00	600	-27.4		65	0.4				6.00	600	-27.4		65	0.4			
10.3	238	-61.0	0.50						8.00	600			65	0.4				8.00	600			65	0.4			
10.63	226	-61.0	0.00					270																		

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Продолж. приложения

H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W	H	B	t	Y	U	q	d	V	W
6.0	459	-30.8	0.58	65					0.2	994	-13.0	-3.90						0.2	994	-13.0	-3.90					
6.96	400	-37.6	0.70	60					0.5	957	-7.8	-1.83						0.5	957	-7.8	-1.83					
7.0	398	-37.8	0.82	60				372	0.55	951	-7.3	0.00						0.55	951	-7.3	0.00					
8.0	342	-46.0	0.54	54					0.97	900	-7.4							0.97	900	-7.4						
8.88	300	-52.8	0.76	53					1.0	896	-7.5							1.0	896	-7.5						
9.0	294	-53.6	0.76	53					1.42	850	-8.1							1.42	850	-8.1						
10.0	251	-60.8	0.72	51					1.5	841	-8.2	0.16						1.5	841	-8.2	0.16					
10.72	224	-64.2	0.47	49					1.88	800	-9.0	0.24						1.88	800	-9.0	0.24					
11.0	214	-64.2	0.00	48				343	2.0	787	-9.4	0.44						2.0	787	-9.4	0.44					
11.4	200	-61.8		47					2.5	738	-11.6							2.5	738	-11.6						
12.0	181	-59.2	-0.50	46					2.91	700	-13.5							2.91	700	-13.5						
13.0	154	-57.6	-0.16	44				259	3.0	692	-13.8	0.44						3.0	692	-13.8	0.44					
14.0	132	-57.6	0.00	41					4.0	606	-18.4	0.46						4.0	606	-18.4	0.46					
15.0	112	-57.6	0.00	40					4.05	600	-18.8							4.05	600	-18.8						
15.68	100	-57.6	0.00	39				254	5.0	529	-25.0	0.65						5.0	529	-25.0	0.65					
16.0	95	-57.6	0.00	39					5.41	500	-28.1							5.41	500	-28.1						
17.0	82	-57.6	0.00	39				253	6.0	460	-31.8	0.68						6.0	460	-31.8	0.68					
17.52	76	-57.6	0.00	39					8.0	343	-46.7	0.77						8.0	343	-46.7	0.77					
15.10	1498	$\rho = 80^{\circ}01'$	$\lambda = 201^{\circ}36'$						8.89	300	-53.6	0.78						8.89	300	-53.6	0.78					
			1/0 CI						10.0	232	-60.5	0.60						10.0	232	-60.5	0.60					
0.0	021	-20.2		86																						
0.16	000	-14.0		138																						

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Продолж. приложения

H	B	t	T	U	q	d	V	W	H	B	t	T	U	q	d	V	W
2.0	783	-14.1	0.34	94	1.4												
2.5	783	-16.7	0.52	94	1.1												
3.0	700	-19.4	0.9	93	0.9												
3.5	686	-20.5	0.76	92	0.8			345									
4.0	600	-28.0	0.76	87	0.4												
4.5	597	-28.1	0.76	87	0.4												
5.0	519	-33.4	0.53	83													
5.25	500	-34.7	0.65	82													
6.0	449	-40.0	0.65	80													
6.75	400	-46.5	0.81	77													
7.0	387	-48.1	0.81	77				348									
8.0	332	-52.8	0.47	74													
8.43	311	-54.3	0.35														
8.75	300	-54.3															
9.0	284	-54.3	0.00														
9.38	275	-54.3	0.00														
10.0	244	-51.6	-0.33					333									
10.5	226	-49.7	-0.38														
11.0	208	-49.7	0.00														
11.28	200	-49.7	0.00														
12.0	179	-49.7	0.00														
13.0	154	-49.7	0.00														
14.0	132	-49.7	0.00					293									

WIND OBSERVATIONS BY DAMPER VANE

by
M. M. Wikitin

Source:

Materialy nabludenii nauchno-issledovatel'skoi drel'fuishchei stantsii 1950/51 goda, Ed. M. M. Semov, Leningrad, Izd. 'Morskoi transport', 1954. Vol. III, pp. 496-498 and Appendix, pp. 499-516.

Wind observations, made as frequently and accurately as possible, are required to show the relation between ice drift and wind, and between wind and currents. The data provided by the Tret'iakov wind gauge* used at the station was not always accurate enough for these needs. However, the idea of making a special apparatus that would assure the necessary accuracy in reading wind direction and velocity only came into being during work at the station (besides requirement of accuracy, the instrument had to be operated directly from the hydrologists' tent and not require an additional observer). M. S. Komarov worked out the construction plans and prepared a device based on a damper arrangement. This device was applied successfully during the hydrological observations and provided valuable data for study of the drift and currents in the central part of the Arctic Basin.

The hourly observations of wind by the damper vane, made during current observations, were carried out from 21 July 1950 through 8 April 1951 by M. M. Somov, M. M. Nikitin and Z. M. Gudkovich.

The damper vane (Fig. 1) consisted of a contact anemometer (1), a vane (2) with a damper (3), and a recording device, i.e. a counter of the anemometer contacts (10). The contact anemometer was used to determine wind force, it closed the circuit every 100 rotations. Two wires led from the anemometer to the contact counter. The initial sensitivity of the anemometer was 0.8 m/sec.

The vane consisted of two parts. The first was the vane proper, made of two duralumin plates set at an angle of about 20° and fastened with a metal tube that rotated freely on ball bearings. The rod indicating wind direction formed an extension of the plates. At the end of the rod there was a lead weight which balanced the system. The total length of the vane was 460 mm. The second part, the damper, was a mechanism designed to suppress the movements (tackings) of the vane by absorbing their energy. The damper consisted of the cylindrical section of a container 30 mm high and 160 mm in diameter and was placed 180 mm below the vane. Inside the box there was a metal plate 25x150 mm, rigidly fastened to the rotating tube of the vane. The box itself was attached to the immobile pipe which acted as the wind apparatus support.

*Tret'iakov wind gauge. A portable instrument for determining the velocity and direction of the wind under field conditions. The wind velocity is measured by the deflection of a freely suspended metal plate having a spoon-shaped form. The direction of the wind is determined by a special vane included in the construction of the instrument. The scale for this wind gauge was obtained experimentally from determinations in an aerodynamic tube (Tr. note). Source: *Meteorologicheskii Slovar'*, Khromov and Mamontova, p. 283

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The vane-plate system rotated freely around its own axis. Anti-freeze oil was poured into the box of the damper. Thus, the plate, rotating in the oil of the damper box, acted as a brake during abrupt oscillations of the vane. Thanks to this, a more accurate reading of the wind direction could be made, and what is more not just the direction of a single gust, but the resultant for the observation period.

The contact anemometer was firmly attached to the upper end of the support rod. A metal azimuth circle (4) was attached to the support rod, below the damper. It was 260 mm in diameter and marked off in degrees from 0 to 360, with scale divisions of 5°; the degree numbers appeared every 20°. The diameter of the azimuth circle was somewhat less than the length of the vane so that the position of the vane indicator could be read on the disk from below; the vane always received wind pressure parallel to the air current.

A garland of six flashlight bulbs (7) with a reflector 160 mm in diameter was used to illuminate the azimuth circle. Wires (inside the support rod) led from the contact anemometer into the tent and were connected to the counter and the storage battery.

The recording apparatus was an ordinary contact counter with an electric magnet. During an anemometer contact the electric magnet made contact with and turned the ratchet wheel one cog. This ratchet wheel was connected with the arrow indicator. The counter mechanism was contained in a round box with a dial, each division of which corresponded to a one-cog turn of the ratchet wheel. Thus one anemometer contact corresponded to one scale division on the dial. The counter was fed by three flashlight batteries connected in series. The support rod of the wind apparatus was a duralumin tube 22 mm in diameter.

The wind apparatus was mounted through the air vent (9) of the hydrologists' tent and held by three cable lines attached to the lower tent supports.

The damper vane stood 3.7 mm above the hydrologists' tent, and about 6 m above the ice surface (Fig. 2). The vane could be studied without taking it down from the tent, because of a joint (8) made in the support rod at the air vent. It could be raised or lowered by one of the cable lines.

The azimuth circle was oriented in a N-S direction during clear weather at noon, local time, by placing one of the cable lines in the shadow of the mast of the vane, in the plane of the true meridian. The 0-180° line of the azimuth circle was made to coincide with the direction of this cable. During the polar night the azimuth circle was oriented in the same way, using the moon.

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After the damper vane had been set up (21 June 1950), all the lengthy observations of currents were made by means of hourly wind measurements. Unfortunately, frequent rime deposits in the winter period interfered with work and the observations had to be stopped, since cleansing of the instrument did not give the desired effect.

The damper vane assured much higher accuracy than the Tret'iakov wind gauge used at the station, which is indicated by the following comparative data:

	Direction	Velocity
Wind apparatus with damper vane	±2-3°	0.1 m/sec
Tret'iakov wind gauge	±10-12°	1.0 m/sec

The damper vane observations took very little time and did not take the observer away from his basic work. The counter of the contact anemometer was switched in for 10 minutes. The wind direction (through the air vent of the tent) was determined for the middle of this period. The wind velocity in meters per second was determined from the number of anemometer contacts for the 10-minute period by means of a calibration curve. Thus, without leaving the tent, the observers could make the hourly determinations of wind force and direction along with their oceanographic work. Observations were made according to Moscow time.

The observations were processed at the Arctic Institute by M. M. Nikitin and Z. M. Gudkovich and consisted of the following: After the data obtained from the damper vane and the Tret'iakov wind gauge had been compared, all doubtful data, due chiefly to the deposit of rime on the vane, were excluded. Then the changes in the orientation of the vane* were determined from the azimuth observations,** corrections were made for the rotation of the floe and the true wind direction was obtained. After all adjustments had been made and the corrections had been entered, tables of the observed wind were constructed and are given in the Appendix (q.v.).

*Orientations for true N-S were made on 19 July and 27 December 1950, on 25 January and 3 and 18 March 1951.

**See N. A. Milläev, "Astronmicheskie nablüdeniä" (Astronomical observations), this same series, Vol. II.

Figure Captions

- Fig. 1: Damper vane.
- | | |
|------------------------|------------------------------------|
| 1. anemometer | 6. attachment for guy-wire support |
| 2. vane | 7. illuminator |
| 3. damper | 8. joint |
| 4. azimuth circle | 9. air vent |
| 5. direction indicator | 10. anemometer-contact counter |

Fig. 2: Wind apparatus with the damper vane above the work tent.

Appendix

Wind observations made with the damper vane.

- Column 1: Date
 2: Moscow time, hours
 3: Moscow time, minutes
 4: Wind direction
 5: Wind velocity (m/sec)
 6: Comments

Comments in order of appearance (Column 6)

- P. 501 - Damper was oiled.
- 503 - Direction determined by the Tret'iaikov wind gauge.
- 505 - The anemometer counter did not work.
- 506 - Damper vane covered with rime.
 Damper vane cleansed of rime.
- 507 - Anemometer covered with rime.
 Anemometer cleansed of rime.
 Damper vane covered with rime from 0900 to 2200 hours.
 Damper vane covered with rime; observations stopped.
- 508 - Damper vane did not work.
- 510 - Damper vane checked.
- 512 - Anemometer counter repaired.

The following word appears frequently in columns 4-5:

ШТЯТ which means calm weather

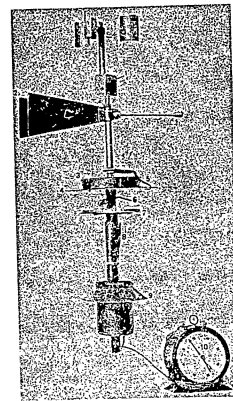
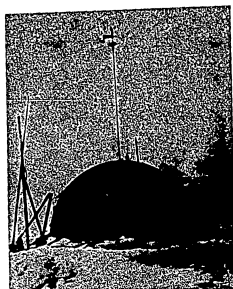


Рис. 1. Демонстрационный флюгер:
1 — индикатор; 2 — флюгер; 3 — демобор;
4 — указатель; 5 — приспособление для крепления оттоков;
6 — ось; 7 — шарнир; 8 — вентилятор;
9 — стержень; 10 — контакты индикатора.



УМЕРЯЮЩИЙ РАБОТУ СТАНОВИТСЯ СЛЕДСТВИЕМ
ПОДГОТОВКИ РАБОТЫ НА ПЛАТФОРМЕ

APPENDIX

See translated text for column headings and additional notes.

Приложение

НАБЛЮДЕНИЯ НАД ВЕТРОМ ПО ДЕМПФЕРНОМУ ФЛЮГЕРУ

Дата	Время (мос- ковское)			Ветер		Приме- чание	Дата	Время (мос- ковское)			Ветер		Приме- чание
	ч.	м.	с.	напра- вление	со- рость (м/сек)			ч.	м.	с.	напра- вление	со- рость (м/сек)	
1	2	3	4	5	6		1	2	3	4	5	6	
1950 год													
21/VII	6	35		34°	0.8		30/VII	0	30	283°	1.8		
7	25	34		34	1.1		1	35	288	3.0			
8	05	34		34	1.1		2	30	248	3.0			
8	25	34		34	1.5		3	30	273	3.3			
8	55	42		34	1.8		4	30	273	2.6			
9	40	75		34	2.5		5	20	243	2.6			
10	45	90		34	2.2		9	00	238	1.5			
11	35	74		34	2.5		10	00	238	1.5			
12	10	77		34	3.0		11	00	236	0.8			
12	40	77		34	2.5		12	00	—	2.5			
13	25	91		34	2.2		13	20	243	3.1			
14	05	72		34	2.5		14	15	264	2.1			
14	50	88		34	3.3		15	10	243	1.8			
15	30	85		34	3.3		16	05	243	1.8			
29/VII	4	40		34	3.0		17	05	275	2.2			
5	30	272		34	2.6		18	05	275	1.0			
6	40	282		34	2.2		19	05	296	1.1			
7	45	282		34	2.6		20	05	215	2.2			
8	45	275		34	2.2		21	00	218	2.0			
9	45	275		34	2.6		22	00	222	2.2			
10	40	267		34	1.8		23	00	223	2.2			
11	35	234		34	1.8		31/VII	0	00	253	1.8		
12	35	235		34	1.5		1	00	256	1.8			
13	35	231		34	1.5		2	00	221	2.6			
14	45	232		34	1.5		3	00	218	1.8			
15	50	234		34	2.6		4	00	200	2.6			
16	40	272		34	2.6		5	00	203	3.0			
17	40	283		34	1.9		6	00	223	2.2			
18	40	294		34	1.9		7	00	223	3.3			
19	35	308		34	2.6		8	00	243	2.2			
20	30	318		34	2.2		9	00	235	1.8			
21	30	323		34	2.2		10	00	243	1.8			
22	30	328		34	1.5		11	00	243	1.1			
23	20	323		34	1.0		12	00	238	1.1			
							13	00	188	1.5			
							14	00	221	1.1			

Продолж. приложения

Дата	Время (мос- ковское)			Ветер		Приме- чание	Дата	Время (мос- ковское)			Ветер		Приме- чание
	ч.	м.	с.	напра- вление	сила			ч.	м.	с.	напра- вление	сила	
1	2	3	4	5	6	7	8	9	10	11	12	13	
1/VII	15	00		218°	1.1		3/VIII	5	00	139°	5.1	Произве- дена за- ливка наском демп- фера	
	16	00		227	1.1			6	00	139	5.7		
	17	00		180	1.5			7	15	139	6.7		
	18	00		182	2.6			8	00	149	6.6		
	19	00		182	2.2			9	30	149	5.7		
	20	00		173	2.6			10	00	149	5.4		
	21	00		173	1.5			11	00	149	5.4		
	22	00		170	1.1			12	00	149	5.4		
	23	00		150	3.0			14	00	144	6.7		
	0	00		139	2.6			15	00	149	7.0		
	1	00		165	2.6			16	00	149	6.7		
	2	00		157	2.2			17	00	149	7.0		
	3	00		141	1.8			18	00	149	6.0		
	4	00			2.9			19	00	149	6.7		
	5	00		141	2.6			20	00	139	6.7		
6	00		139	3.3		21	00	139	6.0				
7	00		126	4.0		22	00	139	6.7				
8	00		129	4.1		23	00	139	6.7				
9	00		129	4.8		0	00	139	6.7				
10	00		124	4.4		2	30	144	7.2				
11	00		124	4.8		3	30	144	—				
12	00		119	4.8		8	45	149	6.7				
13	00		124	5.1									
14	00		114	5.1									
15	00		114	5.4									
16	00		114	5.7									
17	00		124	5.4		10	00	149	7.0				
18	00		129	5.7		11	00	149	6.6				
19	00		124	5.1		12	00	149	7.0				
20	00		129	5.7		13	00	154	7.0				
21	00		134	4.1		14	00	144	6.4				
22	00		139	5.4		15	00	144	7.2				
23	00		134	5.7		16	00	144	6.7				
0	00		139	5.7		17	00	139	4.8				
1	00		139	6.1		18	00	144	6.4				
2	00		139	6.1		19	00	144	7.0				
3	00		139	5.7		20	00	144	6.7				
4	00		139	5.1		21	00	144	7.2				

Продолж. приложения

Дата	Время (мос- ковское)			Ветер		Приме- чание	Дата	Время (мос- ковское)			Ветер		Приме- чание
	ч.	м.	с.	напра- вление	сила			ч.	м.	с.	напра- вление	сила	
1	2	3	4	5	6	7	8	9	10	11	12	13	
4/VIII	22	00		139°	7.5		6/VIII	13	00	253°	3.3		
	23	00		134	8.0			14	00	248	2.2		
	0	00		129	8.0			15	00	253	1.8		
	1	00		134	7.2			16	10	263	3.0		
	2	00		134	7.2			17	05	263	3.7		
	3	00		134	6.9			18	05	259	3.0		
	4	00		149	5.1			19	00	263	4.0		
	5	15		149	7.2			20	00	268	3.3		
	6	00		149	7.2			21	00	278	3.7		
	7	00		154	7.5			22	00	273	4.4		
	8	00		149	6.9			23	00	283	4.0		
	9	00		149	7.2			0	05	273	—		
10	00		149	7.2		1	40	268	4.1				
11	00		149	6.7		2	35	278	3.3				
12	30		159	6.7		3	00	278	3.3				
13	30		164	5.4		4	00	283	3.3				
14	30		159	5.7		5	00	283	3.3				
15	30		159	5.1		6	00	278	3.3				
16	30		149	4.8		7	00	293	3.3				
17	30		149	5.1		8	00	288	2.6				
18	30		149	4.4		9	00	298	3.3				
19	30		149	4.0		10	00	308	2.6				
20	30		154	4.4		11	00	303	3.0				
21	30		159	4.0		12	00	303	2.6				
22	30		169	4.0		13	40	298	2.6				
23	30		184	4.0		14	10	313	2.2				
0	30		183	3.7		15	00	288	1.8				
1	00		188	3.7		16	00	273	1.8				
2	00		213	4.4		17	00	273	1.5				
4	15		213	4.7		18	00	штыль -					
5	00		213	4.1		19	00	288	1.1				
6	10		213	3.7		20	00	268	0.8				
7	10		208	3.7		21	00	штыль					
8	30		213	3.3		22	00	253	1.1				
9	00		223	3.7		23	00	208	1.8				
10	00		223	2.9		0	00	208	1.1				
11	00		223	2.6		1	00	163	1.8				
12	00		228	2.2		2	00	138	2.2				

Продолж. приложения

Дата	Время (мос-ковское)			Ветер		Приме-чание	Дата	Время (мос-ковское)			Ветер		Приме-чание
	ч.	м.	с.	напра-вление	ско-рость (м/сек)			ч.	м.	с.	напра-вление	ско-рость (м/сек)	
1	2	3	4	5	6	7	8	9	10	11	12	13	
	3	00	143°	3.0				17	00	213°	6.7		
	4	00	143	3.0				17	30	223	4.8		
	5	00	133	4.1				18	00	228	4.4		
	6	10	138	4.1				19	30	218	5.4		
	7	00	133	4.4				20	00	213	6.0		
	8	10	133	5.0				21	00	213	6.7		
	9	00	138	5.1				22	00	228	5.7		
	10	00	133	5.4				23	00	223	5.4		
	11	00	133	5.7				23	30	233	6.0		
	12	00	123	6.0			9/VIII	0	00	219	4.8		
	13	00	123	6.7				1	00	234	6.7		
	14	00	123	6.4				2	00	219	5.4		
	15	00	123	7.0				3	00	209	4.8		
	16	00	128	7.2				4	00	224	—		
	17	00	133	7.8				5	00	219	4.8		
	18	00	138	7.8				6	00	219	5.4		
	19	00	143	7.0				7	00	204	4.8		
	20	00	133	8.1				8	00	209	4.4		
	21	10	123	6.7				9	00	199	3.8		
	22	00	123	6.4				10	00	199	3.7		
	23	00	118	6.4				11	00	189	3.0		
8/VIII	0	10	118	6.4				12	00	179	2.6		
	1	40	108	5.7				13	00	174	2.6		
	2	00	98	5.1				14	00	174	1.5		
	3	10	108	5.4				15	00	174	1.1		
	4	00	98	4.8				16	00	174	0.8		
	5	00	93	5.1				16	15	штиль	—		
	6	00	93	4.4				17	00	—	1.3		
	7	00	113	3.0				18	00	—	2.2		
	8	20	113	1.5				18	40	360	2.2	Напра-вление опреде-лено по ветро-муру Третья-кова	
	9	10	123	1.5									
	10	00	123	1.1									
	11	00	123	1.1									
	12	00	188	1.1									
	13	00	188	1.1									
	14	00	188	3.3				20	00	360	3.3		
	15	05	188	3.3				21	00	339	4.8		
	16	00	188	4.0				22	00	334	4.8		
								23	10	324	5.7		

Продолж. приложения

Дата	Время (мос-ковское)			Ветер		Приме-чание	Дата	Время (мос-ковское)			Ветер		Приме-чание
	ч.	м.	с.	напра-вление	ско-рость (м/сек)			ч.	м.	с.	напра-вление	ско-рость (м/сек)	
1	2	3	4	5	6	7	8	9	10	11	12	13	
10/VIII	0	00	319°	6.0				14	05	265°	7.2		
	1	00	299	5.1				15	00	265	7.2		
	2	00	284	6.4				16	10	265	6.0		
	3	10	279	7.8				17	00	260	6.0		
	4	00	270	8.1				18	00	260	7.5		
	5	00	274	7.5				19	00	265	7.8		
	6	15	274	8.3				20	00	260	8.1		
	7	00	269	8.6				21	00	250	7.2		
	8	00	264	8.9				22	00	240	6.0		
	9	00	259	8.3				23	00	250	7.8		
	10	00	259	9.7			12/VIII	0	00	235	7.5		
	11	00	254	8.6				1	00	240	7.5		
	12	00	249	7.8				2	00	245	8.6		
	13	00	244	7.5				3	15	245	8.3		
	14	00	239	6.7				4	25	245	8.9		
	15	00	244	6.4				5	00	240	8.3		
	16	00	234	6.4				6	10	245	7.0		
	17	00	224	7.2				7	00	245	8.6		
	18	00	234	6.0				8	00	245	8.1		
	19	00	229	5.7				9	00	235	5.7		
	20	00	224	4.4				10	00	240	6.0		
	21	00	219	3.7				11	00	240	5.7		
	22	00	217	2.6				12	10	240	5.4		
	23	00	217	1.1				13	00	240	4.8		
11/VIII	0	00	269	0.8				14	00	260	5.7		
	1	15	314	0.8				15	30	270	4.4		
	2	10	354	1.3				16	05	270	4.8		
	3	00	344	1.5				17	00	270	6.4		
	4	20	344	2.6				18	00	275	5.7		
	5	20	329	3.0				19	00	275	6.0		
	6	00	329	—				20	00	290	7.0		
	7	00	329	3.7				21	00	290	7.0		
	8	00	329	4.0				22	00	290	6.4		
	9	20	329	5.1				23	00	300	10.3		
	10	00	330	5.1			13/VIII	0	05	300	9.4		
	11	00	325	5.1				1	00	290	8.1		
	12	15	310	5.4				2	00	290	8.9		
	13	00	265	6.7				3	00	280	9.4		

Продолж. приложения

Дата	Время (московское)			Ветер		Примечание	Дата	Время (московское)			Ветер		Примечание
	ч.	м.	с.	напр-вание	соо-рость (м/сек)			ч.	м.	с.	напр-вание	соо-рость (м/сек)	
1	2	3	4	5	6	7	1	2	3	4	5	6	
14/VIII	4	00	200*	9.7			25/VIII	22	00	286*	3.0		
	5	00	200	9.4				23	00	271	3.7		
	6	00	285	9.7				0	00	266	3.3		
	7	00	280	9.2				1	00	256	3.3		
	8	00	285	9.7				2	00	261	3.3		
	9	00	285	8.9				4	30	251	3.0		
	10	00	290	7.2				5	15	256	3.0		
	11	00	275	7.2				6	00	256	3.7		
	12	00	271	7.2				7	00	256	4.4		
	13	00	271	7.0				8	15	256	4.4		
	14	00	271	7.5				9	00	261	4.4		
	15	00	266	8.1				10	00	261	4.4		
	16	00	266	8.9				11	00	266	4.4		
	17	00	271	9.7				12	00	266	2.6		
	18	00	271	9.4				13	00	268	3.0		
	19	00	271	9.4				14	00	266	4.0		
	20	00	271	9.4				15	00	261	3.3		
	21	00	276	9.2				16	05	261	4.0		
	22	00	266	7.8				17	00	261	3.7		
	23	30	281	—		Счетчик анемометра не работал		18	00	256	4.0		
	24	30	291	—				4	30	126	7.0		
25	45	291	—			5	00	126	7.2				
26	00	291	7.0			6	00	131	7.0				
27	20	276	5.7			7	00	131	7.2				
28	00	281	4.4			8	00	131	6.7				
29	00	291	5.4			9	00	131	7.0				
30	00	286	4.0			10	00	131	6.0				
31	00	286	4.4			11	00	131	6.4				
32	00	291	5.4			12	00	126	5.4				
33	00	286	4.0			13	00	126	5.4				
34	00	286	4.4			14	30	126	5.1				
35	00	286	—			15	00	126	5.4				
36	00	286	4.0			16	00	126	4.4				
37	00	286	4.0			17	05	126	5.7				
38	00	286	2.6			18	00	126	—				
39	00	286	4.4			19	00	126	5.4				
40	00	286	4.0			20	30	126	5.4				
41	00	286	3.0			21	30	126	5.1				

Продолж. приложения

Дата	Время (московское)			Ветер		Примечание	Дата	Время (московское)			Ветер		Примечание
	ч.	м.	с.	напр-вание	соо-рость (м/сек)			ч.	м.	с.	напр-вание	соо-рость (м/сек)	
1	2	3	4	5	6	7	1	2	3	4	5	6	
26/VIII	22	30	126*	4.4			9/IX	6	10	339*	7.5		
	23	30	131	4.0				7	00	329	7.8		
	0	20	132	4.0				8	00	324	6.0		
	1	15	122	3.7				9	00	324	4.8		
	1	50	122	4.0				10	00	299	3.0		
	2	50	112	3.7				0	00	253	1.1		
	3	50	122	3.7				1	00	248	1.8		
	5	15	92	3.7				2	00	238	2.2		
	6	00	84	3.7				3	00	238	1.5		
	7	25	77	4.0				4	00	233	1.8		
31/VIII	2	40	359	10.3			5	00	233	1.1			
	3	10	344	10.3			6	00	173	3.0			
	4	00	359	10.0			7	00	178	3.3			
	5	00	359	9.7			8	00	173	3.7			
	6	20	359	9.2			9	00	158	3.0			
	7	00	354	8.6			5	00	248	0.6			
	8	00	359	8.9			6	00	193	0.6			
	9	00	359	8.9			7	00	178	2.2			
	10	00	354	8.9			8	00	198	2.6			
	11	00	354	8.9			9	00	233	3.7			
1/IX	12	00	354	9.7			10	00	248	4.8			
	13	00	339	9.7			11	00	248	5.4			
	14	00	359	9.4			12	00	243	5.4			
	15	00	359	9.2			13	00	243	5.7			
	16	00	349	8.9			14	00	253	3.3			
	17	00	350	8.6			15	00	—	4.4	Флюгер открылся изморозью		
	18	00	350	7.2									
	19	05	349	8.6									
	19	55	349	8.3			16	00	—	3.3			
	21	05	344	8.1			17	00	—	2.6			
21	55	344	7.2			18	00	—	2.6				
23	00	334	7.8			19	00	—	3.0				
0	00	339	8.3			20	00	—	2.6				
1	30	339	6.7			21	00	—	2.6				
2	15	—	7.2			22	00	203	2.6	Флюгер опущен от изморози			
3	00	339	7.8										
4	00	344	7.5										
5	10	339	7.2			23	00	198	1.1				

Продолж. приложения

Дата	Время (москвское)			Ветер		Примечание	Дата	Время (москвское)			Ветер		Примечание
	ч.	м.	с.	направление	сила			ч.	м.	с.	направление	сила	
1	2	3	4	5	6		1	2	3	4	5	6	
	0	00	168°	1.5			9	00	—	6.0	С 9 до 22 ч. флюгер был открыт кильротью		
	1	00	168	1.1									
	2	00	143	1.8									
	3	00	143	1.8									
	4	00	133	—									
						Анемометр покрываеся изморозью	10	15	—	5.1			
							11	00	—	5.4			
							12	00	—	4.8			
							13	00	—	4.0			
	5	00	123	—			14	00	—	3.3			
	6	00	118	—			15	00	—	2.6			
	7	00	108	1.5		Анемометр очищен от изморози	16	00	—	1.8			
							17	00	—	1.5			
	8	00	113	1.5			18	00	—	1.8			
	9	00	118	2.2			19	00	—	1.5			
	10	00	123	2.6			20	00	—	1.5			
	11	00	123	3.0			22	00	—	1.8			
	12	00	123	3.7			23	00	283°	1.8			
	13	00	123	3.7			0	20	298	2.6			
	14	00	113	5.1			2	00	308	2.2			
	15	00	118	6.0			3	00	308	1.5			
	16	00	113	6.0			4	00	313	2.6			
	17	00	123	8.3			5	00	348	3.7			
	18	00	123	8.9			6	00	3	3.0			
	19	00	118	9.4			7	10	358	1.5			
	20	00	128	10.6			8	00	358	0.8	Флюгер покрываеся изморозью		
	21	00	133	10.6							Флюгер покрываеся изморозью		
	22	00	138	10.6							Флюгер покрываеся изморозью		
	23	25	138	10.3							Флюгер покрываеся изморозью		
4/X	0	00	143	9.7									
	1	00	143	10.0									
	2	00	148	10.0									
	3	35	153	10.0									
	4	00	158	9.4									
	5	00	158	9.2									
	6	00	158	8.1									
	7	30	163	7.2									
	8	00	168	6.7									

Продолж. приложения

Дата	Время (москвское)			Ветер		Примечание	Дата	Время (москвское)			Ветер		Примечание
	ч.	м.	с.	направление	сила			ч.	м.	с.	направление	сила	
1	2	3	4	5	6		1	2	3	4	5	6	
1951 год													
9/I	17	00	286°	5.7			6	00	185°	2.6			
	18	00	286	5.1			7	00	190	2.2			
	19	00	291	5.1			7	30	185	2.2			
	20	00	291	4.8			8	30	185	1.8			
	21	00	286	5.1			9	00	190	1.8			
	22	00	251	5.4			10	00	205	1.1			
	23	00	246	5.4			12	00	штиль	1.5			
10/I	0	00	235	5.4			13	00	*				
	1	00	230	5.4			14	00	*				
	2	10	225	5.1			15	00	*				
	3	10	220	4.4			16	00	*				
	4	00	210	5.4			17	30	190	0.7			
	5	00	215	5.4			18	00	190	0.7			
	6	00	230	6.4			19	00	185	0.7			
	7	00	225	5.1			02	00	180	0.7			
	8	00	225	4.4			21	00	—	0.7			
	9	00	215	4.0							Флюгер не работ.		
	10	00	215	4.8									
	11	00	215	4.4			22	00	—	1.1			
	12	00	220	4.8			23	00	—	1.8			
	13	00	210	4.8			0	00	—	1.5			
	14	00	210	5.1			1	00	—	0.7			
	15	00	205	5.1			2	00	—	1.5			
	16	00	205	4.8			3	00	штиль				
	17	00	195	4.4			4	00	—	1.1			
	18	00	195	4.0			5	00	—	1.8			
	19	00	190	4.4			6	00	—	1.5			
	19	50	190	4.0			7	00	—	1.1			
	21	00	190	3.7			8	00	—	2.6			
	22	00	190	3.7			9	30	134	2.2			
	23	00	190	3.7			10	00	139	1.8			
11/I	0	00	190	4.0			11	00	129	1.5			
	1	00	190	4.0			12	15	134	1.5			
	2	00	190	4.0			13	00	124	1.5			
	3	00	190	3.7			14	00	139	1.8			
	4	15	190	3.3			15	00	124	1.5			
	5	00	190	3.0			16	00	124	0.7			
							17	00	119	1.1			

Продолж. приложения

Дата	Время (моск- овское)			Ветер		Приме- чание	Дата	Время (моск- овское)			Ветер		Приме- чание
	ч.	м.	с.	напра- вление	ско- рость			ч.	м.	с.	напра- вление	ско- рость	
1	2	3	4	5	6	1	2	3	4	5	6		
13/I	18	00		114	0.7		15/I	7	00	214*	2.6		
	19	00		штиль				8	00	214	3.0		
	20	00						9	00	214	1.8		
	21	00		114	0.7			10	00	219	2.2		
	22	00		штиль				11	00	214	2.6		
	23	00						12	00	219	2.6		
	0	00						13	00	214	2.2		
	1	00						14	00	219	2.2		
	2	00						15	00	224	2.6		
	3	00						16	00	224	2.6		
	4	00						17	00	224	3.0		
	4	30		189*	1.1			18	00	214	2.2		
	5	00		194	1.5			19	00	219	3.0		
	6	00		204	1.1			20	00	224	3.7		
	7	00		214	1.8			21	00	229	3.7		
	8	00		224	2.6			22	00	229	3.7		
	9	15		229	2.6			23	00	229	3.0		
	10	00		224	3.0			0	00	219	3.0		
11	00		229	3.3		1	00	224	3.3				
12	00		229	3.0		3	00	224	3.3				
13	00		229	4.0		4	00	224	3.0				
14	00		224	3.0		5	00	219	3.7				
15	00		224	2.6		6	00	219	3.7				
16	00		224	3.0		7	00	219	4.0				
17	00		219	2.6		8	05	224	4.0				
18	00		219	2.2		9	00	229	5.1				
12	00		219	2.6		10	00	234	5.1				
20	00		214	2.6		11	00	234	5.1				
21	00		209	2.6		12	00	234	5.1				
22	00		209	2.6		13	00	234	5.4				
23	00		204	2.2		14	00	239	4.8				
0	00		204	3.0		15	00	239	4.8				
1	00		204	2.2		16	00	239	5.1				
2	15		204	3.0		17	00	239	5.4				
3	10		204	2.6		18	00	239	5.1				
4	00		204	2.6		19	00	239	5.4				
5	00		204	2.2		20	00	239	5.1				
6	10		209	3.0		21	00	239	4.8				

Продолж. приложения

Дата	Время (моск- овское)			Ветер		Приме- чание	Дата	Время (моск- овское)			Ветер		Приме- чание
	ч.	м.	с.	напра- вление	ско- рость			ч.	м.	с.	напра- вление	ско- рость	
1	2	3	4	5	6	1	2	3	4	5	6		
16/I	22	00		239*	4.4	Произ- ведена проверка флюгера	18/I	10	00	244*	0.8		
	23	00		239	3.7				11	00	штиль		
	0	00		239	4.0				12	00			
	1	00		239	4.0				13	00	239	1.1	
	2	00		239	4.8				14	00	234	1.5	
	3	00		239	4.0				15	00	штиль		
	4	10		239	3.3				16	00			
	5	00		244	3.0				17	00			
	6	05		249	3.7				18	00			
	7	10		249	3.3				19	00			
	8	30		249	3.3				20	00			
	9	00		249	3.3				21	00			
	10	00		244	2.6				22	00	180	0.7	
	11	00		244	3.3				23	00	180	0.7	
	12	00		244	3.3				0	00	175	1.5	
	13	00		244	3.3				1	00	165	1.1	
	14	00		244	3.0				2	00	150	1.8	
	15	00		249	2.6				3	00	145	2.2	
16	00		249	3.0		4	05	145	2.6				
17	00		249	3.3		5	00	140	2.6				
18	00		259	3.0		6	00	135	2.2				
19	00		244	1.0		7	00	135	3.3				
20	00		244	2.2		8	00	125					
21	00		244	2.6		8	30	140	3.7				
22	00		230	2.6		9	00	135					
23	00		239	1.5		9	30	135	4.4				
0	00		244	1.8		10	00	145	4.4				
1	00		239	2.2		11	00	135	4.0				
2	00		244	1.5		12	00	135	4.4				
3	00		244	1.1		13	00	135	4.4				
4	00		штиль			14	00	145	4.4				
5	00		239	1.5		15	00	140	5.1				
6	00		244	1.5		16	00	145	5.1				
7	00		239	1.8		17	00	145	4.8				
8	00		244	0.8		18	00	150	5.2				
9	15		239	1.5		19	00	155	4.8				
						20	00	160	5.4				
						21	00	150	4.8				

Продолж. приложения

Дата	Время (мос-ковское)			Ветер		Приме-чание	Дата	Время (мос-ковское)			Ветер		Приме-чание
	ч.	м.	с.	напра-вление	ско-рость (М/сек)			ч.	м.	с.	напра-вление	ско-рость (М/сек)	
1	2	3	4	5	6	1	2	3	4	5	6		
19/1	22	00	160°	4.8		21/1	11	00	186°	4.0			
	23	00	165	3.7			12	00	186	4.8			
	0	00	165	2.6			13	00	186	4.4			
	1	00	165	3.7			14	00	186	4.8			
	2	00	165	4.0			15	00	186	4.4			
	3	00	170	4.8			16	00	186	4.8			
	4	00	180	3.7			17	00	191	4.4			
	5	05	190	4.8			18	30	186	3.7			
	6	00	190	4.0			19	00	186	4.0			
	7	00	190	4.0			20	00	191	4.8			
	8	00	185	4.0			21	40	186	4.4			
	9	00	190	4.8			22	00	186	4.4			
	9	30	190	5.1			23	00	186	3.7			
	10	30	190	4.4			0	00	186	4.8			
	11	00	190	4.0			1	00	186	4.4			
	12	00	190	4.0			2	00	186	3.7			
	13	00	185	3.7			3	00	186	4.0			
	14	00	185	3.7			4	00	176	3.0			
	15	00	180	4.0			5	00	171	3.3			
	16	00	185	3.7			6	00	171	3.3			
17	00	185	3.7		7	00	171	2.2					
18	00	180	4.0		8	25	196	3.3					
19	00	185	3.7		9	00	151	3.3					
20	00	185	3.7		10	00	141	3.0					
21	00	185	4.0		11	00	141	4.0					
22	00	185	4.8		12	00	141	4.8					
23	00	190	5.1		13	00	141	4.4					
20/1	0	00	195	4.4		14	00	141	5.4				
	1	00	190	3.7		15	00	141	5.1				
	2	15	180	3.0		16	00	141	5.1				
	3	30	180	3.3		17	00	141	6.0				
	4	00	190	4.4		18	00	136	5.7				
	5	00	190	4.4		19	00	136	7.0				
	6	00	190	4.8		20	00	126	7.8				
	7	00	185	4.8		21	00	131	8.9				
	8	00	185	4.4		22	00	141	9.2				
	9	05	185	5.4		23	00	136	8.6				
10	10	191	6.0										

Продолж. приложения

Дата	Время (мос-ковское)			Ветер		Приме-чание	Дата	Время (мос-ковское)			Ветер		Приме-чание
	ч.	м.	с.	напра-вление	ско-рость (М/сек)			ч.	м.	с.	напра-вление	ско-рость (М/сек)	
1	2	3	4	5	6	1	2	3	4	5	6		
22/1	0	00	136°	9.4		Ремонт счетчика анемометра	24/1	12	00	231°	3.3		
	1	00	141	9.2				13	05	226	3.3		
	2	05	136	—				14	00	216	3.7		
	3	30	146	—				15	00	216	4.0		
	4	00	151	—				16	00	216	4.0		
	5	00	151	10.8				17	00	216	4.0		
	7	15	171	8.9				18	10	216	4.8		
	8	10	161	6.0				19	00	221	4.4		
	9	35	166	7.8				20	00	211	3.7		
	10	00	171	7.8				21	00	201	4.4		
	11	00	176	7.8				22	00	201	4.0		
23/1	12	00	176	5.4		23	00	191	3.3				
	13	00	176	5.4		0	00	191	3.7				
	14	00	176	5.7		1	00	191	4.4				
	15	00	181	5.1		2	00	186	4.8				
	16	00	196	4.4		3	05	186	—				
	17	00	196	3.3		4	20	181	6.4				
	18	00	201	3.7		5	15	181	6.4				
	19	00	211	3.3		6	00	176	7.8				
	20	00	211	2.6		7	00	171	8.3				
	21	00	216	3.0		8	00	171	7.8				
	22	00	236	4.0		9	30	166	8.9				
24/1	0	00	251	3.3		10	00	166	10.6				
	1	00	251	3.7		11	00	166	12.7				
	2	10	251	4.0		12	00	171	13.2				
	3	00	251	2.6		13	00	191	11.6				
	4	00	256	3.3		14	00	196	10.6				
	5	00	246	3.0		15	00	201	8.6				
	6	00	246	3.0		16	00	205	7.2				
	7	00	241	3.7		17	00	211	6.7				
	8	00	236	4.0		18	00	221	6.7				
	9	00	231	3.7		19	00	226	5.4				
	10	00	226	3.3		20	00	241	5.4				
25/1	11	00	231	4.0		21	00	245	5.1				
						22	00	210	8.3				
						23	00	215	7.2				

Продолж. приложения

Дата	Время (мос- ковское)			Ветер		Приме- чание	Дата	Время (мос- ковское)			Ветер		Приме- чание
	ч.	м.	с.	напр.- важние	спо- рость (м/сек)			ч.	м.	с.	напр.- важние	спо- рость (м/сек)	
1	2	3	4	5	6	1	2	3	4	5	6		
26/II	0	00	220°	7.2		23/III	21	10	338°	2.6			
	1	00	210	7.2			22	00	318	2.6			
	2	05	210	7.0			23	15	318	3.7			
	3	00	210	7.2			0	00	318	3.7			
	4	00	215	7.0			1	00	318	4.0			
	5	00	215	6.7			2	05	338	2.6			
	6	00	200	6.7			3	00	323	3.3			
	8	05	210	6.7			4	30	323	3.7			
	9	00	200	6.0			5	00	328	5.1			
	10	05	195	6.4			6	10	328	6.7			
	11	00	190	6.7			7	00	333	6.7			
	12	00	205	6.0			8	00	328	5.1			
	13	00	195	4.8			9	00	328	5.4			
	14	00	180	5.4			10	00	338	6.0			
	15	00	175	4.0			11	15	338	5.4			
	16	00	180	4.8			12	00	343	5.7			
	17	00	180	4.0			13	00	334	4.4			
	18	00	180	4.0			14	15	339	4.0			
	19	00	180	4.0			15	00	344	4.0			
	20	15	185	5.1			16	15	339	4.0			
22/III	6	40	322	3.3		17	00	339	3.3				
	7	00	327	3.7		18	00	339	3.3				
	8	00	322	2.2		19	10	339	2.2				
	9	15	327	3.3		20	00	339	3.0				
	10	00	328	3.7		21	00	339	3.0				
	11	00	333	4.0		22	00	339	3.3				
	12	00	328	3.7		23	00	339	3.7				
	13	00	328	3.7		0	00	344	4.0				
	14	15	328	4.0		2	15	334	6.0				
	15	00	328	3.7		3	00	334	6.0				
24/III	4	30	334	6.0		4	30	334	6.0				
	6	20	344	5.4		6	20	344	5.4				
	7	00	339	5.1		7	00	339	5.1				
	8	20	339	5.4		8	20	339	5.4				
	10	00	335	5.7		10	00	360	6.0				
	11	00	360	6.0		11	00	360	6.0				
	12	00	5	5.7		12	00	5	5.7				
13	00	10	6.0		13	00	10	6.0					

Продолж. приложения

Дата	Время (мос- ковское)			Ветер		Приме- чание	Дата	Время (мос- ковское)			Ветер		Приме- чание
	ч.	м.	с.	напр.- важние	спо- рость (м/сек)			ч.	м.	с.	напр.- важние	спо- рость (м/сек)	
1	2	3	4	5	6	1	2	3	4	5	6		
25/III	14	00	10°	5.4		27/III	4	00	10°	4.0			
	15	00	5	5.4			5	00	15	4.0			
	16	00	15	6.0			6	15	15	4.0			
	17	15	15	5.1			7	15	15	2.6			
	18	00	5	4.0			8	00	20	2.6			
	19	05	15	4.8			9	15	30	3.3			
	20	00	10	4.4			10	20	30	3.0			
	21	00	15	5.1			11	20	40	1.8			
	22	00	10	4.8			12	20	40	1.5			
	23	00	10	5.1			13	00	45	1.5			
	0	00	5	5.1			14	00	35	1.1			
	1	05	5	4.8			15	00	45	1.5			
	2	05	360	5.4			16	00	45	1.5			
	3	00	5	6.0			17	00	45	0.8			
4	00	5	5.1		18	00	шталь						
5	00	5	5.1		19	00							
6	10	20	5.4		20	00							
7	45	15	4.0		21	00							
8	00	20	4.0		22	00							
9	00	20	4.0		23	00							
10	00	30	4.8		0	00							
11	00	25	4.4		1	00							
12	00	25	4.0		2	00							
13	00	35	3.3		3	00							
14	30	20	3.0		4	00							
15	00	10	2.6		5	00							
16	30	15	3.3		6	00							
17	00	15	3.0		7	00							
18	00	10	3.0		8	00							
19	00	25	4.0		9	00							
20	00	25	3.3		10	00							
21	00	15	3.3		11	00							
22	00	25	3.7		12	00							
23	00	25	4.0		13	00							
0	00	10	3.7		14	00							
26/III	1	20	15	4.4		15	00						
	2	20	5	4.0		16	00						
	3	10	15	4.4									

Продолж. приложения

Дата	Время (моск-овское)			Ветер		Приме-чание	Дата	Время (моск-овское)			Ветер		Приме-чание
	ч.	м.	с.	напр-вление	сила			ч.	м.	с.	напр-вление	сила	
1	2	3	4	5	6	7	8	9	10	11	12	13	
	17	00		штиль			7	00	90°	1.8			
	18	00		*			8	00	90	1.5			
	19	00		95°	1.8		9	00	90	1.5			
	20	00		95	1.5		10	00	90	1.5			
	21	00		95	2.6		11	00	90	1.1			
	22	15		115	2.6		19	05	106	2.2			
	23	00		120	3.3		20	00	111	2.2			
	23	30		штиль			21	00	101	1.7			
28/III	0	00		*			22	15	96	2.2			
	1	00		*			0	20	105	2.2			
	2	00		*			1	20	101	2.2			
	3	00		*			2	15	105	2.2			
	4	00		*			3	15	106	2.2			
	5	00		*			4	00	106	2.6			
	6	00		90	1.1		5	00	111	3.3			
	7	00		штиль			6	00	105	2.6			
	8	15		70	1.8		7	10	116	3.0			
	9	00		70	1.1		8	00	116	3.0			
	10	00		100	1.5		9	00	121	3.0			
	11	00		105	1.1		10	00	121	2.6			
	12	00		105	1.5		11	25	121	1.8			
	13	00		105	0.8		13	15	96	1.1			
	14	00		105	1.1		14	00	96	1.5			
	15	00		штиль			15	00	96	1.5			
	16	00		105	1.1		16	00	101	1.5			
	17	00		105	1.1		17	00	101	0.8			
	19	00		штиль			18	00	101	1.1			
	20	00		*			22	00	96	1.1			
	21	00		105	1.5		23	00	91	1.1			
	22	00		штиль			0	30	96	2.2			
29/III	0	00		*			1	00	96	2.2			
	1	00		110	1.1		2	05	101	2.6			
	2	00		110	1.8		3	00	96	2.6			
	3	00		115	2.6		4	00	111	1.8			
	4	00		105	1.5		5	00	106	1.8			
	5	00		105	1.8		6	25	106	2.2			
	6	00		95	1.8		7	00	111	3.0			
							8	00	106	2.6			

Продолж. приложения

Дата	Время (моск-овское)			Ветер		Приме-чание	Дата	Время (моск-овское)			Ветер		Приме-чание
	ч.	м.	с.	напр-вление	сила			ч.	м.	с.	напр-вление	сила	
1	2	3	4	5	6	7	8	9	10	11	12	13	
	9	00		116°	2.2								
	10	00		101	1.8			6	25	202°	3.0		
	11	00		101	1.8			7	00	197	3.3		
	12	00		106	2.6			8	45	207	4.0		
	13	00		101	2.6			9	40	202	4.0		
	14	00		96	2.2			10	20	202	4.0		
	15	00		91	2.2			11	00	207	4.0		
	16	00		86	2.2			12	00	207	4.4		
	17	00		91	3.0			13	00	207	4.0		
	18	30		86	1.8		8/IV	14	00	207	3.3		
	19	00		86	1.8			2	00	штиль			
	20	00		86	1.8			3	00	*			
	21	15		71	2.2			4	00	*			
	22	00		71	1.8			5	00	*			
	23	10		76	2.6			6	00	*			
1/IV	0	00		76	2.6			7	00	*			
5/IV	3	30		192	2.6			8	00	*			
	4	00		202	3.3			9	00	*			
	5	00		197	3.3			10	00	*			
								11	00	*			

Продолж. приложения

Дата	Время (мос- ковское)		Ветер		Приме- чание	Дата	Время (мос- ковское)		Ветер		Приме- чание
	ч.	м.	напра- вление	ско- рость (м/сек)			ч.	м.	напра- вление	ско- рость (м/сек)	
1	2	3	4	5	6	1	2	3	4	5	6
	17	00	штиль				7	00	90°	1.8	
	18	00	"				8	00	90	1.5	
	19	00	95°	1.8			9	00	90	1.5	
	20	00	95	1.5			10	00	90	1.5	
	21	00	95	2.6			11	00	90	1.1	
	22	15	115	2.6			19	05	106	2.2	
	23	00	120	3.3			20	00	101	2.2	
	23	30	штиль				21	00	101	1.7	
28/III	0	00	"				22	15	96	2.2	
	1	00	"			30/III	0	20	106	2.2	
	2	00	"				1	20	101	2.2	
	3	00	"				2	15	106	2.2	
	4	00	"				3	15	106	2.2	
	5	00	"				4	00	106	2.6	
	6	00	90	1.1			5	00	111	3.3	
	7	00	штиль				6	00	106	2.6	
	8	15	70	1.8			7	10	116	3.0	
	9	00	70	1.1			8	00	116	3.0	
	10	00	100	1.5			9	00	121	3.0	
	11	00	105	1.1			10	00	121	2.6	
	12	00	105	1.5			11	25	121	1.8	
	13	00	105	0.8			13	15	96	1.1	
	14	00	105	1.1			14	00	96	1.5	
	15	00	штиль				15	00	96	1.5	
	16	00	105	1.1			16	00	101	1.5	
	17	00	105	1.1			17	00	101	0.8	
	19	00	штиль				18	00	101	1.1	
	20	00	"				22	00	96	1.1	
	21	00	105	1.5			23	00	91	1.1	
	22	00	штиль			31/III	0	30	96	2.2	
	23	00	"				1	00	96	2.2	
29/III	0	00	"				2	05	101	2.6	
	1	00	110	1.1			3	00	96	2.6	
	2	00	110	1.8			4	00	111	1.8	
	3	00	115	2.6			5	00	106	1.8	
	4	00	105	1.5			6	25	106	2.2	
	5	00	105	1.8			7	00	111	3.0	
	6	00	95	1.8			8	00	106	2.6	

Продолж. приложения

Дата	Время (москвское)			Ветер		Примечание	Дата	Время (москвское)			Ветер		Примечание
	ч.	м.	с.	напра-вление	сил-а (м/сек)			ч.	м.	с.	напра-вление	сил-а (м/сек)	
1	2	3	4	5	6	1	2	3	4	5	6		
	14	00		10*	5.4			4	00	10*	4.0		
	15	00		5	5.4			5	00	15	4.0		
	16	00		15	6.0			6	15	15	4.0		
	17	15		15	5.1			7	15	15	2.6		
	18	00		5	4.0			8	00	20	2.6		
	19	05		15	4.8			9	15	30	3.3		
	20	00		10	4.4			10	20	30	3.0		
	21	00		15	5.1			11	20	40	1.8		
	22	00		10	4.8			12	20	40	1.5		
	23	00		10	5.1			13	00	45	1.5		
25/III	0	00		5	5.1			14	00	35	1.1		
	1	05		5	4.8			15	00	45	1.5		
	2	05	360	5	5.4			16	00	45	1.5		
	3	00		5	6.0			17	00	45	0.8		
	4	00		5	5.1			18	00	штиль			
	5	00		5	5.1			19	00	.			
	6	10	20	5.4				20	00	.			
	7	45	15	4.0				21	00	.			
	8	00	20	4.0				22	00	.			
	9	00	20	4.0				23	00	.			
	10	00	30	4.8			27/III	0	00	.			
	11	00	25	4.4				1	00	.			
	12	00	25	4.0				2	00	.			
	13	00	35	3.3				3	00	.			
	14	30	20	3.0				4	00	.			
	15	00	10	2.6				5	00	.			
	16	30	15	3.3				6	00	.			
	17	00	15	3.0				7	00	.			
	18	00	10	3.0				8	00	.			
	19	00	25	4.0				9	00	.			
	20	00	25	3.3				10	00	.			
	21	00	15	3.3				11	00	.			
	22	00	25	3.7				12	00	.			
	23	00	25	4.0				13	00	.			
26/III	0	00	10	3.7				14	00	.			
	1	20	15	4.4				15	00	.			
	2	20	5	4.0				16	00	.			
	3	10	15	4.4						.			